Form 3160-5 (June 2019)

UNITED STATES DEPARTMENT OF THE INTERIOR

| FORM APPROVED |
|--------------------------|
| OMB No. 1004-0137 |
| Expires: October 31, 202 |

| BURI | EAU OF LAND MANAGEMENT | 5. Lease Serial No. | 5. Lease Serial No. NMNM110838 | | | | |
|---|--|--|--|--|--|--|--|
| Do not use this f | OTICES AND REPORTS ON Vorm for proposals to drill or to Jse Form 3160-3 (APD) for su | 6. If Indian, Allottee of | or Tribe Name | | | | |
| SUBMIT IN 1 | TRIPLICATE - Other instructions on pag | 7. If Unit of CA/Agre | eement, Name and/or No. | | | | |
| 1. Type of Well Oil Well Gas W | /ell Other | | 8. Well Name and No |). ICY 7 FED/749H | | | |
| 2. Name of Operator EOG RESOURCE | CES INCORPORATED | | 9. API Well No. | 30-025-51855 | | | |
| | BY 2, HOUSTON, TX 77(3b. Phone No. (713) 651-70 | | | 10. Field and Pool or Exploratory Area WC-025 G-08 S253235G; LOWER BONE SPRING | | | |
| 4. Location of Well (Footage, Sec., T.,R SEC 7/T25S/R33E/NMP | .,M., or Survey Description) | | 11. Country or Parish LEA/NM | , State | | | |
| 12. CHE | CK THE APPROPRIATE BOX(ES) TO IN | DICATE NATURE OF N | OTICE, REPORT OR OT | HER DATA | | | |
| TYPE OF SUBMISSION | | TYPE OF | ACTION | | | | |
| Notice of Intent | Acidize Deep Alter Casing Hyde | pen | Production (Start/Resume) Reclamation | Water Shut-Off Well Integrity | | | |
| Subsequent Report | | | Recomplete Temporarily Abandon | Other | | | |
| Final Abandonment Notice | Convert to Injection Plug | Back V | Water Disposal | | | | |
| the Bond under which the work will completion of the involved operation completed. Final Abandonment Not is ready for final inspection.) Icy 7 Fed 512H (FKA 749H) Algorithms and EOG respectfully requests and Change name from Icy 7 Fed 50 Change SHL from T-25-S, R-3 to T-25-S, R-33-E, Sec 18, 200 Change BHL from T-25-S, R-3 | amendment to our approved APD for th 749H to Icy 7 Fed 512H. 3-E, Sec 18, 201' FNL, 1359' FWL, Lea I' FNL, 1359' FWL, Lea Co., N.M. 3-E, Sec 19, 2540' FNL, 1650' FWL, Le 40' FNL, 1650' FWL, Lea Co., N.M. | file with BLM/BIA. Requippletion or recompletion its, including reclamation, its well to reflect the following to Co., NM, | ired subsequent reports mu in a new interval, a Form 3 have been completed and | ust be filed within 30 days following 8160-4 must be filed once testing has been | | | |
| CRAIG RICHARDSON / Ph: (432) | ** / | Regulatory Spec | cialist | | | | |
| Signature | | Date | 08/21/2 | 2023 | | | |
| | THE SPACE FOR FED | ERAL OR STATE | OFICE USE | | | | |
| Approved by | | | | | | | |
| CHRISTOPHER WALLS / Ph: (575 | s) 234-2234 / Approved | Petroleum Title | | 08/24/2023 Date | | | |
| | ned. Approval of this notice does not warrar quitable title to those rights in the subject le duct operations thereon. | | AD | | | | |
| Title 19 II C C Section 1001 and Title 43 | STLS C Section 1212 make it a crime for a | ny parsan knavyinaky and | willfully to make to any d | apartment or aganay of the United States | | | |

Title 18 U.S.C Section 1001 and Title 43 U.S.C Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United State any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

(Instructions on page 2)

GENERAL INSTRUCTIONS

This form is designed for submitting proposals to perform certain well operations and reports of such operations when completed as indicated on Federal and Indian lands pursuant to applicable Federal law and regulations. Any necessary special instructions concerning the use of this form and the number of copies to be submitted, particularly with regard to local area or regional procedures and practices, are either shown below, will be issued by or may be obtained from the local Federal office.

SPECIFIC INSTRUCTIONS

Item 4 - Locations on Federal or Indian land should be described in accordance with Federal requirements. Consult the local Federal office for specific instructions.

Item 13: Proposals to abandon a well and subsequent reports of abandonment should include such special information as is required by the local Federal office. In addition, such proposals and reports should include reasons for the abandonment; data on any former or present productive zones or other zones with present significant fluid contents not sealed off by cement or otherwise; depths (top and bottom) and method of placement of cement plugs; mud or other material placed below, between and above plugs; amount, size, method of parting of any casing, liner or tubing pulled and the depth to the top of any tubing left in the hole; method of closing top of well and date well site conditioned for final inspection looking for approval of the abandonment. If the proposal will involve **hydraulic fracturing operations**, you must comply with 43 CFR 3162.3-3, including providing information about the protection of usable water. Operators should provide the best available information about all formations containing water and their depths. This information could include data and interpretation of resistivity logs run on nearby wells. Information may also be obtained from state or tribal regulatory agencies and from local BLM offices.

NOTICES

The privacy Act of 1974 and the regulation in 43 CFR 2.48(d) provide that you be furnished the following information in connection with information required by this application.

AUTHORITY: 30 U.S.C. 181 et seq., 351 et seq., 25 U.S.C. 396; 43 CFR 3160.

PRINCIPAL PURPOSE: The information is used to: (1) Evaluate, when appropriate, approve applications, and report completion of subsequent well operations, on a Federal or Indian lease; and (2) document for administrative use, information for the management, disposal and use of National Resource lands and resources, such as: (a) evaluating the equipment and procedures to be used during a proposed subsequent well operation and reviewing the completed well operations for compliance with the approved plan; (b) requesting and granting approval to perform those actions covered by 43 CFR 3162.3-2, 3162.3-3, and 3162.3-4; (c) reporting the beginning or resumption of production, as required by 43 CFR 3162.4-1(c)and (d) analyzing future applications to drill or modify operations in light of data obtained and methods used.

ROUTINE USES: Information from the record and/or the record will be transferred to appropriate Federal, State, local or foreign agencies, when relevant to civil, criminal or regulatory investigations or prosecutions in connection with congressional inquiries or to consumer reporting agencies to facilitate collection of debts owed the Government.

EFFECT OF NOT PROVIDING THE INFORMATION: Filing of this notice and report and disclosure of the information is mandatory for those subsequent well operations specified in 43 CFR 3162.3-2, 3162.3-4.

The Paperwork Reduction Act of 1995 requires us to inform you that:

The BLM collects this information to evaluate proposed and/or completed subsequent well operations on Federal or Indian oil and gas leases.

Response to this request is mandatory.

The BLM would like you to know that you do not have to respond to this or any other Federal agency-sponsored information collection unless it displays a currently valid OMB control number.

BURDEN HOURS STATEMENT: Public reporting burden for this form is estimated to average 8 hours per response, including the time for reviewing instructions, gathering and maintaining data, and completing and reviewing the form. Direct comments regarding the burden estimate or any other aspect of this form to U.S. Department of the Interior, Bureau of Land Management (1004-0137), Bureau Information Collection Clearance Officer (WO-630), 1849 C St., N.W., Mail Stop 401 LS, Washington, D.C. 20240

(Form 3160-5, page 2)

Additional Information

Additional Remarks

Change target formation to Second Bone Spring Sand.

Update casing and cement program to current design.

Update the Pool as reflected in the C-102.

Location of Well

0. SHL: TR P / 876 FSL / 357 FEL / TWSP: 25S / RANGE: 33E / SECTION: 7 / LAT: 32.1402661 / LONG: -103.60399 (TVD: 0 feet, MD: 0 feet) PPP: TR A / 100 FNL / 430 FEL / TWSP: 25S / RANGE: 33E / SECTION: 18 / LAT: 32.1375833 / LONG: -103.6042271 (TVD: 13067 feet, MD: 13146 feet) BHL: TR H / 2539 FNL / 430 FEL / TWSP: 25S / RANGE: 33E / SECTION: 19 / LAT: 32.116364 / LONG: -103.6042315 (TVD: 13332 feet, MD: 20967 feet)

DISTRICT I 6161 Fax: (575) 393-0720 DISTRICT II DISTRICT III DISTRICT IV DISTRICT IV 1220 S. St. Francis Dr., Santa Fe, NM 87505 Phone: (505) 476-3460 Fax: (505) 476-3462

State of New Mexico Energy, Minerals & Natural Resources Department OIL CONSERVATION DIVISION 1220 South St. Francis Dr. Santa Fe, New Mexico 87505

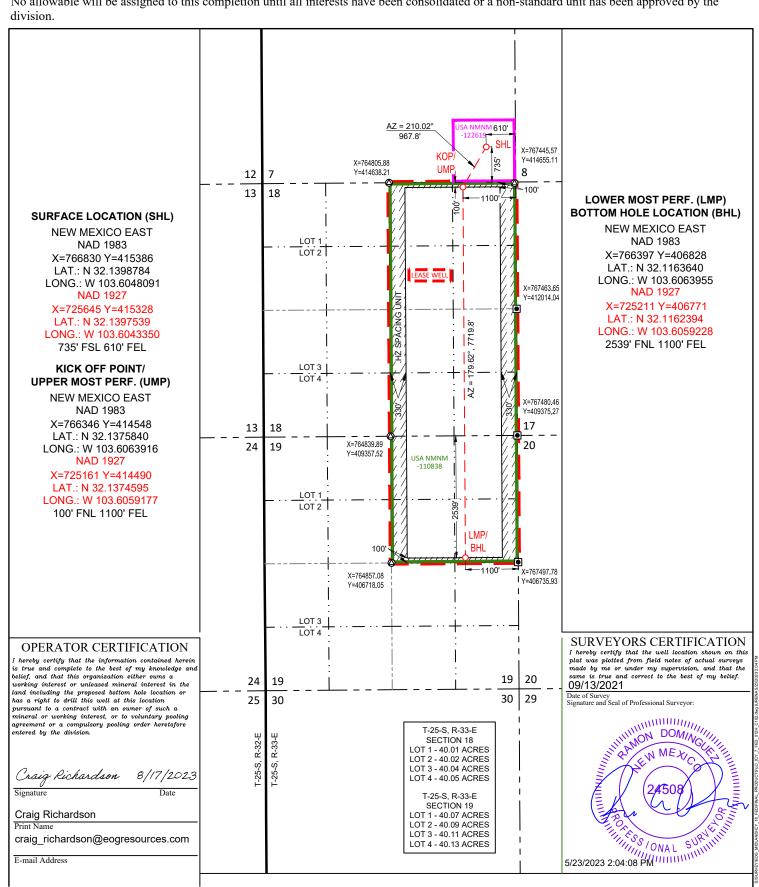
Form C-102 Revised August 1, 2011 Submit one copy to appropriate District Office

☐ AMENDED REPORT

WELL LOCATION AND ACREAGE DEDICATION PLAT

| API Number Pool Code | | | | | | Pool Name | | | | | |
|--------------------------------|--|-------------------------|------------------|------------|---------------|---------------------------------------|---------------|----------------|--------|--|--|
| 3 | 30-025- 51855 97903 | | | | | WC-025 G-08 S253235G; Lwr Bone Spring | | | | | |
| Property Co | ode | | • | | Property Name | | | Well Number | | | |
| 326335 | | ICY 7 FED 5 | | | | | | 2H | | | |
| OGRID N | 0. | Operator Name Elevation | | | | | | on | | | |
| 7377 EOG RESOURCES, INC. 3482' | | | | | | | 82' | | | | |
| | Surface Location | | | | | | | | | | |
| UL or lot no. | Section | Township | Range | Lot Idn | Feet from the | North/South line | Feet from the | East/West line | County | | |
| P | 7 | 25-S | 33-E - | | 735' | SOUTH | 610' | EAST | LEA | | |
| | Bottom Hole Location If Different From Surface | | | | | | | | | | |
| UL or lot no. | Section | Township | Range | Lot Idn | Feet from the | North/South line | Feet from the | East/West line | County | | |
| Н | 19 | 25-S | 33-E | - | 2539' | NORTH | 1100' | EAST | LEA | | |
| Dedicated Acres | Joint or | Infill | Consolidated Coo | le Ord | ler No. | - | - | - | | | |
| 480.00 | | | | LEASE WELL | | | | | | | |

No allowable will be assigned to this completion until all interests have been consolidated or a non-standard unit has been approved by the





Revised Permit Information 05/10/2023:

Well Name: Icy 7 Fed 512H

Location: SHL: 201' FNL & 1359' FWL, Section 18, T-25-S, R-33-E, Lea Co., N.M.

BHL: 2540' FNL & 1650' FWL, Section 19, T-25-S, R-33-E, Lea Co., N.M.

Casing Program A:

| Hole | Interval MD | | Interval TVD | | Csg | | | |
|--------|-------------|---------|--------------|---------|---------|--------|---------|------|
| Size | From (ft) | To (ft) | From (ft) | To (ft) | OD | Weight | Grade | Conn |
| 16" | 0 | 1,110 | 0 | 1,110 | 13-3/8" | 54.5# | J-55 | STC |
| 11" | 0 | 4,807 | 0 | 4,800 | 9-5/8" | 40# | J-55 | LTC |
| 6-3/4" | 0 | 17,392 | 0 | 9,818 | 5-1/2" | 17# | HCP-110 | LTC |

Variance is requested to waive the centralizer requirements for the 9-5/8" casing in the 11" hole size. An expansion additive will be utilized, in the cement slurry, for the entire length of the 11" hole interval to maximize cement bond and zonal isolation.

Variance is also requested to waive any centralizer requirements for the 5-1/2" casing in the 6-3/4" hole size. An expansion additive will be utilized, in the cement slurry, for the entire length of the 6-3/4" hole interval to maximize cement bond and zonal isolation.

EOG requests permission to allow deviation from the 0.422" annulus clearance requirement for the intermediate (salt) section from Onshore Order #2 under the following conditions:

- The variance is not applicable within the Potash Boundaries or Capitan Reef areas.
- Operator takes responsibility to get casing to set point in the event that the clearance causes stuck pipe issues.

Cementing Program:

| Ctint | nung 110 | 51 4111. | | |
|-------------------|-----------|------------|---------------|---|
| Depth | No. Sacks | Wt. ppg | Yld Ft3/sk | Slurry Description |
| 1,110' 13-3/8" | 340 | 13.5 | 1.73 | Lead: Class C + 4.0% Bentonite Gel + 0.5% CaCl2 + 0.25 lb/sk Cello-Flake (TOC @ Surface) |
| | 100 | 14.8 | 1.34 | Tail: Class C + 0.6% FL-62 + 0.25 lb/sk Cello-Flake + 0.2% Sodium Metasilicate (TOC @ 910') |
| 4,800' 9-5/8" | 460 | 12.7 | 2.22 | Lead: Class C + 10% NaCl + 6% Bentonite Gel + 3% MagOx (TOC @ Surface) |
| | 100 | 14.8 | 1.32 | Tail: Class C + 10% NaCL + 3% MagOx (TOC @ 3,840') |
| 17,392' 5-1/2" | 280 | 10.5 | 3.21 | Lead: Class H + 0.4% Halad-344 + 0.35% HR-601 + 3% Microbond (TOC @ 4,300') |
| | 570 | 13.2 | 1.52 | Tail: Class H + 5% NEX-020 + 0.2% NAC-102 + 0.15% NAS-725 + 0.5% NFL-549 + 0.2% NFP-703 + 1% NBE-737 + 0.3% NRT-241 (TOC @ 9350') |



| Additive | Purpose | | | |
|---------------------|---|--|--|--|
| Bentonite Gel | Lightweight/Lost circulation prevention | | | |
| Calcium Chloride | Accelerator | | | |
| Cello-flake | Lost circulation prevention | | | |
| Sodium Metasilicate | Accelerator | | | |
| MagOx | Expansive agent | | | |
| Pre-Mag-M | Expansive agent | | | |
| Sodium Chloride | Accelerator | | | |
| FL-62 | Fluid loss control | | | |
| Halad-344 | Fluid loss control | | | |
| Halad-9 | Fluid loss control | | | |
| HR-601 | Retarder | | | |
| Microbond | Expansive Agent | | | |

Note: Cement volumes based on bit size plus at least 25% excess in the open hole plus 10% excess in the cased-hole overlap section.

Mud Program:

| Depth (TVD) | Type | Type Weight (ppg) | | Water Loss |
|------------------|-------------|-------------------|-------|------------|
| 0 – 1,110' | Fresh - Gel | 8.6-8.8 | 28-34 | N/c |
| 1,110' – 4,800' | Brine | 8.6-8.8 | 28-34 | N/c |
| 4,800' – 17,392' | Oil Base | 8.8-9.5 | 58-68 | N/c - 6 |

Wellhead & Offline Cementing:

EOG Resources Inc. (EOG) respectfully requests a variance from the minimum standards for well control equipment testing of Onshore Order No. 2 (item III.A.2.a.i) to allow a testing schedule of the blow out preventer (BOP) and blow out prevention equipment (BOPE) along with Batch Drilling & Offline cement operations to include the following:

- Full BOPE test at first installation on the pad.
- Full BOPE test every 21 days per Onshore Order No. 2.
- Function test BOP elements per Onshore Order No. 2.
- Break testing BOP and BOPE coupled with batch drilling operations and option to
 offline cement and/or remediate (if needed) any surface or intermediate sections,
 according to attached offline cementing support documentation.
- After the well section is secured, the BOP will be disconnected from the wellhead and walked with the rig to another well on the pad.
- TA cap will also be installed per Wellhead vendor procedure and pressure inside the casing will be monitored via the valve on the TA cap as per standard batch drilling ops.
- See attached "EOG BLM Variance 3a -Offline Cement Intermediate Operational Procedure"



TUBING REQUIREMENTS

EOG respectively requests an exception to the following NMOCD rule:

• 19.15.16.10 Casing AND TUBING RQUIREMENTS:

J (3): "The operator shall set tubing as near the bottom as practical and tubing perforations shall not be more than 250 feet above top of pay zone."

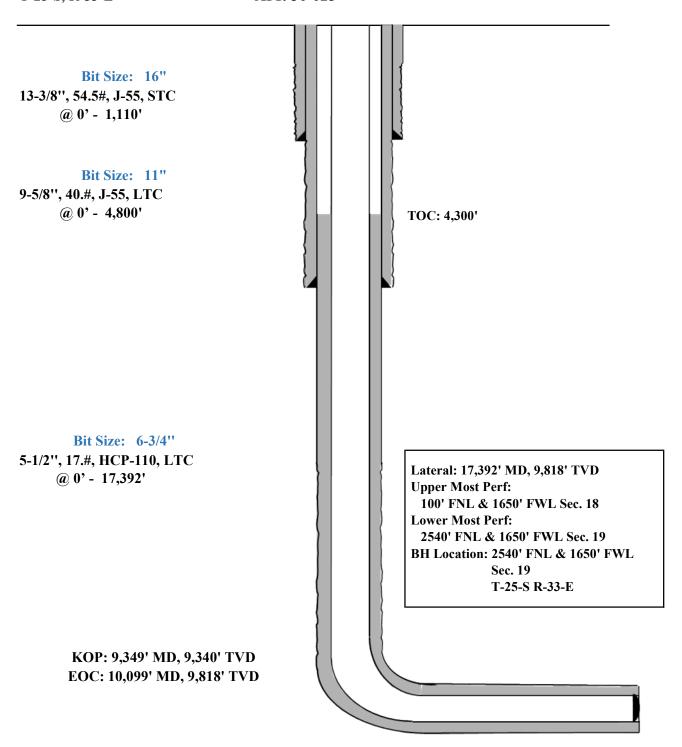
With horizontal flowing and gas lifted wells an end of tubing depth placed at or slightly above KOP is a conservative way to ensure the tubing stays clean from debris, plugging, and allows for fewer well interventions post offset completion. The deeper the tubulars are run into the curve, the higher the probability is that the tubing will become stuck in sand and or well debris as the well produces over time. An additional consideration for EOT placement during artificial lift installations is avoiding the high dog leg severity and inclinations found in the curve section of the wellbore to help improve reliability and performance. Dog leg severity and inclinations tend not to hamper gas lifted or flowing wells, but they do effect other forms of artificial lift like rod pump or ESP (electric submersible pump). Keeping the EOT above KOP is an industry best practice for those respective forms of artificial lift.



201' FNL Revised Wellbore A: KB: 3512' 1359' FWL GL: 3487'

Section 18

T-25-S, R-33-E API: 30-025-****





Revised Permit Information 05/10/2023:

Well Name: Icy 7 Fed 512H

Location: SHL: 201' FNL & 1359' FWL, Section 18, T-25-S, R-33-E, Lea Co., N.M.

BHL: 2540' FNL & 1650' FWL, Section 19, T-25-S, R-33-E, Lea Co., N.M.

Casing Program B:

| Hole | Interval MD | | Interval TVD | | Csg | | | |
|---------|--------------------|---------|--------------|---------|---------|--------|---------|--------|
| Size | From (ft) | To (ft) | From (ft) | To (ft) | OD | Weight | Grade | Conn |
| 13-1/2" | 0 | 1,110 | 0 | 1,110 | 10-3/4" | 40.5# | J-55 | STC |
| 9-7/8" | 0 | 4,009 | 0 | 4,000 | 8-5/8" | 32# | J-55 | BTC-SC |
| 9-7/8" | 4,009 | 4,809 | 4,000 | 4,800 | 8-5/8" | 32# | P110-EC | BTC-SC |
| 6-3/4" | 0 | 17,392 | 0 | 9,818 | 5-1/2" | 17# | HCP-110 | LTC |

Cementing Program:

| | Cementing 110grunn | | | | | | | | | |
|--------------------|--------------------|------------|---------------|---|--|--|--|--|--|--|
| Depth | No. Sacks | Wt. ppg | Yld Ft3/sk | Slurry Description | | | | | | |
| 1,110' 10-3/4'' | 370 | 13.5 | 1.73 | Lead: Class C + 4.0% Bentonite Gel + 0.5% CaCl2 + 0.25 lb/sk Cello- Flake (TOC @ Surface) | | | | | | |
| | 110 | 14.8 | 1.34 | Tail: Class C + 0.6% FL-62 + 0.25 lb/sk Cello-Flake + 0.2% Sodium Metasilicate (TOC @ 910') | | | | | | |
| 4,800' 8-5/8" | 320 | 12.7 | 2.22 | Lead: Class C + 10% NaCl + 6% Bentonite Gel + 3% MagOx (TOC @ Surface) | | | | | | |
| | 100 | 14.8 | 1.32 | Tail: Class C + 10% NaCL + 3% MagOx (TOC @ 3,840') | | | | | | |
| 17,392' 5-1/2'' | 510 | 10.5 | 3.21 | Lead: Class H + 0.4% Halad-344 + 0.35% HR-601 + 3% Microbond (TOC @ 4,300') | | | | | | |
| | 590 | 13.2 | 1.52 | Tail: Class H + 5% NEX-020 + 0.2% NAC-102 + 0.15% NAS-725 + 0.5% NFL-549 + 0.2% NFP-703 + 1% NBE-737 + 0.3% NRT-241 (TOC @ 9350') | | | | | | |



Variance is requested to waive the centralizer requirements for the 8-5/8" casing in the 9-7/8" hole size. An expansion additive will be utilized, in the cement slurry, for the entire length of the 9-7/8" hole interval to maximize cement bond and zonal isolation.

Variance is also requested to waive any centralizer requirements for the 5-1/2" casing in the 6-3/4" hole size. An expansion additive will be utilized, in the cement slurry, for the entire length of the 6-3/4" hole interval to maximize cement bond and zonal isolation.

EOG requests permission to allow deviation from the 0.422" annulus clearance requirement for the intermediate (salt) section from Onshore Order #2 under the following conditions:

- The variance is not applicable within the Potash Boundaries or Capitan Reef areas.
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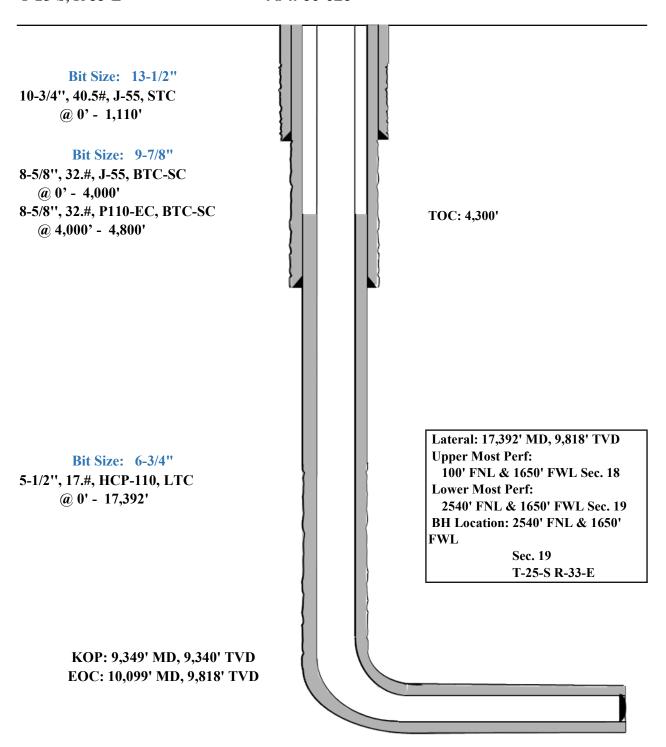
- Full BOPE test at first installation on the pad.
- Full BOPE test every 21 days per Onshore Order No. 2.
- Function test BOP elements per Onshore Order No. 2.
- Break testing BOP and BOPE coupled with batch drilling operations and option to offline cement and/or remediate (if needed) any surface or intermediate sections, according to attached offline cementing support documentation.
- After the well section is secured, the BOP will be disconnected from the wellhead and walked with the rig to another well on the pad.
- TA cap will also be installed per Wellhead vendor procedure and pressure inside the casing will be monitored via the valve on the TA cap as per standard batch drilling ops.
- See attached "EOG BLM Variance 3a -Offline Cement Intermediate Operational Procedure"



201' Revised Wellbore B: KB: 3512' GL: 3487'

Section 18

T-25-S, R-33-E API: 30-025-*****





GEOLOGIC NAME OF SURFACE FORMATION:

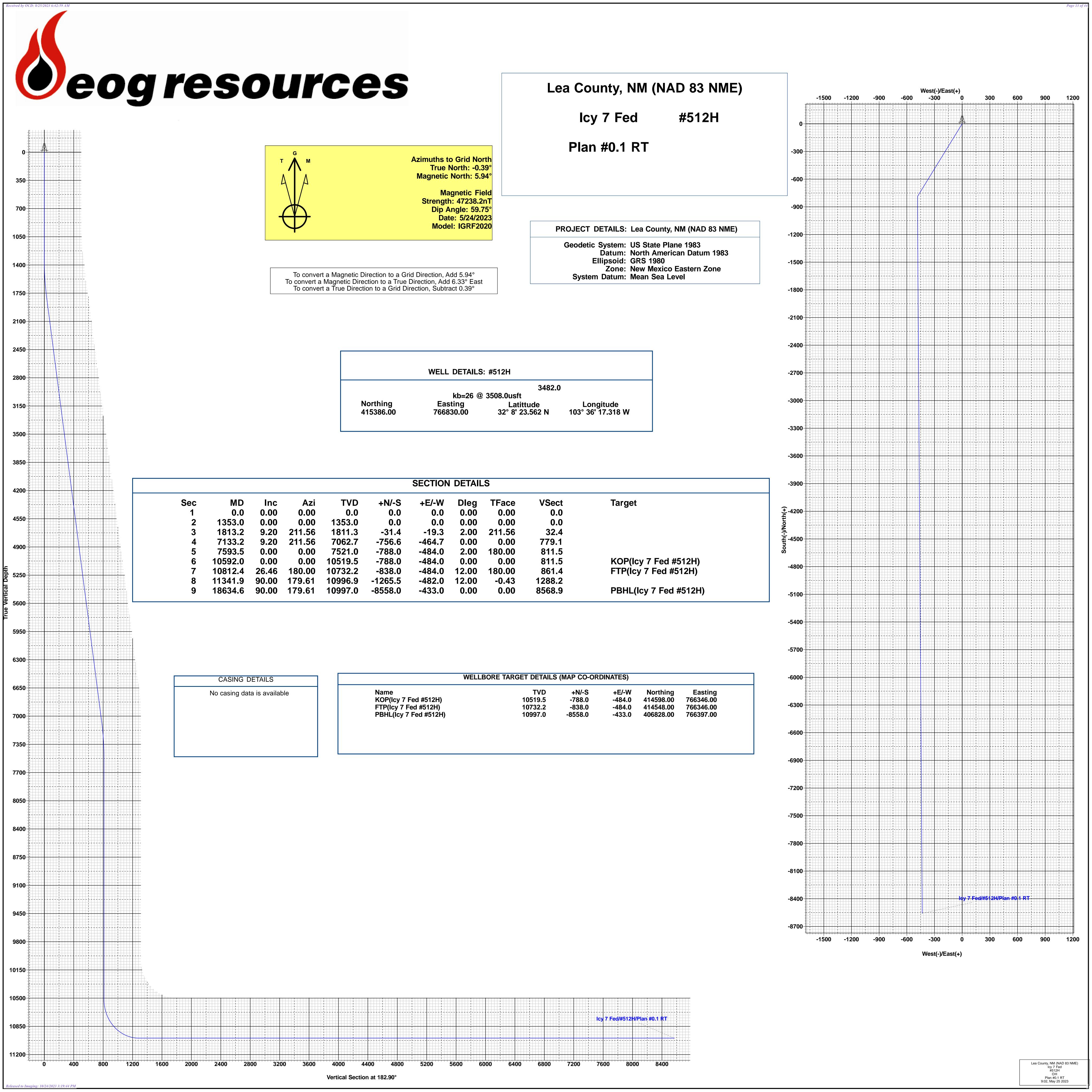
Permian

ESTIMATED TOPS OF IMPORTANT GEOLOGICAL MARKERS:

| Rustler | 1,006' |
|------------------------|---------|
| Tamarisk Anhydrite | 1,084' |
| Top of Salt | 1,353' |
| Base of Salt | 4,698' |
| Lamar | 4,937' |
| Bell Canyon | 4,963' |
| Cherry Canyon | 5,941' |
| Brushy Canyon | 7,521' |
| Bone Spring Lime | 9,067' |
| Leonard (Avalon) Shale | 9,165' |
| 1st Bone Spring Sand | 10,064' |
| 2nd Bone Spring Shale | 10,262' |
| 2nd Bone Spring Sand | 10,629' |
| 3rd Bone Spring Carb | 11,139' |
| 3rd Bone Spring Sand | 11,777' |
| TD | 9,818' |
| | |

ESTIMATED DEPTHS OF ANTICIPATED FRESH WATER, OIL OR GAS:

| Upper Permian Sands | 0- 400' | Fresh Water |
|------------------------|---------|-------------|
| Bell Canyon | 4,963' | Oil |
| Cherry Canyon | 5,941' | Oil |
| Brushy Canyon | 7,521' | Oil |
| Leonard (Avalon) Shale | 9,165' | Oil |
| 1st Bone Spring Sand | 10,064' | Oil |
| 2nd Bone Spring Shale | 10,262' | Oil |
| 2nd Bone Spring Sand | 10,629' | Oil |





Midland

Lea County, NM (NAD 83 NME) lcy 7 Fed #512H

OH

Plan: Plan #0.1 RT

Standard Planning Report

24 May, 2023



Database: Company:

Project:

PEDM Midland

Lea County, NM (NAD 83 NME)

Site: Icy 7 Fed Well: #512H Wellbore: ОН

Plan #0.1 RT Design:

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Well #512H

kb=26 @ 3508.0usft kb=26 @ 3508.0usft

Grid

Minimum Curvature

Project Lea County, NM (NAD 83 NME)

Map System: Geo Datum:

Map Zone:

US State Plane 1983 North American Datum 1983 New Mexico Eastern Zone

System Datum:

Mean Sea Level

Icy 7 Fed Site

Northing: 415,386.00 usft Site Position: Latitude: 32° 8' 23.562 N From: Мар Easting: 766,827.00 usft Longitude: 103° 36' 17.353 W

Position Uncertainty: 0.0 usft Slot Radius: 13-3/16 "

Well #512H

Well Position +N/-S 0.0 usft Northing: 415,386.00 usft Latitude: 32° 8' 23.562 N 766,830.00 usft +E/-W 0.0 usft Easting: Longitude: 103° 36' 17.318 W 3,482.0 usft

Position Uncertainty 0.0 usft Wellhead Elevation: usft **Ground Level:**

0.39 **Grid Convergence:**

ОН Wellbore

Declination Field Strength Magnetics **Model Name** Sample Date Dip Angle (°) (°) (nT) 47,238.22364898 IGRF2020 5/24/2023 6.33 59.75

Design Plan #0.1 RT

Audit Notes:

Version: Phase: PLAN Tie On Depth: 0.0

Vertical Section: Depth From (TVD) +N/-S +E/-W Direction (usft) (usft) (usft) (°) 182.90 0.0 0.0 0.0

Plan Survey Tool Program Date 5/24/2023

Depth From Depth To

(usft) (usft) Survey (Wellbore) **Tool Name** Remarks

18,632.6 Plan #0.1 RT (OH) EOG MWD+IFR1 0.0

MWD + IFR1



Database: PEDM Company: Midland

Project: Lea County, NM (NAD 83 NME)

 Site:
 lcy 7 Fed

 Well:
 #512H

 Wellbore:
 OH

 Design:
 Plan #0.1 RT

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Well #512H

kb=26 @ 3508.0usft kb=26 @ 3508.0usft

Grid

| Plan Sections | | | | | | | | | | |
|-----------------------------|--------------------|----------------|-----------------------------|-----------------|-----------------|-------------------------------|------------------------------|-----------------------------|------------|---------------------|
| Measured Depth (usft) | Inclination (°) | Azimuth (°) | Vertical Depth (usft) | +N/-S (usft) | +E/-W (usft) | Dogleg Rate (°/100usft) | Build Rate (°/100usft) | Turn Rate (°/100usft) | TFO (°) | Target |
| 0.0 | 0.00 | 0.00 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 1,353.0 | 0.00 | 0.00 | 1,353.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 1,813.2 | 9.20 | 211.56 | 1,811.3 | -31.4 | -19.3 | 2.00 | 2.00 | 0.00 | 211.56 | |
| 7,133.2 | 9.20 | 211.56 | 7,062.7 | -756.6 | -464.7 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 7,593.5 | 0.00 | 0.00 | 7,521.0 | -788.0 | -484.0 | 2.00 | -2.00 | 0.00 | 180.00 | |
| 10,592.0 | 0.00 | 0.00 | 10,519.5 | -788.0 | -484.0 | 0.00 | 0.00 | 0.00 | 0.00 | KOP(Icy 7 Fed #512F |
| 10,812.4 | 26.46 | 180.00 | 10,732.2 | -838.0 | -484.0 | 12.00 | 12.00 | 81.65 | 180.00 | FTP(Icy 7 Fed #512H |
| 11,341.9 | 90.00 | 179.61 | 10,996.9 | -1,265.5 | -482.0 | 12.00 | 12.00 | -0.07 | -0.43 | |
| 18,634.6 | 90.00 | 179.61 | 10,997.0 | -8,558.0 | -433.0 | 0.00 | 0.00 | 0.00 | 0.00 | PBHL(Icy 7 Fed #512 |



Database: PEDM Company: Midland

Project: Lea County, NM (NAD 83 NME)

 Site:
 lcy 7 Fed

 Well:
 #512H

 Wellbore:
 OH

 Position:
 Plan #0.1

Local Co-ordinate Reference:

TVD Reference:
MD Reference:
North Reference:

Survey Calculation Method:

Well #512H kb=26 @ 3508.0usft kb=26 @ 3508.0usft

Grid Minimum Curvature

| Planned Survey Measured Depth | Inclination | | | | | | | | |
|---------------------------------|-------------|----------------|-----------------------------|-----------------|-----------------|-------------------------------|-------------------------------|------------------------------|-----------------------------|
| | | | | | | | | | |
| (usft) | (°) | Azimuth (°) | Vertical Depth (usft) | +N/-S (usft) | +E/-W (usft) | Vertical Section (usft) | Dogleg Rate (°/100usft) | Build Rate (°/100usft) | Turn Rate (°/100usft) |
| 0.0 | 0.00 | 0.00 | 0.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 100.0 | 0.00 | 0.00 | 100.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 200.0 | 0.00 | 0.00 | 200.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 300.0 | 0.00 | 0.00 | 300.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 400.0 | 0.00 | 0.00 | 400.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 500.0 | 0.00 | 0.00 | 500.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 600.0 | 0.00 | 0.00 | 600.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 700.0 | 0.00 | 0.00 | 700.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 800.0 | 0.00 | 0.00 | 800.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 900.0 | 0.00 | 0.00 | 900.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 1,000.0 | 0.00 | 0.00 | 1,000.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 1,100.0 | 0.00 | 0.00 | 1,100.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 1,200.0 | 0.00 | 0.00 | 1,200.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 1,300.0 | 0.00 | 0.00 | 1,300.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 1,353.0 | 0.00 | 0.00 | 1,353.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 1,400.0 | 0.94 | 211.56 | 1,400.0 | -0.3 | -0.2 | 0.3 | 2.00 | 2.00 | 0.00 |
| 1,500.0 | 2.94 | 211.56 | 1,499.9 | -3.2 | -2.0 | 3.3 | 2.00 | 2.00 | 0.00 |
| 1,600.0 | 4.94 | 211.56 | 1,599.7 | -9.1 | -5.6 | 9.3 | 2.00 | 2.00 | 0.00 |
| 1,700.0 | 6.94 | 211.56 | 1,699.2 | -17.9 | -11.0 | 18.4 | 2.00 | 2.00 | 0.00 |
| 1,800.0 | 8.94 | 211.56 | 1,798.2 | -29.7 | -18.2 | 30.5 | 2.00 | 2.00 | 0.00 |
| 1,813.2 | 9.20 | 211.56 | 1,811.3 | -31.4 | -19.3 | 32.4 | 2.00 | 2.00 | 0.00 |
| 1,900.0 | 9.20 | 211.56 | 1,896.9 | -43.3 | -26.6 | 44.5 | 0.00 | 0.00 | 0.00 |
| 2,000.0 | 9.20 | 211.56 | 1,995.6 | -56.9 | -34.9 | 58.6 | 0.00 | 0.00 | 0.00 |
| 2,100.0 | 9.20 | 211.56 | 2,094.3 | -70.5 | -43.3 | 72.6 | 0.00 | 0.00 | 0.00 |
| 2,200.0 | 9.20 | 211.56 | 2,193.0 | -84.2 | -51.7 | 86.7 | 0.00 | 0.00 | 0.00 |
| 2,300.0 | 9.20 | 211.56 | 2,291.8 | -97.8 | -60.1 | 100.7 | 0.00 | 0.00 | 0.00 |
| 2,400.0 | 9.20 | 211.56 | 2,390.5 | -111.4 | -68.4 | 114.7 | 0.00 | 0.00 | 0.00 |
| 2,500.0 | 9.20 | 211.56 | 2,489.2 | -125.0 | -76.8 | 128.8 | 0.00 | 0.00 | 0.00 |
| 2,600.0 | 9.20 | 211.56 | 2,587.9 | -138.7 | -85.2 | 142.8 | 0.00 | 0.00 | 0.00 |
| 2,700.0 | 9.20 | 211.56 | 2,686.6 | -152.3 | -93.5 | 156.8 | 0.00 | 0.00 | 0.00 |
| 2,800.0 | 9.20 | 211.56 | 2,785.3 | -165.9 | -101.9 | 170.9 | 0.00 | 0.00 | 0.00 |
| 2,900.0 | 9.20 | 211.56 | 2,884.0 | -179.6 | -110.3 | 184.9 | 0.00 | 0.00 | 0.00 |
| 3,000.0 | 9.20 | 211.56 | 2,982.7 | -193.2 | -118.7 | 198.9 | 0.00 | 0.00 | 0.00 |
| 3,100.0 | 9.20 | 211.56 | 3,081.5 | -206.8 | -127.0 | 213.0 | 0.00 | 0.00 | 0.00 |
| 3,200.0 | 9.20 | 211.56 | 3,180.2 | -220.5 | -135.4 | 227.0 | 0.00 | 0.00 | 0.00 |
| 3,300.0 | 9.20 | 211.56 | 3,278.9 | -234.1 | -143.8 | 241.1 | 0.00 | 0.00 | 0.00 |
| 3,400.0 | 9.20 | 211.56 | 3,377.6 | -247.7 | -152.1 | 255.1 | 0.00 | 0.00 | 0.00 |
| 3,500.0 | 9.20 | 211.56 | 3,476.3 | -261.3 | -160.5 | 269.1 | 0.00 | 0.00 | 0.00 |
| 3,600.0 | 9.20 | 211.56 | 3,575.0 | -275.0 | -168.9 | 283.2 | 0.00 | 0.00 | 0.00 |
| 3,700.0 | 9.20 | 211.56 | 3,673.7 | -288.6 | -177.3 | 297.2 | 0.00 | 0.00 | 0.00 |
| 3,800.0 | 9.20 | 211.56 | 3,772.4 | -302.2 | -185.6 | 311.2 | 0.00 | 0.00 | 0.00 |
| 3,900.0 | 9.20 | 211.56 | 3,871.2 | -315.9 | -194.0 | 325.3 | 0.00 | 0.00 | 0.00 |
| 4,000.0 | 9.20 | 211.56 | 3,969.9 | -329.5 | -202.4 | 339.3 | 0.00 | 0.00 | 0.00 |
| 4,100.0 | 9.20 | 211.56 | 4,068.6 | -343.1 | -210.8 | 353.3 | 0.00 | 0.00 | 0.00 |
| 4,200.0 | 9.20 | 211.56 | 4,167.3 | -356.8 | -219.1 | 367.4 | 0.00 | 0.00 | 0.00 |
| 4,300.0 | 9.20 | 211.56 | 4,266.0 | -370.4 | -227.5 | 381.4 | 0.00 | 0.00 | 0.00 |
| 4,400.0 | 9.20 | 211.56 | 4,364.7 | -384.0 | -235.9 | 395.4 | 0.00 | 0.00 | 0.00 |
| 4,500.0 | 9.20 | 211.56 | 4,463.4 | -397.6 | -244.2 | 409.5 | 0.00 | 0.00 | 0.00 |
| 4,600.0 | 9.20 | 211.56 | 4,562.1 | -411.3 | -252.6 | 423.5 | 0.00 | 0.00 | 0.00 |
| 4,700.0 | 9.20 | 211.56 | 4,660.9 | -424.9 | -261.0 | 437.6 | 0.00 | 0.00 | 0.00 |
| 4,800.0 | 9.20 | 211.56 | 4,759.6 | -438.5 | -269.4 | 451.6 | 0.00 | 0.00 | 0.00 |
| 4,900.0 | 9.20 | 211.56 | 4,858.3 | -452.2 | -277.7 | 465.6 | 0.00 | 0.00 | 0.00 |
| 5,000.0 | 9.20 | 211.56 | 4,957.0 | -465.8 | -286.1 | 479.7 | 0.00 | 0.00 | 0.00 |
| 5,100.0 | 9.20 | 211.56 | 5,055.7 | -479.4 | -294.5 | 493.7 | 0.00 | 0.00 | 0.00 |



Database: PEDM Company: Midland

Project: Lea County, NM (NAD 83 NME)

 Site:
 Icy 7 Fed

 Well:
 #512H

 Wellbore:
 OH

 Design:
 Plan #0.1 RT

Local Co-ordinate Reference:

TVD Reference:
MD Reference:
North Reference:

Survey Calculation Method:

Well #512H

kb=26 @ 3508.0usft kb=26 @ 3508.0usft

Grid

| Design: | Plan #0.1 R1 | | | | | | | | |
|-----------------------------|--------------------|----------------|-----------------------------|-----------------|-----------------|-------------------------------|-------------------------------|------------------------------|-----------------------------|
| Planned Survey | | | | | | | | | |
| Measured Depth (usft) | Inclination (°) | Azimuth (°) | Vertical Depth (usft) | +N/-S (usft) | +E/-W (usft) | Vertical Section (usft) | Dogleg Rate (°/100usft) | Build Rate (°/100usft) | Turn Rate (°/100usft) |
| 5,200.0 | 9.20 | 211.56 | 5,154.4 | -493.1 | -302.8 | 507.7 | 0.00 | 0.00 | 0.00 |
| 5,300.0 | 9.20 | 211.56 | 5,253.1 | -506.7 | -311.2 | 521.8 | 0.00 | 0.00 | 0.00 |
| 5,400.0 | 9.20 | 211.56 | 5,351.8 | -520.3 | -319.6 | 535.8 | 0.00 | 0.00 | 0.00 |
| 5,500.0 | 9.20 | 211.56 | 5,450.5 | -534.0 | -328.0 | 549.8 | 0.00 | 0.00 | 0.00 |
| 5,600.0 | 9.20 | 211.56 | 5,549.3 | -547.6 | -336.3 | 563.9 | 0.00 | 0.00 | 0.00 |
| 5,700.0 | 9.20 | 211.56 | 5,648.0 | -561.2 | -344.7 | 577.9 | 0.00 | 0.00 | 0.00 |
| 5,800.0 | 9.20 | 211.56 | 5,746.7 | -574.8 | -353.1 | 592.0 | 0.00 | 0.00 | 0.00 |
| 5,900.0 | 9.20 | 211.56 | 5,845.4 | -588.5 | -361.4 | 606.0 | 0.00 | 0.00 | 0.00 |
| 6,000.0 | 9.20 | 211.56 | 5,944.1 | -602.1 | -369.8 | 620.0 | 0.00 | 0.00 | 0.00 |
| 6,100.0 | 9.20 | 211.56 | 6,042.8 | -615.7 | -378.2 | 634.1 | 0.00 | 0.00 | 0.00 |
| 6,200.0 | 9.20 | 211.56 | 6,141.5 | -629.4 | -386.6 | 648.1 | 0.00 | 0.00 | 0.00 |
| 6,300.0 | 9.20 | 211.56 | 6,240.2 | -643.0 | -394.9 | 662.1 | 0.00 | 0.00 | 0.00 |
| 6,400.0 | 9.20 | 211.56 | 6,339.0 | -656.6 | -403.3 | 676.2 | 0.00 | 0.00 | 0.00 |
| 6,500.0 | 9.20 | 211.56 | 6,437.7 | -670.3 | -411.7 | 690.2 | 0.00 | 0.00 | 0.00 |
| 6,600.0 | 9.20 | 211.56 | 6,536.4 | -683.9 | -420.1 | 704.2 | 0.00 | 0.00 | 0.00 |
| 6,700.0 | 9.20 | 211.56 | 6,635.1 | -697.5 | -428.4 | 718.3 | 0.00 | 0.00 | 0.00 |
| 6,800.0 | 9.20 | 211.56 | 6,733.8 | -711.1 | -436.8 | 732.3 | 0.00 | 0.00 | 0.00 |
| 6,900.0 | 9.20 | 211.56 | 6,832.5 | -724.8 | -445.2 | 746.3 | 0.00 | 0.00 | 0.00 |
| 7,000.0 | 9.20 | 211.56 | 6,931.2 | -738.4 | -453.5 | 760.4 | 0.00 | 0.00 | 0.00 |
| 7,100.0 | 9.20 | 211.56 | 7,029.9 | -752.0 | -461.9 | 774.4 | 0.00 | 0.00 | 0.00 |
| 7,133.2 | 9.20 | 211.56 | 7,062.7 | -756.6 | -464.7 | 779.1 | 0.00 | 0.00 | 0.00 |
| 7,200.0 | 7.87 | 211.56 | 7,128.8 | -765.0 | -469.9 | 787.8 | 2.00 | -2.00 | 0.00 |
| 7,300.0 | 5.87 | 211.56 | 7,228.1 | -775.2 | -476.1 | 798.3 | 2.00 | -2.00 | 0.00 |
| 7,400.0 | 3.87 | 211.56 | 7,327.7 | -782.4 | -480.6 | 805.7 | 2.00 | -2.00 | 0.00 |
| 7,500.0 | 1.87 | 211.56 | 7,427.6 | -786.7 | -483.2 | 810.1 | 2.00 | -2.00 | 0.00 |
| 7,593.5 | 0.00 | 0.00 | 7,521.0 | -788.0 | -484.0 | 811.5 | 2.00 | -2.00 | 0.00 |
| 7,600.0 | 0.00 | 0.00 | 7,527.5 | -788.0 | -484.0 | 811.5 | 0.00 | 0.00 | 0.00 |
| 7,700.0 | 0.00 | 0.00 | 7,627.5 | -788.0 | -484.0 | 811.5 | 0.00 | 0.00 | 0.00 |
| 7,800.0 | 0.00 | 0.00 | 7,727.5 | -788.0 | -484.0 | 811.5 | 0.00 | 0.00 | 0.00 |
| 7,900.0 | 0.00 | 0.00 | 7,827.5 | -788.0 | -484.0 | 811.5 | 0.00 | 0.00 | 0.00 |
| 8,000.0 | 0.00 | 0.00 | 7,927.5 | -788.0 | -484.0 | 811.5 | 0.00 | 0.00 | 0.00 |
| 8,100.0 | 0.00 | 0.00 | 8,027.5 | -788.0 | -484.0 | 811.5 | 0.00 | 0.00 | 0.00 |
| 8,200.0 | 0.00 | 0.00 | 8,127.5 | -788.0 | -484.0 | 811.5 | 0.00 | 0.00 | 0.00 |
| 8,300.0 | 0.00 | 0.00 | 8,227.5 | -788.0 | -484.0 | 811.5 | 0.00 | 0.00 | 0.00 |
| 8,400.0 | 0.00 | 0.00 | 8,327.5 | -788.0 | -484.0 | 811.5 | 0.00 | 0.00 | 0.00 |
| 8,500.0 | 0.00 | 0.00 | 8,427.5 | -788.0 | -484.0 | 811.5 | 0.00 | 0.00 | 0.00 |
| 8,600.0 | 0.00 | 0.00 | 8,527.5 | -788.0 | -484.0 | 811.5 | 0.00 | 0.00 | 0.00 |
| 8,700.0 | 0.00 | 0.00 | 8,627.5 | -788.0 | -484.0 | 811.5 | 0.00 | 0.00 | 0.00 |
| 8,800.0 | 0.00 | 0.00 | 8,727.5 | -788.0 | -484.0 | 811.5 | 0.00 | 0.00 | 0.00 |
| 8,900.0 | 0.00 | 0.00 | 8,827.5 | -788.0 | -484.0 | 811.5 | 0.00 | 0.00 | 0.00 |
| 9,000.0 | 0.00 | 0.00 | 8,927.5 | -788.0 | -484.0 | 811.5 | 0.00 | 0.00 | 0.00 |
| 9,100.0 | 0.00 | 0.00 | 9,027.5 | -788.0 | -484.0 | 811.5 | 0.00 | 0.00 | 0.00 |
| 9,200.0 | 0.00 | 0.00 | 9,127.5 | -788.0 | -484.0 | 811.5 | 0.00 | 0.00 | 0.00 |
| 9,300.0 | 0.00 | 0.00 | 9,227.5 | -788.0 | -484.0 | 811.5 | 0.00 | 0.00 | 0.00 |
| 9,400.0 | 0.00 | 0.00 | 9,327.5 | -788.0 | -484.0 | 811.5 | 0.00 | 0.00 | 0.00 |
| 9,500.0 | 0.00 | 0.00 | 9,427.5 | -788.0 | -484.0 | 811.5 | 0.00 | 0.00 | 0.00 |
| 9,600.0 | 0.00 | 0.00 | 9,527.5 | -788.0 | -484.0 | 811.5 | 0.00 | 0.00 | 0.00 |
| 9,700.0 | 0.00 | 0.00 | 9,627.5 | -788.0 | -484.0 | 811.5 | 0.00 | 0.00 | 0.00 |
| 9,800.0 | 0.00 | 0.00 | 9,727.5 | -788.0 | -484.0 | 811.5 | 0.00 | 0.00 | 0.00 |
| 9,900.0 | 0.00 | 0.00 | 9,827.5 | -788.0 | -484.0 | 811.5 | 0.00 | 0.00 | 0.00 |
| 10,000.0 | 0.00 | 0.00 | 9,927.5 | -788.0 | -484.0 | 811.5 | 0.00 | 0.00 | 0.00 |
| 10,100.0 | 0.00 | 0.00 | 10,027.5 | -788.0 | -484.0 | 811.5 | 0.00 | 0.00 | 0.00 |
| 10,200.0 | 0.00 | 0.00 | 10,127.5 | -788.0 | -484.0 | 811.5 | 0.00 | 0.00 | 0.00 |
| 10,300.0 | 0.00 | 0.00 | 10,227.5 | -788.0 | -484.0 | 811.5 | 0.00 | 0.00 | 0.00 |



Database: PEDM Company: Midland

Project: Lea County, NM (NAD 83 NME)

 Site:
 lcy 7 Fed

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MD Reference:
North Reference:

Survey Calculation Method:

Well #512H

kb=26 @ 3508.0usft kb=26 @ 3508.0usft

Grid

| Pales Pale Pales | Design: | | FIAII #U. I KI | | | | | | | | |
|--|---------|--------------|----------------|--------|----------|----------|--------|---------|--------------|------------|--------------|
| Measured Depth Inclination Azimuth Depth (usht) (ush | Diamas | d Cumrau | | | | | | | | | |
| Depth Inclination Cyst | Planne | a Survey | | | | | | | | | |
| 10,400.0 0.00 0.00 10,327.5 788.0 484.0 811.5 0.00 0.00 0.00 10,500.0 0.00 10,500.0 0.00 10,500.0 0.00 10,500.0 0.00 10,500.0 0.00 10,500.0 0.00 10,500.0 0.00 0.00 0.00 0.00 10,500.0 0.00 0.00 0.00 0.00 0.00 10,500.0 0.00 0.00 0.00 0.00 0.00 0.00 0. | | Depth | | | Depth | | | Section | Rate | Rate | Rate |
| 10,550.0 0.00 0.00 10,427.5 7-88.0 -484.0 811.5 0.00 0.00 0.00 0.00 | | (usit) | (*) | (*) | (usit) | (usπ) | (usπ) | (usit) | (/ loousit) | (7100usit) | (/ loousit) |
| 10.592.0 | | 10,400.0 | 0.00 | 0.00 | 10,327.5 | -788.0 | -484.0 | 811.5 | 0.00 | 0.00 | 0.00 |
| 10.592.0 | | | | | | -788.0 | -484.0 | | 0.00 | 0.00 | 0.00 |
| NOTE | | | | | | 700.0 | | | 0.00 | | 2.22 |
| 10,800.0 | | | | 0.00 | 10,519.5 | -788.0 | -484.0 | 811.5 | 0.00 | 0.00 | 0.00 |
| 10,825.0 3.97 180.00 10,872.5 -788.1 -484.0 812.6 12.00 12.00 0.00 10,675.0 9.97 180.00 10,675.2 -484.0 818.6 12.00 12.00 0.00 10,675.0 9.97 180.00 10,620.1 -795.2 -484.0 818.6 12.00 12.00 0.00 10,700.0 12.07 180.00 10,620.8 -806.4 -484.0 823.6 12.00 12.00 0.00 10,735.0 15.97 180.00 10,676.8 -806.4 -484.0 823.6 12.00 12.00 0.00 10,750.0 18.97 180.00 10,674.0 -832.6 -484.0 839.8 12.00 12.00 0.00 10,750.0 18.97 180.00 10,732.2 -838.0 -484.0 837.3 12.00 12.00 0.00 10,800.0 24.97 180.00 10,732.2 -838.0 -484.0 865.0 12.00 12.00 0.00 10,812.4 26.46 180.00 10,732.2 -838.0 -484.0 865.0 12.00 12.00 0.00 10,812.5 12.00 12.00 0.00 10,812.5 12.00 12.00 0.00 10,812.5 12.00 12.00 0.00 10,812.5 27.97 179.98 10,743.4 -843.8 -484.0 867.1 12.00 12.00 0.00 10,812.5 12.00 12.00 0.00 10,800.0 30.97 179.93 10,765.2 -865.1 -484.0 867.1 12.00 12.00 -0.19 10,850.0 30.97 179.87 10,866.6 -884.0 -883.8 997.3 12.00 12.00 -0.11 10,950.0 42.97 179.82 10,844.9 -916.1 -483.9 997.3 12.00 12.00 -0.12 10,950.0 42.97 179.82 10,844.9 -916.1 -483.9 993.4 12.00 12.00 -0.00 10,950.0 42.97 179.82 10,844.9 -916.1 -483.9 993.4 12.00 12.00 -0.00 10,950.0 49.97 179.78 10,866.6 -892.0 -483.7 975.2 12.00 12.00 -0.00 11,050.0 54.97 179.78 10,866.6 -892.0 -483.7 975.2 12.00 12.00 -0.00 11,050.0 54.97 179.78 10,866.9 -921.0 -483.5 10,854.10 12.00 12.00 -0.00 11,050.0 54.97 179.78 10,866.9 -921.0 -483.5 10,854.10 12.00 12.00 -0.00 11,050.0 69.97 179.73 10,866.9 -921.0 -483.5 10,854.10 12.00 12.00 -0.00 11,050.0 69.97 179.78 10,866.9 -921.0 -483.5 10,854.10 12.00 12.00 -0.00 11,050.0 69.97 179.79 10,986.9 -1.03. | | | • | | | | | | | | |
| 10,650,0 6.87 180,00 10,677,4 .791,5 .484,0 815,0 12,00 12,00 0,00 | | , | | | | | | | | | |
| 10,675.0 9.97 180.00 10,602.1 7.795.2 484.0 818.6 12.00 12.00 0.00 10,775.0 15.97 180.00 10,650.8 806.4 444.0 828.8 12.00 12.00 0.00 10,750.0 18.97 180.00 10,650.8 806.4 444.0 828.8 12.00 12.00 0.00 10,750.0 18.97 180.00 10,674.7 813.9 484.0 837.3 12.00 12.00 0.00 10,750.0 18.97 180.00 10,721.0 822.7 484.0 846.1 12.00 12.00 0.00 10,800.0 24.97 180.00 10,721.0 822.7 484.0 846.1 12.00 12.00 0.00 10,800.0 24.97 180.00 10,721.0 823.6 484.0 866.0 12.00 12.00 0.00 10,802.5 27.97 179.98 10,743.4 843.8 484.0 867.1 12.00 12.00 0.00 10,855.0 30.97 179.93 10,765.2 866.1 484.0 867.1 12.00 12.00 0.01 10,855.0 30.97 179.83 10,765.2 866.1 484.0 867.1 12.00 12.00 0.01 10,950.0 36.97 179.84 10,825.0 889.5 483.9 907.3 12.00 12.00 0.01 10,950.0 42.97 179.82 10,844.9 916.1 483.9 907.3 12.00 12.00 0.01 10,950.0 42.97 179.82 10,844.9 916.1 483.9 938.4 12.00 12.00 0.00 10,975.0 48.97 179.78 10,876.6 992.0 483.7 975.2 12.00 12.00 0.00 10,975.0 54.97 179.78 10,876.6 992.0 483.7 975.2 12.00 12.00 0.00 11,050.0 64.97 179.78 10,876.6 991.0 483.7 975.2 12.00 12.00 0.00 11,050.0 64.97 179.78 10,876.6 991.0 483.7 975.2 12.00 12.00 0.00 11,050.0 64.97 179.78 10,876.6 991.0 483.7 975.2 12.00 12.00 0.00 11,150.0 66.97 179.78 10,876.6 991.0 483.8 483.4 1,056.8 12.00 12.00 0.00 11,150.0 66.97 179.78 10,876.6 991.0 483.3 1,114.5 12.00 12.00 0.00 11,150.0 66.97 179.78 10,986.9 1,078.6 483.1 1,101.7 12.00 12.00 0.00 11,150.0 66.97 179.78 10,986.9 1,078.6 483.1 1,101.7 12.00 12.00 0.00 11,150.0 66.97 179.76 10,986.9 1,078.6 483.1 1,101.7 12.00 12.00 0.00 0.00 11,150.0 10,000 179.61 10,98 | | | | | | | | | | | |
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| 10,725.0 15.97 180.00 10,650.8 -806.4 -484.0 828.8 12.00 12.00 0.00 10,775.0 18.97 180.00 10,671.7 -813.9 -484.0 846.1 12.00 12.00 0.00 10,800.0 24.97 180.00 10,721.0 -852.6 -484.0 846.1 12.00 12.00 0.00 10,812.4 26.46 180.00 10,732.2 -838.0 -484.0 861.4 12.00 12.00 0.00 10,812.4 26.46 180.00 10,732.2 -838.0 -484.0 861.4 12.00 12.00 0.00 10,812.4 26.46 180.00 10,732.2 -838.0 -484.0 861.4 12.00 12.00 0.00 10,855.0 27.97 179.98 10,743.4 -843.8 -484.0 867.1 12.00 12.00 -0.19 10,850.0 30.97 179.93 10,765.2 -866.1 -484.0 867.1 12.00 12.00 -0.14 10,900.0 36.97 179.87 10,806.6 -884.0 -483.9 907.3 12.00 12.00 -0.14 10,900.0 36.97 179.87 10,806.6 -884.0 -483.9 907.3 12.00 12.00 -0.12 10,955.0 39.97 179.87 10,806.6 -884.0 -483.9 907.3 12.00 12.00 -0.10 10,975.0 45.97 179.80 10,866.8 -933.6 -483.8 958.8 12.00 12.00 -0.00 10,975.0 45.97 179.80 10,866.8 -933.6 -483.8 956.8 12.00 12.00 -0.00 10,975.0 45.97 179.80 10,876.6 -962.0 -483.7 975.2 12.00 12.00 -0.00 11,005.0 44.97 179.78 10,876.6 -962.0 -483.7 975.2 12.00 12.00 -0.00 11,005.0 54.97 179.78 10,876.6 -962.0 -483.7 975.2 12.00 12.00 -0.00 11,005.0 54.97 179.76 10,876.6 -962.0 -483.7 975.2 12.00 12.00 -0.00 11,005.0 54.97 179.76 10,885.6 -971.3 -483.7 975.2 12.00 12.00 -0.00 11,005.0 54.97 179.76 10,885.6 -971.3 -483.7 175.6 12.00 12.00 -0.00 11,005.0 54.97 179.76 10,885.6 -971.3 -483.7 175.6 12.00 12.00 -0.00 11,005.0 54.97 179.76 10,985.0 -1,035.7 -483.3 1,073.0 12.00 12.00 -0.00 11,005.0 54.97 179.76 10,986.9 -1,035.7 -483.3 1,073.0 12.00 12.00 -0.00 11,005.0 11,005.0 13.97 179.76 10,986.9 -1,035.7 -483.3 1,073.0 12.0 | | 10 700 0 | 12 97 | 180 00 | 10 626 6 | -800.2 | -484 N | 823.6 | 12.00 | 12 00 | 0.00 |
| 10,750.0 18.97 180.00 10,674.7 813.9 484.0 887.3 12.00 12.00 0.00 10,775.0 21.97 180.00 10,688.1 822.7 484.0 866.0 12.00 12.00 0.00 10,800.0 24.97 180.00 10,721.0 832.6 484.0 866.0 12.00 12.00 0.00 10,812.4 26.46 180.00 10,732.2 838.0 484.0 861.4 12.00 12.00 0.00 10,812.4 26.46 180.00 10,732.2 838.0 484.0 861.4 12.00 12.00 0.00 10,812.4 26.46 180.00 10,732.2 838.0 484.0 867.1 12.00 12.00 -0.19 10,855.0 30.97 179.93 10,765.2 856.1 484.0 867.1 12.00 12.00 -0.17 10,875.0 33.97 179.93 10,765.2 869.5 484.0 862.8 12.00 12.00 -0.14 10,900.0 30.97 179.67 10,866.6 884.0 485.9 907.3 12.00 12.00 -0.14 10,905.0 42.97 179.67 10,866.6 884.0 485.9 907.3 12.00 12.00 -0.10 10,975.0 45.97 179.82 10,844.9 -916.1 483.9 932.4 12.00 12.00 -0.09 11,0975.0 45.97 179.86 10,862.8 -933.6 483.8 956.8 12.00 12.00 -0.08 11,000.0 48.97 179.78 10,879.6 -952.0 483.7 995.8 12.00 12.00 -0.07 11,025.0 51.97 179.75 10,910.4 -991.4 483.6 10.14 12.00 12.00 -0.07 11,025.0 51.97 179.75 10,910.4 -991.4 483.6 10.14 12.00 12.00 -0.07 11,025.0 57.97 179.75 10,910.4 -991.4 483.6 10.14 12.00 12.00 -0.06 11,107.0 69.97 179.76 10,862.8 -971.3 483.7 10,66.4 12.00 12.00 -0.06 11,107.0 69.97 179.76 10,985.9 -1,035.9 483.3 1,056.8 12.00 12.00 -0.06 11,107.0 69.97 179.75 10,946.5 -1,055.9 483.3 1,056.8 12.00 12.00 -0.06 11,107.0 69.97 179.76 10,985.9 -1,037.9 483.3 1,056.8 12.00 12.00 -0.05 11,125.0 69.97 179.68 10,985.9 -1,037.9 483.3 1,079.9 12.00 12.00 -0.05 11,125.0 69.97 179.68 10,985.9 -1,037.9 483.3 1,079.9 12.00 12.00 -0.05 11,125.0 69.97 179.68 10,985.9 -1,037.9 483.3 1,079.9 12.00 12.00 -0.05 11,125.0 | | | | | , | | | | | | |
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| FTPRICY 7 Fed #812H) 10.825.0 | | | | | | | | | | | |
| 10,825.0 27.97 179.93 10,743.4 -843.8 -494.0 879.4 12.00 12.00 -0.17 10,875.0 30.97 179.93 10,765.2 -866.1 -484.0 879.4 12.00 12.00 -0.17 10,875.0 33.97 179.87 10,806.6 -884.0 -483.9 907.3 12.00 12.00 -0.12 10,905.0 38.97 179.87 10,806.6 -884.0 -483.9 907.3 12.00 12.00 -0.12 10,905.0 38.97 179.84 10,826.2 -899.5 -483.9 922.8 12.00 12.00 -0.10 10,950.0 42.97 179.82 10,844.9 -916.1 -483.9 939.4 12.00 12.00 -0.09 10,975.0 45.97 179.80 10,862.8 -933.6 -483.8 958.6 12.00 12.00 -0.08 11,000.0 48.97 179.80 10,895.6 -971.3 -483.7 975.2 12.00 12.00 -0.08 11,000.0 48.97 179.76 10,895.6 -971.3 -483.7 975.2 12.00 12.00 -0.07 11,025.0 51.97 179.76 10,895.6 -971.3 -483.7 994.5 12.00 12.00 -0.07 11,025.0 51.97 179.75 10,910.4 -991.4 -483.6 1,014.5 12.00 12.00 -0.06 11,100.0 60.97 179.72 10,869.9 -10,337 483.4 10,668.8 12.00 12.00 -0.06 11,100.0 60.97 179.72 10,869.9 -10,337 483.4 10,668.8 12.00 12.00 -0.05 11,125.0 63.97 179.77 10,945.5 -1,095.9 483.3 1,079.0 12.00 12.00 -0.05 11,125.0 63.97 179.77 10,945.5 -1,095.9 483.3 1,079.0 12.00 12.00 -0.05 11,125.0 63.97 179.77 10,945.5 -1,095.9 483.3 1,079.0 12.00 12.00 -0.05 11,125.0 63.97 179.76 10,986.9 -1,037.6 483.1 1,101.7 12.00 12.00 -0.05 11,125.0 63.97 179.76 10,986.9 -1,037.6 483.1 1,101.7 12.00 12.00 -0.05 11,125.0 63.97 179.76 10,986.9 -1,125.6 482.9 1,148.6 12.00 12.00 -0.05 11,125.0 75.97 179.66 10,987.1 1,149.7 482.6 1,197.0 12.00 12.00 -0.04 11,125.0 75.97 179.66 10,987.1 1,149.7 482.6 1,197.0 12.00 12.00 -0.04 11,125.0 75.97 179.66 10,987.1 1,198.6 442.7 1,172.6 12.00 12.00 -0.04 11,125.0 75.97 179.66 10,987.1 1,198.6 442.7 1,172.6 12.00 12.00 -0.04 11,125.0 75.97 179.66 10,987.3 10,988.1 -1,174.1 482.6 1,197.0 12.00 12.00 -0.04 11,125.0 75.97 179.66 10,987.9 1,128.5 482.1 1,197.0 12.00 12.00 -0.04 11,125.0 75.97 179.66 10,989.9 1,123.5 482.1 1,197.0 12.00 12.00 -0.04 11,125.0 75.97 179.66 10,989.9 1,123.5 483.0 1,198.2 12.00 12.00 12.00 10.00 11,100.0 90.00 179.61 10,996.9 -1,233.5 480.3 1,486.2 0.00 0.00 0.00 0.00 11,100.0 90.00 179.61 10,996.9 -1,233.5 486.3 480.3 | | 10,812.4 | 26.46 | 180.00 | 10,732.2 | -838.0 | -484.0 | 861.4 | 12.00 | 12.00 | 0.00 |
| 10,850 0 30,97 179,93 10,765.2 -856.1 -484.0 82,8 12.00 12.00 -0.14 10,900.0 36,97 179,90 10,768.2 -859.5 -484.0 82,8 12.00 12.00 -0.14 10,900.0 36,97 179,87 10,806.6 -884.0 -483.9 907.3 12.00 12.00 -0.12 10,950.0 39,97 179,84 10,826.2 -889.5 -483.9 907.3 12.00 12.00 -0.12 10,950.0 42,97 179.82 10,844.9 -916.1 -483.9 934.4 12.00 12.00 -0.09 10,975.0 45,97 179.82 10,844.9 -916.1 -483.9 934.4 12.00 12.00 -0.09 11,0975.0 45,97 179.80 10,862.8 -933.6 -483.9 956.8 12.00 12.00 -0.08 11,000.0 48,97 179.78 10,876.6 -952.0 -483.7 952. 12.00 12.00 -0.07 11,025.0 51,97 179,76 10,895.6 -971.3 -483.7 994.5 12.00 12.00 -0.07 11,050.0 54,97 179,75 10,910.4 -991.4 -483.6 1,014.5 12.00 12.00 -0.06 11,075.0 57.97 179,73 10,924.2 -1.012.2 483.5 10,354.4 12.00 12.00 -0.06 11,1705.0 57.97 179,72 10,936.9 -1.033.7 -483.4 10,568.8 12.00 12.00 -0.05 11,150.0 66.97 179,72 10,936.9 -1.033.7 -483.4 10,568.8 12.00 12.00 -0.05 11,150.0 66.97 179,72 10,936.9 -1.035.9 483.1 1,101.7 12.00 12.00 -0.05 11,150.0 66.97 179,70 10,958.9 -1,078.6 -483.1 1,101.7 12.00 12.00 -0.05 11,150.0 66.97 179,70 10,958.9 -1,078.6 -483.1 1,101.7 12.00 12.00 -0.05 11,150.0 68.97 179.66 10,982.7 -1,149.7 -482.7 1,172.6 12.00 12.00 -0.04 11,225.0 75.97 179.66 10,982.7 -1,149.7 -482.7 1,172.6 12.00 12.00 -0.04 11,225.0 75.97 179.66 10,982.7 -1,149.7 -482.7 1,172.6 12.00 12.00 -0.04 11,255.0 75.97 179.66 10,982.7 -1,149.7 -482.7 1,172.6 12.00 12.00 -0.04 11,255.0 75.97 179.66 10,982.7 -1,149.7 -482.6 1,197.1 12.00 12.00 -0.04 11,255.0 75.97 179.66 10,982.7 -1,149.7 -482.6 1,197.1 12.00 12.00 -0.04 11,255.0 75.97 179.66 10,982.7 -1,149.7 -482.6 1,197.1 12.00 12.00 -0.04 11,255.0 75.97 179.66 10,982.7 -1,148.5 -482.1 12,113.0 12.00 12.00 -0.04 11,255.0 75.97 179.66 10,989.9 -1,223.5 -480.3 1,246.4 12.00 12.00 -0.04 11,341.9 90.00 179.61 10,996.9 -1,223.5 -480.3 1,545.8 0.00 0.00 0.00 0.00 11,500.0 90.00 179.61 10,996.9 -1,223.5 -480.3 1,545.8 0.00 0.00 0.00 0.00 0.00 11,900.0 90.00 179.61 10,996.9 -1,223.5 -476.9 2,045.0 0.00 0.00 0.00 0.00 12,200.0 90.00 179.61 10,997 | | FTP(Icy 7 Fe | d #512H) | | | | | | | | |
| 10,850 0 30,97 179,93 10,765.2 -856.1 -484.0 82,8 12.00 12.00 -0.14 10,900.0 36,97 179,90 10,768.2 -859.5 -484.0 82,8 12.00 12.00 -0.14 10,900.0 36,97 179,87 10,806.6 -884.0 -483.9 907.3 12.00 12.00 -0.12 10,950.0 39,97 179,84 10,826.2 -889.5 -483.9 907.3 12.00 12.00 -0.12 10,950.0 42,97 179.82 10,844.9 -916.1 -483.9 934.4 12.00 12.00 -0.09 10,975.0 45,97 179.82 10,844.9 -916.1 -483.9 934.4 12.00 12.00 -0.09 11,0975.0 45,97 179.80 10,862.8 -933.6 -483.9 956.8 12.00 12.00 -0.08 11,000.0 48,97 179.78 10,876.6 -952.0 -483.7 952. 12.00 12.00 -0.07 11,025.0 51,97 179,76 10,895.6 -971.3 -483.7 994.5 12.00 12.00 -0.07 11,050.0 54,97 179,75 10,910.4 -991.4 -483.6 1,014.5 12.00 12.00 -0.06 11,075.0 57.97 179,73 10,924.2 -1.012.2 483.5 10,354.4 12.00 12.00 -0.06 11,1705.0 57.97 179,72 10,936.9 -1.033.7 -483.4 10,568.8 12.00 12.00 -0.05 11,150.0 66.97 179,72 10,936.9 -1.033.7 -483.4 10,568.8 12.00 12.00 -0.05 11,150.0 66.97 179,72 10,936.9 -1.035.9 483.1 1,101.7 12.00 12.00 -0.05 11,150.0 66.97 179,70 10,958.9 -1,078.6 -483.1 1,101.7 12.00 12.00 -0.05 11,150.0 66.97 179,70 10,958.9 -1,078.6 -483.1 1,101.7 12.00 12.00 -0.05 11,150.0 68.97 179.66 10,982.7 -1,149.7 -482.7 1,172.6 12.00 12.00 -0.04 11,225.0 75.97 179.66 10,982.7 -1,149.7 -482.7 1,172.6 12.00 12.00 -0.04 11,225.0 75.97 179.66 10,982.7 -1,149.7 -482.7 1,172.6 12.00 12.00 -0.04 11,255.0 75.97 179.66 10,982.7 -1,149.7 -482.7 1,172.6 12.00 12.00 -0.04 11,255.0 75.97 179.66 10,982.7 -1,149.7 -482.6 1,197.1 12.00 12.00 -0.04 11,255.0 75.97 179.66 10,982.7 -1,149.7 -482.6 1,197.1 12.00 12.00 -0.04 11,255.0 75.97 179.66 10,982.7 -1,149.7 -482.6 1,197.1 12.00 12.00 -0.04 11,255.0 75.97 179.66 10,982.7 -1,148.5 -482.1 12,113.0 12.00 12.00 -0.04 11,255.0 75.97 179.66 10,989.9 -1,223.5 -480.3 1,246.4 12.00 12.00 -0.04 11,341.9 90.00 179.61 10,996.9 -1,223.5 -480.3 1,545.8 0.00 0.00 0.00 0.00 11,500.0 90.00 179.61 10,996.9 -1,223.5 -480.3 1,545.8 0.00 0.00 0.00 0.00 0.00 11,900.0 90.00 179.61 10,996.9 -1,223.5 -476.9 2,045.0 0.00 0.00 0.00 0.00 12,200.0 90.00 179.61 10,997 | | • • | • | 179.98 | 10,743.4 | -843.8 | -484.0 | 867.1 | 12.00 | 12.00 | -0.19 |
| 10,875.0 33.97 179.87 10,786.2 -889.5 -484.0 892.8 12.00 12.00 -0.14 | | | | | | | -484.0 | 879.4 | | | -0.17 |
| 10,900 36,97 179,87 10,806.6 -884.0 -483.9 907.3 12.00 12.00 -0.12 | | | | | | | | | | | |
| 10,925.0 39.97 179.84 10,826.2 -899.5 -483.9 922.8 12.00 12.00 -0.10 10,950.0 42.97 179.82 10,844.9 -916.1 483.9 939.4 12.00 12.00 -0.09 10,975.0 45.97 179.80 10,862.8 -933.6 -483.8 956.8 12.00 12.00 -0.08 11,000.0 48.97 179.78 10,879.6 -952.0 -483.7 975.2 12.00 12.00 -0.07 11,025.0 51.97 179.76 10,895.6 -952.0 -483.7 975.2 12.00 12.00 -0.07 11,050.0 54.97 179.75 10,910.4 -991.4 -483.6 1,014.5 12.00 12.00 -0.06 11,075.0 57.97 179.73 10,924.2 -1,012.2 -483.5 1,035.4 12.00 12.00 -0.06 11,075.0 57.97 179.73 10,924.2 -1,012.2 -483.5 1,035.4 12.00 12.00 -0.06 11,105.0 69.97 179.72 10,936.9 -1,033.7 483.4 10,56.8 12.00 12.00 -0.05 11,125.0 63.97 179.71 10,948.5 -1,055.9 483.3 1,079.0 12.00 12.00 -0.05 11,125.0 63.97 179.70 10,958.9 -1,078.6 483.1 1,101.7 12.00 12.00 -0.05 11,125.0 69.97 179.68 10,988.1 -1,101.9 483.0 1,124.9 12.00 12.00 -0.05 11,125.0 69.97 179.68 10,988.1 -1,101.9 483.0 1,124.9 12.00 12.00 -0.05 11,125.0 72.97 179.67 10,976.0 -1,125.6 482.9 1,148.6 12.00 12.00 -0.05 11,125.0 72.97 179.67 10,976.0 -1,125.6 482.9 1,148.6 12.00 12.00 -0.04 11,125.0 72.97 179.67 10,982.7 -1,149.7 482.7 1,172.6 12.00 12.00 -0.04 11,125.0 78.97 179.64 10,992.3 -1,198.7 482.4 1,221.6 12.00 12.00 -0.04 11,125.0 81.97 179.64 10,992.3 -1,198.7 482.4 1,221.6 12.00 12.00 -0.04 11,325.0 87.97 179.64 10,992.3 -1,198.7 482.4 1,221.6 12.00 12.00 -0.04 11,341.9 90.00 179.61 10,996.9 -1,223.5 481.6 1,346.2 0.00 0.00 0.00 0.00 179.61 10,996.9 -1,223.5 481.6 1,346.2 0.00 0.00 0.00 0.00 179.61 10,996.9 -1,223.5 476.9 1,485.3 0.00 0.00 0.00 0.00 179.61 10,996.9 -1,223.5 476.9 1,445.5 0.00 0.00 0.00 0.00 0.00 12,000 90.00 179.61 10,996.9 -1,223.5 476.9 1,445.5 0.00 0.00 0.00 0.00 0.00 12,000 90.00 179.61 10,996.9 -1,223.5 476.9 2,444.4 0.00 0.00 0.00 0.00 12,000 90.00 179.61 10,996.9 -1,223.5 476.9 2,444.9 0.00 0.00 0.00 0.00 12,000 90.00 179.61 10,997.0 -2,223.5 476.6 2,244.7 0.00 0.00 0.00 0.00 12,000 90.00 179.61 10,997.0 -2,223.5 476.9 2,444.4 0.00 0.00 0.00 0.00 12,000 90.00 179.61 10,997.0 -2,223.5 476.9 2,444.4 0.00 0.00 0.00 0.00 | | | | | | | | | | | |
| 10,950 | | | | | | | | | | | |
| 10,975 | | -, | | | , | | | | | | |
| 11,000.0 | | 10,950.0 | | 179.82 | 10,844.9 | -916.1 | -483.9 | 939.4 | 12.00 | | -0.09 |
| 11,025.0 51.97 179.76 10,895.6 -971.3 -483.7 994.5 12.00 12.00 -0.07 | | 10,975.0 | 45.97 | 179.80 | 10,862.8 | -933.6 | -483.8 | 956.8 | 12.00 | 12.00 | -0.08 |
| 11,050.0 54.97 179.75 10,910.4 -991.4 -483.6 1,014.5 12.00 12.00 -0.06 11,075.0 57.97 179.73 10,924.2 -1,012.2 -483.5 1,035.4 12.00 12.00 -0.06 11,1075.0 57.97 179.72 10,936.9 -1,033.7 -483.4 1,056.8 12.00 12.00 -0.06 11,125.0 63.97 179.72 10,936.9 -1,033.7 -483.4 1,056.8 12.00 12.00 -0.05 11,125.0 63.97 179.70 10,958.9 -1,078.6 -483.1 1,079.0 12.00 12.00 -0.05 11,150.0 66.97 179.70 10,958.9 -1,078.6 -483.1 1,101.7 12.00 12.00 -0.05 11,175.0 69.97 179.67 10,976.0 -1,125.6 -482.9 1,148.6 12.00 12.00 -0.05 11,200.0 72.97 179.66 10,982.7 -1,149.7 -482.7 1,172.6 12.00 12.00 -0.04 11,225.0 75.97 179.66 10,982.7 -1,149.7 -482.7 1,172.6 12.00 12.00 -0.04 11,275.0 81.97 179.64 10,992.3 -1,198.7 -482.4 1,221.6 12.00 12.00 -0.04 11,300.0 84.97 179.63 10,995.1 -1,223.6 -482.3 1,246.4 12.00 12.00 -0.04 11,325.0 87.97 179.65 10,998.6 -1,248.5 -482.1 1,271.3 12.00 12.00 -0.04 11,341.9 90.00 179.61 10,996.9 -1,233.5 -481.6 1,346.2 0.00 12.00 -0.04 11,400.0 90.00 179.61 10,996.9 -1,233.5 -481.6 1,346.2 0.00 0.00 0.00 11,500.0 90.00 179.61 10,996.9 -1,233.5 -481.6 1,346.2 0.00 0.00 0.00 0.00 11,500.0 90.00 179.61 10,996.9 -1,233.5 -481.6 1,346.2 0.00 0.00 0.00 0.00 11,500.0 90.00 179.61 10,996.9 -1,233.5 -481.6 1,845.7 0.00 0.00 0.00 0.00 11,500.0 90.00 179.61 10,996.9 -1,233.5 -481.6 1,845.7 0.00 0.00 0.00 0.00 11,500.0 90.00 179.61 10,996.9 -1,233.5 -480.3 1,545.8 0.00 0.00 0.00 0.00 11,500.0 90.00 179.61 10,996.9 -1,233.5 -478.6 1,645.7 0.00 0.00 0.00 0.00 11,500.0 90.00 179.61 10,996.9 -1,233.5 -478.6 1,645.7 0.00 0.00 0.00 0.00 11,500.0 90.00 179.61 10,996.9 -1,233.5 -478.6 1,645.7 0.00 0.00 0.00 0.00 11,500.0 90.00 179.61 10,996.9 -1,233.5 -478.6 1,645.7 0.00 0.00 0.00 0.00 11,500.0 90.00 179.61 10,996.9 -1,233.5 -478.6 1,645.7 0.00 0.00 0.00 0.00 12,200.0 90.00 179.61 10,997.0 -2,233.5 -478.6 1,645.7 0.00 0.00 0.00 0.00 0.00 12,200.0 90.00 179.61 10,997.0 -2,233.5 -478.6 1,945.2 0.00 0.00 0.00 0.00 0.00 12,200.0 90.00 179.61 10,997.0 -2,233.5 -478.6 1,945.2 0.00 0.00 0.00 0.00 0.00 12,200.0 90.00 179.61 10,997.0 -2,233.5 | | 11,000.0 | 48.97 | 179.78 | 10,879.6 | -952.0 | -483.7 | 975.2 | 12.00 | 12.00 | -0.07 |
| 11,075.0 | | 11,025.0 | 51.97 | 179.76 | 10,895.6 | -971.3 | -483.7 | 994.5 | 12.00 | 12.00 | -0.07 |
| 11,075.0 | | 11 050 0 | 54.07 | 170.75 | 10 010 4 | 001.4 | 102 6 | 1 014 5 | 12.00 | 12.00 | 0.06 |
| 11,100.0 | | | | | | | | | | | |
| 11,125.0 63.97 179.71 10,948.5 -1,056.9 -483.3 1,079.0 12.00 -0.05 11,150.0 66.97 179.08 10,958.9 -1,078.6 -483.1 1,101.7 12.00 12.00 -0.05 11,175.0 69.97 179.68 10,968.1 -1,101.9 -483.0 1,124.9 12.00 12.00 -0.05 11,200.0 72.97 179.66 10,982.7 -1,149.7 -482.9 1,148.6 12.00 12.00 -0.04 11,250.0 75.97 179.66 10,982.7 -1,149.7 -482.6 1,197.0 12.00 12.00 -0.04 11,250.0 75.97 179.64 10,992.3 -1,149.7 -482.4 1,220.0 12.00 -0.04 11,275.0 81.97 179.64 10,995.1 -1,223.6 -482.3 1,246.4 12.00 12.00 -0.04 11,300.0 84.97 179.62 10,996.9 -1,265.5 -482.3 1,246.4 12.00 12.00 -0.04 | | | | | | | | | | | |
| 11,150.0 66.97 179.70 10,958.9 -1,078.6 -483.1 1,101.7 12.00 12.00 -0.05 11,175.0 69.97 179.67 10,976.0 -1,125.6 -482.9 1,148.6 12.00 12.00 -0.04 11,200.0 72.97 179.66 10,982.7 -1,149.7 -482.9 1,148.6 12.00 12.00 -0.04 11,250.0 78.97 179.66 10,982.7 -1,149.7 -482.6 1,197.0 12.00 12.00 -0.04 11,250.0 78.97 179.65 10,988.1 -1,174.1 -482.6 1,197.0 12.00 12.00 -0.04 11,275.0 81.97 179.63 10,995.1 -1,223.6 -482.4 1,221.6 12.00 12.00 -0.04 11,300.0 84.97 179.62 10,996.9 -1,223.6 -482.3 1,246.4 12.00 12.00 -0.04 11,341.9 90.00 179.61 10,996.9 -1,265.5 -482.0 1,288.2 12.00 12.00 -0.04 11,500.0 90.00 179.61 10,996.9 <th></th> <td></td> | | | | | | | | | | | |
| 11,175.0 69.97 179.68 10,968.1 -1,101.9 -483.0 1,124.9 12.00 12.00 -0.05 11,200.0 72.97 179.67 10,976.0 -1,125.6 -482.9 1,148.6 12.00 12.00 -0.04 11,255.0 75.97 179.65 10,988.1 -1,174.1 -482.7 1,172.6 12.00 12.00 -0.04 11,255.0 78.97 179.65 10,988.1 -1,174.1 -482.6 1,197.0 12.00 12.00 -0.04 11,275.0 81.97 179.64 10,992.3 -1,198.7 -482.4 1,221.6 12.00 12.00 -0.04 11,300.0 84.97 179.63 10,995.1 -1,223.6 -482.3 1,246.4 12.00 12.00 -0.04 11,325.0 87.97 179.61 10,996.9 -1,248.5 -482.1 1,271.3 12.00 12.00 -0.04 11,340.0 90.00 179.61 10,996.9 -1,323.5 -481.6 1,346.2 12.00 | | | | | | | | | | | |
| 11,200.0 72.97 179.67 10,976.0 -1,125.6 -482.9 1,148.6 12.00 12.00 -0.04 11,250.0 75.97 179.66 10,982.7 -1,149.7 -482.7 1,172.6 12.00 12.00 -0.04 11,250.0 78.97 179.65 10,988.1 -1,174.1 -482.6 1,197.0 12.00 12.00 -0.04 11,275.0 81.97 179.64 10,992.3 -1,198.7 -482.4 1,221.6 12.00 12.00 -0.04 11,300.0 84.97 179.63 10,995.1 -1,223.6 -482.3 1,246.4 12.00 12.00 -0.04 11,325.0 87.97 179.62 10,996.9 -1,265.5 -482.1 1,271.3 12.00 12.00 -0.04 11,400.0 90.00 179.61 10,996.9 -1,323.5 -481.6 1,346.2 0.00 0.00 0.00 11,500.0 90.00 179.61 10,996.9 -1,523.5 -481.0 1,446.0 0.00 0.00 0.00 11,600.0 90.00 179.61 10,996.9 | | 11,150.0 | 66.97 | 179.70 | 10,958.9 | -1,078.6 | -483.1 | 1,101.7 | 12.00 | 12.00 | -0.05 |
| 11,200.0 72.97 179.67 10,976.0 -1,125.6 -482.9 1,148.6 12.00 12.00 -0.04 11,225.0 75.97 179.66 10,982.7 -1,149.7 -482.7 1,172.6 12.00 12.00 -0.04 11,250.0 78.97 179.65 10,988.1 -1,198.7 -482.4 1,197.0 12.00 12.00 -0.04 11,275.0 81.97 179.64 10,992.3 -1,198.7 -482.4 1,221.6 12.00 12.00 -0.04 11,300.0 84.97 179.63 10,995.1 -1,223.6 -482.3 1,246.4 12.00 12.00 -0.04 11,325.0 87.97 179.62 10,996.9 -1,248.5 -482.1 1,271.3 12.00 12.00 -0.04 11,341.9 90.00 179.61 10,996.9 -1,265.5 -482.0 1,282.2 12.00 12.00 -0.04 11,400.0 90.00 179.61 10,996.9 -1,233.5 -481.6 1,346.2 0.00 0.00 0.00 11,500.0 90.00 179.61 10,996.9 | | 11,175.0 | 69.97 | 179.68 | 10,968.1 | -1,101.9 | -483.0 | 1,124.9 | 12.00 | 12.00 | -0.05 |
| 11,225.0 75.97 179.66 10,982.7 -1,149.7 -482.7 1,172.6 12.00 12.00 -0.04 11,250.0 78.97 179.65 10,988.1 -1,174.1 -482.6 1,197.0 12.00 12.00 -0.04 11,250.0 81.97 179.64 10,992.3 -1,198.7 -482.4 1,221.6 12.00 12.00 -0.04 11,300.0 84.97 179.63 10,995.1 -1,223.6 -482.3 1,246.4 12.00 12.00 -0.04 11,325.0 87.97 179.62 10,996.6 -1,248.5 -482.1 1,271.3 12.00 12.00 -0.04 11,341.9 90.00 179.61 10,996.9 -1,265.5 -482.0 1,288.2 12.00 12.00 -0.04 11,500.0 90.00 179.61 10,996.9 -1,523.5 -481.6 1,346.2 0.00 0.00 0.00 11,600.0 90.00 179.61 10,996.9 -1,523.5 -480.3 1,545.8 0.00 0.00 0.00 11,700.0 90.00 179.61 10,996.9 | | | | | , | , | | | | | |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | | | | | | | | | |
| 11,275.0 81.97 179.64 10,992.3 -1,198.7 -482.4 1,221.6 12.00 12.00 -0.04 11,300.0 84.97 179.63 10,995.1 -1,223.6 -482.3 1,246.4 12.00 12.00 -0.04 11,325.0 87.97 179.62 10,996.9 -1,248.5 -482.1 1,271.3 12.00 12.00 -0.04 11,441.9 90.00 179.61 10,996.9 -1,265.5 -482.0 1,288.2 12.00 12.00 -0.04 11,400.0 90.00 179.61 10,996.9 -1,323.5 -481.6 1,346.2 0.00 0.00 0.00 0.00 11,500.0 90.00 179.61 10,996.9 -1,523.5 -481.0 1,446.0 0.00 0.00 0.00 11,600.0 90.00 179.61 10,996.9 -1,523.5 -480.3 1,545.8 0.00 0.00 0.00 11,700.0 90.00 179.61 10,996.9 -1,723.5 -478.6 1,645.7 0.00 0.00 0.00 11,900.0 90.00 179.61 10,9 | | | | | | , | | | | | |
| 11,300.0 84.97 179.63 10,995.1 -1,223.6 -482.3 1,246.4 12.00 12.00 -0.04 11,325.0 87.97 179.62 10,996.6 -1,248.5 -482.1 1,271.3 12.00 12.00 -0.04 11,341.9 90.00 179.61 10,996.9 -1,265.5 -482.0 1,288.2 12.00 12.00 -0.04 11,400.0 90.00 179.61 10,996.9 -1,323.5 -481.6 1,346.2 0.00 0.00 0.00 11,500.0 90.00 179.61 10,996.9 -1,523.5 -481.0 1,446.0 0.00 0.00 0.00 11,600.0 90.00 179.61 10,996.9 -1,523.5 -480.3 1,545.8 0.00 0.00 0.00 11,700.0 90.00 179.61 10,996.9 -1,623.5 -479.6 1,645.7 0.00 0.00 0.00 11,800.0 90.00 179.61 10,996.9 -1,823.5 -478.3 1,845.3 0.00 0.00 0.00 12,000.0 90.00 179.61 10,997.0 -2, | | | | | | | | | | | |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | | | | | | | | | |
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| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | | | | | | | | | |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | | | | | | | | | |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | 11,500.0 | 90.00 | 179.61 | 10,996.9 | -1,423.5 | -481.0 | 1,446.0 | 0.00 | 0.00 | 0.00 |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | 11 600 0 | 90 00 | 179 61 | 10 996 9 | -1 523 5 | -480.3 | 1 545 8 | 0.00 | 0.00 | 0.00 |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | | | | | | | | | |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | | | | | | | | | |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | | | | | | | | | |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | | | | | | | | | |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | 12,000.0 | | 179.01 | | | -411.0 | 1,940.2 | 0.00 | 0.00 | 0.00 |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | | | | | -476.9 | 2,045.0 | 0.00 | 0.00 | 0.00 |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | 12,200.0 | 90.00 | 179.61 | | | -476.2 | 2,144.9 | 0.00 | 0.00 | 0.00 |
| 12,400.0 90.00 179.61 10,997.0 -2,323.5 -474.9 2,344.5 0.00 0.00 0.00 12,500.0 90.00 179.61 10,997.0 -2,423.5 -474.2 2,444.4 0.00 0.00 0.00 12,600.0 90.00 179.61 10,997.0 -2,523.5 -473.6 2,544.2 0.00 0.00 0.00 12,700.0 90.00 179.61 10,997.0 -2,623.5 -472.9 2,644.0 0.00 0.00 0.00 12,800.0 90.00 179.61 10,997.0 -2,723.5 -472.2 2,743.9 0.00 0.00 0.00 12,900.0 90.00 179.61 10,997.0 -2,823.5 -471.5 2,843.7 0.00 0.00 0.00 | | 12,300.0 | 90.00 | 179.61 | 10,997.0 | | -475.6 | 2,244.7 | 0.00 | 0.00 | 0.00 |
| 12,500.0 90.00 179.61 10,997.0 -2,423.5 -474.2 2,444.4 0.00 0.00 0.00 12,600.0 90.00 179.61 10,997.0 -2,523.5 -473.6 2,544.2 0.00 0.00 0.00 12,700.0 90.00 179.61 10,997.0 -2,623.5 -472.9 2,644.0 0.00 0.00 0.00 12,800.0 90.00 179.61 10,997.0 -2,723.5 -472.2 2,743.9 0.00 0.00 0.00 12,900.0 90.00 179.61 10,997.0 -2,823.5 -471.5 2,843.7 0.00 0.00 0.00 | | 12,400.0 | 90.00 | 179.61 | 10,997.0 | | -474.9 | 2,344.5 | 0.00 | 0.00 | 0.00 |
| 12,600.0 90.00 179.61 10,997.0 -2,523.5 -473.6 2,544.2 0.00 0.00 0.00 12,700.0 90.00 179.61 10,997.0 -2,623.5 -472.9 2,644.0 0.00 0.00 0.00 12,800.0 90.00 179.61 10,997.0 -2,723.5 -472.2 2,743.9 0.00 0.00 0.00 12,900.0 90.00 179.61 10,997.0 -2,823.5 -471.5 2,843.7 0.00 0.00 0.00 | | | | | | | | | | | |
| 12,700.0 90.00 179.61 10,997.0 -2,623.5 -472.9 2,644.0 0.00 0.00 0.00 0.00 12,800.0 90.00 179.61 10,997.0 -2,723.5 -472.2 2,743.9 0.00 0.00 0.00 12,900.0 90.00 179.61 10,997.0 -2,823.5 -471.5 2,843.7 0.00 0.00 0.00 | | | | | | | | | | | |
| 12,800.0 90.00 179.61 10,997.0 -2,723.5 -472.2 2,743.9 0.00 0.00 0.00 12,900.0 90.00 179.61 10,997.0 -2,823.5 -471.5 2,843.7 0.00 0.00 0.00 | | | | | | | | | | | |
| 12,900.0 90.00 179.61 10,997.0 -2,823.5 -471.5 2,843.7 0.00 0.00 0.00 | | | | | | | | | | | |
| | | | | | | | | | | | |
| 13,000.0 90.00 179.61 10,997.0 -2,923.5 -470.9 2,943.5 0.00 0.00 0.00 | | | | | | | | | | | |
| | | 13,000.0 | 90.00 | 179.61 | 10,997.0 | -2,923.5 | -470.9 | 2,943.5 | 0.00 | 0.00 | 0.00 |



Database: PEDM Company: Midland

Project: Lea County, NM (NAD 83 NME)

 Site:
 Icy 7 Fed

 Well:
 #512H

 Wellbore:
 OH

 Design:
 Plan #0.1 RT

Local Co-ordinate Reference: TVD Reference:

MD Reference: North Reference:

Survey Calculation Method:

Well #512H

kb=26 @ 3508.0usft kb=26 @ 3508.0usft

Grid

| esign: | Plan #0.1 RT | | | | | | | | |
|-----------------------------|-----------------|------------------|-----------------------------|----------------------|------------------|-------------------------------|-------------------------------|------------------------------|-----------------------------|
| lanned Survey | | | | | | | | | |
| Measured Depth (usft) | Inclination (°) | Azimuth (°) | Vertical Depth (usft) | +N/-S (usft) | +E/-W (usft) | Vertical Section (usft) | Dogleg Rate (°/100usft) | Build Rate (°/100usft) | Turn Rate (°/100usft) |
| 13,100.0 | 90.00 | 179.61 | 10,997.0 | -3,023.5 | -470.2 | 3,043.4 | 0.00 | 0.00 | 0.00 |
| 13,200.0 | 90.00 | 179.61 | 10,997.0 | -3,123.5 | -469.5 | 3,143.2 | 0.00 | 0.00 | 0.00 |
| 13,300.0 | 90.00 | 179.61 | 10,997.0 | -3,223.5 | -468.9 | 3,243.0 | 0.00 | 0.00 | 0.00 |
| 13,400.0 | 90.00 | 179.61 | 10,997.0 | -3,323.5 | -468.2 | 3,342.9 | 0.00 | 0.00 | 0.00 |
| 13,500.0 | 90.00 | 179.61 | 10,997.0 | -3,423.5 | -467.5 | 3,442.7 | 0.00 | 0.00 | 0.00 |
| 13,600.0 | 90.00 | 179.61 | 10,997.0 | -3,523.5 | -466.8 | 3,542.6 | 0.00 | 0.00 | 0.00 |
| 13,700.0 | 90.00 | 179.61 | 10,997.0 | -3,623.5 | -466.2 | 3,642.4 | 0.00 | 0.00 | 0.00 |
| 13,800.0 | 90.00 | 179.61 | 10,997.0 | -3,723.5 | -465.5 | 3,742.2 | 0.00 | 0.00 | 0.00 |
| 13,900.0 | 90.00 | 179.61 | 10,997.0 | -3,823.5 | -464.8 | 3,842.1 | 0.00 | 0.00 | 0.00 |
| 14,000.0 | 90.00 | 179.61 | 10,997.0 | -3,923.5 | -464.1 | 3,941.9 | 0.00 | 0.00 | 0.00 |
| 14,100.0 | 90.00 | 179.61 | 10,997.0 | -4,023.5 | -463.5 | 4,041.7 | 0.00 | 0.00 | 0.00 |
| 14,200.0 | 90.00 | 179.61 | 10,997.0 | -4,123.5 | -462.8 | 4,141.6 | 0.00 | 0.00 | 0.00 |
| 14,200.0 | 90.00 | 179.61 | 10,997.0 | -4,123.5 -4,223.5 | -462.6 -462.1 | 4,141.6 | 0.00 | 0.00 | 0.00 |
| | | | 10,997.0 | | | | | | |
| 14,400.0 14,500.0 | 90.00 90.00 | 179.61 179.61 | 10,997.0 | -4,323.4 -4,423.4 | -461.5 -460.8 | 4,341.2 4,441.1 | 0.00 0.00 | 0.00 0.00 | 0.00 0.00 |
| | | | | , | | | | | |
| 14,600.0 | 90.00 | 179.61 | 10,997.0 | -4,523.4 | -460.1 | 4,540.9 | 0.00 | 0.00 | 0.00 |
| 14,700.0 | 90.00 | 179.61 | 10,997.0 | -4,623.4 | -459.4 | 4,640.8 | 0.00 | 0.00 | 0.00 |
| 14,800.0 | 90.00 | 179.61 | 10,997.0 | -4,723.4 | -458.8 | 4,740.6 | 0.00 | 0.00 | 0.00 |
| 14,900.0 | 90.00 | 179.61 | 10,997.0 | -4,823.4 | -458.1 | 4,840.4 | 0.00 | 0.00 | 0.00 |
| 15,000.0 | 90.00 | 179.61 | 10,997.0 | -4,923.4 | -457.4 | 4,940.3 | 0.00 | 0.00 | 0.00 |
| 15,100.0 | 90.00 | 179.61 | 10,997.0 | -5,023.4 | -456.8 | 5,040.1 | 0.00 | 0.00 | 0.00 |
| 15,200.0 | 90.00 | 179.61 | 10,997.0 | -5,123.4 | -456.1 | 5,139.9 | 0.00 | 0.00 | 0.00 |
| 15,300.0 | 90.00 | 179.61 | 10,997.0 | -5,223.4 | -455.4 | 5,239.8 | 0.00 | 0.00 | 0.00 |
| 15,400.0 | 90.00 | 179.61 | 10,997.0 | -5,323.4 | -454.7 | 5,339.6 | 0.00 | 0.00 | 0.00 |
| 15,500.0 | 90.00 | 179.61 | 10,997.0 | -5,423.4 | -454.1 | 5,439.4 | 0.00 | 0.00 | 0.00 |
| 15,600.0 | 90.00 | 179.61 | 10,997.0 | -5,523.4 | -453.4 | 5,539.3 | 0.00 | 0.00 | 0.00 |
| 15,700.0 | 90.00 | 179.61 | 10,997.0 | -5,623.4 | -452.7 | 5,639.1 | 0.00 | 0.00 | 0.00 |
| 15,800.0 | 90.00 | 179.61 | 10,997.0 | -5,723.4 | -452.1 | 5,738.9 | 0.00 | 0.00 | 0.00 |
| 15,900.0 | 90.00 | 179.61 | 10,997.0 | -5,823.4 | -451.4 | 5,838.8 | 0.00 | 0.00 | 0.00 |
| 16,000.0 | 90.00 | 179.61 | 10,997.0 | -5,923.4 | -450.7 | 5,938.6 | 0.00 | 0.00 | 0.00 |
| 16,100.0 | 90.00 | 179.61 | 10,997.0 | -6,023.4 | -450.0 | 6,038.5 | 0.00 | 0.00 | 0.00 |
| 16,200.0 | 90.00 | 179.61 | 10,997.0 | -6,123.4 | -449.4 | 6,138.3 | 0.00 | 0.00 | 0.00 |
| 16,300.0 | | 179.61 | 10,997.0 | -6,123.4 -6,223.4 | -449.4 -448.7 | | 0.00 | 0.00 | 0.00 |
| | 90.00 | | | | | 6,238.1 | | | |
| 16,400.0 16,500.0 | 90.00 90.00 | 179.61 179.61 | 10,997.0 10,997.0 | -6,323.4 -6,423.4 | -448.0 -447.3 | 6,338.0 6,437.8 | 0.00 0.00 | 0.00 0.00 | 0.00 0.00 |
| | | | | , | | | | | |
| 16,600.0 | 90.00 | 179.61 | 10,997.0 | -6,523.4 | -446.7 | 6,537.6 | 0.00 | 0.00 | 0.00 |
| 16,700.0 | 90.00 | 179.61 | 10,997.0 | -6,623.4 | -446.0 | 6,637.5 | 0.00 | 0.00 | 0.00 |
| 16,800.0 | 90.00 | 179.61 | 10,997.0 | -6,723.4 | -445.3 | 6,737.3 | 0.00 | 0.00 | 0.00 |
| 16,900.0 17,000.0 | 90.00 90.00 | 179.61 179.61 | 10,997.0 10,997.0 | -6,823.4 -6,923.4 | -444.7 -444.0 | 6,837.1 6,937.0 | 0.00 0.00 | 0.00 0.00 | 0.00 0.00 |
| | | | | | | | | | |
| 17,100.0 | 90.00 | 179.61 | 10,997.0 | -7,023.4 | -443.3 | 7,036.8 | 0.00 | 0.00 | 0.00 |
| 17,200.0 | 90.00 | 179.61 | 10,997.0 | -7,123.4 | -442.6 | 7,136.7 | 0.00 | 0.00 | 0.00 |
| 17,300.0 | 90.00 | 179.61 | 10,997.0 | -7,223.4 | -442.0 | 7,236.5 | 0.00 | 0.00 | 0.00 |
| 17,400.0 | 90.00 | 179.61 | 10,997.0 | -7,323.4 | -441.3 | 7,336.3 | 0.00 | 0.00 | 0.00 |
| 17,500.0 | 90.00 | 179.61 | 10,997.0 | -7,423.4 | -440.6 | 7,436.2 | 0.00 | 0.00 | 0.00 |
| 17,600.0 | 90.00 | 179.61 | 10,997.0 | -7,523.4 | -440.0 | 7,536.0 | 0.00 | 0.00 | 0.00 |
| 17,700.0 | 90.00 | 179.61 | 10,997.0 | -7,623.4 | -439.3 | 7,635.8 | 0.00 | 0.00 | 0.00 |
| 17,800.0 | 90.00 | 179.61 | 10,997.0 | -7,723.4 | -438.6 | 7,735.7 | 0.00 | 0.00 | 0.00 |
| 17,900.0 | 90.00 | 179.61 | 10,997.0 | -7,823.4 | -437.9 | 7,835.5 | 0.00 | 0.00 | 0.00 |
| 18,000.0 | 90.00 | 179.61 | 10,997.0 | -7,923.4 | -437.3 | 7,935.3 | 0.00 | 0.00 | 0.00 |
| 18,100.0 | 90.00 | 179.61 | 10,997.0 | -8,023.4 | -436.6 | 8,035.2 | 0.00 | 0.00 | 0.00 |
| 18,200.0 | 90.00 | 179.61 | 10,997.0 | -8,123.4 | -435.9 | 8,135.0 | 0.00 | 0.00 | 0.00 |
| 18,300.0 | 90.00 | 179.61 | 10,997.0 | -8,223.4 | -435.2 | 8,234.8 | 0.00 | 0.00 | 0.00 |
| 18,400.0 | 90.00 | 179.61 | 10,997.0 | -8,323.4 | -434.6 | 8,334.7 | 0.00 | 0.00 | 0.00 |



Database: PEDM Company: Midland

Project: Lea County, NM (NAD 83 NME)

 Site:
 lcy 7 Fed

 Well:
 #512H

 Wellbore:
 OH

 Design:
 Plan #0.1 RT

Local Co-ordinate Reference:

TVD Reference:
MD Reference:
North Reference:
Survey Calculation Method:

Well #512H kb=26 @ 3508.0usft kb=26 @ 3508.0usft

Grid

| Planned Survey | | | | | | | | | |
|-----------------------------|-----------------------|------------------|-----------------------------|----------------------|------------------|-------------------------------|-------------------------------|------------------------------|-----------------------------|
| Measured Depth (usft) | Inclination (°) | Azimuth (°) | Vertical Depth (usft) | +N/-S (usft) | +E/-W (usft) | Vertical Section (usft) | Dogleg Rate (°/100usft) | Build Rate (°/100usft) | Turn Rate (°/100usft) |
| 18,500.0 | 90.00 | 179.61 | 10,997.0 | -8,423.4 | -433.9 | 8,434.5 | 0.00 | 0.00 | 0.00 |
| 18,600.0 18,634.6 | 90.00 90.00 | 179.61 179.61 | 10,997.0 10,997.0 | -8,523.4 -8,558.0 | -433.2 -433.0 | 8,534.4 8,568.9 | 0.00 0.00 | 0.00 0.00 | 0.00 0.00 |
| PBHL(Icy 7 | PBHL(Icy 7 Fed #512H) | | | | | | | | |

| Design Targets | | | | | | | | | |
|--|------------------|-----------------|---------------|-----------------|-----------------|--------------------|-------------------|-----------------|-------------------|
| Target Name - hit/miss target - Shape | Dip Angle (°) | Dip Dir. (°) | TVD (usft) | +N/-S (usft) | +E/-W (usft) | Northing (usft) | Easting (usft) | Latitude | Longitude |
| KOP(Icy 7 Fed #512H) - plan hits target cel - Point | 0.00 nter | 0.00 | 10,519.5 | -788.0 | -484.0 | 414,598.00 | 766,346.00 | 32° 8′ 15.796 N | 103° 36' 23.009 W |
| FTP(Icy 7 Fed #512H) - plan hits target cer - Point | 0.00 nter | 0.00 | 10,732.2 | -838.0 | -484.0 | 414,548.00 | 766,346.00 | 32° 8′ 15.302 N | 103° 36' 23.013 W |
| PBHL(Icy 7 Fed #512H) - plan hits target cer - Point | | 0.00 | 10,997.0 | -8,558.0 | -433.0 | 406,828.00 | 766,397.00 | 32° 6′ 58.906 N | 103° 36' 23.025 W |

Received by OCD: 8/25/2023 6:42:59 AM



Salt Section Annular Clearance Variance Request

Daniel Moose

Current Design (Salt Strings)

0.422" Annular clearance requirement

- Casing collars shall have a minimum clearance of 0.422 inches on all sides in the hole/casing annulus, with recognition that variances can be granted for justified exceptions.
- 12.25" Hole x 9.625"40# J55/HCK55 LTC Casing
 - 1.3125" Clearance to casing OD
 - 0.8125" Clearance to coupling OD
- 9.875" Hole x 8.75" 38.5# P110 Sprint-SF Casing
 - 0.5625" Clearance to casing OD
 - 0.433" Clearance to coupling OD

Annular Clearance Variance Request

EOG request permission to allow deviation from the 0.422" annulus clearance requirement for the intermediate (salt) section from Onshore Order #2 under the following conditions:

- The variance is not applicable within the Potash Boundaries or Capitan Reef areas.
- Operator takes responsibility to get casing to set point in the event that the clearance causes stuck pipe issues

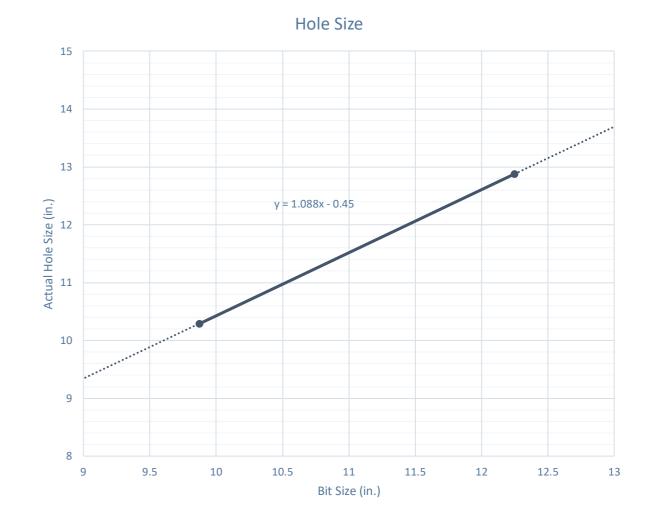
Volumetric Hole Size Calculation

Hole Size Calculations Off Cement Volumes

- Known volume of cement pumped
- Known volume of cement returned to surface
- Must not have had any losses
- Must have bumped plug

Average Hole Size

- 12.25" Hole
 - 12.88" Hole
 - 5.13% diameter increase
 - 10.52% area increase
 - 0.63" Average enlargement
 - 0.58" Median enlargement
 - 179 Well Count
- 9.875" Hole
 - 10.30" Hole
 - 4.24% diameter increase
 - 9.64% area increase
 - 0.42" Average enlargement
 - 0.46" Median enlargement
 - 11 Well Count

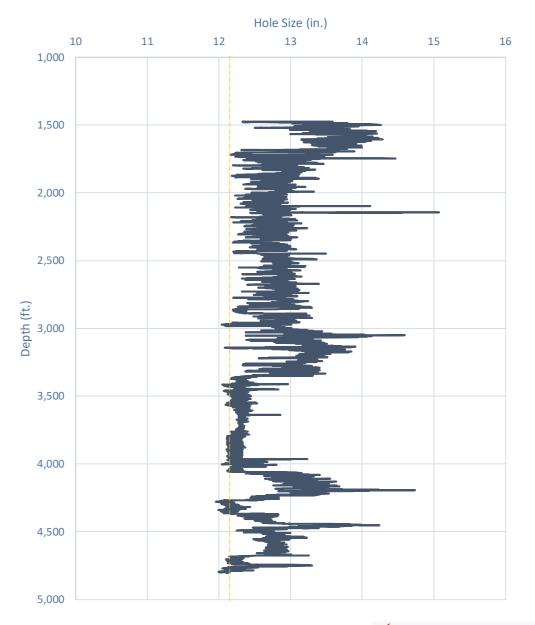


Modelo 10 Fed Com #501H

Caliper Hole Size (12.25")

Average Hole Size

- 12.25" Bit
 - 12.76" Hole
 - 4.14% diameter increase
 - 8.44% area increase
 - 0.51" Average enlargement
 - 0.52" Median enlargement
 - Brine

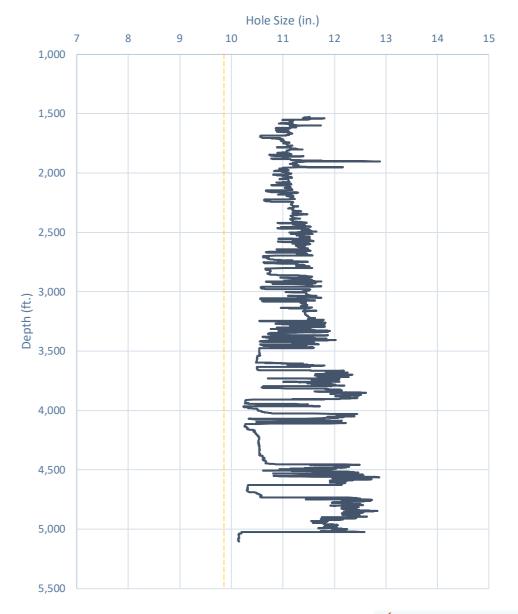


Caliper Hole Size (9.875")

Average Hole Size

- 9.875" Hole
 - 11.21" Hole
 - 13.54% diameter increase
 - 28.92% area increase
 - 1.33" Average enlargement
 - 1.30" Median enlargement
 - EnerLite

Whirling Wind 11 Fed Com #744H



Design A

Proposed 11" Hole with 9.625" 40# J55/HCK55 LTC Casing

- 11" Bit + 0.52" Average hole enlargement = 11.52" Hole Size
 - 0.9475" Clearance to casing OD

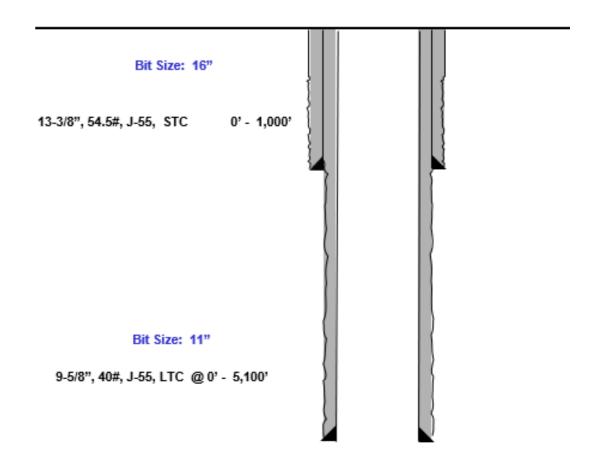
$$=\frac{11.52-9.625}{2}$$

• 0.4475" Clearance to coupling OD

$$=\frac{11.52-10.625}{2}$$

- Previous Shoe 13.375" 54.5# J55 STC
 - 0.995" Clearance to coupling OD (~1,200' overlap)

$$=\frac{12.615-10.625}{2}$$



Design B

Proposed 9.875" Hole with 8.625" 32# J55/P110 BTC-SC Casing

- 9.875" Bit + 0.42" Average hole enlargement = 10.295" Hole Size
 - 0.835" Clearance to casing OD

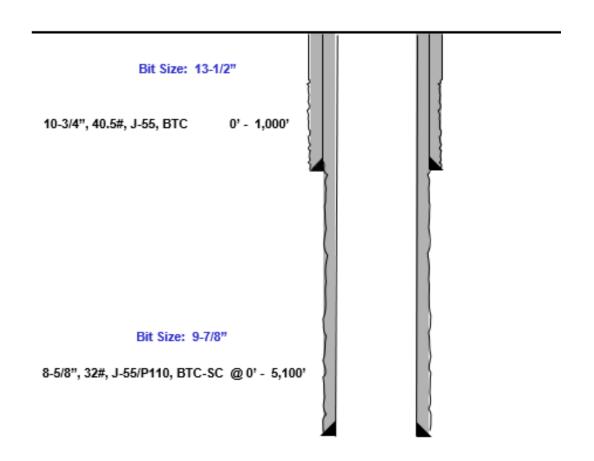
$$=\frac{10.295-8.625}{2}$$

• 0.585" Clearance to coupling OD

$$=\frac{10.295-9.125}{2}$$

- Previous Shoe 10.75" 40.5# J55 STC
 - 0.4625" Clearance to coupling OD (~1,200' overlap)

$$=\frac{10.05-9.125}{2}$$



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Nom. Pipe Body Area

Casing Spec Sheets

PERFORMANCE DATA

API LTC 9.625 in K55 HC 40.00 lbs/ft **Technical Data Sheet**

| Tubular Parameters | | | | | | | | |
|--------------------|--------|--------|------------------------------|-------|------|--|--|--|
| Size | 9.625 | in | Minimum Yield | 55 | ksi | | | |
| Nominal Weight | 40.00 | lbs/ft | Minimum Tensile | 95 | ksi | | | |
| Grade | K55 HC | | Yield Load | 629 | kips | | | |
| PE Weight | 38.94 | lbs/ft | Tensile Load | 1088 | kips | | | |
| Wall Thickness | 0.395 | in | Min. Internal Yield Pressure | 3,950 | psi | | | |
| Nominal ID | 8.835 | in | Collapse Pressure | 3600 | psi | | | |
| Drift Diameter | 8 750 | in | | • | 1 | | | |

in²

| Connection Parameters | | | | | | | |
|------------------------------|--------|-------|--|--|--|--|--|
| Connection OD | 10.625 | in | | | | | |
| Coupling Length | 10.500 | in | | | | | |
| Threads Per Inch | 8 | tpi | | | | | |
| Standoff Thread Turns | 3.50 | turns | | | | | |
| Make-Up Loss | 4.750 | in | | | | | |
| Min. Internal Yield Pressure | 3,950 | psi | | | | | |

11.454

Pipe Body and API Connections Performance Data

13.375 54.50/0.380 J55 PDF

New Search »

« Back to Previous List

| USC Metric |
|------------|
| |

| 6/8/2015 10:04:37 AM | | | | | |
|----------------------------------|--------|--------|-----|--------|----------|
| Mechanical Properties | Ptpe | втс | LTC | STC | |
| Minimum Yield Strength | 55,000 | - | - | - | psi |
| Maximum Yield Strength | 80,000 | - | - | - | psi |
| Minimum Tensile Strength | 75,000 | - | - | - | psi |
| Dimensions | Ptpe | втс | LTC | STC | |
| Outside Diameter | 13.375 | 14.375 | - | 14.375 | in. |
| Wall Thickness | 0.380 | - | - | - | in. |
| Inside Diameter | 12.615 | 12.615 | - | 12.615 | in. |
| Standard Drift | 12.459 | 12.459 | - | 12.459 | in. |
| Alternate Drift | _ | _ | - | - | in. |
| Nominal Linear Weight, T&C | 54.50 | - | - | - | lbs/ft |
| Plain End Weight | 52.79 | - | - | - | lbs/ft |
| Performance | Pipe | втс | LTC | STC | |
| Minimum Collapse Pressure | 1,130 | 1,130 | - | 1,130 | psi |
| Minimum Internal Yield Pressure | 2,740 | 2,740 | - | 2,740 | psi |
| Minimum Pipe Body Yield Strength | 853.00 | - | - | - | 1000 lbs |
| Joint Strength | - | 909 | - | 514 | 1000 lbs |
| Reference Length | - | 11,125 | - | 6,290 | ft |
| Make-Up Data | Ptpe | втс | LTC | STC | |
| Make-Up Loss | - | 4.81 | - | 3.50 | in. |
| Minimum Make-Up Torque | - | - | - | 3,860 | ft-lbs |
| Maximum Make-Up Torque | - | - | - | 6,430 | ft-lbs |

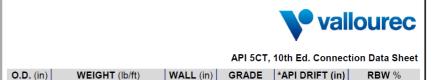
87.5

Casing Spec Sheets

Pipe Body and API Connections Performance Data

10.750 40.50/0.350 J55 PDF

New Search » « Back to Previous List USC Metric 6/8/2015 10:14:05 AM BTC LTC STC Ptpe **Mechanical Properties** Minimum Yield Strength 55,000 psi Maximum Yield Strength 80,000 Minimum Tensile Strength 75,000 psi BTC LTC Pipe STC 11.750 Outside Diamete 10.750 11.750 in. Wall Thickness 0.350 Inside Diameter 10.050 10.050 10.050 Standard Drift 9.894 9.894 in. Alternate Drift in. 40.50 Nominal Linear Weight, T&C lbs/ft 38.91 lbs/ft Plain End Weight Performance Ptpe BTC STC Minimum Collapse Pressure psi Minimum Internal Yield Pressure 3.130 3.130 3.130 629.00 1000 lbs Minimum Pipe Body Yield Strength 700 420 Joint Strength 1000 lbs Reference Length 11,522 6,915 BTC STC Make-Up Data Ptpe 4.81 Make-Up Loss 3.50 in. Minimum Make-Up Torque 3,150 ft-lbs



J55

0.352

| Material Properties (PE) | | | | | | |
|---------------------------|----|-----|--|--|--|--|
| Pipe | | | | | | |
| Minimum Yield Strength: | 55 | ksi | | | | |
| Maximum Yield Strength: | 80 | ksi | | | | |
| Minimum Tensile Strength: | 75 | ksi | | | | |
| Coupling | | | | | | |
| Minimum Yield Strength: | 55 | ksi | | | | |
| Maximum Yield Strength: | 80 | ksi | | | | |
| Minimum Tensile Strength: | 75 | ksi | | | | |

Nominal:

Plain End:

8.625

MADE IN USA

#Od

NTS

#0/M

7.875

DA

S2L2

S

VALLOUREC

5,250

ft-lbs

32.00

31.13

| Pipe Body Data (PE) | | | | | | | |
|-----------------------|--|--|--|--|--|--|--|
| Geometry | | | | | | | |
| 7.92 inch | | | | | | | |
| 9.149 in ² | | | | | | | |
| 7.875 inch | | | | | | | |
| Performance | | | | | | | |
| 503 kips | | | | | | | |
| 2,530 psi | | | | | | | |
| 3,930 psi | | | | | | | |
| | | | | | | | |

7.796

| API Connection Data Coupling OD: 9.625" | | | | | |
|---|----------|--------|--|--|--|
| STC Performance | | | | | |
| STC Internal Pressure: | 3,930 | psi | | | |
| STC Joint Strength: | 372 | kips | | | |
| LTC Performance | | | | | |
| LTC Internal Pressure: | 3,930 | psi | | | |
| LTC Joint Strength: | 417 | kips | | | |
| SC-BTC Performance - Cլ | olg OD = | 9.125" | | | |
| BTC Internal Pressure: | 3,930 | psi | | | |
| BTC Joint Strength: | 503 | kips | | | |

| API Connection Torque | | | | | | | |
|--|---------------------|-------|-------|------|-------|--|--|
| | STC Torque (ft-lbs) | | | | | | |
| Min: | 2,793 | Opti: | 3,724 | Max: | 4,655 | | |
| | | | | | | | |
| LTC Torque (ft-lbs) | | | | | | | |
| Min: | 3,130 | Opti: | 4,174 | Max: | 5,217 | | |
| | | | | | | | |
| BTC Torque (ft-lbs) | | | | | | | |
| follow API guidelines regarding positional make up | | | | | | | |
| | | | | | | | |

*Alt. Drift will be used unless API Drift is specified on order.

**If above API connections do not suit your needs, VAM® premium connections are available up to 100% of pipe body ratings.

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Maximum Make-Up Torque



Break-test BOP & Offline Cementing:

EOG Resources Inc. (EOG) respectfully requests a variance from the minimum standards for well control equipment testing of ECFR Title 43 Part 3172.6(b)(9)(iv) to allow a testing schedule of the blow out preventer (BOP) and blow out prevention equipment (BOPE) along with Batch Drilling & Offline cement operations to include the following:

- Full BOPE test at first installation on the pad.
- Full BOPE test every 21 days.
- This test will be conducted for 5M rated hole intervals only.
- Each rig requesting the break-test variance is capable of picking up the BOP without damaging components using winches, following API Standard 53, Well Control Equipment Systems for Drilling Wells (Fifth edition, December 2018, Annex C. Table C.4) which recognizes break testing as an acceptable practice.
- Function tests will be performed on the following BOP elements:
 - Annular **à** during each full BOPE test
 - Upper Pipe Rams **à** On trip ins where FIT required
 - Blind Rams **à** Every trip
 - Lower Pipe Rams à during each full BOPE test
- Break testing BOP and BOPE coupled with batch drilling operations and option to offline cement and/or remediate (if needed) any surface or intermediate sections, according to attached offline cementing support documentation.
- After the well section is secured, the BOP will be disconnected from the wellhead and walked with the rig to another well on the pad.
- TA cap will also be installed per Wellhead vendor procedure and pressure inside the
 casing will be monitored via the valve on the TA cap as per standard batch drilling
 ops.

Blind Rams

Roadside Kill

Test plug

Break Test Diagram (HCR valve)

Steps

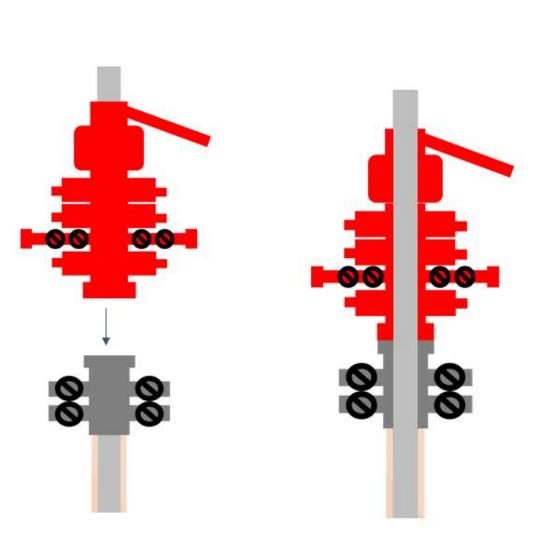
HCR

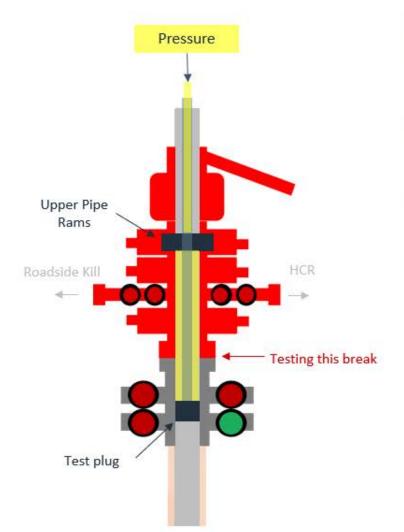
Testing this break

Pressure

- 1. Set plug in wellhead (lower barrier)
- 2. Close Blind Rams (upper barrier)
- 3. Close roadside kill
- 4. Open HCR (pressure application)
- Open wellhead valves below test plug to ensure if leak past test plug, pressure won't be applied to wellbore
- Tie BOP testers high pressure line to main choke manifold crown valve
- 7. Pressure up to test break
- Bleed test pressure from BOP testing unit

Break Test Diagram (Test Joint)





Steps

- Set plug in with test joint wellhead (lower barrier)
- 2. Close Upper Pipe Rams (upper barrier)
- 3. Close roadside kill
- 4. Close HCR
- Open wellhead valves below test plug to ensure if leak past test plug, pressure won't be applied to wellbore
- Tie BOP testers high pressure line to top of test joint
- 7. Pressure up to test break
- Bleed test pressure from BOP testing unit



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Cement Program

1. No changes to the cement program will take place for offline cementing.

Summarized Operational Procedure for Intermediate Casing

- 1. Run casing as per normal operations. While running casing, conduct negative pressure test and confirm integrity of the float equipment back pressure valves.
 - a. Float equipment is equipped with two back pressure valves rated to a minimum of 5,000 psi.
- 2. Land production casing on mandrel hanger through BOP.
 - a. If casing is unable to be landed with a mandrel hanger, then the casing will be cemented online.
- 3. Break circulation and confirm no restrictions.
 - a. Ensure no blockage of float equipment and appropriate annular returns.
 - b. Perform flow check to confirm well is static.
- 4. Set pack-off
 - a. If utilizing a fluted/ported mandrel hanger, ensure well is static on the annulus and inside the casing by filling the pipe with kill weight fluid, remove landing joint, and set annular packoff through BOP. Pressure test to 5,000 psi for 10 min.
 - b. If utilizing a solid mandrel hanger, ensure well is static on the annulus and inside the casing by filling the pipe with kill weight fluid. Pressure test seals to 5,000 psi for 10 min. Remove landing joint through BOP.
- 5. After confirmation of both annular barriers and the two casing barriers, install TA plug and pressure test to 5,000 psi for 10 min. Notify the BLM with intent to proceed with nipple down and offline cementing.
 - a. Minimum 4 hrs notice.
- 6. With the well secured and BLM notified, nipple down BOP and secure on hydraulic carrier or cradle.
 - a. Note, if any of the barriers fail to test, the BOP stack will not be nippled down until after the cement job has concluded and both lead and tail slurry have reached 500 psi.
- 7. Skid/Walk rig off current well.
- 8. Confirm well is static before removing TA Plug.
 - a. Cementing operations will not proceed until well is under control. (If well is not static, notify BLM and proceed to kill)
 - b. Casing outlet valves will provide access to both the casing ID and annulus. Rig or third party pump truck will kill well prior to cementing.
 - c. Well control plan can be seen in Section B, Well Control Procedures.
 - d. If need be, rig can be moved back over well and BOP nippled back up for any further remediation.



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- e. Diagram for rig positioning relative to offline cementing can be seen in Figure 4.
- 9. Rig up return lines to take returns from wellhead to pits and rig choke.
 - a. Test all connections and lines from wellhead to choke manifold to 5,000 psi high for 10 min.
 - If either test fails, perform corrections and retest before proceeding.
 - c. Return line schematics can be seen in Figure 3.
- 10. Remove TA Plug from the casing.
- 11. Install offline cement tool.
 - a. Current offline cement tool schematics can be seen in Figure 1 (Cameron) and Figure 2 (Cactus).
- 12. Rig up cement head and cementing lines.
 - a. Pressure test cement lines against cement head to 80% of casing burst for 10 min.
- 13. Break circulation on well to confirm no restrictions.
 - a. If gas is present on circulation, well will be shut in and returns rerouted through gas buster.
 - b. Max anticipated time before circulating with cement truck is 6 hrs.
- 14. Pump cement job as per plan.
 - a. At plug bump, test casing to 0.22 psi/ft or 1500 psi, whichever is greater.
 - b. If plug does not bump on calculated, shut down and wait 8 hrs or 500 psi compressive strength, whichever is greater before testing casing.
- 15. Confirm well is static and floats are holding after cement job.
 - a. With floats holding and backside static:
 - i. Remove cement head.
 - b. If floats are leaking:
 - i. Shut-in well and WOC (Wait on Cement) until tail slurry reaches 500 psi compressive strength and the casing is static prior to removing cement head.
 - c. If there is flow on the backside:
 - i. Shut in well and WOC until tail slurry reaches 500 psi compressive strength. Ensure that the casing is static prior to removing cement head.
- 16. Remove offline cement tool.
- 17. Install night cap with pressure gauge for monitoring.
- 18. Test night cap to 5,000 psi for 10 min.



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Example Well Control Plan Content

A. Well Control Component Table

The table below, which covers the cementing of the <u>5M MASP (Maximum Allowable Surface Pressure) portion of the well</u>, outlines the well control component rating in use. This table, combined with the mud program, documents that two barriers to flow can be maintained at all times, independent of the BOP nippled up to the wellhead.

Intermediate hole section, 5M requirement

| Component | RWP |
|--------------------------|-----|
| Pack-off | 10M |
| Casing Wellhead Valves | 10M |
| Annular Wellhead Valves | 5M |
| TA Plug | 10M |
| Float Valves | 5M |
| 2" 1502 Lo-Torque Valves | 15M |

B. Well Control Procedures

Well control procedures are specific to the rig equipment and the operation at the time the kick occurs. Below are the minimal high-level tasks prescribed to assure a proper shut-in while circulating and cementing through the Offline Cement Adapter.

General Procedure While Circulating

- 1. Sound alarm (alert crew).
- 2. Shut down pumps.
- 3. Shut-in Well (close valves to rig pits and open valve to rig choke line. Rig choke will already be in the closed position).
- 4. Confirm shut-in.
- 5. Notify tool pusher/company representative.

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- 6. Read and record the following:
 - a. SICP (Shut in Casing Pressure) and AP (Annular Pressure)
 - b. Pit gain
 - c. Time
 - d. Regroup and identify forward plan to continue circulating out kick via rig choke and mud/gas separator. Circulate and adjust mud density as needed to control well.

General Procedure While Cementing

- 1. Sound alarm (alert crew).
- 2. Shut down pumps.
- 3. Shut-in Well (close valves to rig pits and open valve to rig choke line. Rig choke will already be in the closed position).
- 4. Confirm shut-in.
- 5. Notify tool pusher/company representative.
- 6. Open rig choke and begin pumping again taking returns through choke manifold and mud/gas separator.
- 7. Continue to place cement until plug bumps.
- 8. At plug bump close rig choke and cement head.
- 9. Read and record the following
 - a. SICP and AP
 - b. Pit gain
 - c. Time
 - d. Shut-in annulus valves on wellhead

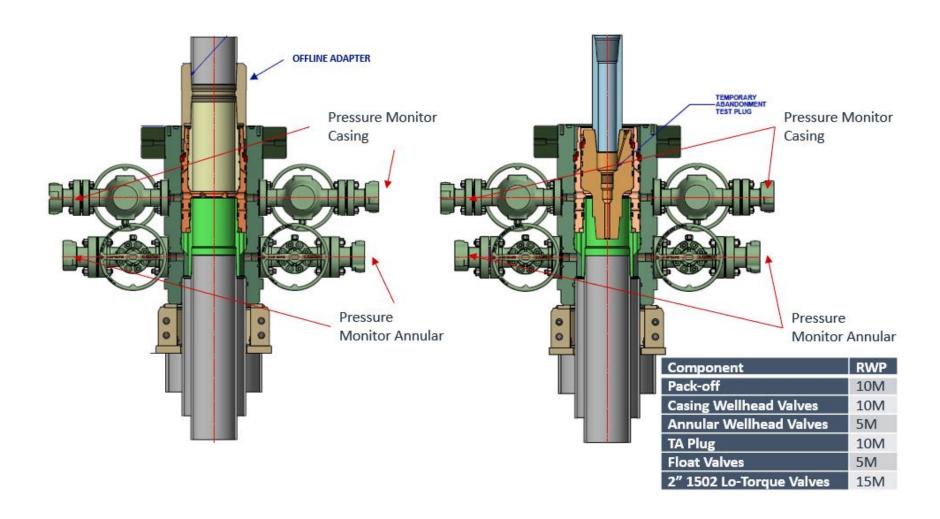
General Procedure After Cementing

- 1. Sound alarm (alert crew).
- 2. Shut-in Well (close valves to rig pits and open valve to rig choke line. Rig choke will already be in the closed position).
- 3. Confirm shut-in.
- 4. Notify tool pusher/company representative.
- 5. Read and record the following:
 - a. SICP and AP
 - b. Pit gain
 - c. Time
 - d. Shut-in annulus valves on wellhead



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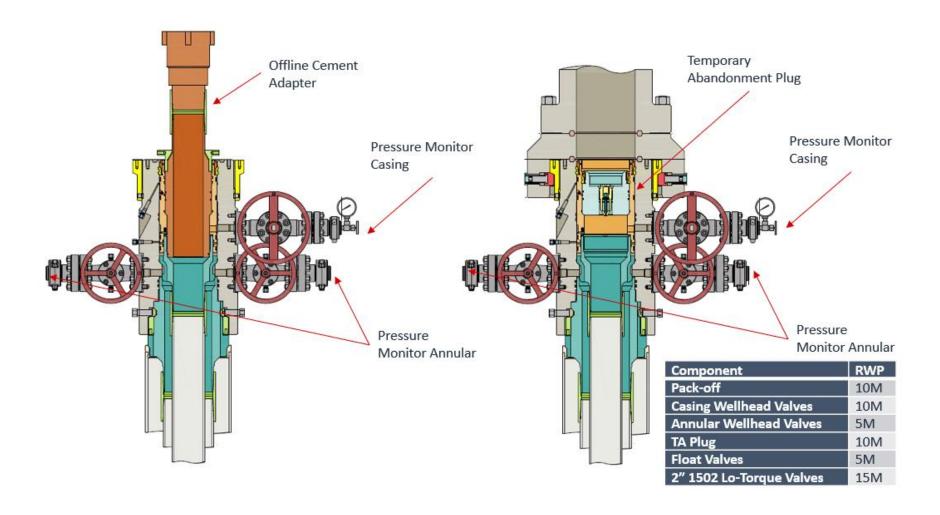
Figure 1: Cameron TA Plug and Offline Adapter Schematic





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Figure 2: Cactus TA Plug and Offline Adapter Schematic

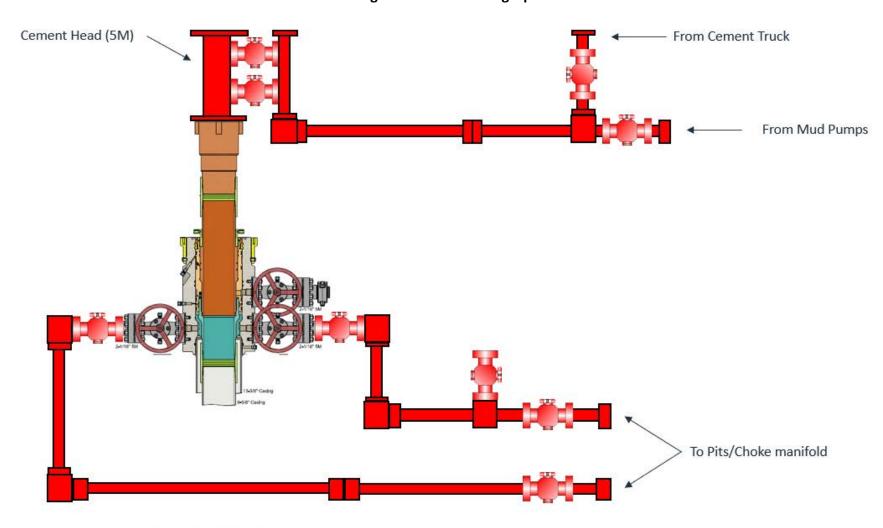


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Figure 3: Back Yard Rig Up



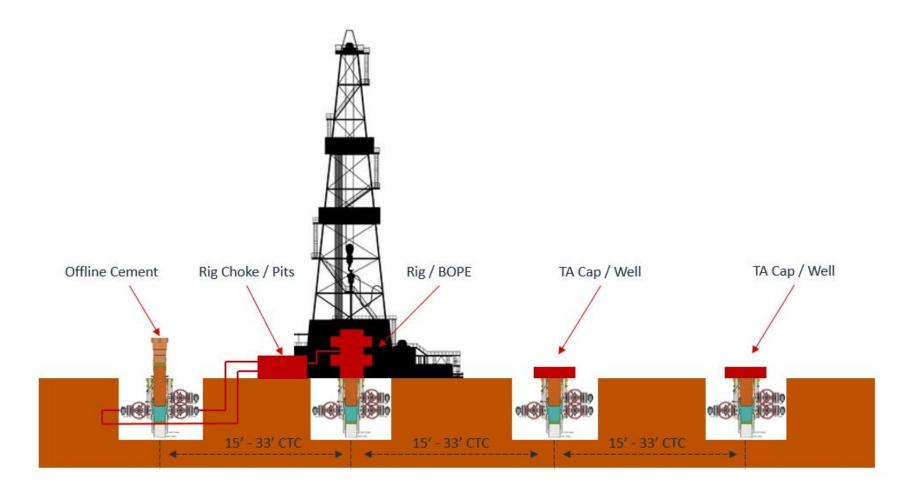
*** All Lines 10M rated working pressure

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Figure 4: Rig Placement Diagram



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District I
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811 S. First St., Artesia, NM 88210 Phone:(575) 748-1283 Fax:(575) 748-9720

District III 1000 Rio Brazos Rd., Aztec, NM 87410 Phone:(505) 334-6178 Fax:(505) 334-6170

1220 S. St Francis Dr., Santa Fe, NM 87505 Phone:(505) 476-3470 Fax:(505) 476-3462

State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division 1220 S. St Francis Dr. **Santa Fe, NM 87505**

CONDITIONS

Action 257575

CONDITIONS

| Operator: | OGRID: |
|-------------------|--------------------------------------|
| EOG RESOURCES INC | 7377 |
| P.O. Box 2267 | Action Number: |
| Midland, TX 79702 | 257575 |
| | Action Type: |
| | [C-103] NOI Change of Plans (C-103A) |

CONDITIONS

| Created By | Condition | Condition Date |
|---------------|-----------|----------------|
| pkautz | None | 10/24/2023 |