Well Name	Well Number	US Well Number	Lease Number	Case Number	Operator
PAINT 4-33 FED	712H	3002551955	NMLC061863A	NMLC061863A	DEVON
PAINT 4-33 FED	622H	3002551953	NMLC061863A	NMLC061863A	DEVON

# **Notice of Intent**

Sundry ID: 2749314

Type of Submission: Notice of Intent

Date Sundry Submitted: 09/07/2023

Date proposed operation will begin: 09/04/2023

Type of Action: APD Change

Time Sundry Submitted: 09:08

Sundry Print Repor

09/18/2023

**Procedure Description:** ENGINEERING ONLY Devon Energy Production Company, L.P. respectfully requests approval for optional surface casing/drilling plan of 10-3/4" surface casing inside of 14-3/4" surface hole at previously permitted set depths. Devon Energy Production Company, L.P. will circulate class C cement to surface behind the 10-3/4" casing. Pipe connections and bradenhead information has also been updated. Devon also request a break test variance for the subject wells. Please see attached documentation.

# **NOI Attachments**

# **Procedure Description**

PAINT\_4\_33\_FED\_COM\_712H\_14.75in\_20230905082723.pdf

PAINT\_4\_33\_FED\_COM\_622H\_14.75in\_20230905082723.pdf

10.750\_45.5\_J55\_SEAH\_20230905082723.pdf

break\_test\_variance\_BOP\_20230905082645.pdf

8.625in\_32lb\_P110EC\_SPRINT\_FJ\_09.16.2022\_20230904065646.pdf

5.5in\_x\_20.00lb\_P110EC\_DWC\_C\_IS\_PLUS\_\_\_5\_23\_2023\_20230904065645.pdf

# **Conditions of Approval**

## **Specialist Review**

Paint\_4\_33\_Fed\_Com\_712H622H\_Sundry\_ID\_2749314\_20230913084928.pdf

# **Operator**

I certify that the foregoing is true and correct. Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction. Electronic submission of Sundry Notices through this system satisfies regulations requiring a

Operator Electronic Signature: CHELSEY GREEN

Signed on: SEP 04, 2023 06:46 AM

Name: DEVON ENERGY PRODUCTION COMPANY LP

State:

Title: Regulatory Compliance Professional

Street Address: 333 West Sheridan Avenue

City: Oklahoma City State: OK

Phone: (405) 228-8595

Email address: Chelsey.Green@dvn.com

# Field

**Representative Name:** 

Street Address:

City:

Phone:

Email address:

# **BLM Point of Contact**

BLM POC Name: LONG VO BLM POC Phone: 5752345972 Disposition: Approved Signature: Long Vo BLM POC Title: Petroleum EngineerBLM POC Email Address: LVO@BLM.GOVDisposition Date: 09/13/2023

Zip:



# <u>10-3/4"</u> <u>45.50#</u> <u>0.400"</u> <u>J-55</u>

# **Dimensions (Nominal)**

Outside Diameter Wall Inside Diameter Drift	10.750 0.400 9.950 9.875	in. in. in. in.
Weight, T&C Weight, PE	45.500 44.260	lbs/ft lbs/ft
Internal Yield Pressure at Minimum Yield		
Collapse	2090	psi
Internal Yields Pressure		
PE	3580	psi
STC	3580	psi
BTC	3580	psi
Yield Strength, Pipe Body	715	1000 lbs
Joint Strength, STC		
STC	493	1000 lbs
BTC	796	1000 lbs

Note: SeAH Steel has produced this specification sheet for general information only. SeAH does not assume liability or responsibility for any loss or injury resulting from the use of information or data contained herein. All applications for the material described are at the customer's own risk and responsibility.



# **Connection Data Sheet**

OD (in.)	WEIGHT (lbs./ft.)	WALL (in.)	GRADE	DRIFT (in.)	RBW%	CONNECTION
5.500	Nominal: 20.00 Plain End: 19.83	0.361	VST P110 EC	4.653	87.5	DWC/C-IS PLUS

#### PIPE PROPERTIES

Nominal OD	5.500	in.
Nominal ID	4.778	in.
Nominal Area	5.828	sq.in.
Grade Type	API 5CT; Vallourec Sourced Material Only	
Min. Yield Strength	125	ksi
Max. Yield Strength	140	ksi
Min. Tensile Strength	135	ksi
Yield Strength	729	klb
Ultimate Strength	787	klb
Min. Internal Yield	14,360	psi
*High Collapse*	12,090	psi

#### **CONNECTION PROPERTIES**

Semi-Premium T&C	
6.300	in.
4.778	in.
4.125	in.
9.250	in.
5.828	sq.in.
100.0%	of pipe
	6.300 4.778 4.125 9.250 5.828 100.0% 100.0% 100.0%

#### **CONNECTION PERFORMANCES** 729 klb Yield Strength Parting Load 787 klb **Compression Rating** 729 klb Min. Internal Yield 14,360 psi \*High Collapse\* 12,090 psi Maximum Uniaxial Bend Rating 104.2 °/100 ft Ref String Length w 1.4 Design Factor 26,040 ft

FIELD TORQUE VALUES		
Min. Make-up Torque	16,600	ft.lbs
Opti. Make-up Torque	17,850	ft.lbs
Max. Make-up Torque	19,100	ft.lbs
Min. Shoulder Torque	1,660	ft.lbs
Max. Shoulder Torque	13,280	ft.lbs
Max. Delta Turn	0.200	Turns
+Max Operational Torque	24,300	ft.lbs
+Maximum Torsional Value (MTV)	26,730	ft.lbs

#### +Maximum Operational Torque and Maximum Torsional Value Only Valid with Vallourec P110EC Material

#### For detailed information on performance properties, refer to DWC Connection Data Notes on following page(s).

Connection specifications within the control of VAM USA were correct as of the date printed. Specifications are subject to change without notice. Certain connection specifications are dependent on the mechanical properties of the pipe. Mechanical properties of mill proprietary pipe grades were obtained from mill publications and are subject to change. Properties of mill proprietary grades should be confirmed with the mill. Users are advised to obtain current connection specifications and verify pipe mechanical properties for each application.

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#### 05/23/2023 4:11 PM



VAM USA 2107 CityWest Boulevard Suite 1300 Houston, TX 77042 Phone: 713-479-3200 Fax: 713-479-3234 VAM USA Sales E-mail: <u>VAMUSAsales@vam-usa.com</u> Tech Support E-mail: tech.support@vam-usa.com

## DWC Connection Data Notes:

- 1. DWC connections are available with a seal ring (SR) option.
- 2. All standard DWC/C connections are interchangeable for a given pipe OD. DWC connections are interchangeable with DWC/C-SR connections of the same OD and wall.
- 3. Connection performance properties are based on nominal pipe body and connection dimensions.
- DWC connection internal and external pressure resistance is calculated using the API rating for buttress connections. API Internal pressure resistance is calculated from formulas 31, 32, and 35 in the API Bulletin 5C3.
- 5. DWC joint strength is the minimum pipe body yield strength multiplied by the connection critical area.
- 6. API joint strength is for reference only. It is calculated from formulas 42 and 43 in the API Bulletin 5C3.
- 7. Bending efficiency is equal to the compression efficiency.
- 8. The torque values listed are recommended. The actual torque required may be affected by field conditions such as temperature, thread compound, speed of make-up, weather conditions, etc.
- 9. Connection yield torque is not to be exceeded.
- Reference string length is calculated by dividing the joint strength by both the nominal weight in air and a design factor (DF) of 1.4. These values are offered for reference only and do not include load factors such as bending, buoyancy, temperature, load dynamics, etc.
- 11. DWC connections will accommodate API standard drift diameters.
- 12. DWC/C family of connections are compatible with API Buttress BTC connections. Please contact tech.support@vam-usa.com for details on connection ratings and make-up.

Connection specifications within the control of VAM USA were correct as of the date printed. Specifications are subject to change without notice. Certain connection specifications are dependent on the mechanical properties of the pipe. Mechanical properties of mill proprietary pipe grades were obtained from mill publications and are subject to change. Properties of mill proprietary grades should be confirmed with the mill. Users are advised to obtain current connection specifications and verify pipe mechanical properties for each application.

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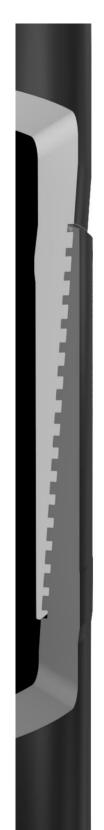


Grade Type

Min. Yield Strength

Max. Yield Strength

Min. Ultimate Tensile Strength



Issued on: 16 Sep. 2022 by Logan Van Gorp								
	Issued	on: 1	16 :	Sep.	2022	by Logan	Van	Gorp



#### et

2.614

5.978

65.0

65.0

in.

sqin. % of pipe

% of pipe

80.0 % of pipe

100 % of pipe

HI	GH	ER	то	RQ	UE '	VER	SIC	N

	Conne	ection	Data	a Sheet

OD 8 5/8 in.	Weight (lb/ft) Nominal: 32.00 Plain End: 31.13	Wall Th 0.352 ir		Grade P110EC	Alt. Drift: 7.875 in.	Connection VAM <sup>®</sup> SPRINT-FJ
	PIPE PROPERTIES CONNECTION PROPERTIES					
Nominal OD		8.625	in.	Connection Type		Semi-Premium Integral Flush
Nominal ID		7.921	in.	Connection OD (nom	ו):	8.665 in.
Nominal Cross Sectio	n Area	9.149	sqin.	Connection ID (nom)	):	7.954 in.

Make-Up Loss

Critical Cross Section

Compression Efficiency

Internal Pressure Efficiency

External Pressure Efficiency

Tension Efficiency

High Yield

ksi

ksi

ksi

125

140

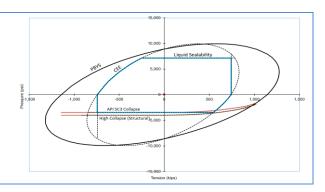
135

CONNECTION PERFORMANCES		
Tensile Yield Strength	744	klb
Compression Resistance	744	klb
Max. Internal Pressure	7,150	psi
Structural Collapse Resistance	4,000	psi
Max. Structural Bending	41	°/100ft
Max. Bending with Sealability	10	°/100ft

TORQUE VALU	ES	
Min. Make-up torque	23,000	ft.lb
Opt. Make-up torque	25,500	ft.lb
Max. Make-up torque	28,000	ft.lb
Max. Torque with Sealability (MTS)	48,000	ft.lb

\* 87.5% RBW

VAM® SPRINT-FJ is a semi-premium flush connection designed for shale applications, where maximum clearance and high tension capacity are required for intermediate casing strings.



#### Do you need help on this product? - Remember no one knows VAM<sup>®</sup> like VAM<sup>®</sup>

canada@vamfieldservice.com usa@vamfieldservice.com mexico@vamfieldservice.com brazil@vamfieldservice.com

uk@vamfieldservice.com dubai@vamfieldservice.com nigeria@vamfieldservice.com angola@vamfieldservice.com

Over 140 VAM® Specialists available worldwide 24/7 for Rig Site Assistance

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singapore@vamfieldservice.com

australia@vamfieldservice.com

# Section 2 - Blowout Preventer Testing Procedure

# Variance Request

Devon Energy requests to only test BOP connection breaks after drilling out of surface casing and while skidding between wells which conforms to API Standard 53 and industry standards. This test will include the Top Pipe Rams, HCR, Kill Line Check Valve, QDC (quick disconnect to wellhead) and Shell of the 10M BOPE to 5M for 10 minutes. If a break to the flex hose that runs to the choke manifold is required due to repositioning from a skid, the HCR will remain open during the shell test to include that additional break. The variance only pertains to intermediate hole-sections and no deeper than the Bone Springs Formation where 5M BOP tests are required. The initial BOP test will follow OOGO2.III.A.2.i, and subsequent tests following a skid will only test connections that are broken. The annular preventer will be tested to 100% working pressure. This variance will meet or exceed OOGO2.III.A.2.i per the following: Devon Energy will perform a full BOP test per OOGO2.III.A.2.i before drilling out of the intermediate casing string(s) and starting the production hole, before starting any hole section that requires a 10M test, before the expiration of the allotted 14-days for 5M intermediate batch drilling or when the drilling rig is fully mobilized to a new well pad, whichever is sooner. We will utilize a 200' TVD tolerance between intermediate shoes as the cutoff for a full BOP test. The BLM will be contacted 4hrs prior to a BOPE test. The BLM will be notified if and when a well control event is encountered. Break test will be a 14 day interval and not a 30 day full BOPE test interval. If in the event break testing is not utilized, then a full BOPE test would be conducted.

1. Well Control Response:

1. Primary barrier remains fluid

2. In the event of an influx due to being underbalanced and after a realized gain or flow, the order of closing BOPE is as follows:

- a) Annular first
- b) If annular were to not hold, Upper pipe rams second (which were tested on the skid BOP test)
- c) If the Upper Pipe Rams were to not hold, Lower Pipe Rams would be third



# 1. Geologic Formations

TVD of target	12391	Pilot hole depth	N/A
MD at TD:	22611	Deepest expected fresh water	

Basin

Dusin			
	Depth	Water/Mineral	
Formation	(TVD)	Bearing/Target	Hazards*
	from KB	Zone?	
Rustler	770		
Salt	1075		
Base of Salt	4420		
Delaware	4690		
Cherry Canyon	5570		
Brushy Canyon	6980		
1st Bone Spring Lime	8530		
Bone Spring 1st	9630		
Bone Spring 2nd	10230		
3rd Bone Spring Lime	10760		
Bone Spring 3rd	11480		
Wolfcamp	11950		

\*H2S, water flows, loss of circulation, abnormal pressures, etc.

	Wt Wt				Casing Interval		Casing Interval	
Hole Size	Csg. Size	(PPF)	Grade Conn		From (MD)	To (MD)	From (TVD)	To (TVD)
14 3/4	10 3/4	45.5	J55	BTC	0	795	0	795
9 7/8	8 5/8	32	P110	Sprint FJ	0	11950	0	11950
7 7/8	5 1/2	20	P110	DWC / C-IS+	0	22611	0	12391

#### 2. Casing Program

•All casing strings will be tested in accordance with 43 CFR 3172. Must have table for contingency casing.

#### 3. Cementing Program

Assuming no returns are established while drilling, Devon requests to pump a two stage cement job on the intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brushy Canyon and the second stage performed as a bradenhead squeeze with planned cement from the Brushy Canyon to surface. The final cement top will be verified by Echo-meter. Devon will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program. Devon will report to the BLM the volume of fluid (limited to 1 bbls) used to flush intermediate casing valves following backside cementing procedures.

Casing	# Sks	тос	Wt. ppg	Yld (ft3/sack)	Slurry Description
Surface	485	Surf	13.2	1.44	Lead: Class C Cement + additives
Int 1	494	Surf	13.0	2.3	2nd State: Bradenhead Squeeze - Lead: Class C Cement + additives
Int I	571	7018	13.2	1.44	Tail: Class H / C + additives
Production	117	9790	9	3.27	Lead: Class H /C + additives
Production	1432	11790	13.2	1.44	Tail: Class H / C + additives

Casing String	% Excess
Surface	50%
Intermediate 1	30%
Prod	10%

.

BOP installed and tested before drilling which hole?	Size?	Min. Required WP	Туре		~	Tested to:	
			Anı	nular	X	50% of rated working pressure	
Int 1	13-5/8"	5M		d Ram	Х		
	15 5/0	5101	-	Ram		5M	
			Doub	le Ram	X	5111	
			Other*				
	13-5/8"		Annul	ar (5M)	Х	100% of rated working pressure	
Production		10M	Blind Ram		Х		
Troduction		Pipe Ram			10M		
				le Ram	X	10111	
			Other*				
			Annul	ar (5M)			
			Blind	d Ram			
			Pipe	Ram			
			Doub	le Ram			
			Other*				
N A variance is requested for	A variance is requested for the use of a diverter on the surface casing. See attached for schematic.						
A variance is requested to run a 5 M annular on a 10M system							

## 4. Pressure Control Equipment (Three String Design)

#### 5. Mud Program (Three String Design)

Section	Туре	Weight (ppg)
Surface	FW Gel	8.5-9
Intermediate	DBE / Cut Brine	10-10.5
Production	OBM	10-10.5

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times.

What will be used to monitor the loss or gain of fluid?	PVT/Pason/Visual Monitoring
---	-----------------------------

#### 6. Logging and Testing Procedures

Logging,	Logging, Coring and Testing					
	Will run GR/CNL from TD to surface (horizontal well - vertical portion of hole). Stated logs run will be in the					
Х	Completion Rpeort and sbumitted to the BLM.					
	No logs are planned based on well control or offset log information.					
	Drill stem test? If yes, explain.					
	Coring? If yes, explain.					

Addition	al logs planned	Interval
	Resistivity	Int. shoe to KOP
	Density	Int. shoe to KOP
Х	CBL	Production casing
Х	Mud log	Intermediate shoe to TD
	PEX	

#### 7. Drilling Conditions

Condition	Specfiy what type and where?			
BH pressure at deepest TVD	6766			
Abnormal temperature	No			

Mitigation measure for abnormal conditions. Describe. Lost circulation material/sweeps/mud scavengers.

Hydrogren Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrationsgreater than 100 ppm, the operator will comply with the provisions of 43 CFR 3176. If Hydrogen Sulfide is encounteredmeasured values and formations will be provided to the BLM.NH2S is present

Y H2S plan attached.

## 8. Other facets of operation

Is this a walking operation? Potentially

- 1 If operator elects, drilling rig will batch drill the surface holes and run/cement surface casing; walking the rig to next wells on the pad.
- 2 The drilling rig will then batch drill the intermediate sections and run/cement intermediate casing; the wellbore will be isolated with a blind flange and pressure gauge installed for monitoring the well before walking to the next well.
- 3 The drilling rig will then batch drill the production hole sections on the wells with OBM, run/cement production casing, and install TA caps or tubing heads for completions.

NOTE: During batch operations the drilling rig will be moved from well to well however, it will not be removed from the pad until all wells have production casing run/cemented.

Will be pre-setting casing? Potentially

- 1 Spudder rig will move in and batch drill surface hole.
  - a. Rig will utilize fresh water based mud to drill surface hole to TD. Solids control will be handled entirely on a closed loop basis.,
- 2 After drilling the surface hole section, the spudder rig will run casing and cement following all of the applicable rules and regulations (43 CFR 3172, all COAs and NMOCD regulations).

 $^{3}$  The wellhead will be installed and tested once the surface casing is cut off and the WOC time has been reached.

- 4 A blind flange with the same pressure rating as the wellhead will be installed to seal the wellbore. Pressure will be monitored with a pressure gauge installed on the wellhead.
- 5 Spudder rig operations is expected to take 4-5 days per well on a multi-well pa.
- 6 The NMOCD will be contacted and notified 24 hours prior to commencing spudder rig operations.
- 7 Drilling operations will be performed with drilling rig. A that time an approved BOP stack will be nippled up and tested on the wellhead before drilling operations commences on each well.
  - a. The NMOCD will be contacted / notified 24 hours before the drilling rig moves back on to the pad with the pre-set surface casing.

#### Attachments

X Directional Plan Other, describe



Well Name	Well Number	US Well Number	Lease Number	Case Number	Operator
PAINT 4-33 FED	712H	3002551955	NMLC061863A	NMLC061863A	DEVON
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# **Notice of Intent**

Sundry ID: 2749314

Type of Submission: Notice of Intent

Date Sundry Submitted: 09/07/2023

Date proposed operation will begin: 09/04/2023

Type of Action: APD Change

Time Sundry Submitted: 09:08

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# **NOI Attachments**

# **Procedure Description**

PAINT\_4\_33\_FED\_COM\_712H\_14.75in\_20230905082723.pdf

PAINT\_4\_33\_FED\_COM\_622H\_14.75in\_20230905082723.pdf

10.750\_45.5\_J55\_SEAH\_20230905082723.pdf

break\_test\_variance\_BOP\_20230905082645.pdf

8.625in\_32lb\_P110EC\_SPRINT\_FJ\_09.16.2022\_20230904065646.pdf

5.5in\_x\_20.00lb\_P110EC\_DWC\_C\_IS\_PLUS\_\_\_5\_23\_2023\_20230904065645.pdf

I certify that the foregoing is true and correct. Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction. Electronic submission of Sundry Notices through this system satisfies regulations requiring a

Operator Electronic Signature: CHELSEY GREEN Name: DEVON ENERGY PRODUCTION COMPANY LP Title: Regulatory Compliance Professional Street Address: 333 West Sheridan Avenue City: Oklahoma City State: OK Phone: (405) 228-8595 Email address: Chelsey.Green@dvn.com

State:

# Field

**Representative Name:** 

Street Address:

City:

Phone:

Email address:

Zip:

Signed on: SEP 04, 2023 06:46 AM

.

# PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

<b>OPERATOR'S NAME:</b>	Devon Energy Production Company LP			
LEASE NO.:	NMLC061863A			
LOCATION:	Section, T.23 S., R.30 E., NMPM			
COUNTY:	Eddy County, New Mexico			
WELL NAME & NO.:	Paint 4-33 Fed Com 712H			
SURFACE HOLE FOOTAGE:	200'/S & 1767'/W			
<b>BOTTOM HOLE FOOTAGE</b>	20'/N & 1650'/W			
ATS/API ID:	3002551955			
APD ID:				
Sundry ID:	2749314			
WELL NAME & NO.:	Paint 4-33 Fed Com 622H			
SURFACE HOLE FOOTAGE:	200'/S & 1827'/W			
<b>BOTTOM HOLE FOOTAGE</b>	20'/N & 2090'/W			
ATS/API ID:	3002551953			
APD ID:				
Sundry ID:	2749314			

COA

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<b>***</b>			1
H2S	Yes 🝷		
Potash	None		
Cave/Karst	Low		
Potential			
Cave/Karst	Critical		
Potential			
Variance	C None	🖸 Flex Hose	C Other
Wellhead	Conventional and Multibov	vl 🔽	
Other	□ 4 String	Capitan Reef	□ WIPP
		None -	
Other	Pilot Hole	C Open Annulus	
	None 🝷		
Cementing	Contingency Squeeze	Echo-Meter	Primary Cement
	None	Int 1 🔻	Squeeze
		·	None 👻
Special	□ Water	COM	Unit Unit
Requirements	Disposal/Injection		
Special	Batch Sundry		
Requirements	-		
Special	Break Testing	□ Offline	Casing
Requirements		Cementing	Clearance
Variance			

# A. HYDROGEN SULFIDE

A Hydrogen Sulfide (H2S) Drilling Plan shall be activated 500 feet prior to drilling into the **Delaware** formation. As a result, the Hydrogen Sulfide area must meet **43 CFR part 3170 Subpart 3176** requirements, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, please provide measured values and formations to the BLM.

# **B. CASING**

- 1. The 10-3/4 inch surface casing shall be set at approximately 875 feet (a minimum of 25 feet (Lea County) into the Rustler Anhydrite, above the salt, and below usable fresh water) and cemented to the surface. The surface hole shall be 14 3/4 inch in diameter.
  - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of

six hours after pumping cement and ideally between 8-10 hours after completing the cement job.

- b. Wait on cement (WOC) time for a primary cement job will be a minimum of <u>8</u> <u>hours</u> or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
- c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
- d. If cement falls back, remedial cementing will be done prior to drilling out that string.

# Intermediate casing must be kept fluid filled to meet BLM minimum collapse requirement.

2. The minimum required fill of cement behind the 8-5/8 inch intermediate casing is:

# **Option 1 (Single Stage):**

• Cement to surface. If cement does not circulate see B.1.a, c-d above.

# **Option 2:**

Operator has proposed to cement in two stages by conventionally cementing the first stage and performing a bradenhead squeeze on the second stage, contingent upon no returns to surface.

- a. First stage: Operator will cement with intent to reach the top of the **Brushy** Canyon at 6980' (571 sxs Class H/C+ additives).
- b. Second stage:
  - Operator will perform bradenhead squeeze and top-out. Cement to surface. If cement does not reach surface, the appropriate BLM office shall be notified. (Squeeze 494 sxs Class C)

Operator has proposed to pump down 10-3/4" X 8-5/8" annulus after primary cementing stage. <u>Operator must run Echo-meter to verify Cement Slurry/Fluid top in the annulus Or operator shall run a CBL from TD of the 8-5/8" casing to surface after the second stage BH to verify TOC.</u>

Submit results to the BLM. No displacement fluid/wash out shall be utilized at the top of the cement slurry between second stage BH and top out. Operator must run one CBL per Well Pad.

If cement does not reach surface, the next casing string must come to surface.

# Operator must use a limited flush fluid volume of 1 bbl following backside cementing procedures.

- 3. The minimum required fill of cement behind the 5-1/2 inch production casing is:
  - Cement should tie-back at least **200 feet** into previous casing string. Operator shall provide method of verification.

# **C. PRESSURE CONTROL**

1. Variance approved to use flex line from BOP to choke manifold. Manufacturer's specification to be readily available. No external damage to flex line. Flex line to be installed as straight as possible (no hard bends).'

# 2.

# **Option 1:**

- a. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be **5000 (5M)** psi. Annular which shall be tested to **5000 (5M)** psi.
- b. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the 8-5/8 inch intermediate casing shoe shall be 10,000 (10M) psi. Variance is approved to use a 5000 (5M) Annular which shall be tested to 5000 (5M) psi.

# **Option 2:**

- a. Operator has proposed a multi-bowl wellhead assembly. This assembly will only be tested when installed on the 10-3/4 inch surface casing. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be 10,000 (10M) psi. Variance is approved to use a 5000 (5M) Annular which shall be tested to 5000 (5M) psi.
  - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
  - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
  - c. Manufacturer representative shall install the test plug for the initial BOP test.
  - d. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.

e. Whenever any seal subject to test pressure is broken, all the tests in OOGO2.III.A.2.i must be followed.

# **D. SPECIAL REQUIREMENT (S)**

# **Communitization Agreement**

- The operator will submit a Communitization Agreement to the Santa Fe Office, 301 Dinosaur Trail Santa Fe, New Mexico 87508, at least 90 days before the anticipated date of first production from a well subject to a spacing order issued by the New Mexico Oil Conservation Division. The Communitization Agreement will include the signatures of all working interest owners in all Federal and Indian leases subject to the Communitization Agreement (i.e., operating rights owners and lessees of record), or certification that the operator has obtained the written signatures of all such owners and will make those signatures available to the BLM immediately upon request.
- The operator will submit an as-drilled survey well plat of the well completion, but are not limited to, those specified in 43 CFR part 3170 Subpart 3171
- If the operator does not comply with this condition of approval, the BLM may take enforcement actions that include, but are not limited to, those specified in 43 CFR 3163.1.
- In addition, the well sign shall include the surface and bottom hole lease numbers. <u>When the Communitization Agreement number is known, it shall also be on the sign.</u>

# **BOPE Break Testing Variance (Approved)**

- BOPE Break Testing is ONLY permitted for 5M BOPE or less. (Annular preventer must be tested to a minimum of 70% of BOPE working pressure and shall be higher than the MASP)
- BOPE Break Testing is NOT permitted to drilling the production hole section.
- Variance only pertains to the intermediate hole-sections and no deeper than the Bone Springs formation.
- While in transfer between wells, the BOPE shall be secured by the hydraulic carrier or cradle.
- Any well control event while drilling require notification to the BLM Petroleum Engineer (575-706-2779) prior to the commencement of any BOPE Break Testing operations.
- A full BOPE test is required prior to drilling the first deep intermediate hole section. If any subsequent hole interval is deeper than the first, a full BOPE test will be required. (200' TVD tolerance between intermediate shoes is allowable).
- The BLM is to be contacted (575-689-5981 Lea County) 4 hours prior to BOPE tests.
- As a minimum, a full BOPE test shall be performed at **21**-day intervals.
- In the event any repairs or replacement of the BOPE is required, the BOPE shall test as per Onshore Oil and Gas Order No. 2.
- If in the event break testing is not utilized, then a full BOPE test would be conducted.

# GENERAL REQUIREMENTS

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)

# $\boxtimes$ Eddy County

**EMAIL** or call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220,

BLM\_NM\_CFO\_DrillingNotifications@BLM.GOV (575) 361-2822

# Lea County Call the Hobbs Field Station, 414 West Taylor, Hobbs NM 88240, (575) 689-5981

- 1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.
  - a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after installing and testing the wellhead, by installing a blind flange of like pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).
  - b. When the operator proposes to set surface casing with Spudder Rig
    - Notify the BLM when moving in and removing the Spudder Rig.
    - Notify the BLM when moving in the 2<sup>nd</sup> Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.
    - BOP/BOPE test to be conducted per **43** CFR part **3170** Subpart **3172** as soon as 2nd Rig is rigged up on well.
- 2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the dog house or stairway area.
- 3. The record of the drilling rate along with the GR/N well log run from TD to surface (horizontal well vertical portion of hole) shall be submitted to the BLM office as well as all other logs run on the borehole 30 days from completion. If available, a

digital copy of the logs is to be submitted in addition to the paper copies. The Rustler top and top and bottom of Salt are to be recorded on the Completion Report.

# A. CASING

- 1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.
- <u>Wait on cement (WOC) for Potash Areas:</u> After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends, 2) until cement has been in place at least <u>24 hours</u>. WOC time will be recorded in the driller's log. The casing intergrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 3. <u>Wait on cement (WOC) for Water Basin:</u> After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least <u>8 hours</u>. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements. The casing intergrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 4. Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.
- 5. No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.
- 6. On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.
- 7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.

- 8. Whenever a casing string is cemented in the R-111-P potash area, the NMOCD requirements shall be followed.
- B. PRESSURE CONTROL
- All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in 43 CFR part 3170 Subpart 3172 and API STD 53 Sec. 5.3.
- 2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor.
- 3. 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.
- 4. If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:
  - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
  - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
  - c. Manufacturer representative shall install the test plug for the initial BOP test.
  - d. Whenever any seal subject to test pressure is broken, all the tests in OOGO2.III.A.2.i must be followed.
  - e. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- 5. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
  - a. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after

installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead cement), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).

- b. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the cement plug. The BOPE test can be initiated after bumping the cement plug with the casing valve open. (only applies to single stage cement jobs, prior to the cement setting up.)
- c. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer and can be initiated immediately with the casing valve open. The operator also has the option of utilizing an independent tester to test without a plug (i.e. against the casing) pursuant to 43 CFR part 3170 Subpart 3172 with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for water basin (8 hours) or potash (24 hours) or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).
- d. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.
- e. The results of the test shall be reported to the appropriate BLM office.
- f. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
- g. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.
- h. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per **43 CFR**

# part 3170 Subpart 3172.

# C. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

# D. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area.

Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

LVO 9/13/2023

#### Received by OCD: 9/18/2023 9:56:28 AM

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Form 3160-5 (June 2019)	UNITED STATI DEPARTMENT OF THE BUREAU OF LAND MAN	ON Expir	RM APPROVED MB No. 1004-0137 res: October 31, 2021 JLTIPLE			
Do not use	DRY NOTICES AND REP( this form for proposals well. Use Form 3160-3 (A	6. If Indian, Allottee or MULTIPLE	Tribe Name			
SUB       1. Type of Well       Oil Well	MIT IN TRIPLICATE - Other instr	<ul> <li>7. If Unit of CA/Agreement, Name and/or No.</li> <li>MULTIPLE</li> <li>8. Well Name and No.</li> <li>MULTIPLE</li> </ul>				
2. Name of Operator DEVON ENERGY PRODUCTION COMPANY LP				9. API Well No. MULTIPLE		
3a. Address 333 WEST SHE	3a. Address       333 WEST SHERIDAN AVE, OKLAHOMA CITY,       3b. Phone No. (include area code)         (405) 235-3611				10. Field and Pool or Exploratory Area MULTIPLE	
4. Location of Well <i>(Footage, MULTIPLE</i>	Sec., T.,R.,M., or Survey Description	)		11. Country or Parish, State MULTIPLE		
	12. CHECK THE APPROPRIATE B	OX(ES) TO INDICATE NATURE	OF NOTI	CE, REPORT OR OTHI	ER DATA	
TYPE OF SUBMISSIO	N	TYF	E OF AC	ΓΙΟΝ		
✓ Notice of Intent	Acidize	Deepen Hydraulic Fracturing		uction (Start/Resume) amation	Water Shut-Off Well Integrity	
Subsequent Report	Casing Repair Change Plans	New Construction Plug and Abandon		mplete porarily Abandon	Other	
Final Abandonment No	tice Convert to Injection	Plug Back	Wate	r Disposal		
the proposal is to deepen d the Bond under which the	irectionally or recomplete horizontal work will be perfonned or provide th	ly, give subsurface locations and m the Bond No. on file with BLM/BIA.	easured ar Required	d true vertical depths of subsequent reports must	k and approximate duration thereof. If all pertinent markers and zones. Attach be filed within 30 days following 50-4 must be filed once testing has been	

completion of the involved operations. If the operation results in a multiple completion or recompletion in a new interval, a Form 3160-4 must be filed once testing has been completed. Final Abandonment Notices must be filed only after all requirements, including reclamation, have been completed and the operator has detennined that the site is ready for final inspection.)

#### ENGINEERING ONLY

Devon Energy Production Company, L.P. respectfully requests approval for optional surface casing/drilling plan of 10-3/4" surface casing inside of 14-3/4" surface hole at previously permitted set depths. Devon Energy Production Company, L.P. will circulate class C cement to surface behind the 10-3/4 casing. Pipe connections and bradenhead information has also been updated. Devon also request a break test variance for the subject wells. Please see attached documentation.

14. I hereby certify that the foregoing is true and correct. Name (Printed/Typed)         CHELSEY GREEN / Ph: (405) 228-8595	Regulatory Compliance Professional Title				
Signature	Date	09/04/2	2023		
THE SPACE FOR FEDE	RAL OR STATE	OFICE USE			
Approved by					
	Title		Date		
Conditions of approval, if any, are attached. Approval of this notice does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon.					
Title 18 U.S.C Section 1001 and Title 43 U.S.C Section 1212, make it a crime for any any false, fictitious or fraudulent statements or representations as to any matter within		willfully to make to any o	department or agency of the United States		

(Instructions on page 2)

This form is designed for submitting proposals to perform certain well operations and reports of such operations when completed as indicated on Federal and Indian lands pursuant to applicable Federal law and regulations. Any necessary special instructions concerning the use of this form and the number of copies to be submitted, particularly with regard to local area or regional procedures and practices, are either shown below, will be issued by or may be obtained from the local Federal office.

## SPECIFIC INSTRUCTIONS

*Item 4* - Locations on Federal or Indian land should be described in accordance with Federal requirements. Consult the local Federal office for specific instructions.

*Item 13:* Proposals to abandon a well and subsequent reports of abandonment should include such special information as is required by the local Federal office. In addition, such proposals and reports should include reasons for the abandonment; data on any former or present productive zones or other zones with present significant fluid contents not sealed off by cement or otherwise; depths (top and bottom) and method of placement of cement plugs; mud or other material placed below, between and above plugs; amount, size, method of parting of any casing, liner or tubing pulled and the depth to the top of any tubing left in the hole; method of closing top of well and date well site conditioned for final inspection looking for approval of the abandonment. If the proposal will involve **hydraulic fracturing operations**, you must comply with 43 CFR 3162.3-3, including providing information about the protection of usable water. Operators should provide the best available information about all formations containing water and their depths. This information could include data and interpretation of resistivity logs run on nearby wells. Information may also be obtained from state or tribal regulatory agencies and from local BLM offices.

# NOTICES

The privacy Act of 1974 and the regulation in 43 CFR 2.48(d) provide that you be furnished the following information in connection with information required by this application.

AUTHORITY: 30 U.S.C. 181 et seq., 351 et seq., 25 U.S.C. 396; 43 CFR 3160.

PRINCIPAL PURPOSE: The information is used to: (1) Evaluate, when appropriate, approve applications, and report completion of subsequent well operations, on a Federal or Indian lease; and (2) document for administrative use, information for the management, disposal and use of National Resource lands and resources, such as: (a) evaluating the equipment and procedures to be used during a proposed subsequent well operation and reviewing the completed well operations for compliance with the approved plan; (b) requesting and granting approval to perform those actions covered by 43 CFR 3162.3-2, 3162.3-3, and 3162.3-4; (c) reporting the beginning or resumption of production, as required by 43 CFR 3162.4-1(c)and (d) analyzing future applications to drill or modify operations in light of data obtained and methods used.

ROUTINE USES: Information from the record and/or the record will be transferred to appropriate Federal, State, local or foreign agencies, when relevant to civil, criminal or regulatory investigations or prosecutions in connection with congressional inquiries or to consumer reporting agencies to facilitate collection of debts owed the Government.

EFFECT OF NOT PROVIDING THE INFORMATION: Filing of this notice and report and disclosure of the information is mandatory for those subsequent well operations specified in 43 CFR 3162.3-2, 3162.3-3, 3162.3-4.

The Paperwork Reduction Act of 1995 requires us to inform you that:

The BLM collects this information to evaluate proposed and/or completed subsequent well operations on Federal or Indian oil and gas leases.

Response to this request is mandatory.

The BLM would like you to know that you do not have to respond to this or any other Federal agency-sponsored information collection unless it displays a currently valid OMB control number.

**BURDEN HOURS STATEMENT:** Public reporting burden for this form is estimated to average 8 hours per response, including the time for reviewing instructions, gathering and maintaining data, and completing and reviewing the form. Direct comments regarding the burden estimate or any other aspect of this form to U.S. Department of the Interior, Bureau of Land Management (1004-0137), Bureau Information Collection Clearance Officer (WO-630), 1849 C St., N.W., Mail Stop 401 LS, Washington, D.C. 20240

# **Additional Information**

# **Batch Well Data**

PAINT 4-33 FED COM 712H, US Well Number: 3002551955, Case Number: NMLC061863A, Lease Number: NMLC061863A, Operator:DEVON ENERGY PRODUCTION COMPANY LP

PAINT 4-33 FED COM 622H, US Well Number: 3002551953, Case Number: NMLC061863A, Lease Number: NMLC061863A, Operator:DEVON ENERGY PRODUCTION COMPANY LP

# 1. Geologic Formations

TVD of target	12391	Pilot hole depth	N/A
MD at TD:	22611	Deepest expected fresh water	

Basin

Dusin			
	Depth	Water/Mineral	
Formation	(TVD)	Bearing/Target	Hazards*
	from KB	Zone?	
Rustler	770		
Salt	1075		
Base of Salt	4420		
Delaware	4690		
Cherry Canyon	5570		
Brushy Canyon	6980		
1st Bone Spring Lime	8530		
Bone Spring 1st	9630		
Bone Spring 2nd	10230		
3rd Bone Spring Lime	10760		
Bone Spring 3rd	11480		
Wolfcamp	11950		

\*H2S, water flows, loss of circulation, abnormal pressures, etc.

		Wt				Interval	Casing	Interval
Hole Size	Csg. Size	(PPF)	Grade	Conn	From (MD)	To (MD)	From (TVD)	To (TVD)
14 3/4	10 3/4	45.5	J55	BTC	0	795	0	795
9 7/8	8 5/8	32	P110	Sprint FJ	0	11950	0	11950
7 7/8	5 1/2	20	P110	DWC / C-IS+	0	22611	0	12391

#### 2. Casing Program

•All casing strings will be tested in accordance with 43 CFR 3172. Must have table for contingency casing.

#### 3. Cementing Program

Assuming no returns are established while drilling, Devon requests to pump a two stage cement job on the intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brushy Canyon and the second stage performed as a bradenhead squeeze with planned cement from the Brushy Canyon to surface. The final cement top will be verified by Echo-meter. Devon will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program. Devon will report to the BLM the volume of fluid (limited to 1 bbls) used to flush intermediate casing valves following backside cementing procedures.

Casing	# Sks	тос	Wt. ppg	Yld (ft3/sack)	Slurry Description
Surface	485	Surf	13.2	1.44	Lead: Class C Cement + additives
Int 1	494	Surf	13.0	2.3	2nd State: Bradenhead Squeeze - Lead: Class C Cement + additives
Int I	571	7018	13.2	1.44	Tail: Class H / C + additives
Production	117	9790	9	3.27	Lead: Class H /C + additives
Production	1432	11790	13.2	1.44	Tail: Class H / C + additives

Casing String	% Excess
Surface	50%
Intermediate 1	30%
Prod	10%

.

BOP installed and tested before drilling which hole?	Size?	Min. Required WP	Туре		~	Tested to:	
			Anı	nular	X	50% of rated working pressure	
Int 1	13-5/8"	5M		d Ram	Х		
	15 5/0	5101		e Ram		5M	
			Doub	le Ram	X	5101	
			Other*				
			Annul	ar (5M)	Х	100% of rated working pressure	
Production	13-5/8"	10M	Blind	d Ram	Х		
Tioduction	15-5/6	1011	Pipe Ram			10M	
			Doub	le Ram	Х	10111	
			Other*				
			Annular (5M)				
			Blind Ram				
			Pipe Ram				
			Doub	le Ram			
			Other*				
N A variance is requested for	the use of a	a diverter or	the surface	casing. See	attached for	schematic.	
Y A variance is requested to a	Y A variance is requested to run a 5 M annular on a 10M system						

## 4. Pressure Control Equipment (Three String Design)

#### 5. Mud Program (Three String Design)

Section	Туре	Weight (ppg)
Surface	FW Gel	8.5-9
Intermediate	DBE / Cut Brine	10-10.5
Production	OBM	10-10.5

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times.

What will be used to monitor the loss or gain of fluid?	PVT/Pason/Visual Monitoring
---	-----------------------------

#### 6. Logging and Testing Procedures

Logging, C	Coring and Testing
	Will run GR/CNL from TD to surface (horizontal well - vertical portion of hole). Stated logs run will be in the
Х	Completion Rpeort and sbumitted to the BLM.
	No logs are planned based on well control or offset log information.
	Drill stem test? If yes, explain.
	Coring? If yes, explain.

Addition	al logs planned	Interval
	Resistivity	Int. shoe to KOP
	Density	Int. shoe to KOP
Х	CBL	Production casing
Х	Mud log	Intermediate shoe to TD
	PEX	

#### 7. Drilling Conditions

Condition	Specfiy what type and where?
BH pressure at deepest TVD	6766
Abnormal temperature	No

Mitigation measure for abnormal conditions. Describe. Lost circulation material/sweeps/mud scavengers.

Hydrogren Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations<br/>greater than 100 ppm, the operator will comply with the provisions of 43 CFR 3176. If Hydrogen Sulfide is encountered<br/>measured values and formations will be provided to the BLM.NH2S is present

Y H2S plan attached.

## 8. Other facets of operation

Is this a walking operation? Potentially

- 1 If operator elects, drilling rig will batch drill the surface holes and run/cement surface casing; walking the rig to next wells on the pad.
- 2 The drilling rig will then batch drill the intermediate sections and run/cement intermediate casing; the wellbore will be isolated with a blind flange and pressure gauge installed for monitoring the well before walking to the next well.
- 3 The drilling rig will then batch drill the production hole sections on the wells with OBM, run/cement production casing, and install TA caps or tubing heads for completions.

NOTE: During batch operations the drilling rig will be moved from well to well however, it will not be removed from the pad until all wells have production casing run/cemented.

Will be pre-setting casing? Potentially

- 1 Spudder rig will move in and batch drill surface hole.
  - a. Rig will utilize fresh water based mud to drill surface hole to TD. Solids control will be handled entirely on a closed loop basis.,
- 2 After drilling the surface hole section, the spudder rig will run casing and cement following all of the applicable rules and regulations (43 CFR 3172, all COAs and NMOCD regulations).

 $^{3}$  The wellhead will be installed and tested once the surface casing is cut off and the WOC time has been reached.

- 4 A blind flange with the same pressure rating as the wellhead will be installed to seal the wellbore. Pressure will be monitored with a pressure gauge installed on the wellhead.
- 5 Spudder rig operations is expected to take 4-5 days per well on a multi-well pa.
- 6 The NMOCD will be contacted and notified 24 hours prior to commencing spudder rig operations.
- 7 Drilling operations will be performed with drilling rig. A that time an approved BOP stack will be nippled up and tested on the wellhead before drilling operations commences on each well.
  - a. The NMOCD will be contacted / notified 24 hours before the drilling rig moves back on to the pad with the pre-set surface casing.

#### Attachments

X Directional Plan Other, describe

# 1. Geologic Formations

TVD of target	12091	Pilot hole depth	N/A
MD at TD:	22300	Deepest expected fresh water	

Basin

Dusin			
	Depth	Water/Mineral	
Formation	(TVD)	Bearing/Target	Hazards*
	from KB	Zone?	
Rustler	770		
Salt	1075		
Base of Salt	4420		
Delaware	4690		
Cherry Canyon	5570		
Brushy Canyon	6980		
1st Bone Spring Lime	8530		
Bone Spring 1st	9630		
Bone Spring 2nd	10230		
3rd Bone Spring Lime	10760		
Bone Spring 3rd	11480		
Wolfcamp	11950		

\*H2S, water flows, loss of circulation, abnormal pressures, etc.

		Wt			Casing	Interval	Casing	Interval
Hole Size	Csg. Size	(PPF)	Grade	Conn	From (MD)	To (MD)	From (TVD)	To (TVD)
14 3/4	10 3/4	45.5	J55	BTC	0	795	0	795
9 7/8	8 5/8	32	P110	Sprint FJ	0	11480	0	11480
7 7/8	5 1/2	20	P110	DWC / C-IS+	0	22300	0	12091

#### 2. Casing Program

•All casing strings will be tested in accordance with 43 CFR 3172. Must have table for contingency casing.

#### 3. Cementing Program

Assuming no returns are established while drilling, Devon requests to pump a two stage cement job on the intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brushy Canyon and the second stage performed as a bradenhead squeeze with planned cement from the Brushy Canyon to surface. The final cement top will be verified by Echo-meter. Devon will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program. Devon will report to the BLM the volume of fluid (limited to 1 bbls) used to flush intermediate casing valves following backside cementing procedures.

Casing	# Sks	тос	Wt. ppg	Yld (ft3/sack)	Slurry Description
Surface	485	Surf	13.2	1.44	Lead: Class C Cement + additives
Int 1	493	Surf 13.0 2.3		2.3	2nd State: Bradenhead Squeeze - Lead: Class C Cement + additives
Int I	519	7004	13.2	1.44	Tail: Class H / C + additives
Production	117	9471	9	3.27	Lead: Class H /C + additives
Production	1433 11471 13.2 1.44		Tail: Class H / C + additives		

Casing String	% Excess
Surface	50%
Intermediate 1	30%
Prod	10%

.

BOP installed and tested before drilling which hole?	Size?	Min. Required WP	Туре		~	Tested to:																																																								
			Anı	nular	X	50% of rated working pressure																																																								
Int 1	13-5/8"	5M		d Ram	X																																																									
Int I	15 5/0	5111		e Ram		- 5M																																																								
			Doub	le Ram	Х	5141																																																								
			Other*																																																											
	13-5/8"	10M	Annular (5M)		X	100% of rated working pressure																																																								
Production			Blind Ram		Х																																																									
Tioduction			10111	10111	1011	1011	1011	1011	1011	10101	10101	10111	10111	10111	10111	10101	10101	10101	10101	10101	10111	10111	1011	10101	10111	10111	10111	10111	10101	1011	1011	1011	1011	1011	1011	1011	10101	10101	10101	10101	10101	10101	10101	10101	10101	10101	10101	10101	10101	10101	10101	10101	10111	1011	10101	10101	10101	10101	10101	10101	Pipe	e Ram
			Double Ram		Х	10111																																																								
			Other*																																																											
			Annular (5M)																																																											
			Blind Ram																																																											
			Pipe Ram																																																											
			Double Ram																																																											
			Other*																																																											
N A variance is requested for	variance is requested for the use of a diverter on the surface casing. See attached for schematic.																																																													
Y A variance is requested to r	A variance is requested to run a 5 M annular on a 10M system																																																													

## 4. Pressure Control Equipment (Three String Design)

#### 5. Mud Program (Three String Design)

Section	Туре	Weight (ppg)
Surface	FW Gel	8.5-9
Intermediate	DBE / Cut Brine	10-10.5
Production	OBM	10-10.5

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times.

What will be used to monitor the loss or gain of fluid?	PVT/Pason/Visual Monitoring
---	-----------------------------

#### 6. Logging and Testing Procedures

Logging,	Logging, Coring and Testing				
	Will run GR/CNL from TD to surface (horizontal well - vertical portion of hole). Stated logs run will be in the				
Х	Completion Rpeort and sbumitted to the BLM.				
	No logs are planned based on well control or offset log information.				
	Drill stem test? If yes, explain.				
	Coring? If yes, explain.				

Additiona	al logs planned	Interval
	Resistivity	Int. shoe to KOP
Density		Int. shoe to KOP
Х	CBL	Production casing
Х	Mud log	Intermediate shoe to TD
	PEX	

#### 7. Drilling Conditions

Condition	Specfiy what type and where?
BH pressure at deepest TVD	6602
Abnormal temperature	No

Mitigation measure for abnormal conditions. Describe. Lost circulation material/sweeps/mud scavengers.

Hydrogren Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations<br/>greater than 100 ppm, the operator will comply with the provisions of 43 CFR 3176. If Hydrogen Sulfide is encountered<br/>measured values and formations will be provided to the BLM.NH2S is present

Y H2S plan attached.

# 8. Other facets of operation

Is this a walking operation? Potentially

- 1 If operator elects, drilling rig will batch drill the surface holes and run/cement surface casing; walking the rig to next wells on the pad.
- 2 The drilling rig will then batch drill the intermediate sections and run/cement intermediate casing; the wellbore will be isolated with a blind flange and pressure gauge installed for monitoring the well before walking to the next well.
- 3 The drilling rig will then batch drill the production hole sections on the wells with OBM, run/cement production casing, and install TA caps or tubing heads for completions.

NOTE: During batch operations the drilling rig will be moved from well to well however, it will not be removed from the pad until all wells have production casing run/cemented.

Will be pre-setting casing? Potentially

- 1 Spudder rig will move in and batch drill surface hole.
  - a. Rig will utilize fresh water based mud to drill surface hole to TD. Solids control will be handled entirely on a closed loop basis.,
- 2 After drilling the surface hole section, the spudder rig will run casing and cement following all of the applicable rules and regulations (43 CFR 3172, all COAs and NMOCD regulations).

 $^{3}$  The wellhead will be installed and tested once the surface casing is cut off and the WOC time has been reached.

- 4 A blind flange with the same pressure rating as the wellhead will be installed to seal the wellbore. Pressure will be monitored with a pressure gauge installed on the wellhead.
- 5 Spudder rig operations is expected to take 4-5 days per well on a multi-well pa.
- 6 The NMOCD will be contacted and notified 24 hours prior to commencing spudder rig operations.
- 7 Drilling operations will be performed with drilling rig. A that time an approved BOP stack will be nippled up and tested on the wellhead before drilling operations commences on each well.
  - a. The NMOCD will be contacted / notified 24 hours before the drilling rig moves back on to the pad with the pre-set surface casing.

#### Attachments

X Directional Plan Other, describe



# <u>10-3/4"</u> <u>45.50#</u> <u>0.400"</u> <u>J-55</u>

# **Dimensions (Nominal)**

Outside Diameter Wall Inside Diameter Drift	10.750 0.400 9.950 9.875	in. in. in. in.
Weight, T&C Weight, PE	45.500 44.260	lbs/ft lbs/ft
Internal Yield Pressure at Minimum Yield		
Collapse	2090	psi
Internal Yields Pressure		
PE	3580	psi
STC	3580	psi
BTC	3580	psi
Yield Strength, Pipe Body	715	1000 lbs
Joint Strength, STC		
STC	493	1000 lbs
BTC	796	1000 lbs

Note: SeAH Steel has produced this specification sheet for general information only. SeAH does not assume liability or responsibility for any loss or injury resulting from the use of information or data contained herein. All applications for the material described are at the customer's own risk and responsibility.

# Section 2 - Blowout Preventer Testing Procedure

# Variance Request

Devon Energy requests to only test BOP connection breaks after drilling out of surface casing and while skidding between wells which conforms to API Standard 53 and industry standards. This test will include the Top Pipe Rams, HCR, Kill Line Check Valve, QDC (quick disconnect to wellhead) and Shell of the 10M BOPE to 5M for 10 minutes. If a break to the flex hose that runs to the choke manifold is required due to repositioning from a skid, the HCR will remain open during the shell test to include that additional break. The variance only pertains to intermediate hole-sections and no deeper than the Bone Springs Formation where 5M BOP tests are required. The initial BOP test will follow OOGO2.III.A.2.i, and subsequent tests following a skid will only test connections that are broken. The annular preventer will be tested to 100% working pressure. This variance will meet or exceed OOGO2.III.A.2.i per the following: Devon Energy will perform a full BOP test per OOGO2.III.A.2.i before drilling out of the intermediate casing string(s) and starting the production hole, before starting any hole section that requires a 10M test, before the expiration of the allotted 14-days for 5M intermediate batch drilling or when the drilling rig is fully mobilized to a new well pad, whichever is sooner. We will utilize a 200' TVD tolerance between intermediate shoes as the cutoff for a full BOP test. The BLM will be contacted 4hrs prior to a BOPE test. The BLM will be notified if and when a well control event is encountered. Break test will be a 14 day interval and not a 30 day full BOPE test interval. If in the event break testing is not utilized, then a full BOPE test would be conducted.

1. Well Control Response:

1. Primary barrier remains fluid

2. In the event of an influx due to being underbalanced and after a realized gain or flow, the order of closing BOPE is as follows:

- a) Annular first
- b) If annular were to not hold, Upper pipe rams second (which were tested on the skid BOP test)
- c) If the Upper Pipe Rams were to not hold, Lower Pipe Rams would be third



Min. Yield Strength

Max. Yield Strength

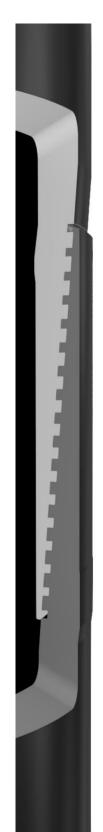
Min. Ultimate Tensile Strength

sqin. % of pipe

% of pipe

80.0 % of pipe

100 % of pipe



Issued on:	16 Sep.	2022 by	Logan Van	Gorp



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	Connection Data Shee

OD	Weight (lb/ft)	Wall TI	۱.	Grade	Alt. Drift:	Connection	
8 5/8 in.	Nominal: 32.00	0.352 i	n.	P110EC	7.875 in.	VAM <sup>®</sup> SPRINT-FJ	
	Plain End: 31.13						
	PIPE PROPERTIES				CONNECTIO	N PROPERTIES	
Nominal OD		8.625 in. Connection Type Semi-Premium Integral Flush					
Nominal ID	Nominal ID 7.921 in. Connection OD (nom): 8.665				in.		
Nominal Cross Section	9.149	sqin.	Connection ID (nom	):	7.954	in.	
Grade Type		Hig	gh Yield	Make-Up Loss		2.614	in.

Critical Cross Section

Compression Efficiency

Internal Pressure Efficiency

External Pressure Efficiency

Tension Efficiency

125

140

135

ksi

ksi

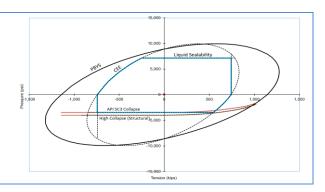
ksi

CONNECTION PERFORMANCES		
Tensile Yield Strength	744	klb
Compression Resistance	744	klb
Max. Internal Pressure	7,150	psi
Structural Collapse Resistance	4,000	psi
Max. Structural Bending	41	°/100ft
Max. Bending with Sealability	10	°/100ft

TORQUE VALU	ES	
Min. Make-up torque	23,000	ft.lb
Opt. Make-up torque	25,500	ft.lb
Max. Make-up torque	28,000	ft.lb
Max. Torque with Sealability (MTS)	48,000	ft.lb

\* 87.5% RBW

VAM® SPRINT-FJ is a semi-premium flush connection designed for shale applications, where maximum clearance and high tension capacity are required for intermediate casing strings.



#### Do you need help on this product? - Remember no one knows VAM<sup>®</sup> like VAM<sup>®</sup>

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Over 140 VAM® Specialists available worldwide 24/7 for Rig Site Assistance





# **Connection Data Sheet**

OD (in.)	WEIGHT (lbs./ft.)	WALL (in.)	GRADE	DRIFT (in.)	RBW%	CONNECTION
5.500	Nominal: 20.00 Plain End: 19.83	0.361	VST P110 EC	4.653	87.5	DWC/C-IS PLUS

#### PIPE PROPERTIES

Nominal OD	5.500	in.
Nominal ID	4.778	in.
Nominal Area	5.828	sq.in.
Grade Type	API 5CT; Vallourec Sourced Material Only	
Min. Yield Strength	125	ksi
Max. Yield Strength	140	ksi
Min. Tensile Strength	135	ksi
Yield Strength	729	klb
Ultimate Strength	787	klb
Min. Internal Yield	14,360	psi
*High Collapse*	12,090	psi

#### **CONNECTION PROPERTIES**

Premium T&C 6.300 4.778 4.125	in. in. in.
4.778	in.
4.125	in
	in.
9.250	in.
5.828	sq.in.
100.0%	of pipe
	9.250 5.828 100.0% 100.0% 100.0%

#### **CONNECTION PERFORMANCES** 729 klb Yield Strength Parting Load 787 klb **Compression Rating** 729 klb Min. Internal Yield 14,360 psi \*High Collapse\* 12,090 psi Maximum Uniaxial Bend Rating 104.2 °/100 ft Ref String Length w 1.4 Design Factor 26,040 ft

FIELD TORQUE VALUES		
Min. Make-up Torque	16,600	ft.lbs
Opti. Make-up Torque	17,850	ft.lbs
Max. Make-up Torque	19,100	ft.lbs
Min. Shoulder Torque	1,660	ft.lbs
Max. Shoulder Torque	13,280	ft.lbs
Max. Delta Turn	0.200	Turns
+Max Operational Torque	24,300	ft.lbs
+Maximum Torsional Value (MTV)	26,730	ft.lbs

#### +Maximum Operational Torque and Maximum Torsional Value Only Valid with Vallourec P110EC Material

#### For detailed information on performance properties, refer to DWC Connection Data Notes on following page(s).

Connection specifications within the control of VAM USA were correct as of the date printed. Specifications are subject to change without notice. Certain connection specifications are dependent on the mechanical properties of the pipe. Mechanical properties of mill proprietary pipe grades were obtained from mill publications and are subject to change. Properties of mill proprietary grades should be confirmed with the mill. Users are advised to obtain current connection specifications and verify pipe mechanical properties for each application.

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## DWC Connection Data Notes:

- 1. DWC connections are available with a seal ring (SR) option.
- 2. All standard DWC/C connections are interchangeable for a given pipe OD. DWC connections are interchangeable with DWC/C-SR connections of the same OD and wall.
- 3. Connection performance properties are based on nominal pipe body and connection dimensions.
- DWC connection internal and external pressure resistance is calculated using the API rating for buttress connections. API Internal pressure resistance is calculated from formulas 31, 32, and 35 in the API Bulletin 5C3.
- 5. DWC joint strength is the minimum pipe body yield strength multiplied by the connection critical area.
- 6. API joint strength is for reference only. It is calculated from formulas 42 and 43 in the API Bulletin 5C3.
- 7. Bending efficiency is equal to the compression efficiency.
- 8. The torque values listed are recommended. The actual torque required may be affected by field conditions such as temperature, thread compound, speed of make-up, weather conditions, etc.
- 9. Connection yield torque is not to be exceeded.
- Reference string length is calculated by dividing the joint strength by both the nominal weight in air and a design factor (DF) of 1.4. These values are offered for reference only and do not include load factors such as bending, buoyancy, temperature, load dynamics, etc.
- 11. DWC connections will accommodate API standard drift diameters.
- 12. DWC/C family of connections are compatible with API Buttress BTC connections. Please contact tech.support@vam-usa.com for details on connection ratings and make-up.

Connection specifications within the control of VAM USA were correct as of the date printed. Specifications are subject to change without notice. Certain connection specifications are dependent on the mechanical properties of the pipe. Mechanical properties of mill proprietary pipe grades were obtained from mill publications and are subject to change. Properties of mill proprietary grades should be confirmed with the mill. Users are advised to obtain current connection specifications and verify pipe mechanical properties for each application.

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#### Paint 4-33 Fed Com 712H

10 3/4	sui	face csg in a	14 3/4	inch hole.		Design	Factors			Surface	2	
Segment	#/ft	Grade		Coupling	Body	Collapse	Burst	Length	B@s	a-B	a-C	Weight
"A"	45.50		j 55	btc	17.97	5.11	0.55	875	9	0.92	9.65	39,813
"B"			,	btc				0				0
	w/8.4#	g mud, 30min Sfc Csg Test	psig: 1.500	Tail Cmt	does not	circ to sfc.	Totals:	875				39,813
omparison o		inimum Required Ceme										,-
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Reg'd				Min Dis
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cp
14 3/4	0.5563	485	698	487	43	9.00	3889	5M				1.50
urst Frac Grac	dient(s) for Segm	ent(s) A, B = , b All > 0	).70. OK.									
									-			
8 5/8	casi	ng inside the	10 3/4			Design	Factors			Int 1		
Segment	#/ft	Grade	,	Coupling	Joint	Collapse	Burst	Length	B@s	a-B	a-C	Weigh
"A"	32.00		p 110	vam sprint fj	1.95	0.61	1.06	11,950	1	1.77	1.03	•
"B"				. ,				0				0
	w/8.4#	g mud, 30min Sfc Csg Test	psig: -210				Totals:	11,950				382,40
	,,			ded to achieve a top of	0	ft from su		875				overlap.
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Rea'd				Min Dis
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cp
9 7/8	0.1261	571	822	1514	-46	10.50	4033	5M				0.61
V Tool(s):	0.1201	3/1	6980	1014	-+0	10.50	sum of sx	Σ CuFt				Σ%exces
<i>v</i> rooi(s).												
	nt yld > 1.35	31	28				1065	1958				29
lass 'C' tail cm								1958	a a			29
Tail cmt 5 1/2	casi	ng inside the	28 8 5/8			Design Fa	<u>ctors</u>			Prod 1		
Tail cmt 5 1/2 Segment	casi #/ft		8 5/8	Coupling	Joint	Collapse	<u>ctors</u> Burst	Length	B@s	a-B	a-C	Weigh
Tail cmt 5 1/2 Segment "A"	casi	ng inside the		Coupling dwc/c is+	<b>Joint</b> 2.94		<u>ctors</u>	Length 22,611	<b>B@s</b> 2			Weigh 452,22
Tail cmt 5 1/2 Segment	casi #/ft	ng inside the	8 5/8			Collapse	<u>ctors</u> Burst 2.12	Length 22,611 0	<u> </u>	a-B	a-C	Weigh 452,22 0
Tail cmt 5 1/2 Segment "A"	casi #/ft 20.00	ng inside the Grade /g mud, 30min Sfc Csg Test (	<b>8 5/8</b> p 110 psig: 2,726	dwc/c is+	2.94	Collapse 1.79	ctors Burst 2.12 Totals:	Length 22,611 0 22,611	<u> </u>	a-B	a-C	Weigh 452,22 0 452,22
Tail cmt 5 1/2 Segment "A"	casi #/ft 20.00	ng inside the Grade /g mud, 30min Sfc Csg Test (	<b>8 5/8</b> p 110 psig: 2,726		2.94	Collapse	ctors Burst 2.12 Totals:	Length 22,611 0	<u> </u>	a-B	a-C	Weigh 452,22 0
Tail cmt 5 1/2 Segment "A"	casi #/ft 20.00	ng inside the Grade /g mud, 30min Sfc Csg Test (	<b>8 5/8</b> p 110 psig: 2,726	dwc/c is+	2.94	Collapse 1.79	ctors Burst 2.12 Totals:	Length 22,611 0 22,611	<u> </u>	a-B	a-C	Weigh 452,22 0 452,22 overlap.
Tail cmt 5 1/2 Segment "A" "B"	<b>casi</b> <b>#/ft</b> 20.00 w/8.4#,	ng inside the Grade /g mud, 30min Sfc Csg Test The cement	8 5/8 p 110 psig: 2,726 volume(s) are inter	dwc/c is+	2.94 11750	Collapse 1.79 ft from su	ctors Burst 2.12 Totals: Irface or a	Length 22,611 0 22,611 200	<u> </u>	a-B	a-C	Weigh 452,22 0 452,22 overlap. Min Dis
Tail cmt 5 1/2 Segment "A" "B" Hole	casi #/ft 20.00 w/8.4#, Annular	ng inside the Grade 'g mud, 30min Sfc Csg Test The cement of 1 Stage	8 5/8 p 110 psig: 2,726 volume(s) are inter 1 Stage	dwc/c is+ nded to achieve a top of Min	2.94 11750 1 Stage	Collapse 1.79 ft from su Drilling	ctors Burst 2.12 Totals: Inface or a Calc	Length 22,611 0 22,611 200 Req'd	<u> </u>	a-B	a-C	Weigh 452,22 0 452,22 overlap. Min Dis
5 1/2 Segment "A" "B" Hole Size	casi #/ft 20.00 w/8.4#, Annular Volume 0.1733	ng inside the Grade 'g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx	8 5/8 p 110 psig: 2,726 volume(s) are inter 1 Stage CuFt Cmt	dwc/c is+ nded to achieve a top of Min Cu Ft	2.94 11750 1 Stage % Excess	Collapse 1.79 ft from su Drilling Mud Wt	ctors Burst 2.12 Totals: Inface or a Calc	Length 22,611 0 22,611 200 Req'd	<u> </u>	a-B	a-C	Weigh 452,22 0 452,22 overlap. Min Dis Hole-Cpl
Tail cmt Tail cmt 51/2 Segment "A" "B" Hole Size 7 7/8 Jass 'C' tail cm #N/A	casi #/ft 20.00 w/8.4#, Annular Volume 0.1733	ng inside the Grade 'g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx	8 5/8 p 110 psig: 2,726 volume(s) are inter 1 Stage CuFt Cmt 2445	dwc/c is+ nded to achieve a top of Min Cu Ft	2.94 11750 1 Stage % Excess	Collapse 1.79 ft from su Drilling Mud Wt 10.50	ctors Burst 2.12 Totals: Irface or a Calc MASP	Length 22,611 0 22,611 200 Req'd	2	<b>a-B</b> 3.56	<b>a-C</b> 3.00	Weigh 452,22 0 452,22 overlap. Min Dis Hole-Cp
Tail cmt Tail cmt 5 1/2 Segment "A" "B" Hole Size 7 7/8 Ilass 'C' tail cm #N/A 0	casi #/ft 20.00 w/8.4#, Annular Volume 0.1733 at yld > 1.35	ng inside the Grade /g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 1549	8 5/8 p 110 psig: 2,726 volume(s) are inter 1 Stage CuFt Cmt	dwc/c is+	2.94 11750 1 Stage % Excess 30	Collapse 1.79 ft from su Drilling Mud Wt 10.50 Design	ctors Burst 2.12 Totals: Inface or a Calc MASP Factors	Length 22,611 0 22,611 200 Req'd BOPE	2	a-B 3.56	a-C 3.00 sing>	Weigh 452,22 0 452,22 overlap. Min Dis Hole-Cp 1.19
Tail cmt 5 1/2 Segment "A" "B" Hole Size 7 7/8 lass 'C' tail cm #N/A 0 Segment	casi #/ft 20.00 w/8.4#, Annular Volume 0.1733	ng inside the Grade 'g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx	8 5/8 p 110 psig: 2,726 volume(s) are inter 1 Stage CuFt Cmt 2445	dwc/c is+	2.94 11750 1 Stage % Excess	Collapse 1.79 ft from su Drilling Mud Wt 10.50	ctors Burst 2.12 Totals: Irface or a Calc MASP	Length 22,611 0 22,611 200 Req'd BOPE	2	a-B 3.56	<b>a-C</b> 3.00	Weigh 452,22 0 452,22 overlap. Min Dis Hole-Cp 1.19 Weigh
Tail cmt 5 1/2 Segment "A" "B" Hole Size 7 7/8 lass 'C' tail cm $\frac{\#N/A}{0}$ Segment "A"	casi #/ft 20.00 w/8.4#, Annular Volume 0.1733 at yld > 1.35	ng inside the Grade /g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 1549	8 5/8 p 110 psig: 2,726 volume(s) are inter 1 Stage CuFt Cmt 2445	dwc/c is+	2.94 11750 1 Stage % Excess 30	Collapse 1.79 ft from su Drilling Mud Wt 10.50 Design	ctors Burst 2.12 Totals: Inface or a Calc MASP Factors	Length 22,611 0 22,611 200 Req'd BOPE	2	a-B 3.56	a-C 3.00 sing>	Weigh 452,22 0 452,22 overlap. Min Dis Hole-Cp 1.19 Weigh 0
Tail cmt Tail cmt 5 1/2 Segment "A" "B" Hole Size 7 7/8 lass 'C' tail cm #N/A 0 Segment	casi #/ft 20.00 w/8.4#, Annular Volume 0.1733 nt yld > 1.35 #/ft	ng inside the Grade 'g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 1549 Grade	8 5/8 p 110 psig: 2,726 volume(s) are inter 1 Stage CuFt Cmt 2445 5 1/2	dwc/c is+	2.94 11750 1 Stage % Excess 30	Collapse 1.79 ft from su Drilling Mud Wt 10.50 Design	ctors Burst 2.12 Totals: urface or a Calc MASP Factors Burst	Length 22,611 0 22,611 200 Req'd BOPE	2	a-B 3.56	a-C 3.00 sing>	Weigh 452,22 0 452,22 overlap. Min Dis Hole-Cp 1.19 1.19
Tail cmt 5 1/2 Segment "A" "B" Hole Size 7 7/8 lass 'C' tail cm $\frac{\#N/A}{0}$ Segment "A"	casi #/ft 20.00 w/8.4#, Annular Volume 0.1733 nt yld > 1.35 #/ft	ng inside the Grade /g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx 1549 Grade	8 5/8 p 110 psig: 2,726 volume(s) are inter 1 Stage CuFt Cmt 2445 5 1/2 psig:	dwc/c is+	2.94 11750 1 Stage % Excess 30 #N/A	Collapse 1.79 ft from su Drilling Mud Wt 10.50 <u>Design</u> Collapse	ctors Burst 2.12 Totals: urface or a Calc MASP Factors Burst	Length 22,611 0 22,611 200 Req'd BOPE Length 0 0 0	2	a-B 3.56	a-C 3.00 sing> a-C	Weigh 452,22 0 452,22 overlap. Min Dis Hole-Cp 1.19 Ueigh 0 0 0
Tail cmt 5 1/2 Segment "A" "B" Hole Size 7 7/8 lass 'C' tail cm #N/A 0 Segment "A" "B"	casi #/ft 20.00 w/8.4#, Annular Volume 0.1733 at yld > 1.35 #/ft w/8.4#,	ng inside the Grade /g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx 1549 Grade /g mud, 30min Sfc Csg Test Cmt vol cs	8 5/8 p 110 psig: 2,726 volume(s) are inter 1 Stage CuFt Cmt 2445 5 1/2 psig: alc below includes	dwc/c is+	2.94 11750 1 Stage % Excess 30 #N/A #N/A	Collapse 1.79 ft from su Drilling Mud Wt 10.50 <u>Design I</u> Collapse ft from su	ctors Burst 2.12 Totals: Inface or a Calc MASP Factors Burst	Length 22,611 0 22,611 200 Req'd BOPE	2	a-B 3.56	a-C 3.00 sing> a-C	Weigh 452,22 overlap. Min Dis Hole-Cp 1.19 Weigh 0 0 0 0 0 0 0
Tail cmt Tail cmt 5 1/2 Segment "A" "B" Hole Size 7 7/8 Iass 'C' tail cm #N/A 0 Segment "A" "B" Hole	casi #/ft 20.00 w/8.4#, Annular Volume 0.1733 tt yld > 1.35 #/ft w/8.4#, Annular	rig inside the Grade (g mud, 30min Sfc Csg Test The cement of 1 Stage Cmt Sx 1549 Grade (g mud, 30min Sfc Csg Test Cmt vol c 1 Stage	8 5/8 p 110 psig: 2,726 volume(s) are inter 1 Stage CuFt Cmt 2445 5 1/2 psig: alc below includes 1 Stage	dwc/c is+	2.94 11750 1 Stage % Excess 30 #N/A #N/A 1 Stage	Collapse 1.79 ft from su Drilling Mud Wt 10.50 <u>Design</u> Collapse ft from su Drilling	ctors Burst 2.12 Totals: Inface or a Calc MASP Factors Burst Totals: Inface or a Calc	Length 22,611 0 22,611 200 Req'd BOPE Length 0 0 0 #N/A Req'd	2	a-B 3.56	a-C 3.00 sing> a-C	Weigh 452,22 overlap. Min Dis Hole-Cp 1.19 Weigh 0 0 0 overlap. Min Dis
Tail cmt Tail cmt 5 1/2 Segment "A" "B" Hole Size 7 7/8 Iass 'C' tail cm #N/A 0 Segment "A" "B" Hole Size	casi #/ft 20.00 w/8.4#, Annular Volume 0.1733 at yld > 1.35 #/ft w/8.4#,	rig inside the Grade (g mud, 30min Sfc Csg Test The cement of 1 Stage Cmt Sx 1 549 Grade (g mud, 30min Sfc Csg Test Cmt vol ca 1 Stage Cmt Sx	8 5/8 p 110 psig: 2,726 volume(s) are inter 1 Stage CuFt Cmt 2445 5 1/2 psig: alc below includes 1 Stage CuFt Cmt	dwc/c is+	2.94 11750 1 Stage % Excess 30 #N/A 1 Stage % Excess	Collapse 1.79 ft from su Drilling Mud Wt 10.50 <u>Design I</u> Collapse ft from su	ctors Burst 2.12 Totals: Inface or a Calc MASP Factors Burst	Length 22,611 0 22,611 200 Req'd BOPE Length 0 0 0 #N/A	2	a-B 3.56	a-C 3.00 sing> a-C	Weigh 452,22 0 452,22 overlap. Min Dis Hole-Cp 1.19 Uveigh 0 0
Tail cmt Tail cmt 5 1/2 Segment "A" "B" Hole Size 7 7/8 lass 'C' tail cm #N/A 0 Segment "A" "B" Hole	casi #/ft 20.00 w/8.4#, Annular Volume 0.1733 tt yld > 1.35 #/ft w/8.4#, Annular	rig inside the Grade (g mud, 30min Sfc Csg Test The cement of 1 Stage Cmt Sx 1549 Grade (g mud, 30min Sfc Csg Test Cmt vol c 1 Stage	8 5/8 p 110 psig: 2,726 volume(s) are inter 1 Stage CuFt Cmt 2445 5 1/2 psig: alc below includes 1 Stage	dwc/c is+	2.94 11750 1 Stage % Excess 30 #N/A #N/A 1 Stage	Collapse 1.79 ft from su Drilling Mud Wt 10.50 <u>Design</u> Collapse ft from su Drilling	ctors Burst 2.12 Totals: Inface or a Calc MASP Factors Burst Totals: Inface or a Calc	Length 22,611 0 22,611 200 Req'd BOPE Length 0 0 0 #N/A Req'd	2	a-B 3.56	a-C 3.00 sing> a-C	Weigh 452,22 overlap. Min Dis Hole-Cp 1.19 Weigh 0 0 0 overlap. Min Dis

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#### Paint 4-33 Fed Com 622H

<b>#/ft</b> 45.50	ce csg in a Grade	j 55	Coupling btc	<b>Body</b> 17.97	Design I Collapse 5.11	Burst 0.57	Length 875	<b>B@s</b> 9	<b>a-B</b> 0.96	<b>a-C</b> 9.65	Weight 39,813	
w/8.4#/g r Proposed to Mini Annular		j 55		17.97	5 11	0.57	875	9	0.96	9.65	30 813	
w/8.4#/g r Proposed to Mini Annular		] 00										
Proposed to Mini Annular			btc		0.11	0.01	0	Ŭ	0.00	2.00	0	
Proposed to Mini Annular		nsig: 1 500	Tail Cmt	does not	circ to sfc.	Totals:	875				39,813	
Annular	mum Dogurod Com		Tui Onit	0003 1101	010 10 310.	Totais.	075				00,010	
	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Reg'd				Min Dis	
volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cp	
0.5563	485	698	487				5M				1.50	
0.5565	400	090	407	43	9.00	3736	IVIC				1.50	
nt(s) for Segmen	t(s) A, B = , b All > (	).70, ОК.		Site plat (pip	e racks S or E)	as per 0.0.1.	.III.D.4.i. not	found.				
casing	inside the	10 3/4			Desian I	Factors			Int 1			
			Coupling	Joint			Lenath	B@s		a-C	Weigh	
		p 110					-	-			-	
		,	i ani opinicij	2.00	0.01		,	- <sup>1</sup>	1.02	1.07	007,000	
w/9 1#/~	nud 20min Sfc Ccc Toot	nsia:				Totals	-				367.36	
w/8.4#/g1			adad to achieve a ten of	0	ft from cu		,				overlap.	
Annular											Min Dis	
	•			•	•							
											Hole-Cp	
0.1261	519		1455	-49	10.50		-				0.61	
											Σ%exces	
	32	28				1012	1881				29	
								-				
L. L.		8 5/8	<u>-</u>									
	Grade							<u> </u>	-		Weigh	
20.00		р 110	dwc/c is+	3.01	1.83	2.18	22,300	2	3.65	3.07	446,00	
							0				0	
w/8.4#/g r	nud, 30min Sfc Csg Test	psig: 2,660				Totals:	22,300				446,00	
	The cement	volume(s) are inter	nded to achieve a top of	11280	ft from su	rface or a	200				overlap.	
Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Req'd				Min Dis	
Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cpl	
0.1733	1550	2446	1910	28	10.50						1.19	
yld > 1.35												
		  			Design	Eactors			boose Ca	sings		
#/ft	Grado	21/2	Courling	#N/A			Longth			U	Weight	
<del>#</del> /IL	Grade			#N/A	Collapse	Buist	•	Bues	a-D	a-0	0	
							-				-	
			0.00				-				0	
w/8.4#/g r							-				0	
											overlap.	
Annular	1 Stage	1 Stage	Min		-	Calc	Req'd				Min Dis	
Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cp	
	#N/A	#N/A	0	#N/A								
		Capitan Reef e	est top XXXX.									
	<pre>#/ft 32.00 w/8.4#/g r Annular Volume 0.1261 dd &gt; 1.35 casing #/ft 20.00 w/8.4#/g r Annular Volume 0.1733 dd &gt; 1.35 #/ft w/8.4#/g r Annular</pre>	32.00          w/8.4#/g mud, 30min Sfc Csg Test         The cement         Annular       1 Stage         Volume       Cmt Sx         0.1261       519         32         td > 1.35         casing inside the         #/ft       Grade         20.00       w/8.4#/g mud, 30min Sfc Csg Test         The cement         Annular       1 Stage         Volume       Cmt Sx         0.1733       1550         td > 1.35       id > 1.35         #/ft       Grade         w/8.4#/g mud, 30min Sfc Csg Test       Cmt Sx         0.1733       1550         td > 1.35       Cmt Vol c         Annular       1 Stage         Volume       Cmt Vol c         Annular       1 Stage         Volume       Cmt Sx	<pre>#/ft Grade 32.00 p 110 w/8.4#/g mud, 30min Sfc Csg Test psig: The cement volume(s) are inter Annular 1 Stage 1 Stage Volume Cmt Sx CuFt Cmt 0.1261 519 747 6980 32 28 id &gt; 1.35 casing inside the 8 5/8 #/ft Grade 20.00 p 110 w/8.4#/g mud, 30min Sfc Csg Test psig: 2,660 The cement volume(s) are inter Annular 1 Stage 1 Stage Volume Cmt Sx CuFt Cmt 0.1733 1550 2446 id &gt; 1.35 </pre>	#/ft       Grade       Coupling         32.00       p 110       vam sprint fj         w/8.4#/g mud, 30min Sfc Csg Test psig: The cement volume(s) are intended to achieve a top of         Annular       1 Stage       1 Stage       Min         Volume       Cmft Sx       CuFt Cmt       Cu Ft         0.1261       519       747       1455         6980         32       28         id > 1.35         casing inside the       8 5/8         #/ft       Grade       Coupling         20.00       p 110       dwc/c is+         w/8.4#/g mud, 30min Sfc Csg Test psig:       2,660         The cement volume(s) are intended to achieve a top of         Annular       1 Stage       1 Stage       Min         Volume       Cmt Sx       CuFt Cmt       Cu Ft         0.1733       1550       2446       1910       1d > 1.35         Full Grade       Coupling         0.00         w/8.4#/g mud, 30min Sfc Csg Test psig:       Cmt vol calc below includes this csg, TOC intended         Cmt vol calc below includes this csg, TOC intended         Aline       1 Stage <td< td=""><td>#/ft       Grade       Coupling       Joint         32.00       p 110       vam sprint fj       2.03         w/8.4#/g mud, 30min Sfc Csg Test psig: The cement volume(s) are intended to achieve a top of 0       0         Annular       1 Stage       Min       1 Stage         Volume       Cmt Sx       CuFt Cmt       Cu Ft       % Excess         0.1261       519       747       1455       -49         6980         32       28         id &gt; 1.35         casing inside the       8 5/8         #/ft       Grade       Coupling       Joint         20.00       p 110       dwc/c is+       3.01         w/8.4#/g mud, 30min Sfc Csg Test psig: 2,660       The cement volume(s) are intended to achieve a top of       11280         Annular       1 Stage       1 Stage       Min       1 Stage         Volume       Cmt Sx       CuFt Cmt       Cu Ft       % Excess         0.1733       1550       2446       1910       28         id &gt; 1.35         Cmt vol calc below includes this csg, TOC intended       #N/A         Min       1 Stage         Volume&lt;</td><td>#/ft       Grade       Coupling       Joint       Collapse         32.00       p 110       vam sprint fj       2.03       0.64         w/8.4#/g mud, 30min 5fc Csg Test psig:       The cement volume(s) are intended to achieve a top of       0       ft from su         Annular       1 Stage       1 Stage       Min       1 Stage       Drilling         Volume       Cmt Sx       CuFt Cmt       Cu Ft       % Excess       Mud Wt         0.1261       519       747       1455       -49       10.50         6980         32       28         id &gt; 1.35         Casing inside the       8 5/8       Design Fai         w/8.4#/g mud, 30min 5fc Csg Test psig:       2,660         The cement volume(s) are intended to achieve a top of       11280       ft from su         Annular       1 Stage       1 Stage       Drilling         Volume       Cmt Sx       CuFt Cmt       Cu Ft       % Excess       Drilling         Volume       1 Stage       1 Stage       Drilling         Volume       Cmt Sx       CuFt Cmt       Cu Ft       % Excess       Mud Wt         <td colsp<="" td=""><td>#/ft       Grade       Coupling       Joint       Collapse       Burst         32.00       p 110       vam sprint fj       2.03       0.64       1.08         w/8.4#/g mud, 30min Sfc Csg Test psig:       Totals:       Totals:       Totals:         Annular       1 Stage       1 Stage       0.64       1.08         Volume       Cmt Sx       CuFt Cmt       Cu Ft       % Excess       Mud Wt       MASP         0.1261       519       747       1455       -49       10.50       3935         0.280       32       28       1012       1012       1012         td &gt; 1.35       5980       3001       1.83       2.18         w/8.4#/g mud, 30min Sfc Csg Test psig:       2,660       Totals:       Collapse       Burst         w/8.4#/g mud, 30min Sfc Csg Test psig:       2,660       Totals:       Totals:         The cement volume(s) are intended to achieve a top of       11280       Totals:       Totals:         Volume       1 Stage       1 Stage       Min       1 Stage       Drilling       Calc         Volume       Cmt Sx       CuFt Cmt       Cu Ft       K Excess       Mud Wt       MASP         1.1733       1550       2446<!--</td--><td>#/ft       Grade       Coupling       Joint       Coillapse       Burst       Length         32.00       p 110       vam sprint fj       2.03       0.64       1.08       11,480         32.00       p 110       vam sprint fj       2.03       0.64       1.08       11,480         wiss.4k/g mud, 30min Src Csg Test psig:       The cement volume(s) are intended to achieve a top of       0       ft from surface or a       875         Annular       1 Stage       Min       1 Stage       Mud Wt       MASP       BOPE         0.1261       519       747       1455       -49       10.50       3935       5M         0.22       28       00       sum of sx       CuFF       Excess       1012       1881         1d &gt; 1.35       32       28       28       1012       1881       22,300       1012       1881         20.00       p 110       dwc/c is+       3.01       1.83       2.18       22,300         w//8.4k/g mud, 30min Src Csg Test psig: 2,660       Totals:       22,300       Totals:       22,300         The cement volume(s) are intended to achieve a top of 11280       114       1832       28       10.50       20         0.1733       1550&lt;</td><td>#/ft       Grade       Coupling       Joint       Collapse       Burst       Length       B@s         32.00       p 110       vam sprint fj       2.03       0.64       1.08       11,480       1         w/8.4#/g mud, 30min Stc Csg Test psig:       Totals:       Totals:       0       11,480       1         Manular       1 Stage       1 Stage       Min       1 Stage       Mul Wit       MASP         0.1261       519       747       1455       -49       10.50       3935       5M         32       28       1012       1881       11280       111280       1881       111280         w/8.4#/g mud, 30min Stc Csg Test psig:       2,660       501       1.83       2.18       2.300       2         w/8.4#/g mud, 30min Stc Csg Test psig:       2,660       Totals:       2,300       2       2       0         w/8.4#/g mud, 30min Stc Csg Test psig:       2,660       Totals:       2,300       2       2       0       2       0       2       0       2       0       2       0       2       0       2       0       2       0       2       0       2       0       2       0       2       0       0</td><td>#/ft         Grade         Coupling         Joint         Collapse         Burst         Length         B@s         a-B           32.00         p 110         vam sprint fj         2.03         0.64         1.08         11,480         1         1         1.82           w/8.4t/g mud, 30min Sfc Csg Test psig:         The cement volume(s) are intended to achieve a top of 0         0         ft from surface or a         875         Red'd         875           Nular         1 Stage         CuFt         % Excess         Drilling         MaXP         BOPE         5M           0.1261         519         747         1455         -49         10.50         3935         5M           32         28         1012         1881         20.0F         1881         20.0F         1881         22.300         2         3.01         1.83         2.18         2.300         2         3.65         0&lt;</td><td>#/ft         Grade         Coupling         Joint         Collapse         Burst         Length         B@s         a-B         a-C           32.00         p 110         vam sprint fj         2.03         0.64         1.08         11.480         1         1.82         1.07           w/8.4#/g mud, 30min Sfc Cag Test psig:         The cement volume(s) are intended to achieve a top of         0         ft from surface or a         875         875           Annular         Chit Sage         1 Stage         Min         1 Stage         100         90         11.480         11.480         11.480           0.1261         519         747         1455         -49         10.05         3935         5M        </td></td></td></td></td<>	#/ft       Grade       Coupling       Joint         32.00       p 110       vam sprint fj       2.03         w/8.4#/g mud, 30min Sfc Csg Test psig: The cement volume(s) are intended to achieve a top of 0       0         Annular       1 Stage       Min       1 Stage         Volume       Cmt Sx       CuFt Cmt       Cu Ft       % Excess         0.1261       519       747       1455       -49         6980         32       28         id > 1.35         casing inside the       8 5/8         #/ft       Grade       Coupling       Joint         20.00       p 110       dwc/c is+       3.01         w/8.4#/g mud, 30min Sfc Csg Test psig: 2,660       The cement volume(s) are intended to achieve a top of       11280         Annular       1 Stage       1 Stage       Min       1 Stage         Volume       Cmt Sx       CuFt Cmt       Cu Ft       % Excess         0.1733       1550       2446       1910       28         id > 1.35         Cmt vol calc below includes this csg, TOC intended       #N/A         Min       1 Stage         Volume<	#/ft       Grade       Coupling       Joint       Collapse         32.00       p 110       vam sprint fj       2.03       0.64         w/8.4#/g mud, 30min 5fc Csg Test psig:       The cement volume(s) are intended to achieve a top of       0       ft from su         Annular       1 Stage       1 Stage       Min       1 Stage       Drilling         Volume       Cmt Sx       CuFt Cmt       Cu Ft       % Excess       Mud Wt         0.1261       519       747       1455       -49       10.50         6980         32       28         id > 1.35         Casing inside the       8 5/8       Design Fai         w/8.4#/g mud, 30min 5fc Csg Test psig:       2,660         The cement volume(s) are intended to achieve a top of       11280       ft from su         Annular       1 Stage       1 Stage       Drilling         Volume       Cmt Sx       CuFt Cmt       Cu Ft       % Excess       Drilling         Volume       1 Stage       1 Stage       Drilling         Volume       Cmt Sx       CuFt Cmt       Cu Ft       % Excess       Mud Wt <td colsp<="" td=""><td>#/ft       Grade       Coupling       Joint       Collapse       Burst         32.00       p 110       vam sprint fj       2.03       0.64       1.08         w/8.4#/g mud, 30min Sfc Csg Test psig:       Totals:       Totals:       Totals:         Annular       1 Stage       1 Stage       0.64       1.08         Volume       Cmt Sx       CuFt Cmt       Cu Ft       % Excess       Mud Wt       MASP         0.1261       519       747       1455       -49       10.50       3935         0.280       32       28       1012       1012       1012         td &gt; 1.35       5980       3001       1.83       2.18         w/8.4#/g mud, 30min Sfc Csg Test psig:       2,660       Totals:       Collapse       Burst         w/8.4#/g mud, 30min Sfc Csg Test psig:       2,660       Totals:       Totals:         The cement volume(s) are intended to achieve a top of       11280       Totals:       Totals:         Volume       1 Stage       1 Stage       Min       1 Stage       Drilling       Calc         Volume       Cmt Sx       CuFt Cmt       Cu Ft       K Excess       Mud Wt       MASP         1.1733       1550       2446<!--</td--><td>#/ft       Grade       Coupling       Joint       Coillapse       Burst       Length         32.00       p 110       vam sprint fj       2.03       0.64       1.08       11,480         32.00       p 110       vam sprint fj       2.03       0.64       1.08       11,480         wiss.4k/g mud, 30min Src Csg Test psig:       The cement volume(s) are intended to achieve a top of       0       ft from surface or a       875         Annular       1 Stage       Min       1 Stage       Mud Wt       MASP       BOPE         0.1261       519       747       1455       -49       10.50       3935       5M         0.22       28       00       sum of sx       CuFF       Excess       1012       1881         1d &gt; 1.35       32       28       28       1012       1881       22,300       1012       1881         20.00       p 110       dwc/c is+       3.01       1.83       2.18       22,300         w//8.4k/g mud, 30min Src Csg Test psig: 2,660       Totals:       22,300       Totals:       22,300         The cement volume(s) are intended to achieve a top of 11280       114       1832       28       10.50       20         0.1733       1550&lt;</td><td>#/ft       Grade       Coupling       Joint       Collapse       Burst       Length       B@s         32.00       p 110       vam sprint fj       2.03       0.64       1.08       11,480       1         w/8.4#/g mud, 30min Stc Csg Test psig:       Totals:       Totals:       0       11,480       1         Manular       1 Stage       1 Stage       Min       1 Stage       Mul Wit       MASP         0.1261       519       747       1455       -49       10.50       3935       5M         32       28       1012       1881       11280       111280       1881       111280         w/8.4#/g mud, 30min Stc Csg Test psig:       2,660       501       1.83       2.18       2.300       2         w/8.4#/g mud, 30min Stc Csg Test psig:       2,660       Totals:       2,300       2       2       0         w/8.4#/g mud, 30min Stc Csg Test psig:       2,660       Totals:       2,300       2       2       0       2       0       2       0       2       0       2       0       2       0       2       0       2       0       2       0       2       0       2       0       2       0       0</td><td>#/ft         Grade         Coupling         Joint         Collapse         Burst         Length         B@s         a-B           32.00         p 110         vam sprint fj         2.03         0.64         1.08         11,480         1         1         1.82           w/8.4t/g mud, 30min Sfc Csg Test psig:         The cement volume(s) are intended to achieve a top of 0         0         ft from surface or a         875         Red'd         875           Nular         1 Stage         CuFt         % Excess         Drilling         MaXP         BOPE         5M           0.1261         519         747         1455         -49         10.50         3935         5M           32         28         1012         1881         20.0F         1881         20.0F         1881         22.300         2         3.01         1.83         2.18         2.300         2         3.65         0&lt;</td><td>#/ft         Grade         Coupling         Joint         Collapse         Burst         Length         B@s         a-B         a-C           32.00         p 110         vam sprint fj         2.03         0.64         1.08         11.480         1         1.82         1.07           w/8.4#/g mud, 30min Sfc Cag Test psig:         The cement volume(s) are intended to achieve a top of         0         ft from surface or a         875         875           Annular         Chit Sage         1 Stage         Min         1 Stage         100         90         11.480         11.480         11.480           0.1261         519         747         1455         -49         10.05         3935         5M        </td></td></td>	<td>#/ft       Grade       Coupling       Joint       Collapse       Burst         32.00       p 110       vam sprint fj       2.03       0.64       1.08         w/8.4#/g mud, 30min Sfc Csg Test psig:       Totals:       Totals:       Totals:         Annular       1 Stage       1 Stage       0.64       1.08         Volume       Cmt Sx       CuFt Cmt       Cu Ft       % Excess       Mud Wt       MASP         0.1261       519       747       1455       -49       10.50       3935         0.280       32       28       1012       1012       1012         td &gt; 1.35       5980       3001       1.83       2.18         w/8.4#/g mud, 30min Sfc Csg Test psig:       2,660       Totals:       Collapse       Burst         w/8.4#/g mud, 30min Sfc Csg Test psig:       2,660       Totals:       Totals:         The cement volume(s) are intended to achieve a top of       11280       Totals:       Totals:         Volume       1 Stage       1 Stage       Min       1 Stage       Drilling       Calc         Volume       Cmt Sx       CuFt Cmt       Cu Ft       K Excess       Mud Wt       MASP         1.1733       1550       2446<!--</td--><td>#/ft       Grade       Coupling       Joint       Coillapse       Burst       Length         32.00       p 110       vam sprint fj       2.03       0.64       1.08       11,480         32.00       p 110       vam sprint fj       2.03       0.64       1.08       11,480         wiss.4k/g mud, 30min Src Csg Test psig:       The cement volume(s) are intended to achieve a top of       0       ft from surface or a       875         Annular       1 Stage       Min       1 Stage       Mud Wt       MASP       BOPE         0.1261       519       747       1455       -49       10.50       3935       5M         0.22       28       00       sum of sx       CuFF       Excess       1012       1881         1d &gt; 1.35       32       28       28       1012       1881       22,300       1012       1881         20.00       p 110       dwc/c is+       3.01       1.83       2.18       22,300         w//8.4k/g mud, 30min Src Csg Test psig: 2,660       Totals:       22,300       Totals:       22,300         The cement volume(s) are intended to achieve a top of 11280       114       1832       28       10.50       20         0.1733       1550&lt;</td><td>#/ft       Grade       Coupling       Joint       Collapse       Burst       Length       B@s         32.00       p 110       vam sprint fj       2.03       0.64       1.08       11,480       1         w/8.4#/g mud, 30min Stc Csg Test psig:       Totals:       Totals:       0       11,480       1         Manular       1 Stage       1 Stage       Min       1 Stage       Mul Wit       MASP         0.1261       519       747       1455       -49       10.50       3935       5M         32       28       1012       1881       11280       111280       1881       111280         w/8.4#/g mud, 30min Stc Csg Test psig:       2,660       501       1.83       2.18       2.300       2         w/8.4#/g mud, 30min Stc Csg Test psig:       2,660       Totals:       2,300       2       2       0         w/8.4#/g mud, 30min Stc Csg Test psig:       2,660       Totals:       2,300       2       2       0       2       0       2       0       2       0       2       0       2       0       2       0       2       0       2       0       2       0       2       0       2       0       0</td><td>#/ft         Grade         Coupling         Joint         Collapse         Burst         Length         B@s         a-B           32.00         p 110         vam sprint fj         2.03         0.64         1.08         11,480         1         1         1.82           w/8.4t/g mud, 30min Sfc Csg Test psig:         The cement volume(s) are intended to achieve a top of 0         0         ft from surface or a         875         Red'd         875           Nular         1 Stage         CuFt         % Excess         Drilling         MaXP         BOPE         5M           0.1261         519         747         1455         -49         10.50         3935         5M           32         28         1012         1881         20.0F         1881         20.0F         1881         22.300         2         3.01         1.83         2.18         2.300         2         3.65         0&lt;</td><td>#/ft         Grade         Coupling         Joint         Collapse         Burst         Length         B@s         a-B         a-C           32.00         p 110         vam sprint fj         2.03         0.64         1.08         11.480         1         1.82         1.07           w/8.4#/g mud, 30min Sfc Cag Test psig:         The cement volume(s) are intended to achieve a top of         0         ft from surface or a         875         875           Annular         Chit Sage         1 Stage         Min         1 Stage         100         90         11.480         11.480         11.480           0.1261         519         747         1455         -49         10.05         3935         5M        </td></td>	#/ft       Grade       Coupling       Joint       Collapse       Burst         32.00       p 110       vam sprint fj       2.03       0.64       1.08         w/8.4#/g mud, 30min Sfc Csg Test psig:       Totals:       Totals:       Totals:         Annular       1 Stage       1 Stage       0.64       1.08         Volume       Cmt Sx       CuFt Cmt       Cu Ft       % Excess       Mud Wt       MASP         0.1261       519       747       1455       -49       10.50       3935         0.280       32       28       1012       1012       1012         td > 1.35       5980       3001       1.83       2.18         w/8.4#/g mud, 30min Sfc Csg Test psig:       2,660       Totals:       Collapse       Burst         w/8.4#/g mud, 30min Sfc Csg Test psig:       2,660       Totals:       Totals:         The cement volume(s) are intended to achieve a top of       11280       Totals:       Totals:         Volume       1 Stage       1 Stage       Min       1 Stage       Drilling       Calc         Volume       Cmt Sx       CuFt Cmt       Cu Ft       K Excess       Mud Wt       MASP         1.1733       1550       2446 </td <td>#/ft       Grade       Coupling       Joint       Coillapse       Burst       Length         32.00       p 110       vam sprint fj       2.03       0.64       1.08       11,480         32.00       p 110       vam sprint fj       2.03       0.64       1.08       11,480         wiss.4k/g mud, 30min Src Csg Test psig:       The cement volume(s) are intended to achieve a top of       0       ft from surface or a       875         Annular       1 Stage       Min       1 Stage       Mud Wt       MASP       BOPE         0.1261       519       747       1455       -49       10.50       3935       5M         0.22       28       00       sum of sx       CuFF       Excess       1012       1881         1d &gt; 1.35       32       28       28       1012       1881       22,300       1012       1881         20.00       p 110       dwc/c is+       3.01       1.83       2.18       22,300         w//8.4k/g mud, 30min Src Csg Test psig: 2,660       Totals:       22,300       Totals:       22,300         The cement volume(s) are intended to achieve a top of 11280       114       1832       28       10.50       20         0.1733       1550&lt;</td> <td>#/ft       Grade       Coupling       Joint       Collapse       Burst       Length       B@s         32.00       p 110       vam sprint fj       2.03       0.64       1.08       11,480       1         w/8.4#/g mud, 30min Stc Csg Test psig:       Totals:       Totals:       0       11,480       1         Manular       1 Stage       1 Stage       Min       1 Stage       Mul Wit       MASP         0.1261       519       747       1455       -49       10.50       3935       5M         32       28       1012       1881       11280       111280       1881       111280         w/8.4#/g mud, 30min Stc Csg Test psig:       2,660       501       1.83       2.18       2.300       2         w/8.4#/g mud, 30min Stc Csg Test psig:       2,660       Totals:       2,300       2       2       0         w/8.4#/g mud, 30min Stc Csg Test psig:       2,660       Totals:       2,300       2       2       0       2       0       2       0       2       0       2       0       2       0       2       0       2       0       2       0       2       0       2       0       2       0       0</td> <td>#/ft         Grade         Coupling         Joint         Collapse         Burst         Length         B@s         a-B           32.00         p 110         vam sprint fj         2.03         0.64         1.08         11,480         1         1         1.82           w/8.4t/g mud, 30min Sfc Csg Test psig:         The cement volume(s) are intended to achieve a top of 0         0         ft from surface or a         875         Red'd         875           Nular         1 Stage         CuFt         % Excess         Drilling         MaXP         BOPE         5M           0.1261         519         747         1455         -49         10.50         3935         5M           32         28         1012         1881         20.0F         1881         20.0F         1881         22.300         2         3.01         1.83         2.18         2.300         2         3.65         0&lt;</td> <td>#/ft         Grade         Coupling         Joint         Collapse         Burst         Length         B@s         a-B         a-C           32.00         p 110         vam sprint fj         2.03         0.64         1.08         11.480         1         1.82         1.07           w/8.4#/g mud, 30min Sfc Cag Test psig:         The cement volume(s) are intended to achieve a top of         0         ft from surface or a         875         875           Annular         Chit Sage         1 Stage         Min         1 Stage         100         90         11.480         11.480         11.480           0.1261         519         747         1455         -49         10.05         3935         5M        </td>	#/ft       Grade       Coupling       Joint       Coillapse       Burst       Length         32.00       p 110       vam sprint fj       2.03       0.64       1.08       11,480         32.00       p 110       vam sprint fj       2.03       0.64       1.08       11,480         wiss.4k/g mud, 30min Src Csg Test psig:       The cement volume(s) are intended to achieve a top of       0       ft from surface or a       875         Annular       1 Stage       Min       1 Stage       Mud Wt       MASP       BOPE         0.1261       519       747       1455       -49       10.50       3935       5M         0.22       28       00       sum of sx       CuFF       Excess       1012       1881         1d > 1.35       32       28       28       1012       1881       22,300       1012       1881         20.00       p 110       dwc/c is+       3.01       1.83       2.18       22,300         w//8.4k/g mud, 30min Src Csg Test psig: 2,660       Totals:       22,300       Totals:       22,300         The cement volume(s) are intended to achieve a top of 11280       114       1832       28       10.50       20         0.1733       1550<	#/ft       Grade       Coupling       Joint       Collapse       Burst       Length       B@s         32.00       p 110       vam sprint fj       2.03       0.64       1.08       11,480       1         w/8.4#/g mud, 30min Stc Csg Test psig:       Totals:       Totals:       0       11,480       1         Manular       1 Stage       1 Stage       Min       1 Stage       Mul Wit       MASP         0.1261       519       747       1455       -49       10.50       3935       5M         32       28       1012       1881       11280       111280       1881       111280         w/8.4#/g mud, 30min Stc Csg Test psig:       2,660       501       1.83       2.18       2.300       2         w/8.4#/g mud, 30min Stc Csg Test psig:       2,660       Totals:       2,300       2       2       0         w/8.4#/g mud, 30min Stc Csg Test psig:       2,660       Totals:       2,300       2       2       0       2       0       2       0       2       0       2       0       2       0       2       0       2       0       2       0       2       0       2       0       2       0       0	#/ft         Grade         Coupling         Joint         Collapse         Burst         Length         B@s         a-B           32.00         p 110         vam sprint fj         2.03         0.64         1.08         11,480         1         1         1.82           w/8.4t/g mud, 30min Sfc Csg Test psig:         The cement volume(s) are intended to achieve a top of 0         0         ft from surface or a         875         Red'd         875           Nular         1 Stage         CuFt         % Excess         Drilling         MaXP         BOPE         5M           0.1261         519         747         1455         -49         10.50         3935         5M           32         28         1012         1881         20.0F         1881         20.0F         1881         22.300         2         3.01         1.83         2.18         2.300         2         3.65         0<	#/ft         Grade         Coupling         Joint         Collapse         Burst         Length         B@s         a-B         a-C           32.00         p 110         vam sprint fj         2.03         0.64         1.08         11.480         1         1.82         1.07           w/8.4#/g mud, 30min Sfc Cag Test psig:         The cement volume(s) are intended to achieve a top of         0         ft from surface or a         875         875           Annular         Chit Sage         1 Stage         Min         1 Stage         100         90         11.480         11.480         11.480           0.1261         519         747         1455         -49         10.05         3935         5M

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District I 1625 N. French Dr., Hobbs, NM 88240 Phone:(575) 393-6161 Fax:(575) 393-0720 District II

811 S. First St., Artesia, NM 88210 Phone:(575) 748-1283 Fax:(575) 748-9720

District III

1000 Rio Brazos Rd., Aztec, NM 87410 Phone:(505) 334-6178 Fax:(505) 334-6170 District IV

1220 S. St Francis Dr., Santa Fe, NM 87505 Phone: (505) 476-3470 Fax: (505) 476-3462

# **State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division** 1220 S. St Francis Dr. Santa Fe, NM 87505

CONDITIONS

Operator:	OGRID:
DEVON ENERGY PRODUCTION COMPANY, LP	6137
333 West Sheridan Ave.	Action Number:
Oklahoma City, OK 73102	266269
	Action Type:
	[C-103] NOI Change of Plans (C-103A)

#### CONDITIONS

Created By	Condition	Condition Date
pkautz	IF ON ANY STRING CEMENT DOES NOT CIRCULATE, A RCBL MUST BE RUN ON THAT STRING OF CASING.	10/2/2023

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