eceined by OCP: 9/25/2023 8:34:09	AM State of New Mexico	)	Form C-103 of
Office <u>District I</u> – (575) 393-6161	Energy, Minerals and Natural R	Resources	Revised July 18, 2013
1625 N. French Dr., Hobbs, NM 88240 District II – (575) 748-1283			WELL API NO. 30-025-51942
811 S. First St., Artesia, NM 88210	OIL CONSERVATION DIV	V 15101V	5. Indicate Type of Lease
<u>District III</u> – (505) 334-6178 1000 Rio Brazos Rd., Aztec, NM 87410	1220 South St. Francis	D1.	STATE STEE
<u>District IV</u> – (505) 476-3460 1220 S. St. Francis Dr., Santa Fe, NM	Santa Fe, NM 87505		6. State Oil & Gas Lease No.
87505			319585
	CES AND REPORTS ON WELLS ALS TO DRILL OR TO DEEPEN OR PLUG BA		7. Lease Name or Unit Agreement Name
DIFFERENT RESERVOIR. USE "APPLIC	ALS TO DRILE OR TO DEEL EN OR TEGG BA	CH	Date 14 State Com
PROPOSALS.)  1. Type of Well: Oil Well	Gas Well Other		3. Well Number 301H
2. Name of Operator	Gus Wen Graner		D. OGRID Number 7377
EOG Resources, Inc.			
3. Address of Operator	102		10. Pool name or Wildcat
P.O. Box 2267, Midland, Texas 797	02		5535 Berry; Bone Spring, North
4. Well Location	220 6 4 6 4 6 4	1: 1 2249	
Unit Letter_O:_ Section 14	feet from the South Township 33E		feet from the Eastline  Lea County
Section 14	11. Elevation (Show whether DR, RKE	Range	Lea County
	3790' GR	, iti, dit, e.e.,	
	PLUG AND ABANDON	MEDIAL WORK MMENCE DRILL SING/CEMENT J HER: nent details, and g	OB
proposed completion or reconstruction of reconstruction of reconstruction of the following changes:  Please update the SHL & casin	mendment to our approved APD	for this well t	o reflect
Spud Date:	7		
I hereby certify that the information a	above is true and complete to the best of	my knowledge a	and belief.
SIGNATURE	TITLE_Sr Regulato	ory Specialist	DATE_9/25/2023
Type or print name Star Harrell For State Use Only	E-mail address: star_harrell@eog	resources.com	PHONE: 432-848-9161
APPROVED BY:	TITLE		DATE
Conditions of Approval (if any):			

DISTRICT I

1625 N. French Dr., Hobbs, NM 88240

Phone: (575) 393-4016 I Fax: (575) 393-0720

DISTRICT II

81 I. S. First St., Artesia, NM 88210

Phone: (575) 748-1238 Fax: (575) 748-9720

DISTRICT III

1000 Rio Brazos Rd., Aztec, NM 87410

Phone: (505) 343-6178 Fax: (505) 334-6170

DISTRICT IV

640.00

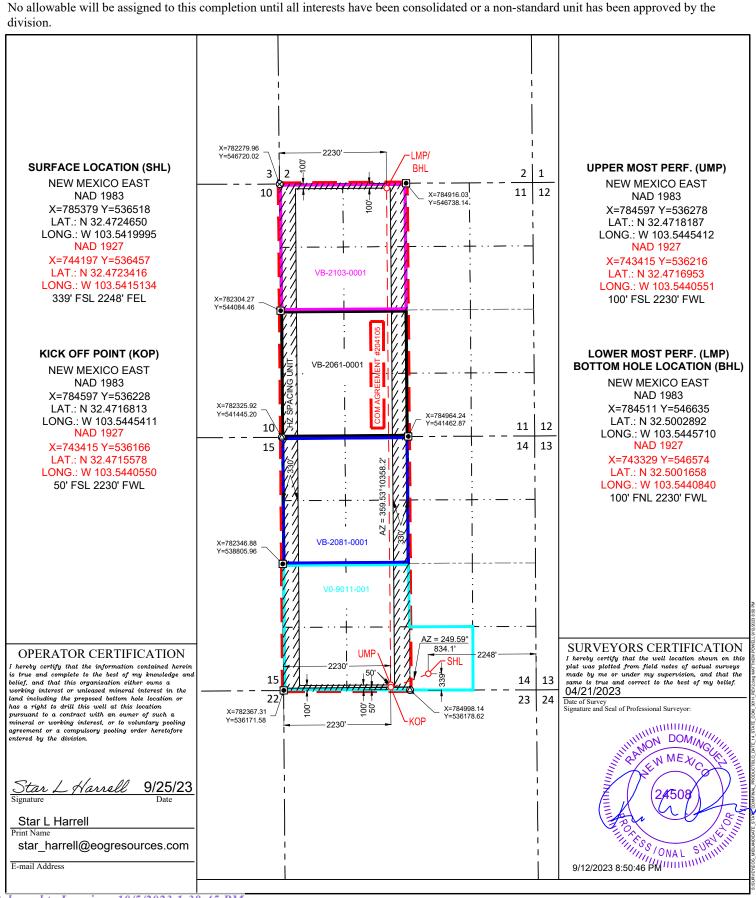
# State of New Mexico Energy, Minerals & Natural Resources Department OIL CONSERVATION DIVISION 1220 South St. Francis Dr. Santa Fe, New Mexico 87505

Form C-102
Revised August 1, 2011
Submit one copy to appropriate
District Office

☐ AMENDED REPORT

	PI Number <b>0-025-51</b> !	942		Pool Code <b>5535</b>		Berry;	Pool Name Bone Spring	, North		
Property C				D	Property Name ATE 14 STATE	E COM		Well Number 301H		
	OGRID No. <b>7377</b>			Operator Name Elevation EOG RESOURCES, INC. 3790'						
					Surface Locati	ion				
UL or lot no.	Section	Township	Range	Lot Idn	Feet from the	North/South line	Feet from the	East/West line	County	
0	14	21-S 33-E - 339' SOUTH 2248'		2248'	EAST	LEA				
			Bott	om Hole I	Location If Diffe	erent From Surfac	e			
UL or lot no.	Section	Township	ownship Range Lot Idn Feet from the North/South line Feet from the						County	
С	11	21-S	33-E - 100' NORTH 2230'						LEA	

COM AGREEMENT #204105



Date 14 State Com #301H Lea County, New Mexico **Proposed Wellbore** 

Design A

KB: 3815' GL: 3790'

2248' FEL **Section 14** T-21-S, R-33-E

339' FSL

API: 30-025-\*\*\*\*

Bit Size: 17-1/2" 13-3/8", 54.5#, J-55, STC @ 0' - 2,040' Bit Size: 12-1/4" 9-5/8", 40.#, J-55, LTC @ 0' - 4000' 9-5/8", 40.#, HCK-55, LTC @ 4,000' - 5,190' Bit Size: 8-3/4" Bit Size: 6-3/4" 5-1/2", 17.#, HCP-110, LTC 5-1/2", 17.#, HCP-110, LTC @ 0' - 9,760' @ 9,760' - 20,432' KOP: 9,752' MD, 9,674' TVD

> Lateral: 20,432' MD, 10,151' TVD BH Location: 100' FNL & 2230' FWL Sec. 11 T-21-S R-33-E

EOC: 10,502' MD, 10,151' TVD

Date 14 State Com #301H Lea County, New Mexico Proposed Wellbore

339' FSL 2248' FEL Section 14 T-21-S, R-33-E

Design B GL: 3790'

KB: 3815'

API: 30-025-\*\*\*\*

Bit Size: 17-1/2" 13-3/8", 54.5#, J-55, STC @ 0' - 2,040' Bit Size: 12-1/4" 9-5/8", 40.#, J-55, LTC @ 0' - 4,000' 9-5/8", 40.#, HCK-55, LTC @ 4,000' - 5,190' Bit Size: 8-3/4" Bit Size: 6-3/4" 6", 22.3#, P110-EC, LTC 6", 22.3#, P110-EC, LTC @ 0' - 9,760' @ 9,760' - 20,432' KOP: 9,752' MD, 9,674' TVD

> Lateral: 20,432' MD, 10,151' TVD BH Location: 100' FNL & 2230' FWL Sec. 11 T-21-S R-33-E

EOC: 10,502' MD, 10,151' TVD



#### Date 14 State Com #301H

#### **Permit Information:**

Location:

SHL: 339' FSL & 2248' FEL, Section 14, T-21-S, R-33-E, Lea Co., N.M. BHL: 100' FNL & 2230' FWL, Section 11, T-21-S, R-33-E, Lea Co., N.M.

#### **Design A**

#### **Casing Program:**

Hole	Interv	al MD	Interval TVD		Csg			
Size	From (ft)	To (ft)	From (ft)	To (ft)	OD	Weight	Grade	Conn
17-1/2"	0	2,040	0	2,040	13-3/8"	54.5#	J-55	STC
12-1/4"	0	4,084	0	4,000	9-5/8"	40#	J-55	LTC
12-1/4"	4,084	5,274	4,000	5,190	9-5/8"	40#	HCK-55	LTC
8-3/4"	0	9,752	0	9,674	5-1/2"	17#	HCP-110	LTC
6-3/4"	9,752	20,432	9,674	10,151	5-1/2"	17#	HCP-110	LTC

**Cement Program:** 

	No.	Wt.	Yld	Shuman Description					
Depth	Sacks	ppg	Ft3/sk	Slurry Description					
2,040'	870	13.5	1.73	Lead: Class C + 4.0% Bentonite + 0.6% CD-32 + 0.5% CaCl2 + 0.25 lb/sk Cello-Flake (TOC @ surface)					
2,040	230 14.8		1.34	Tail: Class C + 0.6% FL-62 + 0.25 lb/sk Cello-Flake + 0.2% Sodium Metasilicate					
	210	12.7	2.22	1st Stage Lead: Class 'C' + 2.00% SMS + 10.00% Salt + 1.10% R-3 + 0.005 pps Static Free + 0.25 pps Cello Flake					
5,270' Stage	200	14.8	1.33	1st Stage Tail: Class 'C' + 0.60% FL-62 + 0.45% CD-32 + 0.15% SMS + 0.30% R-3					
Tool @ 4,100'	ool @ 675 12.7 2.22		2.22	2nd Stage Lead: Class 'C' + 2.00% SMS + 10.0% Salt + 0.65% R-3 + 0.25 pps Cello Flake + 0.005 pps Static Free					
	175	14.8	1.32	2nd Stage Tail: Classs 'C' + 0.60% FL-62 + 0.45% CD-32 + 0.15% SMS + 0.15% R-3 + 0.005 pps Static Free					
20.4221	980	10.5	3.21	Lead: 60:40:0 Class 'C' + 15.00 lb/sk BA-90 + 4.00% MPA-5 + 3.00% SMS + 5.00% A-10 + 1.00% BA-10A + 0.80% ASA-301 + 2.90% R-21 + 8.00 lb/sk LCM-1 + 0.005 lb/sk Static Free					
20,432'	1670	13.2	1.52	Tail: 50:50:2 Class 'H' + 0.65% FL-52 + 0.20% CD-32 + 0.15% SMS + 2.00% Salt + 0.10% R-3 + 0.005 lb/sk Static Free (TOC @ 9,752')					

Mud Program:

Depth	Туре	Veight (pp	Viscosity	Water Loss
0 – 2,040'	Fresh - Gel	8.6-8.8	28-34	N/c
2,040' – 5,190'	Saturated Brine	10.0-10.2	28-34	N/c
5,190' – 20,432' Lateral	Oil Base	8.8-9.5	58-68	N/c



#### Date 14 State Com #301H

#### **Design B**

#### **Casing Program:**

Hole	Interv	al MD	Interval TVD		Csg			
Size	From (ft)	To (ft)	From (ft)	To (ft)	OD	Weight	Grade	Conn
17-1/2"	0	2,040	0	2,040	13-3/8"	54.5#	J-55	STC
12-1/4"	0	4,084	0	4,000	9-5/8"	40#	J-55	LTC
12-1/4"	4,084	5,274	4,000	5,190	9-5/8"	40#	HCK-55	LTC
8-3/4"	0	9,752	0	9,674	6"	22.3#	P110-EC	DWC/C IS
7-7/8"	9,752	20,432	9,674	10,151	6"	22.3#	P110-EC	DWC/C IS

**Cement Program:** 

	No.	Wt.	Yld	Classes Described and
Depth	Sacks	ppg	Ft3/sk	Slurry Description
2,040'	870	13.5	1.73	Lead: Class C + 4.0% Bentonite + 0.6% CD-32 + 0.5% CaCl2 + 0.25 lb/sk Cello-Flake (TOC @ surface)
2,040	230	14.8	1.34	Tail: Class C + 0.6% FL-62 + 0.25 lb/sk Cello-Flake + 0.2% Sodium Metasilicate
	210	12.7	2.22	1st Stage Lead: Class 'C' + 2.00% SMS + 10.00% Salt + 1.10% R-3 + 0.005 pps Static Free + 0.25 pps Cello Flake
5,270' 200 14.8		1.33	1st Stage Tail: Class 'C' + 0.60% FL-62 + 0.45% CD-32 + 0.15% SMS + 0.30% R-3	
@ 4,100'	ge Tool 4,100' 675 12.7		2.22	2nd Stage Lead: Class 'C' + 2.00% SMS + 10.0% Salt + 0.65% R-3 + 0.25 pps Cello Flake + 0.005 pps Static Free
	175	14.8	1.32	2nd Stage Tail: Classs 'C' + 0.60% FL-62 + 0.45% CD-32 + 0.15% SMS + 0.15% R-3 + 0.005 pps Static Free
20.4221	860	10.5	3.21	Lead: 60:40:0 Class 'C' + 15.00 lb/sk BA-90 + 4.00% MPA-5 + 3.00% SMS + 5.00% A-10 + 1.00% BA-10A + 0.80% ASA-301 + 2.90% R-21 + 8.00 lb/sk LCM-1 + 0.005 lb/sk Static Free
20,432'	1250	13.2	1.52	Tail: 50:50:2 Class 'H' + 0.65% FL-52 + 0.20% CD-32 + 0.15% SMS + 2.00% Salt + 0.10% R-3 + 0.005 lb/sk Static Free (TOC @ 9,752')

Mud Program:

Depth	Туре	eight (pp	Viscosity	Water Loss
0 – 2,040'	Fresh - Gel	8.6-8.8	28-34	N/c
2,040' – 5,190'	Saturated Brine	10.0-10.2	28-34	N/c
5,190' – 20,432' Lateral	Oil Base	8.8-9.5	58-68	N/c



#### Date 14 State Com 301H

#### **Tubing Requirements**

EOG respectively requests an exception to the following NMOCD rule:

• 19.15.16.10 Casing AND TUBING RQUIREMENTS: J (3): "The operator shall set tubing as near the bottom as practical and tubing perforations shall not be more than 250 feet above top of pay zone."

With horizontal flowing and gas lifted wells an end of tubing depth placed at or slightly above KOP is a conservative way to ensure the tubing stays clean from debris, plugging, and allows for fewer well interventions post offset completion. The deeper the tubulars are run into the curve, the higher the probability is that the tubing will become stuck in sand and or well debris as the well produces over time. An additional consideration for EOT placement during artificial lift installations is avoiding the high dog leg severity and inclinations found in the curve section of the wellbore to help improve reliability and performance. Dog leg severity and inclinations tend not to hamper gas lifted or flowing wells, but they do effect other forms of artificial lift like rod pump or ESP (electric submersible pump). Keeping the EOT above KOP is an industry best practice for those respective forms of artificial lift.

#### **Special Requirements**

- (A) The surface hole will be drilled without interruption through the fresh water zone(s) and surface casing will be set at  $\pm 2040$ ° to protect subject water sands.
- (B) Oil based drilling fluid will not be utilized until the intermediate casing is set and cemented.
- (C) Cement shall be circulated on all three casing strings.
- (D) A radial cement bond log will be run and submitted to the OCD prior to drilling out of the intermediate casing shoe.
- (E) EOG will evaluate the CBL to determine the quality of cement behind the intermediate casing string, prior to drilling out of the intermediate casing shoe. The CBL must provide verification that there is good cement coverage and strata isolation behind the intermediate casing, including both above and below the Capitan Reef formation.
- (F) The subject CBL evaluation, by EOG, will be submitted to the OCD prior to drilling out of the IC shoe. Any required remediation will be discussed and approved by the OCD. Any required remedial cementing will be done prior to drilling out the IC shoe.
- (G) Since this well is in the Potash Area R111P requires that cement on all 3 strings of casing to circulate to surface.
- (H) If on any casing string cement does not circulate to surface, a radial CBL will be run.



#### Date 14 State Com #301H

#### Hydrogen Sulfide Plan Summary

- A. All personnel shall receive proper H2S training in accordance with Onshore Order III.C.3.a.
- B. Briefing Area: two perpendicular areas will be designated by signs and readily accessible.
- C. Required Emergency Equipment:
  - Well control equipment
  - a. Flare line 150' from wellhead to be ignited by flare gun.
  - b. Choke manifold with a remotely operated choke.
  - c. Mud/gas separator
  - Protective equipment for essential personnel.

#### Breathing apparatus:

- a. Rescue Packs (SCBA) 1 unit shall be placed at each breathing area, 2 shall be stored in the safety trailer.
- b. Work/Escape packs —4 packs shall be stored on the rig floor with sufficient air hose not to restrict work activity.
- c. Emergency Escape Packs —4 packs shall be stored in the doghouse for emergency evacuation.

#### Auxiliary Rescue Equipment:

- a. Stretcher
- b. Two OSHA full body harness
- c. 100 ft 5/8 inch OSHA approved rope
- d. 1-20# class ABC fire extinguisher
- H2S detection and monitoring equipment:

The stationary detector with three sensors will be placed in the upper dog house if equipped, set to visually alarm @ 10 ppm and audible @ 14 ppm. Calibrate a minimum of every 30 days or as needed. The sensors will be placed in the following places: Rig floor / Bell nipple / End of flow line or where well bore fluid is being discharged.

(Gas sample tubes will be stored in the safety trailer)

- Visual warning systems.
  - a. One color code condition sign will be placed at the entrance to the site reflecting the possible conditions at the site.
  - b. A colored condition flag will be on display, reflecting the current condition at the site at the time.
  - c. Two wind socks will be placed in strategic locations, visible from all angles.



#### Date 14 State Com #301H

#### ■ Mud program:

The mud program has been designed to minimize the volume of H2S circulated to surface. The operator will have the necessary mud products to minimize hazards while drilling in H2S bearing zones.

#### ■ Metallurgy:

All drill strings, casings, tubing, wellhead, blowout preventer, drilling spool, kill lines, choke manifold and lines, and valves shall be suitable for H2S service.

#### ■ Communication:

Communication will be via cell phones and land lines where available.



#### Date 14 State Com #301H Emergency Assistance Telephone List

PUBLIC SAFETY:	1	911 o
Lea County Sheriff's Department		(575) 396-3611
Rod Coffman		
Fire Department:		
Carlsbad		(575) 885-3125
Artesia		(575) 746-5050
Hospitals:		
Carlsbad		(575) 887-4121
Artesia		(575) 748-3333
Hobbs		(575) 392-1979
Dept. of Public Safety/Carlsbad		(575) 748-9718
Highway Department		(575) 885-3281
New Mexico Oil Conservation		(575) 476-3440
NMOCD Inspection Group - South		(575) 626-0830
U.S. Dept. of Labor		(575) 887-1174
EOG Resources, Inc.		, ,
EOG / Midland	Office	(432) 686-3600
		, ,
Company Drilling Consultants:		
David Dominque	Cell	(985) 518-5839
Mike Vann	Cell	(817) 980-5507
Drilling Engineer		
Drilling Engineer Stephen Davis	Cell	(432) 235-9789
Matt Day	Cell	(432) 296-4456
Drilling Manager	CCII	(432) 270-4430
Branden Keener	Office	(432) 686-3752
Branden Recher	Cell	(210) 294-3729
Duilling Cunovintendent	Cell	(210) 294-3729
<b>Drilling Superintendent</b> Steve Kelly	Office	(432) 686-3706
Sieve Keny	Cell	(210) 416-7894
H & D Duilling	Cell	(210) 410-7894
H&P Drilling	Office	(422) 562 5757
H&P Drilling H&P 651 Drilling Dig		(432) 563-5757
H&P 651 Drilling Rig	Rig	(903) 509-7131
Tool Pusher:		
Johnathan Craig	Cell	(817) 760-6374
Brad Garrett		
Safety:		
Brian Chandler (HSE Manager)	Office	(432) 686-3695
	Cell	(817) 239-0251



#### **Midland**

Lea County, NM (NAD 83 NME)
Date 14 State Com
#301H

OH

Plan: Plan #0.1

### **Standard Planning Report**

19 September, 2023



Database: PEDM Midlan

Company: Midland
Project: Lea County, NM (NAD 83 NME)

Site: Date 14 State Com

 Well:
 #301H

 Wellbore:
 OH

 Design:
 Plan #0.1

Local Co-ordinate Reference:

TVD Reference:
MD Reference:
North Reference:

**Survey Calculation Method:** 

Well #301H

kb=25' @ 3815.0usft kb=25' @ 3815.0usft

Grid

Minimum Curvature

Project Lea County, NM (NAD 83 NME)

Map System: US State Plane 1983
Geo Datum: North American Datum 1983
Map Zone: New Mexico Eastern Zone

System Datum:

Mean Sea Level

Site Date 14 State Com

 Site Position:
 Northing:
 536,428.00 usft
 Latitude:
 32° 28' 19.914 N

 From:
 Map
 Easting:
 786,265.00 usft
 Longitude:
 103° 32' 20.860 W

Position Uncertainty: 0.0 usft Slot Radius: 13-3/16 "

Well #301H

0.0 usft **Well Position** +N/-S Northing: 536,518.00 usft Latitude: 32° 28' 20.869 N +E/-W 0.0 usft Easting: 785,379.00 usft Longitude: 103° 32' 31.194 W **Position Uncertainty** 0.0 usft Wellhead Elevation: usft **Ground Level:** 3,790.0 usft

Grid Convergence: 0.42  $^{\circ}$ 

Wellbore OH

 Magnetics
 Model Name
 Sample Date
 Declination (°)
 Dip Angle (°)
 Field Strength (nT)

 IGRF2020
 9/19/2023
 6.28
 60.05
 47,405.02684522

Design Plan #0.1

Audit Notes:

Version:Phase:PLANTie On Depth:0.0

 Vertical Section:
 Depth From (TVD) (usft)
 +N/-S +E/-W (usft)
 Direction (usft)

 0.0
 0.0
 0.0
 355.10

Plan Survey Tool Program Date 9/19/2023

Depth From Depth To

(usft) (usft) Survey (Wellbore) Tool Name Remarks

1 0.0 20,432.1 Plan #0.1 (OH) EOG MWD+IFR1

MWD + IFR1



Database: PEDM Company: Midland

Project: Lea County, NM (NAD 83 NME)

Site: Date 14 State Com

 Well:
 #301H

 Wellbore:
 OH

 Design:
 Plan #0.1

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Well #301H

kb=25' @ 3815.0usft kb=25' @ 3815.0usft

Grid

Plan Sections										
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)	TFO (°)	Target
0.0	0.00	0.00	0.0	0.0	0.0	0.00	0.00	0.00	0.00	
2,343.0	0.00	0.00	2,343.0	0.0	0.0	0.00	0.00	0.00	0.00	
2,906.9	11.28	249.65	2,903.3	-19.2	-51.9	2.00	2.00	0.00	249.65	
6,605.8	11.28	249.65	6,530.7	-270.8	-730.1	0.00	0.00	0.00	0.00	
7,169.7	0.00	0.00	7,091.0	-290.0	-782.0	2.00	-2.00	0.00	180.00	
9,752.2	0.00	0.00	9,673.5	-290.0	-782.0	0.00	0.00	0.00	0.00	KOP(Date 14 State C
9,972.6	26.46	0.00	9,886.2	-240.0	-782.0	12.00	12.00	0.00	0.00	FTP(Date 14 State Co
10,502.2	90.00	359.52	10,150.9	187.5	-784.5	12.00	12.00	-0.09	-0.54	
20,432.1	90.00	359.52	10,151.0	10,117.0	-868.0	0.00	0.00	0.00	0.00	PBHL(Date 14 State (

## eog resources

#### **Planning Report**

Database: PEDM Company: Midland

Project: Lea County, NM (NAD 83 NME)

Site: Date 14 State Com

 Well:
 #301H

 Wellbore:
 OH

 Design:
 Plan #0.1

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

**Survey Calculation Method:** 

Well #301H

kb=25' @ 3815.0usft kb=25' @ 3815.0usft

Grid

Design:	Plan #0.1								
Planned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
0.0	0.00	0.00	0.0	0.0	0.0	0.0	0.00	0.00	0.00
100.0	0.00	0.00	100.0	0.0	0.0	0.0	0.00	0.00	0.00
200.0	0.00	0.00	200.0	0.0	0.0	0.0	0.00	0.00	0.00
300.0	0.00	0.00	300.0	0.0	0.0	0.0	0.00	0.00	0.00
400.0	0.00	0.00	400.0	0.0	0.0	0.0	0.00	0.00	0.00
500.0	0.00	0.00	500.0	0.0	0.0	0.0	0.00	0.00	0.00
600.0	0.00	0.00	600.0	0.0	0.0	0.0	0.00	0.00	0.00
700.0	0.00	0.00	700.0	0.0	0.0	0.0	0.00	0.00	0.00
800.0	0.00	0.00	800.0	0.0	0.0	0.0	0.00	0.00	0.00
900.0	0.00	0.00	900.0	0.0	0.0	0.0	0.00	0.00	0.00
1,000.0	0.00	0.00	1,000.0	0.0	0.0	0.0	0.00	0.00	0.00
1,100.0	0.00	0.00	1,100.0	0.0	0.0	0.0	0.00	0.00	0.00
1,200.0	0.00	0.00	1,200.0	0.0	0.0	0.0	0.00	0.00	0.00
1,300.0	0.00	0.00	1,300.0	0.0	0.0	0.0	0.00	0.00	0.00
1,400.0	0.00	0.00	1,400.0	0.0	0.0	0.0	0.00	0.00	0.00
1,500.0	0.00	0.00	1,500.0	0.0	0.0	0.0	0.00	0.00	0.00
1,600.0	0.00	0.00	1,600.0	0.0	0.0	0.0	0.00	0.00	0.00
1,700.0	0.00	0.00	1,700.0	0.0	0.0	0.0	0.00	0.00	0.00
1,800.0	0.00	0.00	1,800.0	0.0	0.0	0.0	0.00	0.00	0.00
1,900.0	0.00	0.00	1,900.0	0.0	0.0	0.0	0.00	0.00	0.00
2,000.0	0.00	0.00	2,000.0	0.0	0.0	0.0	0.00	0.00	0.00
2,100.0	0.00	0.00	2,100.0	0.0	0.0	0.0	0.00	0.00	0.00
2,200.0	0.00	0.00	2,200.0	0.0	0.0	0.0	0.00	0.00	0.00
2,300.0	0.00	0.00	2,300.0	0.0	0.0	0.0	0.00	0.00	0.00
2,343.0	0.00	0.00	2,343.0	0.0	0.0	0.0	0.00	0.00	0.00
2,400.0	1.14	249.65	2,400.0	-0.2	-0.5	-0.2	2.00	2.00	0.00
2,500.0	3.14	249.65	2,499.9	-1.5	-4.0	-1.1	2.00	2.00	0.00
2,600.0	5.14	249.65	2,599.7	-4.0	-10.8	-3.1	2.00	2.00	0.00
2,700.0	7.14	249.65	2,699.1	-7.7	-20.8	-5.9	2.00	2.00	0.00
2,800.0	9.14	249.65	2,798.1	-12.6	-34.1	-9.7	2.00	2.00	0.00
2,906.9	11.28	249.65	2,903.3	-19.2	-51.9	-14.7	2.00	2.00	0.00
3,000.0	11.28	249.65	2,994.6	-25.6	-68.9	-19.6	0.00	0.00	0.00
3,100.0	11.28	249.65	3,092.6	-32.4	-87.3	-24.8	0.00	0.00	0.00
3,200.0	11.28	249.65	3,190.7	-39.2	-105.6	-30.0	0.00	0.00	0.00
3,300.0	11.28	249.65	3,288.8	-46.0	-124.0	-35.2	0.00	0.00	0.00
3,400.0	11.28	249.65	3,386.8	-52.8	-142.3	-40.4	0.00	0.00	0.00
3,500.0	11.28	249.65	3,484.9	-59.6	-160.6	-45.6	0.00	0.00	0.00
3,600.0	11.28	249.65	3,583.0	-66.4	-179.0	-50.8	0.00	0.00	0.00
3,700.0	11.28	249.65	3,681.1	-73.2	-197.3	-56.0	0.00	0.00	0.00
3,800.0	11.28	249.65	3,779.1	-80.0	-215.6	-61.2	0.00	0.00	0.00
3,900.0	11.28	249.65	3,877.2	-86.8	-234.0	-66.4	0.00	0.00	0.00
4,000.0	11.28	249.65	3,975.3	-93.6	-252.3	-71.7	0.00	0.00	0.00
4,100.0	11.28	249.65	4,073.3	-100.4	-270.6	-76.9	0.00	0.00	0.00
4,200.0	11.28	249.65	4,171.4	-107.2	-289.0	-82.1	0.00	0.00	0.00
4,300.0	11.28	249.65	4,269.5	-114.0	-307.3	-87.3	0.00	0.00	0.00
4,400.0	11.28	249.65	4,367.5	-120.8	-325.7	-92.5	0.00	0.00	0.00
4,500.0	11.28	249.65	4,465.6	-127.6	-344.0	-97.7	0.00	0.00	0.00
4,600.0	11.28	249.65	4,563.7	-134.4	-362.3	-102.9	0.00	0.00	0.00
4,700.0	11.28	249.65	4,661.7	-141.2	-380.7	-108.1	0.00	0.00	0.00
4,800.0	11.28	249.65	4,759.8	-148.0	-399.0	-113.3	0.00	0.00	0.00
4,900.0	11.28	249.65	4,857.9	-154.8	-417.3	-118.5	0.00	0.00	0.00
5,000.0	11.28	249.65	4,955.9	-161.6	-435.7	-123.7	0.00	0.00	0.00
5,100.0	11.28	249.65	5,054.0	-168.4	-454.0	-128.9	0.00	0.00	0.00
5,200.0	11.28	249.65	5,152.1	-175.2	-472.4	-134.2	0.00	0.00	0.00



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**Survey Calculation Method:** 

Well #301H

kb=25' @ 3815.0usft kb=25' @ 3815.0usft

Grid

Planned Survey									
Measured			Vertical			Vertical	Dogleg	Build	Turn
Depth	Inclination	Azimuth	Depth	+N/-S	+E/-W	Section	Rate	Rate	Rate
(usft)	(°)	(°)	(usft)	(usft)	(usft)	(usft)	(°/100usft)	(°/100usft)	(°/100usft)
5,300.0	11.28	249.65	5,250.2	-182.0	-490.7	-139.4	0.00	0.00	0.00
5,400.0	11.28	249.65	5,348.2	-188.8	-509.0	-144.6	0.00	0.00	0.00
5,500.0	11.28	249.65	5,446.3	-195.6	-527.4	-149.8	0.00	0.00	0.00
5,600.0	11.28	249.65	5,544.4	-202.4	-545.7	-155.0	0.00	0.00	0.00
5,700.0	11.28	249.65	5,642.4	-209.2	-564.0	-160.2	0.00	0.00	0.00
5,800.0	11.28	249.65	5,740.5	-216.0	-582.4	-165.4	0.00	0.00	0.00
5,900.0	11.28	249.65	5,838.6	-222.8	-600.7	-170.6	0.00	0.00	0.00
6,000.0	11.28	249.65	5,936.6	-229.6	-619.0	-175.8	0.00	0.00	0.00
6,100.0	11.28	249.65	6,034.7	-236.4	-637.4	-181.0	0.00	0.00	0.00
6,200.0	11.28	249.65	6,132.8	-243.2	-655.7	-186.2	0.00	0.00	0.00
6,300.0	11.28	249.65	6,230.8	-250.0	-674.1	-191.4	0.00	0.00	0.00
6,400.0	11.28	249.65	6,328.9	-256.8	-692.4	-196.6	0.00	0.00	0.00
6,500.0	11.28	249.65	6,427.0	-263.6	-710.7	-201.9	0.00	0.00	0.00
6,605.8	11.28	249.65	6,530.7	-270.8	-730.1	-207.4	0.00	0.00	0.00
6,700.0	9.39	249.65	6,623.4	-276.6	-746.0	-211.9	2.00	-2.00	0.00
6,800.0	7.39	249.65	6,722.3	-281.7	-759.7	-215.7	2.00	-2.00	0.00
6,900.0	5.39	249.65	6,821.7	-285.6	-770.1	-218.7	2.00	-2.00	0.00
7,000.0	3.39	249.65	6,921.4	-288.3	-770.1 -777.3	-210.7 -220.8	2.00	-2.00 -2.00	0.00
			6,921.4 7,021.3	-288.3 -289.7	-771.3 -781.2	-220.8 -221.9		-2.00 -2.00	
7,100.0	1.39	249.65					2.00		0.00
7,169.7	0.00	0.00	7,091.0	-290.0	-782.0	-222.1	2.00	-2.00	0.00
7,200.0	0.00	0.00	7,121.3	-290.0	-782.0	-222.1	0.00	0.00	0.00
7,300.0	0.00	0.00	7,221.3	-290.0	-782.0	-222.1	0.00	0.00	0.00
7,400.0	0.00	0.00	7,321.3	-290.0	-782.0	-222.1	0.00	0.00	0.00
7,500.0	0.00	0.00	7,421.3	-290.0	-782.0	-222.1	0.00	0.00	0.00
7,600.0	0.00	0.00	7,521.3	-290.0	-782.0	-222.1	0.00	0.00	0.00
7,700.0	0.00	0.00	7,621.3	-290.0	-782.0	-222.1	0.00	0.00	0.00
7,800.0	0.00	0.00	7,721.3	-290.0	-782.0	-222.1	0.00	0.00	0.00
7,900.0	0.00	0.00	7,821.3	-290.0	-782.0	-222.1	0.00	0.00	0.00
8,000.0	0.00	0.00	7,921.3	-290.0	-782.0	-222.1	0.00	0.00	0.00
8,100.0	0.00	0.00	8,021.3	-290.0	-782.0	-222.1	0.00	0.00	0.00
8,200.0	0.00	0.00	8,121.3	-290.0	-782.0	-222.1	0.00	0.00	0.00
8,300.0	0.00	0.00	8,221.3	-290.0	-782.0	-222.1	0.00	0.00	0.00
8,400.0	0.00	0.00	8,321.3	-290.0	-782.0	-222.1	0.00	0.00	0.00
8,500.0	0.00	0.00	8,421.3	-290.0	-782.0	-222.1	0.00	0.00	0.00
8,600.0	0.00	0.00	8,521.3	-290.0	-782.0	-222.1	0.00	0.00	0.00
8,700.0	0.00	0.00	8,621.3	-290.0 -290.0	-782.0 -782.0	-222.1 -222.1	0.00	0.00	0.00
8,800.0	0.00	0.00	8,721.3	-290.0	-782.0	-222.1	0.00	0.00	0.00
8,900.0	0.00	0.00	8,821.3	-290.0	-782.0	-222.1	0.00	0.00	0.00
9,000.0	0.00	0.00	8,921.3	-290.0	-782.0	-222.1	0.00	0.00	0.00
9,100.0	0.00	0.00	9,021.3	-290.0	-782.0	-222.1	0.00	0.00	0.00
9,200.0	0.00	0.00	9,121.3	-290.0	-782.0	-222.1	0.00	0.00	0.00
9,300.0	0.00	0.00	9,221.3	-290.0	-782.0	-222.1	0.00	0.00	0.00
9,400.0	0.00	0.00	9,321.3	-290.0	-782.0	-222.1	0.00	0.00	0.00
9,500.0	0.00	0.00	9,421.3	-290.0	-782.0	-222.1	0.00	0.00	0.00
9,600.0	0.00	0.00	9,521.3	-290.0	-782.0	-222.1	0.00	0.00	0.00
9,700.0	0.00	0.00	9,621.3	-290.0	-782.0	-222.1	0.00	0.00	0.00
9,752.2	0.00	0.00	9,673.5	-290.0	-782.0	-222.1	0.00	0.00	0.00
·			3,013.3	-230.0	-102.0	-222.1	0.00	0.00	0.00
NUPILIATE 14	State Com #30* 2.74	1 <b>H)</b> 0.00	0.000.0	200 5	700.0	204.5	40.00	40.00	0.00
•		0.00	9,696.3	-289.5	-782.0	-221.5	12.00	12.00	0.00
9,775.0				007.0	700.0	040 7			
9,775.0 9,800.0	5.74	0.00	9,721.2	-287.6	-782.0	-219.7	12.00	12.00	0.00
9,775.0 9,800.0 9,825.0	5.74 8.74	0.00 0.00	9,721.2 9,746.0	-284.5	-782.0	-216.6	12.00	12.00	0.00
9,775.0 9,800.0	5.74	0.00	9,721.2						



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Well #301H

kb=25' @ 3815.0usft kb=25' @ 3815.0usft

Grid

anned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
9,900.0		0.00	9,819.0	-267.3	-782.0	-199.5	12.00	12.00	0.00
9,925.0		0.00	9,842.6	-259.1	-782.0	-191.3	12.00	12.00	0.00
9,950.0		0.00	9,865.7	-249.6	-782.0	-181.8	12.00	12.00	0.00
9,972.6	26.46 14 State Com #301	0.00	9,886.2	-240.0	-782.0	-172.3	12.00	12.00	0.00
·		•							
9,975.0		359.99	9,888.3	-238.9	-782.0	-171.2	12.00	12.00	-0.25
10,000.0		359.94	9,910.3	-227.1	-782.0	-159.4	12.00	12.00	-0.22
10,025.0		359.89	9,931.7	-214.2	-782.0	-146.5	12.00	12.00	-0.19
10,050.0		359.85	9,952.4	-200.1	-782.1	-132.5	12.00	12.00	-0.16
10,075.0	38.74	359.82	9,972.3	-185.0	-782.1	-117.4	12.00	12.00	-0.14
10,100.0		359.79	9,991.3	-168.8	-782.2	-101.3	12.00	12.00	-0.12
10,125.0		359.76	10,009.6	-151.7	-782.2	-84.3	12.00	12.00	-0.11
10,150.0		359.74	10,026.8	-133.6	-782.3	-66.3	12.00	12.00	-0.10
10,175.0		359.71	10,043.2	-114.7	-782.4	-47.4	12.00	12.00	-0.09
10,200.0	53.74	359.69	10,058.5	-94.9	-782.5	-27.7	12.00	12.00	-0.08
10,225.0		359.68	10,072.7	-74.4	-782.6	-7.2	12.00	12.00	-0.07
10,250.0	59.74	359.66	10,085.9	-53.2	-782.7	13.9	12.00	12.00	-0.07
10,275.0	62.74	359.64	10,097.9	-31.2	-782.9	35.8	12.00	12.00	-0.07
10,300.0	65.74	359.63	10,108.8	-8.7	-783.0	58.2	12.00	12.00	-0.06
10,325.0	68.74	359.61	10,118.4	14.3	-783.2	81.2	12.00	12.00	-0.06
10,350.0	71.74	359.60	10,126.9	37.8	-783.3	104.7	12.00	12.00	-0.06
10,375.0		359.58	10,134.1	61.8	-783.5	128.5	12.00	12.00	-0.05
10,400.0		359.57	10,140.1	86.1	-783.7	152.7	12.00	12.00	-0.05
10,425.0		359.56	10,144.7	110.6	-783.9	177.2	12.00	12.00	-0.05
10,450.0		359.54	10,148.1	135.4	-784.1	201.9	12.00	12.00	-0.05
10,475.0	86.74	359.53	10,150.2	160.3	-784.3	226.7	12.00	12.00	-0.05
10,502.2		359.52	10,150.9	187.5	-784.5	253.8	12.00	12.00	-0.05
10,600.0		359.52	10,150.9	285.3	-785.3	351.4	0.00	0.00	0.00
10,700.0		359.52	10,150.9	385.3	-786.2	451.1	0.00	0.00	0.00
10,800.0		359.52	10,150.9	485.3	-787.0	550.8	0.00	0.00	0.00
10,900.0	90.00	359.52	10,150.9	585.3	-787.8	650.5	0.00	0.00	0.00
11,000.0		359.52	10,150.9	685.3	-788.7	750.2	0.00	0.00	0.00
11,100.0		359.52	10,150.9	785.3	-789.5	849.9	0.00	0.00	0.00
11,200.0		359.52	10,151.0	885.3	-790.4	949.6	0.00	0.00	0.00
11,300.0		359.52	10,151.0	985.2	-791.2	1,049.3	0.00	0.00	0.00
11,400.0	90.00	359.52	10,151.0	1,085.2	-792.0	1,149.0	0.00	0.00	0.00
11,500.0		359.52	10,151.0	1,185.2	-792.9	1,143.0	0.00	0.00	0.00
11,600.0		359.52	10,151.0	1,285.2	-793.7	1,348.4	0.00	0.00	0.00
11,700.0		359.52	10,151.0	1,385.2	-794.6	1,448.1	0.00	0.00	0.00
11,800.0		359.52	10,151.0	1,485.2	-795.4	1,547.8	0.00	0.00	0.00
11,900.0		359.52	10,151.0	1,585.2	-796.2	1,647.5	0.00	0.00	0.00
12,000.0		359.52	10,151.0	1,685.2	-790.2 -797.1	1,747.2	0.00	0.00	0.00
12,100.0		359.52	10,151.0	1,785.2	-797.1	1,846.9	0.00	0.00	0.00
12,100.0		359.52	10,151.0	1,785.2	-798.8	1,946.6	0.00	0.00	0.00
12,300.0		359.52	10,151.0	1,985.2	-799.6	2,046.3	0.00	0.00	0.00
12,400.0		359.52	10,151.0	2,085.2	-800.4	2,146.0	0.00	0.00	0.00
12,500.0		359.52	10,151.0	2,185.2	-801.3	2,245.7	0.00	0.00	0.00
12,600.0		359.52	10,151.0	2,285.2	-802.1	2,345.4	0.00	0.00	0.00
12,700.0		359.52	10,151.0	2,385.2	-803.0	2,445.1	0.00	0.00	0.00
12,800.0		359.52	10,151.0	2,485.2	-803.8	2,544.8	0.00	0.00	0.00
12,900.0		359.52	10,151.0	2,585.2	-804.7	2,644.5	0.00	0.00	0.00
13,000.0		359.52	10,151.0	2,685.2	-805.5	2,744.2	0.00	0.00	0.00
13,100.0		359.52	10,151.0	2,785.2	-806.3	2,843.9	0.00	0.00	0.00
13,200.0	90.00	359.52	10,151.0	2,885.2	-807.2	2,943.6	0.00	0.00	0.00



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kb=25' @ 3815.0usft kb=25' @ 3815.0usft

Grid

isign:	FIAII #0. I								
anned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
13,300.0	90.00	359.52	10,151.0	2,985.2	-808.0	3,043.3	0.00	0.00	0.00
13,400.0	90.00	359.52	10,151.0	3,085.2	-808.9	3,143.0	0.00	0.00	0.00
13,500.0	90.00	359.52	10,151.0	3,185.2	-809.7	3,242.7	0.00	0.00	0.00
13,600.0	90.00	359.52	10,151.0	3,285.2	-810.5	3,342.4	0.00	0.00	0.00
13,700.0	90.00	359.52	10,151.0	3,385.2	-811.4	3,442.1	0.00	0.00	0.00
13,800.0	90.00	359.52	10,151.0	3,485.2	-812.2	3,541.8	0.00	0.00	0.00
13,900.0	90.00	359.52	10,151.0	3,585.2	-813.1	3,641.5	0.00	0.00	0.00
14,000.0	90.00	359.52	10,151.0	3,685.2	-813.9	3,741.2	0.00	0.00	0.00
14,100.0	90.00	359.52	10,151.0	3,785.1	-814.7	3,840.9	0.00	0.00	0.00
14,200.0	90.00	359.52	10,151.0	3,885.1	-815.6	3,940.6	0.00	0.00	0.00
14,300.0	90.00	359.52	10,151.0	3,985.1	-816.4	4,040.3	0.00	0.00	0.00
14,400.0	90.00	359.52	10,151.0	4,085.1	-817.3	4,140.0	0.00	0.00	0.00
14,500.0	90.00	359.52	10,151.0	4,185.1	-818.1	4,239.7	0.00	0.00	0.00
14,600.0	90.00	359.52	10,151.0	4,285.1	-819.0	4,339.5	0.00	0.00	0.00
14,700.0 14,800.0	90.00 90.00	359.52 359.52	10,151.0 10,151.0	4,385.1 4.485.1	-819.8 -820.6	4,439.2 4,538.9	0.00 0.00	0.00 0.00	0.00 0.00
				4,485.1					
14,900.0	90.00	359.52	10,151.0	4,585.1	-821.5	4,638.6	0.00	0.00	0.00
15,000.0	90.00	359.52	10,151.0	4,685.1	-822.3	4,738.3	0.00	0.00	0.00
15,100.0	90.00	359.52	10,151.0	4,785.1	-823.2	4,838.0	0.00	0.00	0.00
15,200.0	90.00	359.52	10,151.0	4,885.1	-824.0	4,937.7	0.00	0.00	0.00
15,300.0	90.00	359.52	10,151.0	4,985.1	-824.8	5,037.4	0.00	0.00	0.00
15,400.0	90.00	359.52	10,151.0	5,085.1	-825.7	5,137.1	0.00	0.00	0.00
15,500.0	90.00	359.52	10,151.0	5,185.1	-826.5	5,236.8	0.00	0.00	0.00
15,600.0	90.00	359.52	10,151.0	5,285.1	-827.4	5,336.5	0.00	0.00	0.00
15,700.0	90.00	359.52	10,151.0	5,385.1	-828.2	5,436.2	0.00	0.00	0.00
15,800.0	90.00	359.52	10,151.0	5,485.1	-829.0	5,535.9	0.00	0.00	0.00
15,900.0	90.00	359.52	10,151.0	5,585.1	-829.9	5,635.6	0.00	0.00	0.00
16,000.0	90.00	359.52	10,151.0	5,685.1	-830.7	5,735.3	0.00	0.00	0.00
16,100.0	90.00	359.52	10,151.0	5,785.1	-831.6	5,835.0	0.00	0.00	0.00
16,200.0	90.00	359.52	10,151.0	5,885.1	-832.4	5,934.7	0.00	0.00	0.00
16,300.0	90.00	359.52	10,151.0	5,985.1	-833.2	6,034.4	0.00	0.00	0.00
16,400.0	90.00	359.52	10,151.0	6,085.1	-834.1	6,134.1	0.00	0.00	0.00
16,500.0	90.00	359.52	10,151.0	6,185.1	-834.9	6,233.8	0.00	0.00	0.00
16,600.0	90.00	359.52	10,151.0	6,285.1	-835.8	6,333.5	0.00	0.00	0.00
16,700.0	90.00	359.52	10,151.0	6,385.1	-836.6	6,433.2	0.00	0.00	0.00
16,800.0	90.00	359.52	10,151.0	6,485.1	-837.5	6,532.9	0.00	0.00	0.00
16,900.0	90.00	359.52	10,151.0	6,585.0	-838.3	6,632.6	0.00	0.00	0.00
17,000.0	90.00	359.52 359.52	10,151.0	6,685.0	-030.3 -839.1	6,732.3	0.00	0.00	0.00
17,100.0	90.00	359.52	10,151.0	6,785.0	-840.0	6,832.0	0.00	0.00	0.00
17,100.0	90.00	359.52	10,151.0	6,885.0	-840.8	6,931.7	0.00	0.00	0.00
17,300.0	90.00	359.52	10,151.0	6,985.0	-841.7	7,031.4	0.00	0.00	0.00
17,400.0	90.00	359.52	10,151.0	7,085.0	-842.5	7,131.1	0.00	0.00	0.00
17,500.0	90.00	359.52	10,151.0	7,185.0	-843.3	7,230.8	0.00	0.00	0.00
17,600.0	90.00	359.52	10,151.0	7,285.0	-844.2	7,330.5	0.00	0.00	0.00
17,700.0	90.00	359.52	10,151.0	7,385.0	-845.0	7,430.2	0.00	0.00	0.00
17,800.0	90.00	359.52	10,151.0	7,485.0	-845.9	7,529.9	0.00	0.00	0.00
17,900.0	90.00	359.52	10,151.0	7,585.0	-846.7	7,629.6	0.00	0.00	0.00
18,000.0	90.00	359.52	10,151.0	7,685.0	-847.5	7,729.3	0.00	0.00	0.00
18,100.0	90.00	359.52	10,151.0	7,785.0	-848.4	7,829.0	0.00	0.00	0.00
18,200.0	90.00	359.52	10,151.0	7,885.0	-849.2	7,928.7	0.00	0.00	0.00
18,300.0	90.00	359.52	10,151.0	7,985.0	-850.1	8,028.4	0.00	0.00	0.00
18,400.0	90.00	359.52	10,151.0	8,085.0	-850.9	8,128.1	0.00	0.00	0.00
18,500.0	90.00	359.52	10,151.0	8,185.0	-851.8	8,227.8	0.00	0.00	0.00
18,600.0	90.00	359.52	10,151.0	8,285.0	-852.6	8,327.5	0.00	0.00	0.00



Database: Company: PEDM

Midland

Project: Lea County, NM (NAD 83 NME)
Site: Date 14 State Com

 Well:
 #301H

 Wellbore:
 OH

 Design:
 Plan #0.1

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Well #301H

kb=25' @ 3815.0usft kb=25' @ 3815.0usft

Grid

Planned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
18,700.0	90.00	359.52	10,151.0	8,385.0	-853.4	8,427.2	0.00	0.00	0.00
18,800.0	90.00	359.52	10,151.0	8,485.0	-854.3	8,526.9	0.00	0.00	0.00
18,900.0	90.00	359.52	10,151.0	8,585.0	-855.1	8,626.7	0.00	0.00	0.00
19,000.0	90.00	359.52	10,151.0	8,685.0	-856.0	8,726.4	0.00	0.00	0.00
19,100.0	90.00	359.52	10,151.0	8,785.0	-856.8	8,826.1	0.00	0.00	0.00
19,200.0	90.00	359.52	10,151.0	8,885.0	-857.6	8,925.8	0.00	0.00	0.00
19,300.0	90.00	359.52	10,151.0	8,985.0	-858.5	9,025.5	0.00	0.00	0.00
19,400.0	90.00	359.52	10,151.0	9,085.0	-859.3	9,125.2	0.00	0.00	0.00
19,500.0	90.00	359.52	10,151.0	9,185.0	-860.2	9,224.9	0.00	0.00	0.00
19,600.0	90.00	359.52	10,151.0	9,285.0	-861.0	9,324.6	0.00	0.00	0.00
19,700.0	90.00	359.52	10,151.0	9,385.0	-861.8	9,424.3	0.00	0.00	0.00
19,800.0	90.00	359.52	10,151.0	9,484.9	-862.7	9,524.0	0.00	0.00	0.00
19,900.0	90.00	359.52	10,151.0	9,584.9	-863.5	9,623.7	0.00	0.00	0.00
20,000.0	90.00	359.52	10,151.0	9,684.9	-864.4	9,723.4	0.00	0.00	0.00
20,100.0	90.00	359.52	10,151.0	9,784.9	-865.2	9,823.1	0.00	0.00	0.00
20,200.0	90.00	359.52	10,151.0	9,884.9	-866.0	9,922.8	0.00	0.00	0.00
20,300.0	90.00	359.52	10,151.0	9,984.9	-866.9	10,022.5	0.00	0.00	0.00
20,400.0	90.00	359.52	10,151.0	10,084.9	-867.7	10,122.2	0.00	0.00	0.00
20,432.1	90.00	359.52	10,151.0	10,117.0	-868.0	10,154.2	0.00	0.00	0.00
PBHL(Date 1	14 State Com #3	01H)							

Design Targets									
Target Name - hit/miss target - Shape	Dip Angle (°)	Dip Dir. (°)	TVD (usft)	+N/-S (usft)	+E/-W (usft)	Northing (usft)	Easting (usft)	Latitude	Longitude
KOP(Date 14 State Corr - plan hits target cen - Point	0.00 ter	0.00	9,673.5	-290.0	-782.0	536,228.00	784,597.00	32° 28' 18.057 N	103° 32' 40.347 W
FTP(Date 14 State Com - plan hits target cen - Point	0.00 ter	0.00	9,886.2	-240.0	-782.0	536,278.00	784,597.00	32° 28' 18.552 N	103° 32' 40.343 W
PBHL(Date 14 State Col - plan hits target cen - Point	0.00 ter	0.00	10,151.0	10,117.0	-868.0	546,635.00	784,511.00	32° 30' 1.038 N	103° 32' 40.453 W



1200-

1500-

1800-

2400

6000-

6900-

7500

8100

8400-

8700-

9000-

450

Released to Imaging: 10/5/2023 1:38:45 PM

T M

Azimuths to Grid North
True North: -0.42°
Magnetic North: 5.86°

Magnetic Field Strength: 47405.0nT Dip Angle: 60.05° Date: 9/19/2023 Model: IGRF2020

To convert a Magnetic Direction to a Grid Direction, Add 5.86°
To convert a Magnetic Direction to a True Direction, Add 6.28° East
To convert a True Direction to a Grid Direction, Subtract 0.42°

Lea County, NM (NAD 83 NME)

Date 14 State Com #301H

**Plan #0.1** 

PROJECT DETAILS: Lea County, NM (NAD 83 NME)

Geodetic System: US State Plane 1983
Datum: North American Datum 1983
Ellipsoid: GRS 1980

Zone: New Mexico Eastern Zone System Datum: Mean Sea Level

WELL DETAILS: #301H

3790.0

kb=25' @ 3815.0usft

 Northing
 Easting
 Latittude
 Longitude

 536518.00
 785379.00
 32° 28' 20.869 N
 103° 32' 31.194 W

SECTION DETAILS										
Sec	MD	Inc	Azi	TVD	+N/-S	+E/-W	Dleg	TFace	VSect	Target
1	0.0	0.00	0.00	0.0	0.0	0.0	0.00	0.00	0.0	
2	2343.0	0.00	0.00	2343.0	0.0	0.0	0.00	0.00	0.0	
3	2906.9	11.28	249.65	2903.3	-19.2	-51.9	2.00	249.65	-14.7	
4	6605.8	11.28	249.65	6530.7	-270.8	-730.1	0.00	0.00	-207.4	
5	7169.7	0.00	0.00	7091.0	-290.0	-782.0	2.00	180.00	-222.1	
6	9752.2	0.00	0.00	9673.5	-290.0	-782.0	0.00	0.00	-222.1	KOP(Date 14 State Com #301H)
7	9972.6	26.46	0.00	9886.2	-240.0	-782.0	12.00	0.00	-172.3	FTP(Date 14 State Com #301H)
8	10502.2	90.00	359.52	10150.9	187.5	-784.5	12.00	-0.54	253.8	
9	20432.1	90.00	359.52	10151.0	10117.0	-868.0	0.00	0.00	10154.2	PBHL(Date 14 State Com #301H)

CASING DETAILS

No casing data is available

3150

WELLBORE TARGET DETAILS (MAP CO-ORDINATES) +E/-W Northing TVD +N/-S **Easting** KOP(Date 14 State Com #301H) -290.0 9673.5 536228.00 784597.00 -782.0 FTP(Date 14 State Com #301H) 9886.2 -240.0 -782.0 536278.00 784597.00 PBHL(Date 14 State Com #301H) 10151.0 10117.0 -868.0 546635.00 784511.00

- - - - -

-|-|----

West(-)/East(+)

Vertical Section at 355.10°

Lea County, NM (NAD 83 NME)
Date 14 State Com
#301H
OH
Plan #0.1
11:26, September 19 2023

Received by OCD: 9/25/2023 8:34:09 AM



# Salt Section Annular Clearance Variance Request

**Daniel Moose** 

## **Current Design (Salt Strings)**

#### **0.422"** Annular clearance requirement

- Casing collars shall have a minimum clearance of 0.422 inches on all sides in the hole/casing annulus, with recognition that variances can be granted for justified exceptions.
- 12.25" Hole x 9.625"40# J55/HCK55 LTC Casing
  - 1.3125" Clearance to casing OD
  - 0.8125" Clearance to coupling OD
- 9.875" Hole x 8.75" 38.5# P110 Sprint-SF Casing
  - 0.5625" Clearance to casing OD
  - 0.433" Clearance to coupling OD

## **Annular Clearance Variance Request**

EOG request permission to allow deviation from the 0.422" annulus clearance requirement for the intermediate (salt) section from Onshore Order #2 under the following conditions:

- The variance is not applicable within the Potash Boundaries or Capitan Reef areas.
- Operator takes responsibility to get casing to set point in the event that the clearance causes stuck pipe issues

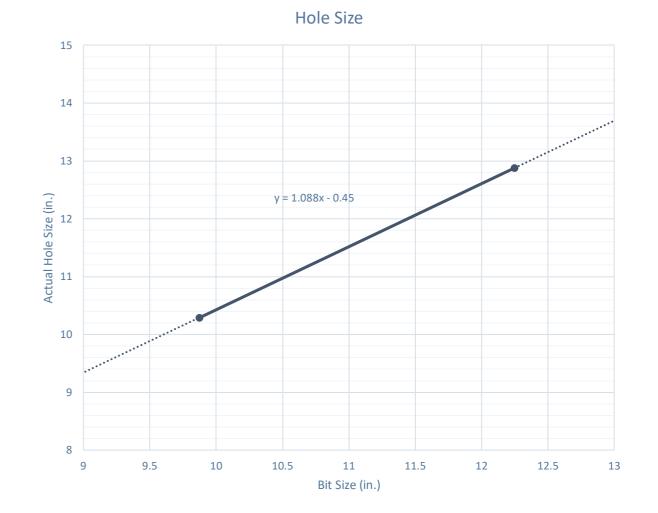
## **Volumetric Hole Size Calculation**

#### **Hole Size Calculations Off Cement Volumes**

- Known volume of cement pumped
- Known volume of cement returned to surface
- Must not have had any losses
- Must have bumped plug

#### **Average Hole Size**

- 12.25" Hole
  - 12.88" Hole
    - 5.13% diameter increase
    - 10.52% area increase
  - 0.63" Average enlargement
  - 0.58" Median enlargement
  - 179 Well Count
- 9.875" Hole
  - 10.30" Hole
    - 4.24% diameter increase
    - 9.64% area increase
  - 0.42" Average enlargement
  - 0.46" Median enlargement
  - 11 Well Count

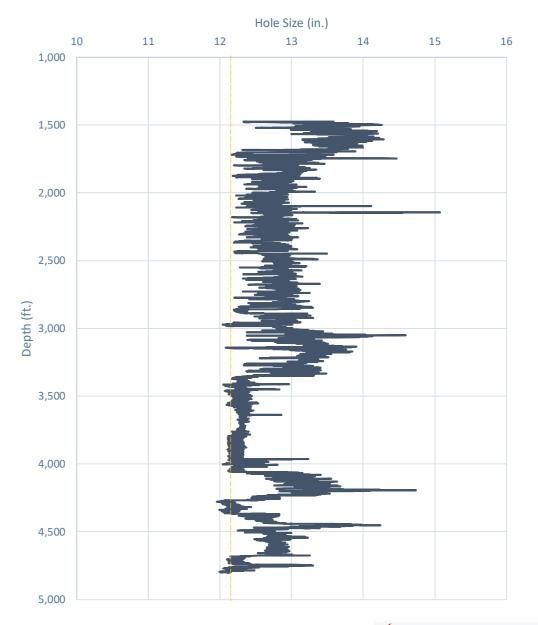


#### Modelo 10 Fed Com #501H

## Caliper Hole Size (12.25")

#### **Average Hole Size**

- 12.25" Bit
  - 12.76" Hole
    - 4.14% diameter increase
    - 8.44% area increase
  - 0.51" Average enlargement
  - 0.52" Median enlargement
  - Brine

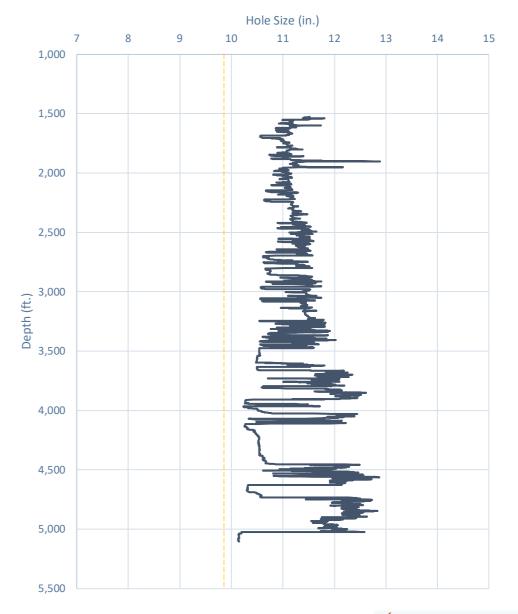


## Caliper Hole Size (9.875")

#### **Average Hole Size**

- 9.875" Hole
  - 11.21" Hole
    - 13.54% diameter increase
    - 28.92% area increase
  - 1.33" Average enlargement
  - 1.30" Median enlargement
  - EnerLite

#### Whirling Wind 11 Fed Com #744H



## **Design A**

# Proposed 11" Hole with 9.625" 40# J55/HCK55 LTC Casing

- 11" Bit + 0.52" Average hole enlargement = 11.52" Hole Size
  - 0.9475" Clearance to casing OD

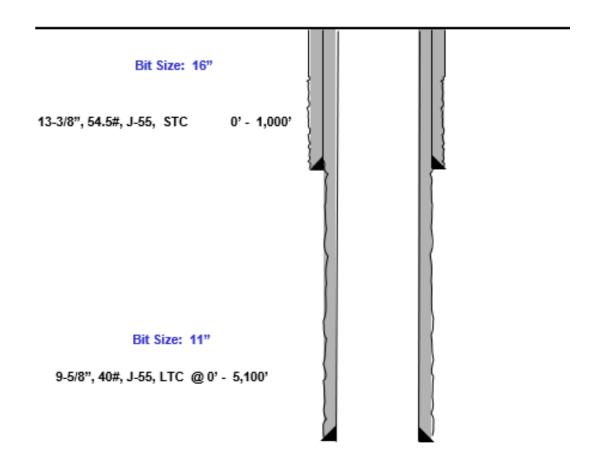
$$=\frac{11.52-9.625}{2}$$

• 0.4475" Clearance to coupling OD

$$=\frac{11.52-10.625}{2}$$

- Previous Shoe 13.375" 54.5# J55 STC
  - 0.995" Clearance to coupling OD (~1,200' overlap)

$$=\frac{12.615-10.625}{^{2}}$$



## **Design B**

## Proposed 9.875" Hole with 8.625" 32# J55/P110 BTC-SC Casing

- 9.875" Bit + 0.42" Average hole enlargement = 10.295" Hole Size
  - 0.835" Clearance to casing OD

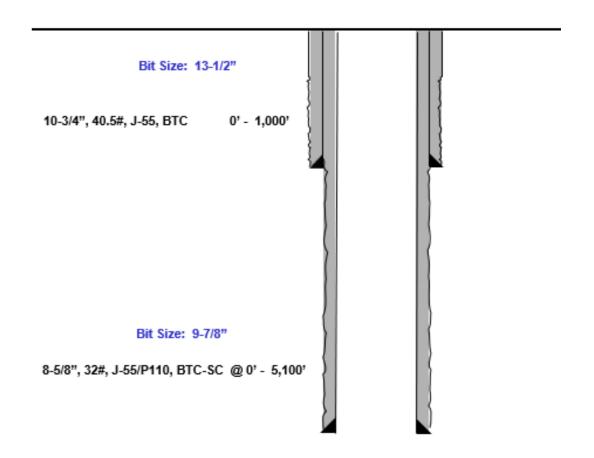
$$=\frac{10.295-8.625}{2}$$

• 0.585" Clearance to coupling OD

$$=\frac{10.295-9.125}{2}$$

- Previous Shoe 10.75" 40.5# J55 STC
  - 0.4625" Clearance to coupling OD (~1,200' overlap)

$$=\frac{10.05-9.125}{2}$$



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# Index

## **Casing Spec Sheets**

#### PERFORMANCE DATA

API LTC 9.625 in 40.00 lbs/ft K55 HC Technical Data Sheet

<b>Tubular Parameters</b>					
Size	9.625	in	Minimum Yield	55	ksi
Nominal Weight	40.00	lbs/ft	Minimum Tensile	95	ksi
Grade	K55 HC		Yield Load	629	kips
PE Weight	38.94	lbs/ft	Tensile Load	1088	kips
Wall Thickness	0.395	in	Min. Internal Yield Pressure	3,950	psi
Nominal ID	8.835	in	Collapse Pressure	3600	psi
Drift Diameter	8.750	in		•	1

in²

Connection Parameters								
Connection OD	10.625	in						
Coupling Length	10.500	in						
Threads Per Inch	8	tpi						
Standoff Thread Turns	3.50	turns						
Make-Up Loss	4.750	in						
Min. Internal Yield Pressure	3,950	psi						

11.454

#### Pipe Body and API Connections Performance Data

13.375 54.50/0.380 J55 PDF

New Search #



« Back to Previous List

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6/8/2015 10:04:37 AM					
Mechanical Properties	Ptpe	втс	LTC	STC	
Minimum Yield Strength	55,000	-	-	-	psi
Maximum Yield Strength	80,000	-	-	-	psi
Minimum Tensile Strength	75,000	-	-	-	psi
Dimensions	Ptpe	втс	LTC	STC	
Outside Diameter	13.375	14.375	-	14.375	in.
Wall Thickness	0.380	-	-	-	in.
Inside Diameter	12.615	12.615	-	12.615	in.
Standard Drift	12.459	12.459	-	12.459	in.
Alternate Drift	-	-	-	-	in.
Nominal Linear Weight, T&C	54.50	-	-	-	lbs/ft
Plain End Weight	52.79	-	-	-	lbs/ft
Performance	Pipe	втс	LTC	STC	
Minimum Collapse Pressure	1,130	1,130	-	1,130	psi
Minimum Internal Yield Pressure	2,740	2,740	-	2,740	psi
Minimum Pipe Body Yield Strength	853.00	-	-	-	1000 lbs
Joint Strength	-	909	-	514	1000 lbs
Reference Length	-	11,125	-	6,290	ft
Make-Up Data	Ptpe	втс	LTC	STC	
Make-Up Loss	-	4.81	-	3.50	in.
Minimum Make-Up Torque	-	-	-	3,860	ft-lbs
Maximum Make-Up Torque	-	-	-	6,430	ft-lbs

Nom. Pipe Body Area

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3,150

5,250

ft-lbs

ft-lbs

## **Casing Spec Sheets**

#### Pipe Body and API Connections Performance Data

10.750 40.50/0.350 J55 PDF

New Search » « Back to Previous List USC Metric 6/8/2015 10:14:05 AM BTC Ptpe STC **Mechanical Properties** Minimum Yield Strength 55,000 psi Maximum Yield Strength 80,000 Minimum Tensile Strength 75,000 psi BTC LTC Pipe STC 11.750 Outside Diamete 10.750 11.750 in. Wall Thickness 0.350 Inside Diameter 10.050 10.050 10.050 Standard Drift 9.894 9.894 in. Alternate Drift in. 40.50 Nominal Linear Weight, T&C lbs/ft 38.91 lbs/ft Plain End Weight Performance Ptpe BTC STC Minimum Collapse Pressure psi Minimum Internal Yield Pressure 3.130 3.130 3.130 629.00 1000 lbs Minimum Pipe Body Yield Strength 700 420 Joint Strength 1000 lbs Reference Length 11,522 6,915 BTC STC Make-Up Data Ptpe 4.81 Make-Up Loss 3.50 in.



Material Properties	(PE)
Pipe	
Minimum Yield Strength:	55 ksi
Maximum Yield Strength:	80 ksi
Minimum Tensile Strength:	75 ksi
Coupling	
Minimum Yield Strength:	55 ksi
Maximum Yield Strength:	80 ksi
Minimum Tensile Strength:	75 ksi

USA

MADE IN

#Od

SLN

#0/M

7.875

DA

S2L2

S

8.625

VALLOUREC STAR

Pipe Body Data (PE)								
Geometry								
Nominal ID:	7.92 inch							
Nominal Area:	9.149 in <sup>2</sup>							
*Special/Alt. Drift:	7.875 inch							
Performar	псе							
Pipe Body Yield Strength:	503 kips							
Collapse Resistance:	2,530 psi							
Internal Yield Pressure: (API Historical)	3,930 psi							

Coupling OD: 9.625"								
STC Performance								
STC Internal Pressure:	3,930	psi						
STC Joint Strength:	372	kips						
LTC Performance								
LTC Internal Pressure:	3,930	psi						
LTC Joint Strength:	417	kips						
SC-BTC Performance - (	SC-BTC Performance - Cplg OD = 9.125"							
BTC Internal Pressure:	3,930	psi						
BTC Joint Strength:	503	kips						

	API Connection Torque							
	STC Torque (ft-lbs)							
Min:	2,793	Opti:	3,724	Max:	4,655			
	LTC Torque (ft-lbs)							
Min:	3,130	Opti:	4,174	Max:	5,217			
	BTC Torque (ft-lbs)							
follow API guidelines regarding positional make up								

\*Alt. Drift will be used unless API Drift is specified on order.

\*\*If above API connections do not suit your needs, VAM® premium connections are available up to 100% of pipe body ratings.

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Minimum Make-Up Torque

Maximum Make-Up Torque



#### **Break-test BOP & Offline Cementing:**

EOG Resources Inc. (EOG) respectfully requests a variance from the minimum standards for well control equipment testing of ECFR Title 43 Part 3172.6(b)(9)(iv) to allow a testing schedule of the blow out preventer (BOP) and blow out prevention equipment (BOPE) along with Batch Drilling & Offline cement operations to include the following:

- Full BOPE test at first installation on the pad.
- Full BOPE test every 21 days.
- This test will be conducted for 5M rated hole intervals only.
- Each rig requesting the break-test variance is capable of picking up the BOP without damaging components using winches, following API Standard 53, Well Control Equipment Systems for Drilling Wells (Fifth edition, December 2018, Annex C. Table C.4) which recognizes break testing as an acceptable practice.
- Function tests will be performed on the following BOP elements:
  - Annular **à** during each full BOPE test
  - Upper Pipe Rams **à** On trip ins where FIT required
  - Blind Rams **à** Every trip
  - Lower Pipe Rams à during each full BOPE test
- Break testing BOP and BOPE coupled with batch drilling operations and option to offline cement and/or remediate (if needed) any surface or intermediate sections, according to attached offline cementing support documentation.
- After the well section is secured, the BOP will be disconnected from the wellhead and walked with the rig to another well on the pad.
- TA cap will also be installed per Wellhead vendor procedure and pressure inside the
  casing will be monitored via the valve on the TA cap as per standard batch drilling
  ops.

Blind Rams

Roadside Kill

Test plug

## **Break Test Diagram (HCR valve)**

#### Steps

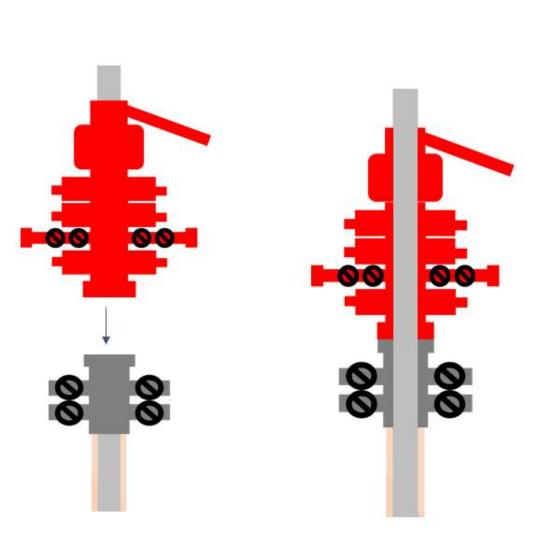
Pressure

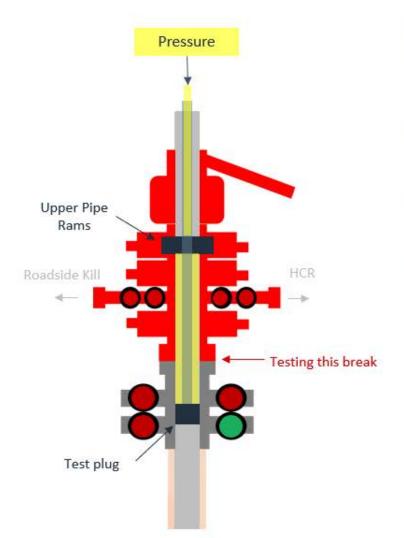
HCR

Testing this break

- 1. Set plug in wellhead (lower barrier)
- 2. Close Blind Rams (upper barrier)
- 3. Close roadside kill
- 4. Open HCR (pressure application)
- Open wellhead valves below test plug to ensure if leak past test plug, pressure won't be applied to wellbore
- Tie BOP testers high pressure line to main choke manifold crown valve
- 7. Pressure up to test break
- Bleed test pressure from BOP testing unit

## **Break Test Diagram (Test Joint)**





#### Steps

- Set plug in with test joint wellhead (lower barrier)
- 2. Close Upper Pipe Rams (upper barrier)

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- 3. Close roadside kill
- Close HCR
- Open wellhead valves below test plug to ensure if leak past test plug, pressure won't be applied to wellbore
- Tie BOP testers high pressure line to top of test joint
- 7. Pressure up to test break
- Bleed test pressure from BOP testing unit



Offline Intermediate Cementing Procedure

2/24/2022

#### **Cement Program**

1. No changes to the cement program will take place for offline cementing.

#### **Summarized Operational Procedure for Intermediate Casing**

- 1. Run casing as per normal operations. While running casing, conduct negative pressure test and confirm integrity of the float equipment back pressure valves.
  - a. Float equipment is equipped with two back pressure valves rated to a minimum of 5,000 psi.
- 2. Land production casing on mandrel hanger through BOP.
  - a. If casing is unable to be landed with a mandrel hanger, then the casing will be cemented online.
- 3. Break circulation and confirm no restrictions.
  - a. Ensure no blockage of float equipment and appropriate annular returns.
  - b. Perform flow check to confirm well is static.
- 4. Set pack-off
  - a. If utilizing a fluted/ported mandrel hanger, ensure well is static on the annulus and inside the casing by filling the pipe with kill weight fluid, remove landing joint, and set annular packoff through BOP. Pressure test to 5,000 psi for 10 min.
  - b. If utilizing a solid mandrel hanger, ensure well is static on the annulus and inside the casing by filling the pipe with kill weight fluid. Pressure test seals to 5,000 psi for 10 min. Remove landing joint through BOP.
- 5. After confirmation of both annular barriers and the two casing barriers, install TA plug and pressure test to 5,000 psi for 10 min. Notify the BLM with intent to proceed with nipple down and offline cementing.
  - a. Minimum 4 hrs notice.
- 6. With the well secured and BLM notified, nipple down BOP and secure on hydraulic carrier or cradle.
  - a. Note, if any of the barriers fail to test, the BOP stack will not be nippled down until after the cement job has concluded and both lead and tail slurry have reached 500 psi.
- 7. Skid/Walk rig off current well.
- 8. Confirm well is static before removing TA Plug.
  - a. Cementing operations will not proceed until well is under control. (If well is not static, notify BLM and proceed to kill)
  - b. Casing outlet valves will provide access to both the casing ID and annulus. Rig or third party pump truck will kill well prior to cementing.
  - c. Well control plan can be seen in Section B, Well Control Procedures.
  - d. If need be, rig can be moved back over well and BOP nippled back up for any further remediation.



Offline Intermediate Cementing Procedure

2/24/2022

- e. Diagram for rig positioning relative to offline cementing can be seen in Figure 4.
- 9. Rig up return lines to take returns from wellhead to pits and rig choke.
  - a. Test all connections and lines from wellhead to choke manifold to 5,000 psi high for 10 min.
  - b. If either test fails, perform corrections and retest before proceeding.
  - c. Return line schematics can be seen in Figure 3.
- 10. Remove TA Plug from the casing.
- 11. Install offline cement tool.
  - a. Current offline cement tool schematics can be seen in Figure 1 (Cameron) and Figure 2 (Cactus).
- 12. Rig up cement head and cementing lines.
  - a. Pressure test cement lines against cement head to 80% of casing burst for 10 min.
- 13. Break circulation on well to confirm no restrictions.
  - a. If gas is present on circulation, well will be shut in and returns rerouted through gas buster.
  - b. Max anticipated time before circulating with cement truck is 6 hrs.
- 14. Pump cement job as per plan.
  - a. At plug bump, test casing to 0.22 psi/ft or 1500 psi, whichever is greater.
  - b. If plug does not bump on calculated, shut down and wait 8 hrs or 500 psi compressive strength, whichever is greater before testing casing.
- 15. Confirm well is static and floats are holding after cement job.
  - a. With floats holding and backside static:
    - i. Remove cement head.
  - b. If floats are leaking:
    - i. Shut-in well and WOC (Wait on Cement) until tail slurry reaches 500 psi compressive strength and the casing is static prior to removing cement head.
  - c. If there is flow on the backside:
    - i. Shut in well and WOC until tail slurry reaches 500 psi compressive strength. Ensure that the casing is static prior to removing cement head.
- 16. Remove offline cement tool.
- 17. Install night cap with pressure gauge for monitoring.
- 18. Test night cap to 5,000 psi for 10 min.



Offline Intermediate Cementing Procedure

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#### **Example Well Control Plan Content**

#### A. Well Control Component Table

The table below, which covers the cementing of the <u>5M MASP (Maximum Allowable Surface Pressure) portion of the well</u>, outlines the well control component rating in use. This table, combined with the mud program, documents that two barriers to flow can be maintained at all times, independent of the BOP nippled up to the wellhead.

Intermediate hole section, 5M requirement

Component	RWP
Pack-off	10M
Casing Wellhead Valves	10M
Annular Wellhead Valves	5M
TA Plug	10M
Float Valves	5M
2" 1502 Lo-Torque Valves	15M

#### **B.** Well Control Procedures

Well control procedures are specific to the rig equipment and the operation at the time the kick occurs. Below are the minimal high-level tasks prescribed to assure a proper shut-in while circulating and cementing through the Offline Cement Adapter.

#### **General Procedure While Circulating**

- 1. Sound alarm (alert crew).
- 2. Shut down pumps.
- 3. Shut-in Well (close valves to rig pits and open valve to rig choke line. Rig choke will already be in the closed position).
- 4. Confirm shut-in.
- 5. Notify tool pusher/company representative.

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- 6. Read and record the following:
  - a. SICP (Shut in Casing Pressure) and AP (Annular Pressure)
  - b. Pit gain
  - c. Time
  - d. Regroup and identify forward plan to continue circulating out kick via rig choke and mud/gas separator. Circulate and adjust mud density as needed to control well.

### **General Procedure While Cementing**

- 1. Sound alarm (alert crew).
- 2. Shut down pumps.
- 3. Shut-in Well (close valves to rig pits and open valve to rig choke line. Rig choke will already be in the closed position).
- 4. Confirm shut-in.
- 5. Notify tool pusher/company representative.
- 6. Open rig choke and begin pumping again taking returns through choke manifold and mud/gas separator.
- 7. Continue to place cement until plug bumps.
- 8. At plug bump close rig choke and cement head.
- 9. Read and record the following
  - a. SICP and AP
  - b. Pit gain
  - c. Time
  - d. Shut-in annulus valves on wellhead

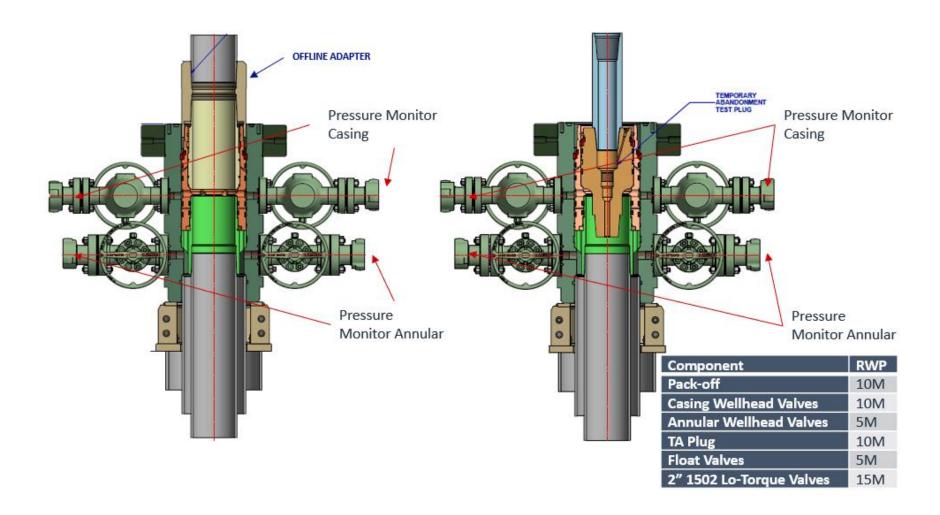
### **General Procedure After Cementing**

- 1. Sound alarm (alert crew).
- 2. Shut-in Well (close valves to rig pits and open valve to rig choke line. Rig choke will already be in the closed position).
- 3. Confirm shut-in.
- 4. Notify tool pusher/company representative.
- 5. Read and record the following:
  - a. SICP and AP
  - b. Pit gain
  - c. Time
  - d. Shut-in annulus valves on wellhead



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Figure 1: Cameron TA Plug and Offline Adapter Schematic



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Figure 2: Cactus TA Plug and Offline Adapter Schematic

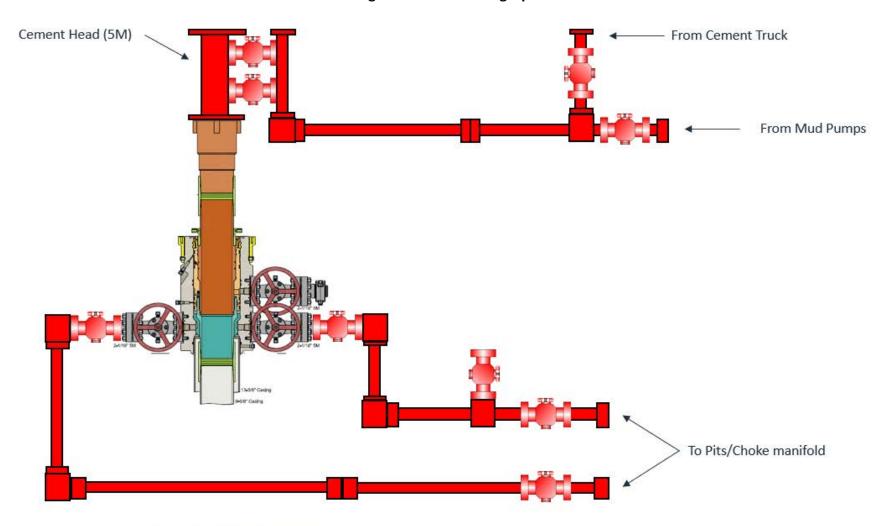


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Figure 3: Back Yard Rig Up



\*\*\* All Lines 10M rated working pressure

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Figure 4: Rig Placement Diagram



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### State of New Mexico Energy, Minerals and Natural Resources Department

Submit Electronically Via E-permitting

Oil Conservation Division 1220 South St. Francis Dr. Santa Fe, NM 87505

## NATURAL GAS MANAGEMENT PLAN

This Natural Gas Management Plan must be submitted with each Application for Permit to Drill (APD) for a new or recompleted well.

## Section 1 – Plan Description Effective May 25, 2021

I. Operator:EOG F	Resources, Inc	OGRID	<b>):</b> 7377		<b>Date:</b> 9/25	5/2023	
II. Type: ⊠ Original	☐ Amendm	ent due to $\square$ 19.15.	27.9.D(6)(a) NN	MAC □ 19.15.27.	9.D(6)(b) NMA	C □ Otl	ner.
If Other, please describe:							
<b>III. Well(s):</b> Provide the be recompleted from a si					wells proposed t	o be dri	lled or proposed to
Well Name	API	ULSTR	Footages	Anticipated Oil BBL/D	Anticipated Gas MCF/D		Anticipated roduced Water BBL/D
DATE 14 STATE COM 301H		O-14-21S-33E	339' FSL & 2248' FEL	+/- 1000	+/- 3500	+/- 30	000
IV. Central Delivery Po V. Anticipated Schedu or proposed to be recom	l <b>le:</b> Provide the pleted from a	e following informa	ntion for each ne	ew or recompleted entral delivery poi	well or set of w	ells proj	posed to be drilled
Well Name	API	Spud Date	TD Reached Date	Completion Commencement			First Production Date
DATE 14 STATE COM 301H		10/01/23	10/15/23	12/08/23	1/08/24	ļ	2/08/24
VI. Separation Equipm VII. Operational Pract Subsection A through For VIII. Best Management during active and planne	ices: ⊠ Attac of 19.15.27.8 t Practices: □	ch a complete descr NMAC. ⊠ Attach a complet	iption of the ac	tions Operator wi	ll take to compl	y with the	he requirements of

## Section 2 – Enhanced Plan EFFECTIVE APRIL 1, 2022

Beginning April 1, 2022, an operator that is not in compliance with its statewide natural gas capture requirement for the applicable reporting area must complete this section.

🛮 Operator certifies that it is not required to complete this section because Operator is in compliance with its statewide natural gas capture requirement for the applicable reporting area.

### IX. Anticipated Natural Gas Production:

Well	API	Anticipated Average Natural Gas Rate MCF/D	Anticipated Volume of Natural Gas for the First Year MCF

### X. Natural Gas Gathering System (NGGS):

Operator	System	ULSTR of Tie-in	Anticipated Gathering	Available Maximum Daily Capacity
			Start Date	of System Segment Tie-in

XI. Map.   Attach an accurate and legible map depicting the location of the well(s), the anticipated pipeline route(s) connecting the
production operations to the existing or planned interconnect of the natural gas gathering system(s), and the maximum daily capacity of
the segment or portion of the natural gas gathering system(s) to which the well(s) will be connected.

XII. Line Capacity. The natural gas gathering system	$\square$ will $\square$ will not have ca	apacity to gather 100% of t	he anticipated natural gas
production volume from the well prior to the date of first	st production.		

<b>XIII. Line Pressure.</b> Operator $\square$ does $\square$ does not anticipate that its existing well(s) connected to the same segment, or positive that its existing well(s) connected to the same segment, or positive that its existing well(s) connected to the same segment, or positive that its existing well(s) connected to the same segment, or positive that its existing well(s) connected to the same segment, or positive that its existing well(s) connected to the same segment, or positive that its existing well(s) connected to the same segment, or positive that its existing well(s) connected to the same segment, or positive that its existing well(s) connected to the same segment.	rtion, of the
natural gas gathering system(s) described above will continue to meet anticipated increases in line pressure caused by the no	ew well(s).

$\square$ Attach Operator's plan to manage production in response to the increase	ced line precente	`

XIV. Confidentiality: $\square$ Operator asserts confidentiality pursuant to Section 71-2-8 NMSA 1978 for the information prov	vided in
Section 2 as provided in Paragraph (2) of Subsection D of 19.15.27.9 NMAC, and attaches a full description of the specific information of the	rmation
for which confidentiality is asserted and the basis for such assertion.	

# Section 3 - Certifications <u>Effective May 25, 2021</u>

Operator certifies that, after reasonable inquiry and based on the available information at the time of submittal: 🗵 Operator will be able to connect the well(s) to a natural gas gathering system in the general area with sufficient capacity to transport one hundred percent of the anticipated volume of natural gas produced from the well(s) commencing on the date of first production, taking into account the current and anticipated volumes of produced natural gas from other wells connected to the pipeline gathering system; or ☐ Operator will not be able to connect to a natural gas gathering system in the general area with sufficient capacity to transport one hundred percent of the anticipated volume of natural gas produced from the well(s) commencing on the date of first production, taking into account the current and anticipated volumes of produced natural gas from other wells connected to the pipeline gathering system. If Operator checks this box, Operator will select one of the following: Well Shut-In. ☐ Operator will shut-in and not produce the well until it submits the certification required by Paragraph (4) of Subsection D of 19.15.27.9 NMAC; or Venting and Flaring Plan. 

Operator has attached a venting and flaring plan that evaluates and selects one or more of the potential alternative beneficial uses for the natural gas until a natural gas gathering system is available, including: power generation on lease; (a) **(b)** power generation for grid; (c) compression on lease; (d) liquids removal on lease;

- reinjection for underground storage; (e)
- **(f)** reinjection for temporary storage;
- **(g)** reinjection for enhanced oil recovery;
- (h) fuel cell production; and
- (i) other alternative beneficial uses approved by the division.

## **Section 4 - Notices**

- 1. If, at any time after Operator submits this Natural Gas Management Plan and before the well is spud:
- (a) Operator becomes aware that the natural gas gathering system it planned to connect the well(s) to has become unavailable or will not have capacity to transport one hundred percent of the production from the well(s), no later than 20 days after becoming aware of such information, Operator shall submit for OCD's approval a new or revised venting and flaring plan containing the information specified in Paragraph (5) of Subsection D of 19.15.27.9 NMAC; or
- Operator becomes aware that it has, cumulatively for the year, become out of compliance with its baseline natural gas capture rate or natural gas capture requirement, no later than 20 days after becoming aware of such information, Operator shall submit for OCD's approval a new or revised Natural Gas Management Plan for each well it plans to spud during the next 90 days containing the information specified in Paragraph (2) of Subsection D of 19.15.27.9 NMAC, and shall file an update for each Natural Gas Management Plan until Operator is back in compliance with its baseline natural gas capture rate or natural gas capture requirement.
- 2. OCD may deny or conditionally approve an APD if Operator does not make a certification, fails to submit an adequate venting and flaring plan which includes alternative beneficial uses for the anticipated volume of natural gas produced, or if OCD determines that Operator will not have adequate natural gas takeaway capacity at the time a well will be spud.

I certify that, after reasonable inquiry, the statements in and attached to this Natural Gas Management Plan are true and correct to the best of my knowledge and acknowledge that a false statement may be subject to civil and criminal penalties under the Oil and Gas Act.

Signature: Star L Harrell
Printed Name: Star L Harrell
Title: Sr Regulatory Specialist
E-mail Address: Star_Harrell@eogresources.com
Date: 9/25/2023
Phone: (432) 848-9161
OIL CONSERVATION DIVISION
(Only applicable when submitted as a standalone form)
Approved By:
Title:
Approval Date:
Conditions of Approval:

### Natural Gas Management Plan Items VI-VIII

# VI. Separation Equipment: Attach a complete description of how Operator will size separation equipment to optimize gas capture.

- Separation equipment will be sized to provide adequate separation for anticipated rates.
- Adequate separation relates to retention time for Liquid Liquid separation and velocity for Gas-Liquid separation.
- Collection systems are appropriately sized to handle facility production rates on all (3) phases.
- Ancillary equipment and metering is selected to be serviced without flow interruptions or the need to release
  gas from the well.

# VII. Operational Practices: Attach a complete description of the actions Operator will take to comply with the requirements of Subsection A through F 19.15.27.8 NMAC.

### **Drilling Operations**

- All flare stacks will be properly sized. The flare stacks will be located at a minimum 100' from the nearest surface hole location on the pad.
- All natural gas produced during drilling operations will be flared, unless there is an equipment malfunction and/or to avoid risk of an immediate and substantial adverse impact on safety and the environment, at which point the gas will be vented.

### Completions/Recompletions Operations

- New wells will not be flowed back until they are connected to a properly sized gathering system.
- The facility will be built/sized for maximum anticipated flowrates and pressures to minimize waste.
- For flowback operations, multiple stages of separation will be used as well as excess VRU and blowers to make sure waste is minimized off the storage tanks and facility.
- During initial flowback, the well stream will be routed to separation equipment.
- At an existing facility, when necessary, post separation natural gas will be flared until it meets pipeline specifications, at which point it will be turned into a collection system.
- At a new facility, post separation natural gas will be vented until storage tanks can safely function, at which point it will be flared until it meets pipeline spec.

#### **Production Operations**

- Weekly AVOs will be performed on all facilities.
- All flares will be equipped with auto-ignition systems and continuous pilot operations.
- After a well is stabilized from liquid unloading, the well will be turned back into the collection system.
- All plunger lift systems will be optimized to limit the amount of waste.
- All tanks will have automatic gauging equipment installed.
- Leaking thief hatches found during AVOs will be cleaned and properly re-sealed.

#### Performance Standards

- Production equipment will be designed to handle maximum anticipated rates and pressure.
- All flared gas will be combusted in a flare stack that is properly sized and designed to ensure proper combustion.
- Weekly AVOs will be performed on all wells and facilities that produce more than 60 Mcfd.

#### Measurement & Estimation

- All volume that is flared and vented that is not measured will be estimated.
- All measurement equipment for flared volumes will conform to API 14.10.
- No meter bypasses with be installed.

• When metering is not practical due to low pressure/low rate, the vented or flared volume will be estimated.

# VIII. Best Management Practices: Attach a complete description of Operator's best management practices to minimize venting during active and planned maintenance.

- During downhole well maintenance, EOG will use best management practices to vent as minimally as possible.
- Prior to the commencement of any maintenance, the tank or vessel will be isolated from the rest of the facilities.
- All valves upstream of the equipment will be closed and isolated.
- After equipment has been isolated, the equipment will be blown down to as low a pressure as possible into the collection system.
- If the equipment being maintained cannot be relieved into the collection system, it shall be released to a tank where the vapor can either be captured or combusted if possible.
- After downhole well maintenance, natural gas will be flared until it reaches pipeline specification.

District I
1625 N. French Dr., Hobbs, NM 88240
Phone: (575) 393-6161 Fax: (575) 393-0720

District II 811 S. First St., Artesia, NM 88210 Phone:(575) 748-1283 Fax:(575) 748-9720

District III 1000 Rio Brazos Rd., Aztec, NM 87410 Phone:(505) 334-6178 Fax:(505) 334-6170

1220 S. St Francis Dr., Santa Fe, NM 87505 Phone:(505) 476-3470 Fax:(505) 476-3462

**State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division** 1220 S. St Francis Dr. **Santa Fe, NM 87505** 

CONDITIONS

Action 268485

### **CONDITIONS**

Operator:	OGRID:
EOG RESOURCES INC	7377
P.O. Box 2267	Action Number:
Midland, TX 79702	268485
	Action Type:
	[C-103] NOI Change of Plans (C-103A)

#### CONDITIONS

Created By	Condition	Condition Date
pkautz	ALL OTHER PREVIOUS COA'S APPLY.	10/5/2023