

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special			Test Date 05-02-91		
Company Chevron U.S.A.			Connection		
Pool EUMONT			Formation Eumont Queen		
Completion Date 04-25-91		Total Depth 3850	Plug Back TD 3710	Elevation	Farm or Lease Name W.A. Ransey NCT-A
Csq. Size 5 1/2	Wt. 14	Set At 3850	Perforations: From 3080 To 3554		Well No. 28
Thq. Size 2 3/8	Wt. 4.7	d 1.995	Set At 3035	Perforations: From OPEN To END	
Type Well - Single - Braconnard - G.C. or G.O. Multiple Single			Packer Set At 3035		County Lea
Producing Thru Tubing	Reservoir Temp. °F 104 @ 3035	Mean Annual Temp. °F 60	Bato. Press. - P _g 13.2		State New Mexico
L 3035	H 3035	G _g .711	% CO ₂ 1.42	% N ₂ 2.86	% H ₂ S Prover
			Meter Run 2.067	Taps Flange	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							181		PKR		72 hrs.
1.	2	X	1.500	38	19.00	67	165		PKR		45 mins.
2.	2	X	1.500	38	25.00	67	151		PKR		45 mins.
3.	2	X	1.500	38	43.00	67	148		PKR		45 mins.
4.	2	X	1.500	38	60.00	67	137		PKR		45 mins.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{sp}	Rate of Flow Q, Mcfd
1	12.76	31.19	51.2	.9933	1.186	1.009	473
2	12.76	35.78	51.2	.9933	1.186	1.009	543
3	12.76	46.92	51.2	.9933	1.186	1.009	712
4	12.76	55.43	51.2	.9933	1.186	1.009	841
5							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
					DRY GAS	DRY	.711	X X X X X X X X	*669	*388
1.	.07	527	1.35	.982						
2.	.07	527	1.35	.982						
3.	.07	527	1.35	.982						
4.	.07	527	1.35	.982						
5.										

NO.	P ₁ ²	P _w ²	P _c ²	P _c ² - P _w ²
1		186.1	34.6	3.1
2		175.4	30.8	6.9
3		180.4	32.5	5.2
4		178.1	31.7	6.0
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 6.283$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 4.078$

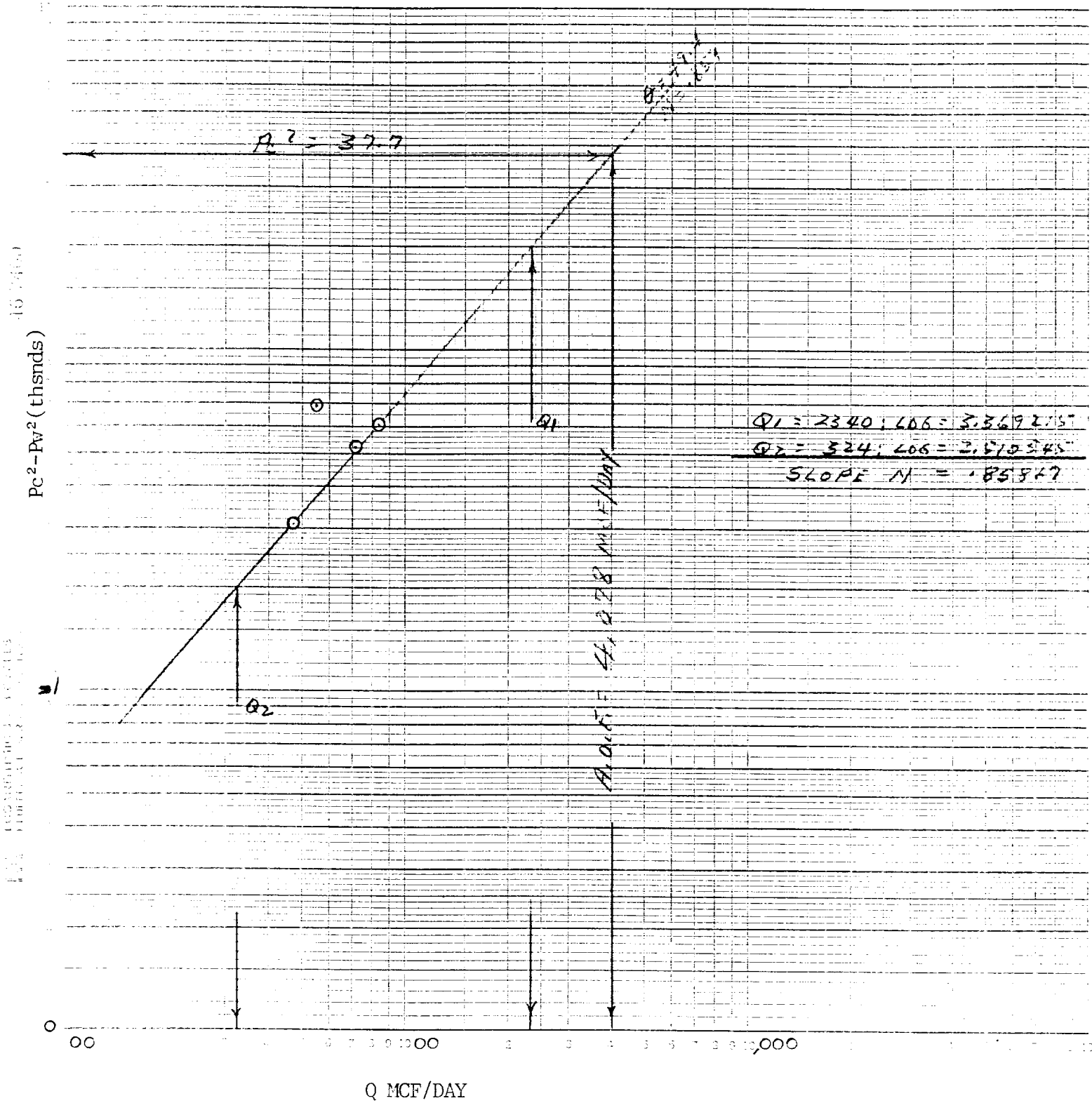
(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 4.849$

Absolute Open Flow	4,078 Mcfd @ 15.025	Angle of Slope θ	49.4	Slope, n	.859
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Remarks: *=corrected to 1.42% CO₂ & 2.86% N₂
NO FLUID PRODUCED DURING TEST

Approved By Division	Conducted By Pro Well Testers	Calculated By EM	Checked By EM
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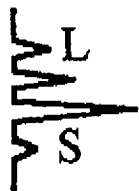
Chevron U.S.A.
 W.A. Ramsey NCT-A, Well #28
 O - 34 - 21 - 56
 Lea County, New Mexico
 05-02-91



Laboratory Services

1331 Tasker Drive
Hobbs, New Mexico 88240

Telephone: (505) 397-3713



FOR: Pro Well Testing & Wireline
Attention: Mr. Merv Buecker
P. O. Box 791
Hobbs, New Mexico 88240

SAMPLE W. A. Ramsey
IDENTIFICATION: NCT-A #28
COMPANY: Chevron U. S. A.
LEASE:
PLANT:

SAMPLE DATA:	DATE SAMPLED: 5/2/91 10:00AM	GAS (XX)	LIQUID ()
	ANALYSIS DATE: 05-02-91	SAMPLED BY: Glen (Pro Well)	
	PRESSURE - PSIG 137.00	ANALYSIS BY: Rolland Perry	
	SAMPLE TEMP. °F 69.00		
	ATMOS. TEMP. °F 73.00		

REMARKS:

COMPONENT ANALYSIS

COMPONENT		MOL PERCENT	GPM	
Oxygen	(O2)			
Hydrogen Sulfide	(H2S)			
Nitrogen	(N2)	2.86		
Carbon Dioxide	(CO2)	1.42		
Methane	(C1)	80.16		
Ethane	(C2)	8.57	2.287	
Propane	(C3)	4.03	1.107	
I-Butane	(IC4)	0.54	0.176	
N-Butane	(NC4)	1.24	0.390	
I-Pentane	(IC5)	0.36	0.131	
N-Pentane	(NC5)	0.31	0.112	
Hexane	(C6)	0.51	0.209	
Heptanes Plus	(C7+)	0.00	0.000	
		<u>100.00</u>	<u>4.412</u>	
BTU/CU.FT. - DRY		1172	MOLECULAR WT	20.5942
AT 14.650 DRY		1168		
AT 14.650 WET		1148	26# GASOLINE -	0.582
AT 15.025 DRY		1198		
AT 15.025 WET		1177		
SPECIFIC GRAVITY -				
CALCULATED		0.711		
MEASURED		0.000		

COMPANY : CHEVRON USA LEASE : W A RAMSEY A WELL NO. : 28 Pc = 194.2 Pc2 = 37.7 *
 UNIT : 0 SECTION : 34 TOWNSHIP : 21 Pt2 = 31.8 Pw = 186.1 *
 L : 3035 H : 3035 L/H : 1 G/GMIX : 0.711 DATE : 5 2 91 27.0 175.4 *
 WCO2 : 1.42 W2 : 2.86 H2S : RANGE : 36 26.0 180.4 *
 d : 1.995 Fr : 0.018231 GH : 2157.9 22.6 178.1 *

VOL 1 : 473 PSIA 1 : 178.2 RESV. TEMP 104.4 Pc2-Pw2 = 3.1 Pw2 = 34.6 *
 VOL 2 : 543 PSIA 2 : 164.2 6.9 30.8 *
 VOL 3 : 712 PSIA 3 : 161.2 SHUT-IN PR = 194.2 5.2 32.5 *
 VOL 4 : 841 PSIA 4 : 150.2 6.0 31.7 *
 PCR : 669 n = 0.859 *
 TCR : 388

LINE	RATE 1		RATE 2		RATE 3		RATE 4		
	'1ST	'2ND	'1ST	'2ND	'1ST	'2ND	'1ST	'2ND	
									Pc2/(Pc2-Pw2) = 12.261
									5.431
									7.278
									6.277
1	QM	0.473	0.473	0.543	0.543	0.712	0.712	0.841	0.841
2	TW	534	534	534	534	534	534	534	534
3	Ts	564.4	564.4	564.4	564.4	564.4	564.4	564.4	564.4
4	T	549.2	549.2	549.2	549.2	549.2	549.2	549.2	549.2
	PR (est)	0.27		0.25		0.24		0.22	
5	Z(est)	0.944	0.942	0.947	0.944	0.947	0.944	0.949	0.945
6	TZ	518.6	517.4	519.9	518.7	520.2	518.6	521.3	519.2
7	GH/TZ	4.161	4.170	4.151	4.160	4.148	4.161	4.140	4.156
8	eS	1.169	1.169	1.168	1.169	1.168	1.169	1.168	1.169
9	1-e-S	0.144	0.145	0.144	0.144	0.144	0.144	0.144	0.144
10	Pt	178.2	178.2	164.2	164.2	161.2	161.2	150.2	150.2
11	Pt2 /1000	31.8	31.8	27.0	27.0	26.0	26.0	22.6	22.6
12	Fr	0.018231	0.018231	0.018231	0.018231	0.018231	0.018231	0.018231	0.018231
13	Fc=FrTZ	9.454	9.434	9.479	9.456	9.484	9.454	9.503	9.466
14	FcQm	4.47	4.46	5.15	5.13	6.75	6.73	7.99	7.96
15	L/H(FcQm)	20.0	19.9	26.5	26.4	45.6	45.3	63.9	63.4
16	Fw	12.889081	12.882411	13.818157	13.808452	16.568624	16.546440	19.184576	19.1458282
17	Pw2	34.6	34.6	30.8	30.8	32.6	32.5	31.7	31.7
18	Ps2	40.5	40.5	36.0	36.0	38.0	38.0	37.1	37.1
19	Ps	201.2	201.2	189.6	189.6	195.0	195.0	192.6	192.5
20	P	189.7	189.7	176.9	176.9	178.1	178.1	171.4	171.3
21	Pr	0.28	0.28	0.26	0.26	0.27	0.27	0.26	0.26
22	Tr	1.42	1.42	1.42	1.42	1.42	1.42	1.42	1.42
23	Z	0.942	0.942	0.944	0.944	0.944	0.944	0.945	0.945

FORM C122-D