		OCD H	lobbs		all	/		
		0001		ATS-14	- 845	フ		
vm 3160-3		HOBBS OC	D	FORM	APPROVEI	)		
Aarch 2012)		DEC 09 21	111	OMB M Expires (	Vo. 1004-0137 October 31, 20	14		
DEPARTMENT OF THE IN	NTERIOR	UEL VO Z	<b>FI</b>	5. Lease Serial No. NMLC061863	-A			
BUREAU OF LAND MANA		DEEDE	D	6. If Indian, Allotee	or Tribe N	ame		
a. Type of work: I DRILL REENTED	R			7. If Unit or CA Agre	ement, Nar	ne and	No.	
b. Type of Well: Oil Well Gas Well Other	<b>√</b> Sin	gle Zone 🔲 Multip	le Zone	8. Lease Name and Trionyx 6 Fed	Well No. 🔇 11H	3	83	87
2. Name of Operator Devon Energy Production Company, L.P	· (613	37)		9. API Well No.	-42	-3	12	
a. Address 333 W. Sheridan 3	Bb. Phone No.	(include area code)		10. Field and Pool, or	Exploratory			, la
Oklahoma City, OK 73102-5010	400-228-	/203 		Paduca; Delawa	arg NO		H G Area	57
At surface 215 FSL & 505 FWL, 7 PP: 330 FSL	& 660 FWL	ORTHOD	OX	Sec. 6 T25S R3	32E	<b>.</b> j 01		
At proposed prod. zone 330 FNL & 660 FWL, 4	תנ	T ACATIO	N.					
<ol> <li>Distance in miles and direction from nearest town or post office* Approximately 21 miles SE of Malaga, NM</li> </ol>		TOCUTTO	<u>.</u>	12. County or Parish Lea County		13. SI NM	ate	
5. Distance from proposed* location to nearest See attached map	16. No. of ac	res in lease	17. Spacin	g Unit dedicated to this	well			•
property or lease line, ft. (Also to nearest drig. unit line, if any)	NMLC061	863-A 1882.6ac	159.73	3 ac				
<ol> <li>Distance from proposed location* See attached map to nearest well, drilling, completed, applied for, on this lease, ft.</li> </ol>	19. Proposed 8285' TVD	Depth 12,792' MD	20. BLM/ CO-110	BIA Bond No. on file 4; NBM-000801				
Elevations (Show whether DF, KDB, RT, GL, etc.) 3438.8 GL	22. Approxim	ate date work will star	t•	23. Estimated duration 45 Days	<i>т</i>			
	24. Attac	ments		(				•
ne following, completed in accordance with the requirements of Onshore	Oil and Gas (	order No.1, must be at	tached to th	is form:				•
. Well plat certified by a registered surveyor.		4. Bond to cover the	ne operatio	ns unless covered by ar	existing b	ond or	ı file (see	
A Drilling Plan. A Surface Use Plan (if the location is on National Forest System L	ands, the	5. Operator certific	ation					
SUPO must be filed with the appropriate Forest Service Office).		6. Such other site BLM.	specific inf	ormation and/or plans a	s may be re	quirec	l by the	
5. Signature -	Name (	Printed/Typed)		and an and a second	Date			:
the me in	Trina	. Couch			04/30/2	014		
Regulatory Analyst					<u></u>			-
pproved by (Signature)	Name	Printed/Typed)			Danov	2	5 20	14
tle FIELD MANAGER	Office				F			•
polication approval does not warrant or certify that the applicant holds	legal or equita	ble title to those righ	ts in the sul	piect lease which would	entitle the a	oplica	ntto	-
nduct operations thereon.	-0							RS
the 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a critates any false, fictitious or fraudulent statements or representations as to	me for any pe any matter wi	son knowingly and v thin its jurisdiction.	villfully to r	nake to any department	or agency (	of the	United	<u>i</u> nc
Continued on page 2)		17		*(Ins	tructions	on ț	bage 2)	:
		Ks,	1.					

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Approval Subject to General Requirements & Special Stipulations Attached

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SEE ATTACHED FOR CONDITIONS OF APPROVAL

#### HOBBS OCD

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#### RECEIVED

B. The amount of funds contributed was derived from the rate schedule established within Appendix B of the MOA. The amount of the funding contribution acknowledged on this form reflects those rates.

C. The BLM will utilize the funding to carry out a program of mitigation at high-priority sites whose study is needed to answer key questions identified within the Regional Research Design.

D. Donating to the fund is voluntary. Industry acknowledges that it is aware it has the right to pay for Class III survey rather than contributing to the mitigation fund, and that it must avoid or

fund data recovery at those sites already recorded that are eligible for nomination to the National Register or whose eligibility is unknown and that any such payments are independent of the mitigation funds established by this MOA.

E. Previously recorded archeological sites determined eligible for nomination to the National Register or whose eligibility remains undetermined must be avoided or mitigated.

F. If any skeletal remains that might be human or funerary objects are discovered by any activities, the land-use applicant will cease activities in the area of discovery, protect the remains, and notify the BLM within 24 hours. The BLM will determine the appropriate treatment of the remains in consultation with culturally affiliated Indian Tribe(s) and lineal descendents. Applicants will be required to pay for treatment of the cultural items independent and outside of the mitigation fund.

mpany-Authorized Officer

05/14/2014 Date

BLM-Authorized Officer

Date

## HOBBS OCD

#### DRILLING PROGRAM

DEC 032014

Devon Energy Production Company, L.P. RECEIVED

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#### 1. Geologic Name of Surface Formation: Quaternary

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#### 2. Estimated Tops of Geological Markers & Depths of Anticipated FW, Oil, or Gas:

а.	Fresh Water	400′	
b.	Rustler	705'	Barren
c.	Top of Salt	1073'	Barren
d.	Base of Salt	4155'	Barren
e.	Delaware	4385'	Oil / Gas
f.	Bell Canyon	4411'	Oil / Gas
g.	Cherry Canyon	5382'	Oil / Gas
h.	Brushy Canyon	6765'	Oil / Gas
i.	Bone Spring	8359'	Oil / Gas
	Total Depths	8285' TVD	12792' MD

#### 3. Pressure Control Equipment:

A 3M 13-5/8" BOP system (Double Ram and Annular preventer) will be installed and tested prior to drilling out the surface casing shoe. The BOP system used to drill the intermediate hole will be tested per BLM Onshore Oil and Gas Order 2.

A 3M 13-5/8" BOP system (Double Ram and Annular preventer) will be installed and tested prior to drilling out the intermediate casing shoe. The BOP system used to drill the production hole will be tested per BLM Onshore Oil and Gas Order 2.

The pipe rams will be operated and checked each 24 hour period and each time the drill pipe is out of the hole. These tests will be logged in the daily driller's log. A 2" kill line and 3" choke line will be incorporated into the drilling spool below the ram BOP. In addition to the rams and annular preventer, additional BOP accessories include a kelly cock, floor safety valve, choke lines, and choke manifold rated at 3,000 psi WP.



Devon requests a variance to use a flexible line with flanged ends between the BOP and the choke manifold (choke line); if an H&P rig drills this well. Otherwise no flex line is needed. The line will be kept as straight as possible with minimal turns.

#### **Auxiliary Well Control and Monitoring Equipment:**

- a. A Kelly cock will be in the drill string at all times.
- b. A full opening drill pipe stabbing valve having the appropriate connections will be on the rig floor at all times.

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#### Casing Program:

4. See COA

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Hole Size	Hole Interval	Casing OD	Casing Interval	Weight (lb/ft)	Collar	Grade	Collapse Design Factor	Burst Design Factor	Tension Design Factor
17-1/2"	0 - 750'	13-3/8"	0 - 750'	48	STC	H-40	2.30	5.16	15.03
12-1/4"	750-4490	9-5/8"	0-4490'	40	втс	HCK-55	1.81	1.69	5.16
8-3/4"	4490-12792'	5-1/2″	0-12792'	17	BTC	P-110	1.88	2.68	4.03

#### **Casing Notes:**

• All casing is new and API approved

#### Maximum Lateral TVD: 8285'

#### 5. Proposed mud Circulations System:

Depth	Mud Weight	Viscosity	Fluid Loss	Type System
0-750'	8.4-8.6	30-34	N/C	FW
750-4490	10.0	28-32	N/C	Brine
4490-12792'	8.6-9.2	28-32	N/C	FW

The necessary mud products for weight addition and fluid loss control will be on location at all times. Visual mud monitoring equipment will be in place to detect volume changes indicating loss or gain of circulating fluid volume. If abnormal pressures are encountered, electronic/mechanical mud monitoring equipment will be installed.

#### 6. Cementing Table:

	String	Number of sx	Weight Ibs/gal	Water Volum e g/sx	Yield cf/sx	Stage; Lead/Tail	Slurry Description		
	13-3/8" Surface	820	14.8	6.32	1.33	Tail	Class C Cement + 0.125 lbs/sack Poly-E-Flake + 63.5% Fresh Water		
	9-5/8"	950	12.9	9.81	1.85	Lead	(65:35) Class C Cement: Poz (Fly Ash): 6% BWOC Bentonite + 5% BWOW Sodium Chloride + 0.125 Ibs/sack Poly-E-Flake + 70.9 % Fresh Water		
	Casing	430	14.8	6.32	1.33	Tail	Class C Cement + 0.125 lbs/sack Poly-E-Flake + 63.5% Fresh Water		
	E 1/3"	370	12.5	10.86	1.96	Lead	(65:35) Class H Cement: Poz (Fly Ash) + 6% BWOC Bentonite + 0.25% BWOC HR-601 + 0.125 lbs/sack Poly- E-Flake + 74.1 % Fresh Water		
-	Production Casing	1330	14.5	5.31	1.21	Tail	(50:50) Class H Cement: Poz (Fly Ash) + 0.5% bwoc HALAD-344 + 0.25% bwoc CFR-3 + 0.2% bwoc HR-601 + 2% bwoc Bentonite + 58.8% Fresh Water		
5	2-Stage	DV Tool @ 5,500ft							
Ĉ	074 <sup>option</sup>	110	11	14.94	2.66	Lead	Tuned Light <sup>®</sup> Cement + 0.125 lb/sk Pol-E-Flake + 76.5% Fresh Water		
		120	14.8	6.32	1.33	Tail	Class C Cement + 0.2% HR-800 + 63.5% Fresh Water		
	5-1/2" Production	440	11	14.94	2.66	Lead	Tuned Light <sup>®</sup> Cement + 0.125 lb/sk Pol-E-Flake + 76.5% Fresh Water		
Set	Casing Single Stage	1330	14.5	5.31	1.21	Tail	(50:50) Class H Cement: Poz (Fly Ash) + 0.5% bwoc HALAD-344 + 0.25% bwoc CFR-3 + 0.2% bwoc HR-601 + 2% bwoc Bentonite + 58.8% Fresh Water		

#### **TOC for all Strings:**

Surface	@	0′
Intermediate	@	0' Canod
Production	@	3990' 20 001

#### Notes:

- Cement volumes Surface 100%, Intermediate 50%, Production based on at least 25% excess
- Actual cement volumes will be adjusted based on fluid caliper and/or caliper log data.
- If severe loss circulation is encountered while drilling the production wellbore, a DV tool will be installed a minimum of 50' below the previous casing shoe and of 200' above the current shoe. If the DV tool has to be moved, the cement volumes will be adjusted proportionately.

#### 7. Logging, Coring, and Testing Program:

- a. Drill stem tests will be based on geological sample shows.
- b. If a drill stem test is anticipated, a procedure, equipment to be used, and safety measures will be provided via sundry notice to the BLM.
- c. Resistivity and porosity logs are planned below the intermediate casing point. Stated logs run will be named in the Completion Report and submitted to the BLM.
- d. No coring program is planned
- e. Additional Testing will be initiated subsequent to setting the production casing. Specific intervals will be targeted based on log evaluation (if applicable), geological sample shows, and drill stem tests.

#### 8. Potential Hazards:

- a. No abnormal pressures or temperatures are expected. There is no known presence of H2S in this area, and none is anticipated to be encountered. If H2S is encountered the operator will comply with the provisions of Onshore Oil and Gas Order No. 6. No lost circulation is expected to occur. All personnel will be familiar with all aspects of safe operation being used to drill this well. Estimated BHP: 3728 psi, and estimated BHT: 141 degrees.
- b. Hydrogen Sulfide detection equipment will be in operation after drilling out the surface casing shoe until the production string is cemented. Breathing equipment will be on location upon drilling the surface casing shoe until total depth is reached.

#### 9. Anticipated Starting Date and Duration of Operations:

a. Road and location construction will begin after the BLM has approved the APD. Anticipated spud date will be as soon after BLM approval and as soon as a rig will be available. Move in operations and drilling is expected to take 20 days. If production casing is run then an additional 30 days will be needed to complete well and construct surface facilities and/or lay flow lines in order to place well on production.



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5D Plan Report

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5D Plan Report

<b>Devon Energ</b>	Y
Field Name:	Lea Co, NM Nad 83 NMEZ
Site Name:	Trionyx 6 Fed 11H
Well Name:	Trionyx 6 Fed 11H
Plan:	P1:V1

08 May 2014



Weatherford International Limited

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5D 7.5.8 : 8 May 2014, 13:24:08 UTC

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		Trionyx 6	Fed 11⊦							
1- -	Map Units : US ft		Com	pany Name :	Devon Energy					
Sield Name	Vertical Reference	Datum (VRD) : Mean S	ea Level							
Field Name	Projected Coordinate System : NAD83 / New Mexico East (ftUS)									
Lea Co, NM Nad 83 NMEZ	Comment :									
мана с стана Х	Units: US ft	North Reference : (	Grid	Convergence	e Angle : 0.33					
e de la composition de	D 11	Northing : 419815.6	9 US ft	Latitude: 32	° 9' 9.62"	· · · · · · · · · · · · · · · · · · ·				
Site Name	Position	Easting : 730733.22	⊍S ft	Longitude :	-103° 43' 16.84	ei .				
Trionyx 6 Fed 11H	Elevation above Mean.Sea.Level:3439.00 US ft Comment :									
8		Position (Offs	ets relative t	o Site Centre	)					
· ·	+N / -S: 0.00 US	t Northing :419815.6	9 US ft							
Slot Name	+E / -W : 0.00 US	ft Easting :730733.22	US ft							
Trionvx 6 Fed	Elevation above Mean Sea Level : 3439.00 US ft									
11H	Comment :									
	Type : Main well		UWI :		Plan:P1:V1					
Well Name	Rig Height <i>Drill F</i> Relative to Mean ft	<i>loor</i> : 25.00 US ft Sea Level: 3464.00 US	Comment : JS							
Trionyx 6 Fed	Closure Distance	: 4731.1 US ft	<b>Closure Azi</b>	<b>nuth :</b> 1.63622	<u>2</u> °					
11H	Vertical Section (	Position of Origin Relat	ive to Slot )							
		+N / -S: 0.00 US ft	+E/-W: 0.00 US ft Az:1.64°							
	Magnetic Paramet	ters								
1	Model : BGGM	Field Strength : 48247.1nT	<b>Dec :</b> 7.39°		<b>Dip :</b> 60.00°	<b>Date :</b> 15/Jul/2014				

Target Set

Name : Trionyx 6 Fed 11H Number of Targets : 1

Comment :

Target	Position (Relative to Slot centre)									
Name:	+N / -S : 4729.17US ft	Northing : 424544.86 US ft	Latitude : 32°9'56.41"							
PBHL 11H	+E/-W : 135.09 US ft	Longitude : -103°43'14.96"								
Shape:	TVD (Drill Floor) : 8285.00	US ft	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,							
Cuboid	Orientation Azimuth : 0.00 Dimensions Length : 20.00	0° <b>Inclination :</b> 0.00° ) US ft <b>Breadth :</b> 20.00 US f	t Height : 20.00 US ft							

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Casing Points (R	elative to Slot	centre, TVD rel	ative to Drill Flo	юг)				
MD (US ft)	Inc (°)	Az (°)	TVD (US ft)	N.Offset (US ft)	t.Offset (US ft)	Northing (US ft)	Easting (US ft)	Name
750.00	0.00	0.00	750.00	0.00	0.00	419815.69	730733.22	13 3/8 in
4490.00	0.00	0.00	4490.00	0.00	0.00	419815.69	730733.22	9 5/8 in

Well path created using minimum curvature

Weatherford International Limited

and the second second

5D Plan Report

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Salient P	oints (Re	lative to	Slot centr	e, TVD rel	ative to	Drill Floc	)			·· .		
MD (US ft)	Inc (°)	· Az (°)	TVD (US ft)	N:Offset (US ft)	E.Offset (US ft)	DES (°/100 US ft)	VS . (US ft)	B.Rate (°/100 US ft)	T.Raté (°/100 US ft)	T.Face (°)	Commen t	
0:00	0:00	0:00	0.00 <sup>7</sup>	0.00	0.00	0:00	0.00	0.00	0.00	0.00		
750.00	0.00	0.00	750.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	13 3/8 in	
4490.00	0.00	0.00	4490.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	9 5/8 in	
7764.13	0.00	0.00	7764:13	0.00	0.00	0.00	0.00	0.00	0.00	0.00	KOP	
8582.31	90.00	1.64	8285.00	520.66	14.87	11.00	520.87	11.00	0.00	1.64	LP	
12792.5 4	90.00	1.64	8285.00	4729.17	135.09	0.00	4731.10	0.00	0.00	0.00	PBHL 6H	

Interpolated I	Points (Relat	tive to Slot c	entre, TVD rel	ative to Drill	Floor)					
MD (US ft)	Inc (°)	Az (°)	TVD (US ft)	N.Offset (US ft)	E.Offset (US ft)	VS (US ft)	DLS (°/100 US ft)	Northing (US ft)	Easting (US ft)	Comment
7700.00	0.00	0.00	7700.00	0.00	0.00	0.00	0.00	419815.69	730733.22	
7764.13	0.00	0.00	7764.13	0.00	0.00	0.00	0.00	419815.69	730733.22	KOP
7800.00	3.95	1.64	7799.97	1.23	0.04	1.23	11.00	419816.92	730733.26	
7900.00	14.95	1.64	7898.46	17.61	0.50	17.62	11.00	419833.30	730733.72	
8000.00	25.95	1.64	7992.02	52.48	1.50	52.50	11.00	419868.17	730734.72	
8100.00	36.95	1.64	8077.20	104.55	2.99	104.59	11.00	419920.24	730736.21	
8200.00	47.95	1.64	8150.88	171.90	4.91	171.97	11.00	419987.59	730738.13	
8300.00	58.95	1.64	8210.35	252.08	7.20	252.18	11.00	420067.77	730740.42	
8400.00	69.95	1.64	8253.42	342.12	9.77	342.26	11.00	420157.81	730742.99	
8500.00	80.95	1.64	8278.51	438.72	12.53	438.90	11.00	420254.41	730745.75	
8582.31	90.00	1.64	8285.00	520.66	14.87	520.87	11.00	420336.35	730748.09	LP
8600.00	90.00	1.64	8285.00	538.34	15.38	538.56	0.00	420354.03	730748.60	
8700.00	90.00	1.64	8285.00	638.30	18.23	638.56	0.00	420453.99	730751.45	
8800.00	90.00	1.64	8285.00	738.26	21.09	738.56	0.00	420553.95	730754:31	
8900.00	90.00	1.64	8285.00	838.22	23.94	838.56	0.00	420653.91	730757.16	
9000.00	90.00	1.64	8285.00	938.18	26.80	938.56	0.00	420753.87	730760.02	
9100.00	90.00	1.64	8285.00	1038.14	29.65	1038.56	0.00	420853.83	730762.87	
9200.00	90.00	1.64	8285.00	1138.10	32.51	1138.56	0.00	420953.79	730765.73	
9300.00	90.00	1.64	8285.00	1238.05	35.37	1238.56	0.00	421053.74	730768.59	
9400.00	90.00	1.64	8285.00	1338.01	38,22	1338.56	0.00	421153.70	730771.44	
9500.00	90.00	1.64	8285.00	1437.97	41.08	1438.56	0.00	421253.66	730774.30	
9600.00	90.00	1.64	8285.00	1537.93	43.93	1538.56	0.00	421353.62	730777.15	
9700.00	90.00	1.64	8285.00	1637.89	46.79	1638.56	0.00	421453.58	730780.01	
9800.00	90.00	1.64	8285.00	1737.85	49.64	1738.56	0.00	421553,54	730782.86	
9900.00	90.00	1.64	8285.00	1837.81	52.50	1838.56	0.00	421653.50	730785.72	
10000.00	90.00	1.64	8285.00	1937.77	55.35	1938.56	0.00	421753.46	730788.57	
10100.00	90.00	1.64	8285.00	2037.73	58.21	2038.56	0.00	421853.42	730791.43	
10200.00	90.00	1.64	8285.00	2137.69	61.06	2138.56	0.00	421953.38	730794.28	
10300.00	90.00	1.64	8285.00	2237.65	63.92	2238.56	0.00	422053.34	730797.14	
10400.00	90.00	1.64	8285.00	2337.61	66.77	2338.56	0.00	422153.30	730799.99	
10500.00	90.00	1.64	8285.00	2437.57	69.63	2438.56	0.00	422253.26	730802.85	
10600.00	90.00	1.64	8285.00	2537.52	72.49	2538.56	0.00	422353.21	730805.71	
10700.00	90.00	1.64	8285.00	2637.48	75.34	2638.56	0.00	422453.17	730808.56	
10800.00	90.00	1.64	8285.00	2737.44	78.20	2738.56	0.00	422553.13	730811.42	
10900.00	90.00	1.64	8285.00	2837.40	81.05	2838.56	0.00	422653.09	730814.27	
11000.00	90.00	1.64	8285.00	2937.36	83.91	2938.56	0.00	422753.05	730817.13	
11100.00	90.00	1.64	8285.00	3037.32	86.76	3038.56	0.00	422853.01	730819.98	
11200.00	90.00	1.64	8285.00	3137.28	89.62	3138.56	0.00	422952.97	730822.84	
11300.00	90.00	1.64	8285.00	3237.24	92,47	3238.56	0.00	423052.93	730825.69	
11400.00	90.00	1.64	8285.00	3337.20	95.33	3338.56	0.00	423152.89	730828.55	
11500.00	90.00	1.64	8285.00	3437.16	98.18	3438.56	0.00	423252.85	730831.40	
11600.00	90.00	1.64	8285.00	3537.12	101.04	3538.56	0.00	423352.81	730834.26	
11700.00	90.00	1.64	8285.00	3637.08	103.89	3638.56	0.00	423452.77	730837.11	
11800.00	90.00	1.64	8285.00	3737.04	106.75	3738.56	0.00	423552,73	730839.97	
11900.00	90.00	1.64	8285.00	3836.99	109.60	3838.56	0.00	423652.68	730842.82	
12000-00	90.00	1.64	8285.00	3936.95	112.46	3938.56	0.00	423752.64	730845.68	
12100.00	90.00	1.64	8285.00	4036.91	115.32	4038.56	0.00	423852.60	730848.54	
12200.00	90.00	1.64	8785.00	4136.97	118 17	4138 56	0.00	423952 56	730851 39	
	20.00	1.04	0203.00	4130.01		-130.00	0.00		,	

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5D 7.5.8 : 8 May 2014, 13:24:08 UTC

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Interpolated I	Points (Relati	ive to Slot o	entre, TVD rel	ative to Drill	Floor)					
MD (US'ft)	Inc (°)	A2 (°)	TVD (US ft)	N.Offset (US ft)	E.Offset (US ft)	VS (US ft)	DLS (°/100 US ft)	Northing (US ft)	Easting (US ft)	Comment
12300.00	90.00	1.64	8285.00	4236.83	121.03	4238:56	0:00	424052.52	730854.25	
12400.00	90.00	1.64	8285.00	4336.79	123.88	4338.56	0.00	424152.48	730857.10	
12500.00	90.00	1.64	8285.00	4436.75	126.74	4438.56	0.00	424252.44	730859.96	
12600.00	90.00	1.64	8285.00	4536.71	129.59	4538.56	0.00	424352.40	730862.81	
12700.00	90.00	1.64	8285.00	4636.67	132.45	4638.56	0.00	424452.36	730865.67	
12792.54	90.00	1.64	8285.00	4729.17	135.09	4731.10	0.00	424544.86	730868.31	PBHL 6H
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5D Anti-Collision Report

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**5D Anti-Collision Report** 

## Devon Energy

Field Name:	Lea Co, NM Nad 83 NMEZ
Site Name:	Trionyx 6 Fed 11H
Well Name:	Trionyx 6 Fed 11H

08 May 2014



Weatherford International Limited

5D 7.5.8 : 8 May 2014, 13:23:31 UTC

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		Trionyx 6	Fed 11F	•		ter ang
	Map Units : US ft		Com	pany Name :	Devon Energy	
	Vertical Reference	Datum (VRD) : Mean S	ea Level			
Field Name	Projected Coordina	te System : NAD83 / N	ew Mexico Eas	st (ftUS)		
Lea Co, NM Nad 83 NMEZ	Comment :					
	Units : US ft	North Reference : (	Grid	Convergence	<b>e Angle :</b> 0:33 <sup>.</sup>	
		Northing : 419815.6	9 US ft	Latitude : 32	2° 9' 9.62"	
Site Name	Position	Easting : 730733.22	US ft	Longitude :	-103° 43' 16.84	jii
Trionyx 6 Fed 11H	Elevation above Mo Comment :	ean Sea Level:3439.00	US ft			
	· · · · · · · · · · · · · · · · · · ·	Position (Offs	ets relative t	o Site Centre	)	and all the state of the state
	+N / -S : 0.00 US ft	Northing :419815.6	9 UŞ ft	Latitude : 32	2°9'9.62"	
Slot Name	+E / -W : 0.00 US f	t Easting :730733.22	US ft	Longitude :	-103°43'16.84"	
Trionyx 6 Fed 11H	Elevation above Me Comment :	ean Sea Level:: 3439.0	0 US ft			
	Type : Main well		UWI :		Plan : Working	g Plan
Well Name	<b>Rig Height</b> <i>Drill Fl</i> . <b>Relative to Mean S</b> ft	<b>oor :</b> 25.00 US ft <b>ea Level:</b> 3464.00 US	Comment :			
Trionyx 6 Fed	Closure Distance :	4731.1 US ft	Closure Azi	muth : 1.6362	2°	
111H	Vertical Section (P	osition of Origin Relat	ive to Slot )			
	,	+N / -S: 0.00 US ft	+E/-W:0	.00 US ft	<b>Az :</b> 1.64°	
	Magnetic Paramete	ers				
	Model : BGGM	Field Strength : 48247.1nT	<b>Dec :</b> 7.39°		<b>Dip :</b> 60.00°	<b>Date :</b> 15/Jul/2014

Collision / Uncertainty	Analysis			
Primary Well	Start MD	End MD	Collision Risk	No. of Std Deviations in Error
	(US ft)	(US ft)	Interval	Computation
Trionyx 6 Fed 11H (p)	0.00	12792.54	100.00	2

#### Secondary Well Names

Trionyx 6 Fed 1H (s)

Anticollision (ceport (crminology) S.Minor, S.Major :Radii of the ellipse of uncertainty at the current location as seen in the along hole direction. PHI :Angle between high-side vector and semi-iminor axis TVD Spread : Total TVD range of the ellipsoid of uncertainty at the current location ES :Distance between the extremities of the primary and secondary uncertainty ellipsoids in the direction Cr-Cr T.Face to Sec :Angle between the Hi-Side vector of the primary well at the current location and line of closest approach between the two wells

Separation factors calculated using Pedal Curve (Independent Uncertainty). Well path created using minimum curvature.

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SECONDARY Well Name	Pri MD (US ft)		Sec MD (US ft)	TVD (US ft)	CC (US ft)	E5 (US ft)		SF	Rīsk
Trionyx 6 Fed 1H (S)	12792.54		13860.00	8285:00	895.79	810.88		10.55	
Secondary Well :	Trionyx 6 Fee	d 1H (s)	(TVD Relative to D	rill Floor (Prim	nary) ; All Azimuth	Relative to GR	ID NORTH	)	
Pri MD (US ff)	TVD (US.ft)	Sec MD	T.Face to Sec	S.Major	S.Minor		ES (US ft)	SF	Risk
0.00	2.00	0.00	91.70-	0.00	0.00	435.44	434.51	470.22	
100.00	100.50	98.51	91.64	0.13	0.13	435.37	434.20	371.83	
200.00	196.83	194.84	91.53	0.37	0.37	435.67	434.04	266.90	
300.00	300.95	298.97	91.40	0.62	0.62	435.98	433.86	206.40	
400.00	400.71	398.72	91.31	0.88	0.88	435.78	433.19	168.44	
500.00	498.14	496.16	91.25	1.11	1.11	435.91	432.86	143.07	
600.00	597.35	595.36	91.17	1.35	1.35	436.43	432.93	124.45	
700.00	697.00	695.02	91.12	1.57	1.57	437.08	433.13	110.56	
800.00	796.73	794.75	91.11	1.76	1,76	437.80	433.58	103.81	
900.00	896.10	894.13	91.08	1.99	1.99	438.62	433.96	94.16	
1000.00	994.89	992.92	91.03	2.22	2.22	439.64	434.51	85.74	
1100.00	1092.91	1090.96	90.99	2.45	2.46	441.02	435.44	79.04	
1200.00	1194.33	1192.38	90.93	2.71	2.71	442.50	435.44	73.05	
1300.00	1294.59	1292.65	90.89	2.95	2.95	443.74	437.22	68.04	
1400.00	1395.28	1393.35	90.85	3.21	3.20	444.88	437.88	63.51	
1500.00	1495.66	1493.73	90.79	3.46	3.46	445.90	438.41	59.53	
1600.00	1595.93	1594.01	90.77	3.71	3.71	445.84	438.87	56.10	
1700.00	1697.00	1695.08	90.77	3.96	3.96	447.63	439.20	53.07	
1800.00	1798.48	1796.57	90.76	4.22	4.21	448.14	439.23	50.28	
1900.00	1899.63	1897.71	90.76	4.45	4.45	448.35	438.98	47.86	
2000.00	2000.55	1998.63	90.75	4.60	4.60	448.33	438.58	45.99	
2100.00	2100.11	2098.20	90.74	4.66	4.66	448.26	438.22	44.68	
2200.00	2199.40	2197.49	90.75	4.75	4.75	448.31	437.96	43.34	
2300.00	2297.92	2296.01	90.78	4.93	4.93	448.61	437.86	41.76	
2400.00	2397.36	2395.45	90.81	5.15	5.15	449.14	437.95	40.14	
2500.00	2494.97	2493.06	90.83	5.39	5.39	449.98	438.32	38.60	
2600.00	2595,70	2593.80	90.88	5.63	5.62	451,04	438.92	37.20	
2700.00	2693.38	2691.49	90,92	5.86	5.86	452,23	439.65	35.96	
2800.00	2792.43	2790.55	90.95	6.11	6.10	453.81	440.78	34.83	
2900.00	2895.03	2893.16	90.99	6.36	6.36	455.22	441.70	33.66	
3000.00	2998.38	2996.52	91.03	6.60	6.59	455.95	441.96	32.59	
3100.00	3098.46	30 <b>9</b> 6,59	91.03	6.83	6.83	456.28	441.83	31.58	
3200.00	3198.25	3196.39	90.99	7.07	7.07	456.64	441.73	30.62	
3300.00	3296.59	3294.73	90.89	7.30	7.30	457.20	441.85	29.78	
3400.00	3398.21	3396.37	90.72	7.51	7.51	457.79	441.99	28.98	
3500.00	3499.67	3497.84	90,53	7.71	7.71	458.02	441.79	28.22	
3600.00	3600.59	3598.76	90,35	7.88	7.88	457.99	441.37	27.56	
3700.00	3698.53	3696.72	90.20	8.08	8.07	458.08	441.05	26.90	
3800.00	3794.81	3793.00	90.10	8.31	8.30	458.80	441.31	26.23	
3900.00	3894.10	3892.29	90.06	8.56	8.56	460.03	442.07	25.61	
4000.00	3990.81	3989.02	90.12	8.78	8.78	461.65	443.23	25.07	
4100.00	4088.07	4086.33	90.37	8.98	8.97	463.94	445.10	24.63	
4200.00	4189.54	4187.88	90.73	9.16	9.16	466.41	447.15	24.23	
4300.00	4291.44	4289.84	91.11	9.34	9.33	468.44	448,79	23.85	
4400.00	4394.17	4392.61	91.42	9.51	9.51	469.98	449.93	23.44	
4500.00	4494.29	4492.76	91.64	9.70	9.69	471.19	450.79	23.10	
4600.00	4595.08	4593.57	91.84	9.88	9.88	472.32	451.49	22.68	
4/00.00	4694.79	4693.29	92.03	10.07	10.07	473.38	452.14	22.28	
4800.00	4/94.85	4/93.37	92.22	10.26	10.26	474,48	452.83	21.92	
4900.00	4894.47	4893.02	92.41	10.46	10.45	4/5.60	453.56	21.58	
5000.00	4993.66	4992.22	92.60	10.66	10.65	475.84	454.37	21.21	
5100.00	5093.95	5092.53	92.77	10.87	10.87	478.15	455.22	20.86	

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Secondary We	II: Trionyx 6	Fed 1H (s) (T)	D Relative to Dr	ill Floor (Prim	ary); All Azimu	th Relative to (	GRID NORTH)		
Pri MD (US ft)	TVD (US fL)	Sec MD (US ft)	T.Face to Sec (°)	S.Major (US ft)	S.Minor (US ft)	CC (US ft)	ES (US ft)	SF	Řísk
5200.00	5194.16	5192.76	92.93	11.09	11.08	479.39	456.02	20.51	
5300.00	5294.56	5293.17	93.07	11.31	11.30	480.57	456.75	20.18	
5400.00	5396.12	5394.74	93.18	11.54	11.53	481.54	457.27	19.84	
5500.00	5496.41	5495.04	93.28	11.76	11.75	482.31	457.60	19.51	
5600.00	5595.20	5593.83	93.35	12.00	11.99	483.17	458.00	19.20	
5700.00	5695.61	5694.25	93.39	12.25	12.24	484.14	458.49	18.88	
5800.00	5795.69	5794.33	93.42	12.50	12.50	485.03	458.90	18.56	
5900.00	5896.77	5895.42	93.47	12.75	12.74	485.81	459.22	18.26	
6000.00	5995.22	5993.87	93.55	12.98	12.97	486.63	459.57	17,99	
6100.00	6097.07	6095.73	93.65	13.22	13.21	487.44	459.94	17.72	
6200.00	6197.95	6196.62	93.73	13.44	13.43	487.94	460.00	17.46	
6300.00	6299.23	6297.90	93.81	13.63	13.62	488.23	459.88	17.22	
6400.00	6399.13	6397.79	93.89	13.82	13.81	488.40	459.64	16.98	
6500.00	6499.13	6497.80	93.96	14.01	14.00	488.58	459.42	16.75	
6600.00	6599.31	6597.99	94.04	14.19	14.18	488.74	459.18	16.53	
6700.00	6699.40	6698.08	94.16	14.37	14.36	488.87	458.91	16.32	
6800.00	6798.27	6796.96	94.33	14.55	14.54	489.10	458.73	16.10	
6900.00	6897.78	6896,48	94,50	14,75	14.74	489.51	458.70	15.89	
7000.00	6997.95	6996.67	94.70	14.95	14.94	489.95	458.71	15.69	
7100.00	7095.95	7094.69	94.94	15.14	15.13	490.56	458.91	15.50	
7200.00	7195.82	7194.58	95.18	15.36	15.35	491.41	459.32	15.31	
7300.00	7294.50	7293.29	95.41	15.57	15.56	492.3 <del>9</del>	459.86	15.14	
7400.00	7394.05	7392.87	95.67	15.80	15.79	493.56	460:59	14:97	
7500.00	7492.68	7491.54	95.91	16.03	16.01	494.89	461.48	14.81	
7600.00	7594.77	7593.64	96.12	16.27	16.25	496.19	462.32	14.65	
7700.00	7694.70	7693.59	96.32	16.50	16.48	497.23	462.91	14.49	
7800.00	7793.96	7792.89	95.01	16.72	16.71	498:47	463.67	14:32	
7900.00	7890.48	7889.44	96.73	16.95	16.93	501.60	466.42	14.26	
8100.00	7905.27	7964.20	99.90	17.17	17.15	508.82	472.94	14.25	
8700.00	9142.92	8141 86	105.50	17.50	17.34	547.02	400.49 E10.07	14.46	
8200.00	9701 77	9300 83	106.02	17.52	17.50	595 73	510.55	15.92	
8400.00	8747 99	8242.05	104.13	17 74	17.03	537.96	600 58	17.07	
8500.00	8255 75	8265 33	07.45	1.7 79	17 77	702.46	664 73	18:67	
8600.00	8270 77	8769.85	98.37	17.80	17.78	775 76	737 88	20.48	
8700.00	8268.69	8267.77	88.13	17.79	17.77	854.59	816.46	22.41	
8800.00	9152.87	9871.57	187.89	25.06	14:47	876.17	848.37	31.53	
8900.00	9152.98	9952.31	188.17	25.96	14.71	877.07	848.54	30.74	
9000.00	9154.69	10043.95	188.48	27.03	15.05	879.69	850.34	29.98	
9100.00	9156.10	10165.13	188.87	28.51	15.60	881.65	851.37	29,12	
9200.00	9155.84	10267.23	189.17	29.75	16.05	882.11	850.88	28,24	
9300.00	9155.52	10367.73	189.44	31.06	16.51	882.47	850.22	27.37	
9400.00	9155.08	10466.37	189.73	32.44	16.98	882.78	849.48	26.51	
9500.00	9155.05	10564.78	190.02	33.84	17.47	883.56	849.15	25.68	
9600.00	9154.33	10672.36	190.37	35.41	17.97	883.77	848.19	24.84	
9700.00	9153.65	10758.78	190.63	36.61	18.47	883.90	847.09	24.01	
9800.00	9155.48	10837.75	190.80	37.70	18.88	886.81	848.85	23.36	
9900.00	9158.28	10935.51	191.04	39.16	19.38	890.47	851.25	22.71	
10000.00	9161.91	11030.49	191,29	40.71	19.93	895.16	854.65	22.09	
10100.00	9163.74	11177.58	191.80	43.11	20.76	897.74	855.59	21.30	
10200.00	9159.62	11297.69	192.33	44.95	21.47	895.64	851.90	20.48	
10300.00	9156.13	11391.06	192.65	46.21	22.02	893.00	847.76	19.74	
10400.00	9154.73	11470.59	192.84	47.36	22.48	892.04	845.43	19.14	
10500.00	9154.61	11562.87	193.03	48.78	23.04	892.66	844.62	18.58	
10600.00	91:55.32	11654.97	193.22	50.17	23.60	894.16	844.56	18.03	
10700.00	9157.04	11746.29	193.34	51.46	24.15	896.59	845.48	17.54	
10800.00	9158.76	11861.02	193.48	53.34	24.90	898.59	845.93	17.07	
10900.00	9159.82	11960.91	193.59	54.82	25.54	900.10	845.91	16.61	

Weatherford International Limited

5D Anti-Collision Report

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Secondary Well :	Trionyx 6	Fed 1H (s) (TV	D Relative to Dr	ill Floor (Prim	ary) ; All Azimu	th Relative to	GRID NORTH)		•
Pri MD (US ft)	TVD (US ft)	Sec MD (US ft)	T.Face to Sec (°)	S.Major (US ft)	S.Minor (US ft)	CC (US ft)	ES (US ft)	SF	Risk
11000.00	9159.75	12071.15	193.69	56.59	26.25	900.33	844.60	16.15	
11100.00	9159.93	12169.40	193.79	58.27	26.89	900.90	843.61	15.73	
11200.00	9158.38	12290.27	193.99	60.27	27.67	900.25	841.33	15.28	
11300.00	9154.98	12399.03	194.15	61.94	28.38	897.61	837.06	14.82	
11400.00	9152.85	12482.71	194.25	63.34	28.93	895.46	833.29	14.40	
11500.00	9152.26	12570.34	194.33	64.71	29.50	895.11	831.35	14.04	
11600.00	9152.50	12672.10	194.36	66.28	30.17	895.47	830.14	13.71	
11700.00	9152.92	12758.93	194.38	67.86	30.74	896.08	829.21	13.40	
11800.00	9154.36	12865.88	194.41	69.44	31.46	897.64	829.18	13.11	
11900.00	9154.90	12967.86	194.42	71.27	32.15	898.19	828.18	12.83	
12000.00	9155.03	13071.66	194.45	72.93	32.85	898.47	826.86	12.55	
12100.00	9155.40	13161.84	194.51	74.61	33.46	899.15	825.93	12.28	
12200.00	9155.96	13266.63	194.61	76.33	34.18	900.10	825.19	12.02	
12300.00	9156.38	13360.46	194.68	77.81	34.81	900.89	824.33	11.77	
12400.00	9157.50	13468.15	194:71	79.61	35.55	902.09	823.91	11.54	
12500.00	9156.07	13586.21	194.85	81.6 <del>9</del>	36.36	901.27	821.35	11.28	
12600.00	9153.92	13687.11	194.98	83.37	37.05	899.60	817.94	11.02	
12700.00	9151.51	13796.10	195.08	85.06	37.80	897.73	814.36	10.77	
12792.54	9149.75	13860.00	195.12	86.14	38.24	895.79	810.88	10.55	



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## Weatherford Drilling Services

GeoDec4 v2.0.0.3

9 . L. M.L La	May 08, 2014	
Customer:	Devon Energy	
Well Name: API Number:	Trionyx 6 Fed 11	1
Rig Name: Location: Block:	Lea Co, NM Nad8	3 NME
Engineer:	RWJ	
NAD83 / New Me	xico East (ftUS)	NAD83 (1986)
Projected Coordin	nate System	Geodetic Coordinate System
Datum: North An	nerican Datum 1983 (	(1986) Datum: North American Datum 1983 (1986)
Ellipsoid: GRS 19	80	Ellipsoid: GRS 1980
-		
EPSG: 2257		EPSG: 4269
EPSG: 2257 North: 419815.69	US Survey Foot	EPSG: 4269 Latitude: 32.152672 Degree
EPSG: 2257 North: 419815.69 East: 730733.22 (	US Survey Foot JS Survey Foot	EPSG: 4269 Latitude: 32.152672 Degree Longitude: -103.721345 Degree
EPSG: 2257 North: 419815.69 East: 730733.22 U Convergence: 0.3	US Survey Foot JS Survey Foot 13°	EPSG: 4269 Latitude: 32.152672 Degree Longitude: -103.721345 Degree
EPSG: 2257 North: 419815.69 East: 730733.22 L Convergence: 0.3 Declination: 7.39	US Survey Foot JS Survey Foot 13°	EPSG: 4269 Latitude: 32.152672 Degree Longitude: -103.721345 Degree
EPSG: 2257 North: 419815.69 East: 730733.22 U Convergence: 0.3 Declination: 7.39 Total Correction:	US Survey Foot JS Survey Foot J3° 7.06°	EPSG: 4269 Latitude: 32.152672 Degree Longitude: -103.721345 Degree
EPSG: 2257 North: 419815.69 East: 730733.22 U Convergence: 0.3 Declination: 7.399 Total Correction: Datum Transform	US Survey Foot JS Survey Foot 3° 7.06° nation: none	EPSG: 4269 Latitude: 32.152672 Degree Longitude: -103.721345 Degree
EPSG: 2257 North: 419815.69 East: 730733.22 L Convergence: 0.3 Declination: 7.399 Total Correction: Datum Transform Geodetic Location	US Survey Foot JS Survey Foot 3° 7.06° nation: none	EPSG: 4269 Latitude: 32.152672 Degree Longitude: -103.721345 Degree
EPSG: 2257 North: 419815.69 East: 730733.22 L Convergence: 0.3 Declination: 7.39 Total Correction: Datum Transform Geodetic Location MSL Elevation	US Survey Foot JS Survey Foot 33° 7.06° nation: none WGS84 = 0 m	EPSG: 4269 Latitude: 32.152672 Degree Longitude: -103.721345 Degree
EPSG: 2257 North: 419815.69 East: 730733.22 L Convergence: 0.3 Declination: 7.399 Total Correction: Datum Transform Geodetic Location MSL Elevation = Latitude =	US Survey Foot JS Survey Foot 3° 7.06° nation: none WGS84 = 0 m = 32° 09' 09.62" N	EPSG: 4269 Latitude: 32.152672 Degree Longitude: -103.721345 Degree
EPSG: 2257 North: 419815.69 East: 730733.22 U Convergence: 0.3 Declination: 7.39 Total Correction: Datum Transform Geodetic Location MSL Elevation = Latitude = Longitude =	US Survey Foot JS Survey Foot 3° 7.06° nation: mone WGS84 = 0 m = 32° 09' 09.62" N = 103° 43' 16.84"	EPSG: 4269 Latitude: 32.152672 Degree Longitude: -103.721345 Degree
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#### **NOTES REGARDING BLOWOUT PREVENTERS**

#### Devon Energy Production Company, L.P. Trionyx 6 Fed 11H

- 1. Drilling Nipple will be constructed so it can be removed mechanically without the aid of a welder. The minimum internal diameter will equal BOP bore.
- 2. Wear ring will be properly installed in head.
- 3. Blowout preventer and all associated filings will be in operable condition to withstand a minimum of 3000psi working pressure.
- 4. All fittings will be flanged.

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- 5. A fill bore safety valve tested to a minimum of 3000psi WP with proper thread connections will be available on the rotary rig floor at all times.
- 6. All choke lines will be anchored to prevent movement.
- 7. All BOP equipment will be equal to or larger in bore than the internal diameter of the last casing string.
- 8. Will maintain a kelly cock attached to the kelly.
- 9. Hand wheels and wrenches will be properly installed and tested for safe operation.
- 10. Hydraulic floor control for blowout preventer will be located as near in proximity to driller's controls as possible.
- 11. All BOP equipment will meet API standards and include a minimum 40 gallon accumulator having two independent means of power to initiate closing operation.



Fluid Technology Quality Document

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Fluid Technology

ContiTech Beattie Corp. Website: <u>www.contitechbeattie.com</u>

Monday, June 14, 2010

RE: Drilling & Production Hoses Lifting & Safety Equipment

To Heimerich & Payne,

A Continental ContiTech hose assembly can perform as intended and suitable for the application regardless of whether the hose is secured or unsecured in its configuration. As a manufacturer of High Pressure Hose Assemblies for use in Drilling & Production, we do offer the corresponding iffing and safety equipment, this has the added benefit of easing the tifting and handling of each hose assembly whilst affording hose longevity by ensuring correct handling methods and procedures as well as securing the hose in the unlikely event of a failure; but in no way does the lifting and safety equipment affect the performance of the hoses providing the hose handled and installed correctly. It is good practice to use lifting & safety equipment but not mandatory

Should you have any questions or require any additional information/clarifications then please do not hesitate to contact us.

ContiTech Beattie is part of the Continental AG Corporation and can offer the full support resources associated with a global organization.

Best regards,

Robin Hodgson Sales Manager ContiTech Beattie Corp

ContiTech Beattie Corp, 11535 Brittmoore Park Drive, Houston, TX 77041 Phore: +1 (832) 327-0141 Pax: +1 (832) 327-0148 www.contitechbeattle.com



# devon

### Commitment Runs Deep



Design Plan Operation and Maintenance Plan Closure Plan

SENM - Closed Loop Systems June 2010

#### I. Design Plan

Devon uses MI SWACO closed loop system (CLS). The MI SWACO CLS is designed to maintain drill solids at or below 5%. The equipment is arranged to progressively remove solids from the largest to the smallest size. Drilling fluids can thus be reused and savings is realized on mud and disposal costs. Dewatering may be required with the centrifuges to insure removal of ultra fine solids.

The drilling location is constructed to allow storm water to flow to a central sump normally the cellar. This insures no contamination leaves the drilling pad in the event of a spill. Storm water is reused in the mud system or stored in a reserve fluid tank farm until it can be reused. All lubricants, oils, or chemicals are removed immediately from the ground to prevent the contamination of storm water. An oil trap is normally installed on the sump if an oil spill occurs during a storm.

A tank farm is utilized to store drilling fluids including fresh water and brine fluids. The tank farm is constructed on a 20 ml plastic lined, bermed pad to prevent the contamination of the drilling site during a spill. Fluids from other sites may be stored in these tanks for processing by the solids control equipment and reused in the mud system. At the end of the well the fluids are transported from the tank farm to an adjoining well or to the next well for the rig.

Prior to installing a closed-loop system on site, the topsoil, if present, will be stripped and stockpiled for use as the final cover or fill at the time of closure.

Signs will be posted on the fence surrounding the closed-loop system unless the closed-loop system is located on a site where there is an existing well, that is operated by Devon.

#### II. Operations and Maintenance Plan

*Primary Shakers:* The primary shakers make the first removal of drill solids from the drilling mud as it leaves the well bore. The shakers are sized to handle maximum drilling rate at optimal screen size. The shakers normally remove solids down to 74 microns.

*Mud Cleaner*: The Mud Cleaner cleans the fluid after it leaves the shakers. A set of hydrocyclones are sized to handle 1.25 to 1.5 times the maximum circulating rate. This ensures all the fluid is being processed to an average cut point of 25 microns. The wet discharged is dewatered on a shaker equipped with ultra fine mesh screens and generally cut at 40 microns.



*Centrifuges*: The centrifuges can be one or two in number depending on the well geometry or depth of well. The centrifuges are sized to maintain low gravity solids at 5% or below. They may or may not need a dewatering system to enhance the removal rates. The centrifuges can make a cut point of 8-10 microns depending on bowl speed, feed rate, solids loading and other factors.

The centrifuge system is designed to work on the active system and be flexible to process incoming fluids from other locations. This set-up is also dependant on well factors.

Dewatering System: The dewatering system is a chemical mixing and dosing system designed to enhance the solids removal of the centrifuge. Not commonly used in shallow wells. It may contain pH adjustment, coagulant mixing and dosing, and polymer mixing and dosing. Chemical flocculation binds ultra fine solids into a mass that is within the centrifuge operating design. The

dewatering system improves the centrifuge cut point to infinity or allows for the return of clear water or brine fluid. This ability allows for the ultimate control of low gravity solids.

*Cuttings Boxes*: Cuttings boxes are utilized to capture drill solids that are discarded from the solids control equipment. These boxes are set upon a rail system that allows for the removal and replacement of a full box of cuttings with an empty one. They are equipped with a cover that insures no product is spilled into the environment during the transportation phase.

*Process Tank*: (Optional) The process tank allows for the holding and process of fluids that are being transferred into the mud system. Additionally, during times of lost circulation the process tank may hold active fluids that are removed for additional treatment. It can further be used as a mixing tank during well control conditions.

Sump and Sump Pump: The sump is used to collect storm water and the pump is used to transfer this fluid to the active system or to the tank for to hold in reserve. It can also be used to collect fluids that may escape during spills. The location contains drainage ditches that allow the location fluids to drain to the sump.

*Reserve Fluids (Tank Farm):* A series of frac tanks are used to replace the reserve pit. These are steel tanks that are equipped with a manifold system and a transfer pump. These tanks can contain any number of fluids used during the drilling process. These can include fresh water, cut brine, and saturated salt fluid. The fluid can be from the active well or reclaimed fluid from other locations. A 20 ml liner and berm system is employed to ensure the fluids do not migrate to the environment during a spill.

If a leak develops, the appropriate division district office will be notified within 48 hours of the discovery and the leak will be addressed. Spill prevention is accomplished by maintaining pump packing, hoses, and pipe fittings to insure no leaks are occurring. During an upset condition the source of the spill is isolated and repaired as soon as it is discovered. Free liquid is removed by a diaphragm pump and returned to the mud system. Loose topsoil may be used to stabilize the spill and the contaminated soil is excavated and placed in the cuttings boxes. After the well is finished and the rig has moved, the entire location is scrapped and testing will be performed to determine if a release has occurred.

All trash is kept in a wire mesh enclosure and removed to an approved landfill when full. All spent motor oils are kept in separate containers and they are removed and sent to an approved recycling center. Any spilled lubricants, pipe dope, or regulated chemicals are removed from soil and sent to landfills approved for these products.

These operations are monitored by Mi Swaco service technicians. Daily logs are maintained to ensure optimal equipment operation and maintenance. Screen and chemical use is logged to maintain inventory control. Fluid properties are monitored and recorded and drilling mud volumes are accounted for in the mud storage farm. This data is kept for end of well review to insure performance goals are met. Lessons learned are logged and used to help with continuous improvement.

A MI SWACO field supervisor manages from 3-5 wells. They are responsible for training personnel, supervising installations, and inspecting sites for compliance of MI SWACO safety and operational policy.

#### III. Closure Plan

A maximum 340' X 340' caliche pad is built per well. All of the trucks and steel tanks fit on this pad. All fluid cuttings go to the steel tanks to be hauled by various trucking companies to an agency approved disposal.

## H&P Flex Rig Location Layout

