HOBBS OCD

(March 2012)	UNITED STATES OCD HODE							
UNITED STATE DEPARTMENT OF THE		SHED.		5. Lease Serial No.				
BUREAU OF LAND MA		ENT		NM LC 060329	P. 11 NT			
APPLICATION FOR PERMIT TO	O DRILL	OR REENTER		6. If Indian, Allotee or N/A	ribe Name			
la. Type of work: DRILL REEN	ITER			7 If Unit or CA Agreeme N/A				
Ib. Type of Well: Oil Well Gas Well Other		Single Zone Multip	le Zone	8. Lease Name and Well Emerald Federal #7	[№] . <38 743			
Name of Operator ConocoPhillips Company	4 2	17817		9. API Well No. 30-025-	40893			
3a. Address P.O. Box 51810		ne No. (include anea code) 88-6913		10. Field and Pool, or Expl	oratory			
Midland, Texas 79710-1810		Maljamar; Yeso West	<4450l					
4. Location of Well (Report location clearly and in accordance with	any State rea	quirements.*)		11. Sec., T. R. M. or Blk.a	nd Survey or Area			
At surface UL A, Sec. 17, T17S, R32E; 990' FNL, 330	'FEL			Sec. 17, T17S, R32E				
At proposed prod. zone UL A, Sec. 17, T17S, R32E; 990								
 Distance in miles and direction from nearest town or post office* approximately 3.5 miles south of Maljamar, New Mexico 				12. County or Parish Lea	13. State NM			
15. Distance from proposed* 330'FEL property or lease line, ft. (Also to nearest drig. unit line, if any)	16. No 323.7	No. of acres in lease 23.76 17. Spacin 40 acres		g Unit dedicated to this well				
18. Distance from proposed location* to nearest well, drilling, completed, applied for, on this lease, ft.	1	. Proposed Depth 20. BLM. .337' MD/TVD ES0088		/BIA Bond No. on file 5				
21. Elevations (Show whether DF, KDB, RT, GL, etc.) 4039' GL	- 1	proximate date work will star /2012	t*	* 23. Estimated duration 20 days				
	24	Attachments		<u></u>				
The following, completed in accordance with the requirements of Ons			tached to thi	s form:				
 Well plat certified by a registered surveyor. A Drilling Plan. A Surface Use Plan (if the location is on National Forest Systematics) 	em Lands, ti	Item 20 above).	•	ns unless covered by an exis	ting bond on file (see			
SUPO must be filed with the appropriate Forest Service Office).			specific info	rmation and/or plans as ma	be required by the			
25. Signature Susan B. Maunder	_	lame <i>(Printed/Typed)</i> Susan B. Maunder		Dat	61/01/8			
Title Senior Regulatory Specialist				_	A A			
Approved by (Signature) /s/George MacDonell	N	Name (Printed/Typs/Geo	rge Ma	ocDonell Date	DEC 1 8 201			
Title 6 FIELD MANAGER	C	Office CARLSBAD	FIELD O	FFICE	<u> </u>			
Application approval does not warrant or certify that the applicant he conduct operations thereon. Conditions of approval, if any, are attached.	olds legal or	equitable title to those right	s in the sub APPR	ect lease which would entitl OVAL FOR TWC	the applicant to YEARS			
Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a States any false, fictitious or fraudulent statements or representations	crime for a	any person knowingly and watter within its jurisdiction.	villfully to m	ake to any department or ag	ency of the United			
(Continued on page 2)			Rosw	ell Controlled W	ater Basin ²⁾			

Karlin

SEE ATTACHED FOR CONDITIONS OF APPROVAL

Approval Subject to General Requirements.
& Special Stipulations Attached

Drilling Plan ConocoPhillips Company Maljamar; Yeso, west

Emerald Federal #7

Lea County, New Mexico

1. Estimated tops of geological markers and estimated depths to water, oil, or gas formations:

The ranges of depths for the formation tops, thicknesses, and planned Total Depths for all the wells to be drilled under this Master Drilling Plan are presented in the table below.

The datum for these depths is RKB (which is 13' above Ground Level).

Formations	Top Depths FT MD	Contents
Quaternary	Surface	Fresh Water
Rustler	810	Anhydrite
Salado (top of salt)	991	Salt
Tansill	2008	Gas, Oil and Water
Yates	2184	Gas, Oil and Water
Seven Rivers	2470	Gas, Oil and Water
Queen	3106	Gas, Oil and Water
Grayburg	3535	Gas, Oil and Water
San Andres	3888	Gas, Oil and Water
Glorieta	5383	Gas, Oil and Water
Paddock	5490	Gas, Oil and Water
Blinebry	5797	Gas, Oil and Water
Tubb	6837	Gas, Oil and Water
Deepest estimated perforation	6837	Deepest estimated perf. is ~ Top of Tubb
Total Depth (maximum)	7037	200' below deepest estimated perforation

All of the water bearing formations identified above will be protected by setting of the <u>8-5/8</u> surface casing <u>25' - 70' into the Rustler formation</u> and circulating of cement from casing shoe to surface in accordance with the provisions of Onshore Oil and Gas Order No. 2 and New Mexico Oil Conservation Division Title 19.

The targeted oil and gas bearing formations identified above will be protected by setting of the _____5-1/2" production casing _____10' off bottom of TD ___ and circulating of cement from casing shoe to surface in accordance with the provisions of Onshore Oil and Gas Order No. 2 and New Mexico Oil Conservation Division Title 19.

(Date: July 24, 2012)

2. Proposed casing program:

Type	Hole Size		Interval D RKB (ft)	OD	Wt	Gr	Conn	MIY	Col	Jt Str		Safety Fac lated per Co Corporate C	nocoPhillips
Турс	(in)	From	То	(inches)	(lb/ft)	Gi	Com	(psi)	(psi)	(klbs)	Burst DF	Collapse DF	Jt Str DF (Tension) Dry/Buoyant
,Cond	20	0	40' – 85' (30' – 75' BGL)	16	0.5" wall	В	Line Pipe	N/A	N/A	N/A	NA	NA	NA
Alt. Cond	20	0	40' – 85' (30' – 75' BGL)	13-3/8	48#	H-40	PE	1730	740	N/A	NA	NA	NA
Surf	12-1/4	0	835' – 880'	8-5/8	24#	J-55	STC	2950	1370	244	2.68	5.43	1.40
Prod	7-7/8	0	6982' – 7027'	5-1/2	17#	L-80	LTC	7740	6290	338	1.15	2.01	1.40

The casing will be suitable for H₂S Service.

The surface and production casing will be set approximately 10' off bottom and we will drill the hole with a 45' range uncertainty for casing set depth to fit the casing string so that the cementing head is positioned at the floor for the cement job.

The production casing will be set 155' to 200' below the deepest estimated perforation to provide rathole for the pumping completion and for the logs to get deep enough to log the interval of interest.

Casing Design (Safety) Factors - BLM Criteria:

Туре	Depth	Wt	MIY	Col	Jt Str	Drill Fluid	Burst	Collapse	Tensile-Dry	Tens-Bouy
Surface Casing	880	24	2950	1370	244000	8.5	7.58	3.52	11.55	13.28
Production Casing	7027	17	7740	6290	338000	10	2.12	1.72	2.83	3.34

Casing Design (Safety) Factors – Additional ConocoPhillips Criteria:

ConocoPhillips casing design policy establishes Corporate Minimum Design Factors (see table below) and requires that service life load cases be considered and provided for in the casing design.

ConocoPhillips Corporate Criteria for Minimum Design Factors

	Contocol timpo Corporate Cit	tona for minimani Booign i dotoro	
	Burst	Collapse	Axial
Casing Design Factors	1.15	1.05	1.4

Burst Design (Safety) Factors - COP Criteria

The maximum internal (burst) load on the Surface Casing occurs when the surface casing is tested to 1000 psi (pressured up to 1100 psi). The maximum internal (burst) load on the Production Casing occurs during the fracture stimulation where the maximum allowable working pressure (MAWP) is the pressure that would fit ConocoPhillips Corporate Criteria for Minimum Design Factors.

Surface Casing Burst Design Factor = Burst Rating / Maximum Pressure during Casing Pressure Test

Production Casing MAWP for the Fracture Stimulation = Minimum Internal Yield / Production Casing Burst Design Factor

Surface Casing Burst Design Factor:

Burst Design Factor (Casing Pressure Test) = 2950 psi / 1100 psi = 2.68

Production Casing Burst Design Factor:

MAWP for the Fracture Stimulation = 7740 psi / 1.15 = 6730

Collapse Design (Safety) Factors – COP Criteria

The maximum collapse load on the Surface Casing occurs when the pressure is released after bumping the plug on the surface casing cement job. The maximum collapse load on the production casing occurs with the well is pumped off on production. We plan to cement the production casing to surface, and therefore the external pressure profile on the production casing should be equal to the pore pressure of the horizons on the outside of the casing which we estimate to be 8.55 ppg gradient.

Surface Casing Collapse Design Factor = Collapse Rating / (Cement Column Hydrostatic Pressure – Displacement Fluid Hydrostatic Pressure)

Production Casing Collapse Design Factor = Collapse Rating / Maximum Possible Pore Pressure

Surface Casing Collapse Design Factor:

Collapse Design Factor = $\frac{1370 \text{ psi}}{(1370 \text{ psi})}$ / $\frac{(1300 \text{ ft} \times 0.052 \times 14.8 \text{ppg})}{(1370 \text{ psi})}$ + $(\frac{1380 \text{ ft} \times 0.052 \times 13.6 \text{ ppg}}{(1370 \text{ psi})})$ - $(\frac{1380 \text{ ft} \times 0.052 \times 13.6 \text{ ppg}}{(1370 \text{ psi})})$ - $(\frac{1380 \text{ ft} \times 0.052 \times 13.6 \text{ ppg}}{(1370 \text{ psi})})$ - $(\frac{1380 \text{ ft} \times 0.052 \times 13.6 \text{ ppg}}{(1370 \text{ psi})})$ - $(\frac{1380 \text{ ft} \times 0.052 \times 13.6 \text{ ppg}}{(1370 \text{ psi})})$ - $(\frac{1380 \text{ ft} \times 0.052 \times 13.6 \text{ ppg}}{(1370 \text{ psi})})$ - $(\frac{1380 \text{ ft} \times 0.052 \times 13.6 \text{ ppg}}{(1370 \text{ psi})})$ - $(\frac{1380 \text{ ft} \times 0.052 \times 13.6 \text{ ppg}}{(1370 \text{ psi})})$ - $(\frac{1380 \text{ ft} \times 0.052 \times 13.6 \text{ ppg}}{(1370 \text{ psi})})$ - $(\frac{1380 \text{ ft} \times 0.052 \times 13.6 \text{ ppg}}{(1370 \text{ psi})})$ - $(\frac{1380 \text{ ft} \times 0.052 \times 13.6 \text{ ppg}}{(1370 \text{ psi})})$ - $(\frac{1380 \text{ ft} \times 0.052 \times 13.6 \text{ ppg}}{(1370 \text{ psi})})$ - $(\frac{1380 \text{ ft} \times 0.052 \times 13.6 \text{ ppg}}{(1370 \text{ psi})})$ - $(\frac{1380 \text{ ft} \times 0.052 \times 13.6 \text{ ppg}}{(1370 \text{ psi})})$ - $(\frac{1380 \text{ ft} \times 0.052 \times 13.6 \text{ ppg}}{(1370 \text{ psi})})$ - $(\frac{1380 \text{ ft} \times 0.052 \times 13.6 \text{ ppg}}{(1370 \text{ psi})})$ - $(\frac{1380 \text{ ft} \times 0.052 \times 13.6 \text{ ppg}}{(1370 \text{ psi})})$ - $(\frac{1380 \text{ ft} \times 0.052 \times 13.6 \text{ ppg}}{(1370 \text{ psi})})$ - $(\frac{1380 \text{ ft} \times 0.052 \times 13.6 \text{ ppg}}{(1370 \text{ psi})})$ - $(\frac{1380 \text{ ft} \times 0.052 \times 13.6 \text{ ppg}}{(1370 \text{ psi})})$ - $(\frac{1380 \text{ ft} \times 0.052 \times 13.6 \text{ ppg}}{(1370 \text{ psi})})$ - $(\frac{1380 \text{ ft} \times 0.052 \times 13.6 \text{ ppg}}{(1370 \text{ psi})})$ - $(\frac{1380 \text{ ft} \times 0.052 \times 13.6 \text{ ppg}}{(1370 \text{ psi})})$ - $(\frac{1380 \text{ ft} \times 0.052 \times 13.6 \text{ ppg}}{(1370 \text{ psi})})$ - $(\frac{1380 \text{ ft} \times 0.052 \times 13.6 \text{ ppg}}{(1370 \text{ psi})})$ - $(\frac{1380 \text{ ft} \times 0.052 \times 13.6 \text{ ppg}}{(1370 \text{ psi})})$ - $(\frac{1380 \text{ ft} \times 0.052 \times 13.6 \text{ ppg}}{(1370 \text{ psi})})$ - $(\frac{1380 \text{ ft} \times 0.052 \times 13.6 \text{ ppg}}{(1370 \text{ psi})})$ - $(\frac{1380 \text{ ft} \times 0.052 \times 13.6 \text{ ppg}}{(1370 \text{ psi})})$

Production Casing Collapse Design Factor:

Collapse Design Factor = 6290 psi / $(8.55 \text{ ppg} \times 0.052 \times 7027)$ ft) = 6290 psi / 3124 psi = 2.01

(Date: July 24, 2012) Page 2 of 8

Axial Design (Safety) Factors - COP Criteria

The maximum axial (tension) load occurs if casing were to get stuck and pulled on to try to get it unstuck.

Maximum Allowable Hookload = Joint Strength Rating / Axial Design Factor

Overpull Margin = Maximum Allowable Hook Load - Air Wt of the String

Surface Casing (Ult. Tensile):

Maximum Allowable Hookload = 244000 lbs/ 1.4 = 174286 lbs Overpull Margin = 174286 lbs - (880 ft x 24 lb/ft) = 153166 lbs Production Casing (Ult. Tensile):

3. Proposed cementing program:

16" or 13-3/8" Conductor:

Cement to surface with rathole mix, ready mix or Class C Neat cement. (Note: The gravel used in the cement is not to exceed 3/8" diameter) TOC at surface.

8-5/8" Surface Casing & Cementing Program: 8-5/8" 24# J-55 STC

The intention for the cementing program for the Surface Casing is to:

- Place the Tail Slurry from the casing shoe to 300' above the casing shoe,
- Bring the Lead Slurry to surface.

Spacer: 20 bbls Fresh Water

	Slurry	Intervals Ft MD		Weight ppg	Sx	Vol Cuft	Additives	Yield ft ³ /sx
Lead	Class C	Surface	535' – 580'	13.6	350	595	4%Bentonite 2%CaCl2 .125%Polyflake 0.2% antifoam Excess =230% based on gauge hole volume	1.70
Tail	Class C	535' – 580'	835' – 880'	14.8	200	268	1% CaCl2 Excess = 100% based on gauge hole volume	1.34

Displacement: Fresh Water.

Note: In accordance with the Pecos District Conditions of Approval, we will Wait on Cement (WOC) for a period of not less than 18 hrs after placement or until at least 500 psi compressive strength has been reached in both the Lead Slurry and Tail Slurry cements on the Surface Casing, whichever is greater.

(Date: July 24, 2012) Page 3 of 8

5-1/2" Production Casing & Cementing Program: 5-1/2" 17# L-80 LTC

The intention for the cementing program for the Production Casing is to:

- Place the Tail Slurry from the casing shoe to a point approximately 200' above the top of the Paddock,
- Bring the Lead Slurry to surface.

Spacer: 20 bbls Fresh Water

	Slurry Intervals Ft MD			, ,		Vol Cuft	Additives	Yield ft³/sx	
Lead	50:50 Poz/C	Surface	5200'	11.8	1000	2640	10% Bentonite 8 lbs/sx Salt 0.4% Fluid loss additive 0.125% LCM if needed Excess = 220% or more if needed based on gauge hole volume	2.64	
Tail	Class H	5200'	6982' – 7027'	16.4	650	696	0.2% Fluid loss additive 0.3% Dispersant 0.15% Retarder 0.2% Antifoam Excess = 100% or more if needed based on gauge hole volume	1.07	

Displacement: Fresh Water with approximately 250 ppm gluteraldehyde biocide.

Proposal for Option to Adjust Production Casing Cement Volumes:

The production casing cement volume presented above are estimates based on gauge 7-7/8" hole. We will adjust these volumes based on the caliper log data for each well and our trends for amount of cement returns to surface. Also, if no caliper log is available for any particular well, we would propose an option to possibly increase the production casing cement volume to account for any uncertainty in regard to the hole volume.

4. Pressure Control Equipment:

A <u>11" 3M</u> system will be installed, used, maintained, and tested accordingly as described in Onshore Oil and Gas Order No. 2.

Our BOP equipment will be:

- o Rotating Head
- o Annular BOP, 11" 3M
- o Blind Ram, 11" 3M
- o Pipe Ram, 11" 3M

After nippling up, and every 30 days thereafter or whenever any seal subject to test pressure is broken followed by related repairs, blowout preventors will be pressure tested. BOP will be inspected and operated at least daily to insure good working order. All pressure and operating tests will be done by an independent service company and recorded on the daily drilling reports. BOP will be tested using a test plug to isolate BOP stack from casing. BOP test will include a low pressure test from 250 to 300 psi for a minimum of 10 minutes or until requirements of test are met, whichever is longer. Ram type preventers and associated equipment will be tested to the approved stack working pressure of 3000 psi isolated by test plug. Annular type preventers will be tested to 50 percent of rated working pressure, and therefore will be tested to 1500 psi. Pressure will be held for at least 10 minutes or until provisions of test are met, whichever is longer. Valve on casing head below test plug will be open during testing of BOP stack. BOP will comply with all provisions of Onshore Oil and Gas Order No. 2 as specified. See Attached BOPE Schematic.

(Date: July 24, 2012)

5. Proposed Mud System

The mud systems that are proposed for use are as follows:

DEPTH	TYPE	Density ppg	FV sec/qt	API Fluid Loss cc/30 min	рН	Vol bbi
0 – Surface Casing Point	Fresh Water or Fresh Water Native Mud	8.5 – 9.0	28 – 40	N.C.	N.C.	120 – 160
Surface Casing Point to TD	Brine (Saturated NaCl ₂)	10	29	N.C.	10 – 11	400 – 750
Conversion to Mud at TD	Brine Based Mud (NaCl ₂)	10	34 – 45	5 – 10	10 – 11	0 – 750

Drilling mud containing H2S shall be degassed in accordance with API RP-49, item 5.14. The gases shall be piped into the flare system. Gas detection equipment and pit level flow monitoring equipment will be on location. ConocoPhillips Company will maintain sufficient mud and weighting material on location at all times.

Proposal for Option to Not Mud Up at TD:

FW, Brine, and Mud volume presented above are estimates based on gauge 12-1/4" or 7-7/8" holes. We will adjust these volume based on hole conditions. Also, we propose an option to not mud up leaving only brine in the hole.

6. Logging, Coring, and Testing Program:

- a. No drill stem tests will be done
- b. Mud logging is planned for the production hole section.
- c. No whole cores are planned
- d. The open hole electrical logging program is planned to be as follows:
 - Total Depth to 2500': Resistivity, Density, and Gamma Ray
 - Total Depth to surface Casing Shoe: Caliper
 - Total Depth to surface, Gamma Ray and Neutron
 - Formation pressure data (XPT) on electric line if needed (optional)
 - Rotary Sidewall Cores on electric line if needed (optional)
 - BHC or Dipole Sonic if needed (optional)
 - Spectral Gamma Ray if needed (optional)

7. Abnormal Pressures and Temperatures:

- No abnormal pressures are expected to be encountered.
- Loss of circulation is a possibility in the horizons below the Top of Grayburg. We expect that normal Loss of Circulation Material will be successful in healing any such loss of circulation events.
 - The bottom hole pressure is expected to be 8.55 ppg gradient.
 - o The expected Bottom Hole Temperature is 115 degrees F.
- The estimated H₂S concentrations and ROE calculations for the gas in the zones to be penetrated are presented in the table below for the various producing horizons in this area:

FORMATION / ZONE	H2S (PPM)	Gas Rate (MCFD)	ROE 100 PPM	ROE 500 PPM
Grayburg / San Andres (from MCA)	14000	38	59	27
Yeso Group	400	433	34	15

ConocoPhillips will comply with the provisions of Oil and Gas Order # 6

(Date: July 24, 2012) Page 5 of 8

6. Anticipated starting date and duration of operations:

Well pad and road constructions will begin as soon as all agency approvals are obtained. Anticipated date to drill these wells begin from late 2012 through the 2013 after receiving approval of the APD.

Attachments:

- Attachment # 1 BOP and Choke Manifold Schematic 3M System
- Attachment # 2 Diagram of Choke Manifold Equipment

Contact Information:

Program prepared by: James Chen Drilling Engineer, ConocoPhillips Company Phone (832) 486-2184 Cell (832) 768-1647 Date: 17 July 2012

(Date: July 24, 2012)

Request for Variance

ConocoPhillips Company

Lease Number: LC 060329 Well: Emerald Federal #7

Location: UL A, Sec. 17, T17S, R32E; 990' FNL and 330' FEL

Date: 09-18-12

Request:

ConocoPhillips Company respectfully requests a variance to install a flexible choke line instead of a straight choke line prescribed in the Onshore Order No. 2, III.A.2.b Minimum standards and enforcement provisions for choke manifold equipment. This request is made under the provision of Onshore Order No. 2, IV Variances from Minimum Standard. The rig to be used to drill this well is equipped with a flexible choke line if the requested variance is approved and determined that the proposed alternative meets the objectives of the applicable minimum standards.

<u>Justifications:</u>

The applicability of the flexible choke line will reduce the number of target tees required to make up from the choke valve to the choke manifold. This configuration will facilitate ease of rig up and BOPE Testing.

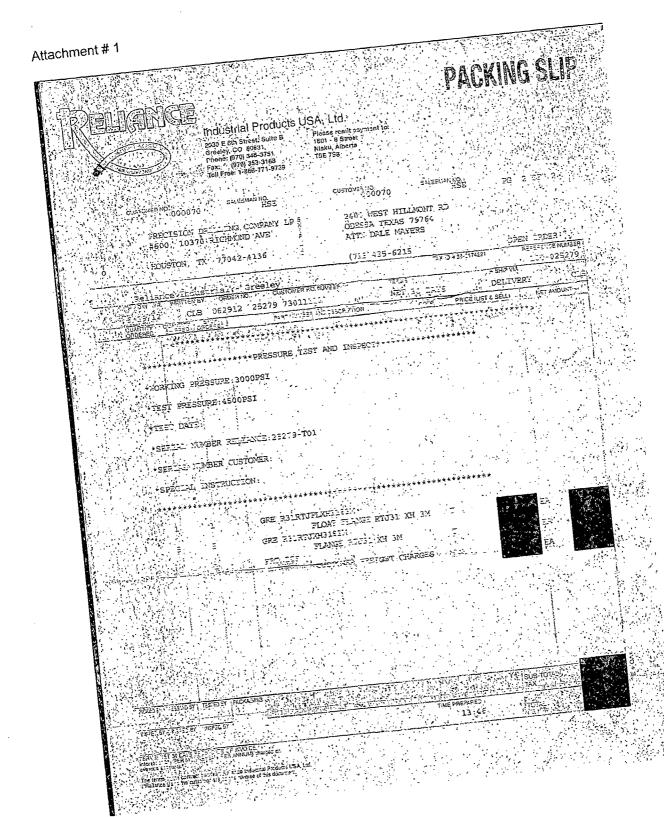
Attachments:

- Attachment # 1 Mill Certification
- Attachment # 2 Specification
- Attachment # 3 Certified & Signed Pressure Test from Manufacturer

Contact Information:

Program prepared by: James Chen Drilling Engineer, ConocoPhillips Company Phone (832) 486-2184 Cell (832) 768-1647

Date: 18 September 2012













Reliance Eliminator Choke & Kill 3000 PSI

This hose can be used as a choke hose which connects the BOP stack to the bleed-off manifold or a kill hose which connects the mud stand pipe to the BOP kill valve.

The Reliance Eliminator Choke & Kill hose contains a specially bonded compounded cover that replaces rubber covered Asbestos, Fibreglass and other fire retardant materials which are prone to damage. This high cut and gouge resistant cover overcomes costly repairs and downtime associated with older designs.

Non	ı. ID	Nor	n OD	We	ight	Min Be	nd Radius	Max	WP
in.	mm,	in.	mm -	lb/fi	kg/m	in.	mm.	psi	Мра
3	76.2	4.53	115.06	8.99	13.31	30	762.0	3000	20,68
3-1/2	88.9	5.00	127	11.01	16.29	36	914.4	3000	20.68

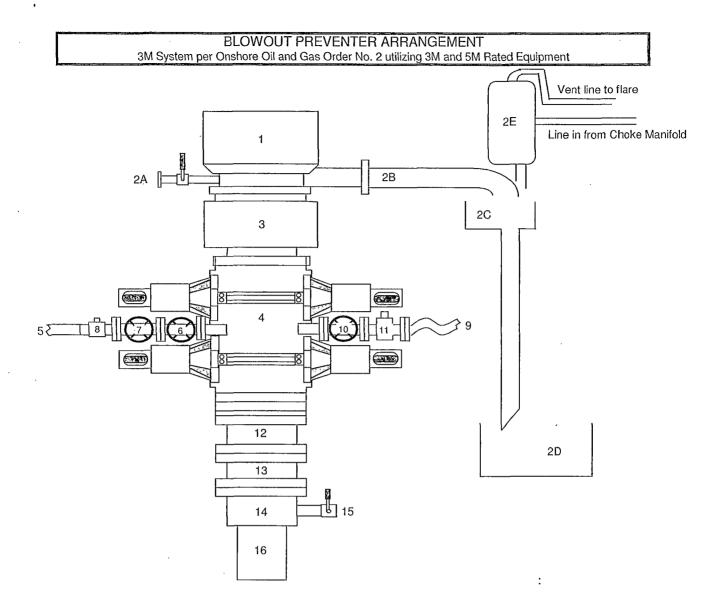


Fittings	Flanges	Hammer Unions	Other
RC4X5055	R35 - 3-1/8 5000# API Type 6B	All Union Configurations	LP Threaded Connection
RC3X5055 RC4X5575	R31 - 3-1/8 3000# API Type 6B		Graylock Custom Ends

Conducted By:

Acceptable Not Acceptable FLORES M.

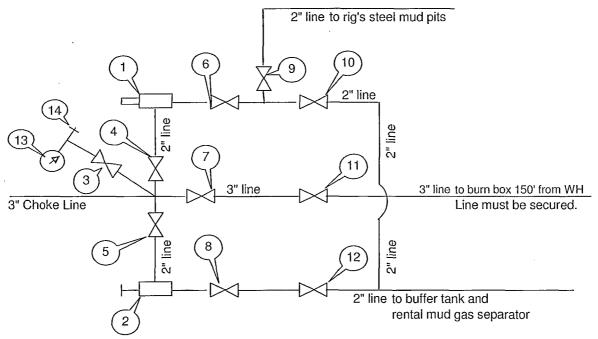
Test Technician



Item	Description
1	Rotating Head, 11"
2A	Fill up Line and Valve
2B	Flow Line (10")
2C	Shale Shakers and Solids Settling Tank
2D	Cuttings Bins for Zero Discharge
2E	Rental Mud Gas Separator with vent line to flare and return line to mud system
3	Annular BOP (11", 3M)
4	Double Ram (11", 3M, equipped with Blind Rams and Pipe Rams)
5	Kill Line (2" flexible hose, 3000 psi WP)-
. 6	Kill Line Valve, Inner (3-1/8", 3000 psi WP)
7 .	Kill Line Valve, Outer (3-1/8", 3000 psi WP)
8	Kill Line Check Valve (2-1/16", 3000 psi WP
9	Choke Line (Stainless Steel Coflex Line, 3-1/8", 3000 psi WP)
10	Choke Line Valve, Inner (3-1/8", 3000 psi WP)
11	Choke Line Valve, Outer, (Hydraulically operated, 3-1/8", 3000 psi WP)
12	Adapter Flange (11" 5M to 11" 3M)
13	Spacer Spool (11", 5M)
14	Casing Head (11" 5M)
15	Ball Valve and Threaded Nipple on Casing Head Outlet, 2" 5M
16	Surface Casing

CHOKE MANIFOLD ARRANGEMENT

3M System per Onshore Oil and Gas Order No. 2 utilizing 3M and 5M Equipment



All Tees must be targeted

Item	Description	
1	Remote Controlled Hydraulically Operated Adjustable Choke, 2-1/16", 3M	
2	Manual Adjustable Choke, 2-1/16", 3M	
3	Gate Valve, 2-1/16" 5M	
4	Gate Valve, 2-1/16" 5M	
5	Gate Valve, 2-1/16" 5M	
6	Gate Valve, 2-1/16" 5M	
7	Gate Valve, 3-1/8" 3M	
8	Gate Valve, 2-1/16" 5M	
9	Gate Valve, 2-1/16" 5M	
10	Gate Valve, 2-1/16" 5M	
11	Gate Valve, 3-1/8" 3M	
12	Gate Valve, 2-1/16" 5M	
13	Pressure Gauge	
14	2" hammer union tie-in point for BOP Tester	

We will test each valve to 3000 psi from the upstream side.

Drawn by:

Steven O. Moore

Chief Drilling Engineer, Mid-Continent Business Unit, ConocoPhillips Company

Date: 14-Sept-2012

Closed Loop System Design, Operating and Maintenance, and Closure Plan

ConocoPhillips Company Well: Emerald Federal #7

Location: Sec. 17, T17S, R32E

Date: 08-07-12

ConocoPhillips proposes the following plan for design, operating and maintenance, and closure of our proposed closed loop system for the above named well:

1. We propose to use a closed loop system with steel pits, haul-off bins, and frac tanks for containing all cuttings, solids, mud, water, brine, and liquids. We will not dig a pit, nor will we use a drying pad, nor will we build an earth pit above ground level, nor will we dispose of or bury any waste on location.

All drilling waste and all drilling fluids (fresh water, brine, mud, cuttings, drill solids, cement returns, and any other liquid or solid that may be involved) will be contained on location in the rig's steel pits or in hauloff.bins or in frac tanks as needed. The intent is as follows:

- We propose to use the rigs's steel pits for containing and maintaining the drilling fluids.
- We propose to remove cuttings and drilled solids from the mud by using solids control equipment and to contain such cuttings and drilled solids on location in haul-off bins.
- We propose that any excess water that may need to be stored on location will be stored in tanks.

The closed loop system components will be inspected daily by each tour and any need repairs will be made immediately. Any leak in the system will be repaired immediately, and any spilled liquids and/or solids will be cleaned immediately, and the area where any such spill occurred will be remediated immediately.

2. Cuttings and solids will be removed from location in haul-off bins by an authorized contractor and disposed of at an authorized facility. For this well, we propose the following disposal facility:

Controlled Recovery Inc, 4507 West Carlsbad Hwy, Hobbs, NM 88240, P.O. Box 388; Hobbs, New Mexico 88241 Toll Free Phone: 877.505.4274, Local Phone Number: 432.638.4076

The physical address for the plant where the disposal facility is located is Highway 62/180 at mile marker 66 (33 miles East of Hobbs, NM and 32 miles West of Carlsbad, NM).

The Permit Number for CRI is R9166

A photograph showing the type of haul-off bins that will be used is attached.

- 3. Mud will be transported by vacuum truck and disposed of at Controlled Recovery Inc at the facility described above.
- 4. Fresh Water and Brine will be hauled off by vacuum truck and disposed of at an authorized salt water disposal well. We propose the following for disposal of fresh water and brine as needed:
 - Nabors Well Services Company, 3221 NW County Rd; Hobbs, NM 88240, PO 5208 Hobbs, NM, 88241, Permit SWD 092. (Well Location: Section 3, T19S R37E)
 - Basic Energy Services, P.O. Box 1869; Eunice, NM 88231 Phone Number: 575.394.2545, Facility located at Hwy 18, Mile Marker 19; Eunice, NM.

James Chen
Drilling Engineer
Office: 832.486.2184
Cell: 832.678.1647

SPECIFICATIONS

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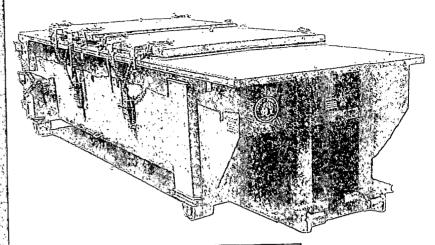
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OPENING: (2) OF X 92" OPENING with EP civiler centered on .

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Heavy Duty Split Metal Rolling Lid



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20 YD	41	53
25 YD	53	65
30 YD	65	77

