eceived by OCD: 5/5/2024 9:54:43 AM U.S. Department of the Interior		Sundry Print Report 02/05/2024
BUREAU OF LAND MANAGEMENT		2000-000-000-000-000-000-000-000-000-00
Well Name: POKER LAKE UNIT 30-19 BS	Well Location: T25S / R31E / SEC 30 / NENE /	County or Parish/State:
Well Number: 108H	<b>Type of Well:</b> CONVENTIONAL GAS WELL	Allottee or Tribe Name:
Lease Number: NMLC061634B	Unit or CA Name:	Unit or CA Number: NMNM71016X
<b>US Well Number:</b> 3001553541	Well Status: Approved Application for Permit to Drill	<b>Operator:</b> XTO PERMIAN OPERATING LLC

## **Notice of Intent**

Sundry ID: 2770586

-

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Type of Submission: Notice of Intent

Date Sundry Submitted: 01/18/2024

Date proposed operation will begin: 02/05/2024

Type of Action: APD Change Time Sundry Submitted: 01:17 6

**Procedure Description:** Pool Code Change, Pool Name Change, First and Last Take Point Changes, Bottomhole Location Change, Drilling Plan Change, Casing/Cement Change, & PPP. XTO Permian Operating, LCC. requests permission to make the following changes to the original APD: No Additional Surface Disturbance Pool Code: 97913 Pool Name: WILDCAT G-06 S253002O FTP: fr/2310'FNL & 330'FEL to 2115'FNL & 2535'FEL LTP: fr/100'FNL & 330'FEL to 2565'FSL & 2535'FEL BHL: fr/50'FNL & 330'FEL to 2664'FSL & 2535'FEL, Section 17-T25S-R31E PPP: 2646' FNL & 2543' FEL Additionally, XTO Permian Operating, LLC. respectfully requests permission to change production casing weight. Casing/Cement design per the attached drilling program. Attachments: C102 Drilling Program MBS Directional Plan BOP Variance Spud Variance

**NOI Attachments** 

**Procedure Description** 

PLU\_30\_19\_BS\_108H\_Sundry\_Attachments\_20240118135623.pdf

Received by OCD: 2/5/2024 9:54:43 AM Well Name: POKER LAKE UNIT 30-19 BS	Well Location: T25S / R31E / SEC 30 / NENE /	County or Parish/State: Page 2 of
Well Number: 108H	<b>Type of Well:</b> CONVENTIONAL GAS WELL	Allottee or Tribe Name:
Lease Number: NMLC061634B	Unit or CA Name:	Unit or CA Number: NMNM71016X
US Well Number: 3001553541	Well Status: Approved Application for Permit to Drill	<b>Operator:</b> XTO PERMIAN OPERATING LLC

# **Conditions of Approval**

#### Additional

Sec\_29\_25S\_31E\_NMP\_Sundry\_2770586\_Poker\_Lake\_Unit\_30\_19\_BS\_108H\_COAs\_20240126111948.pdf

## **Operator**

I certify that the foregoing is true and correct. Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction. Electronic submission of Sundry Notices through this system satisfies regulations requiring a

**Operator Electronic Signature: TERRA SEBASTIAN** 

Name: XTO PERMIAN OPERATING LLC

Title: Regulatory Advisor

Street Address: 6401 HOLIDAY HILL ROAD SUITE 200

City: MIDLAND

Phone: (432) 999-3107

Email address: TERRA.B.SEBASTIAN@EXXONMOBIL.COM

Field

Representative Name: Street Address:

State:

State: TX

Phone:

City:

Email address:

# **BLM Point of Contact**

BLM POC Name: CHRISTOPHER WALLS BLM POC Phone: 5752342234 Disposition: Approved Signature: Chris Walls Signed on: JAN 29, 2024 02:46 PM

BLM POC Title: Petroleum Engineer BLM POC Email Address: cwalls@blm.gov Disposition Date: 02/05/2024

Zip:

## Received by OCD: 2/5/2024 9:54:43 AM

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Form 3160-5 (June 2019)		UNITED STATE PARTMENT OF THE I EAU OF LAND MAN	FORM APPROVED OMB No. 1004-0137 Expires: October 31, 2021 5. Lease Serial No.				
Do not use	e this f	IOTICES AND REPO form for proposals t Use Form 3160-3 (A	6. If Indian, Allottee or Tribe Name				
	BMIT IN	TRIPLICATE - Other instru	uctions on page 2		7. If Unit of CA/Agree	ment, Name and/or No.	
1. Type of Well	Gas V	Vell Other			8. Well Name and No.		
2. Name of Operator					9. API Well No.		
3a. Address 3b			3b. Phone No. (include area code)		10. Field and Pool or Exploratory Area		
4. Location of Well (Footage,	Sec., T.,F	R.,M., or Survey Description)	)		11. Country or Parish, S	State	
	12. CHE	CK THE APPROPRIATE B	OX(ES) TO INDICATE NATURE	OF NOT	ICE, REPORT OR OTH	ER DATA	
TYPE OF SUBMISSIO	DN		TY	PE OF AC	CTION		
Notice of Intent		Acidize	Deepen Hydraulic Fracturing		duction (Start/Resume)	Water Shut-Off Well Integrity	
Subsequent Report		Casing Repair Change Plans	New Construction Plug and Abandon		complete nporarily Abandon	Other	
Final Abandonment No	otice	Convert to Injection	Plug Back	_	ter Disposal		
the proposal is to deepen d the Bond under which the completion of the involved	directiona work wil d operation ment No	Illy or recomplete horizontal be perfonned or provide thors. If the operation results in	ly, give subsurface locations and n e Bond No. on file with BLM/BIA n a multiple completion or recomp	neasured a Require letion in a	and true vertical depths of d subsequent reports mus a new interval, a Form 31	k and approximate duration thereof. If f all pertinent markers and zones. Attach t be filed within 30 days following 60-4 must be filed once testing has been the operator has detennined that the site	

14. I hereby certify that the foregoing is true and correct. Name ( <i>Printed/Typed</i> )		
T	itle	
Signature D	ate	
THE SPACE FOR FEDEF	RAL OR STATE OFICE US	SE
Approved by		
	Title	Date
Conditions of approval, if any, are attached. Approval of this notice does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon.		
Title 18 U.S.C Section 1001 and Title 43 U.S.C Section 1212, make it a crime for any p any false, fictitious or fraudulent statements or representations as to any matter within i		ake to any department or agency of the United States

(Instructions on page 2)

This form is designed for submitting proposals to perform certain well operations and reports of such operations when completed as indicated on Federal and Indian lands pursuant to applicable Federal law and regulations. Any necessary special instructions concerning the use of this form and the number of copies to be submitted, particularly with regard to local area or regional procedures and practices, are either shown below, will be issued by or may be obtained from the local Federal office.

## SPECIFIC INSTRUCTIONS

*Item 4* - Locations on Federal or Indian land should be described in accordance with Federal requirements. Consult the local Federal office for specific instructions.

*Item 13:* Proposals to abandon a well and subsequent reports of abandonment should include such special information as is required by the local Federal office. In addition, such proposals and reports should include reasons for the abandonment; data on any former or present productive zones or other zones with present significant fluid contents not sealed off by cement or otherwise; depths (top and bottom) and method of placement of cement plugs; mud or other material placed below, between and above plugs; amount, size, method of parting of any casing, liner or tubing pulled and the depth to the top of any tubing left in the hole; method of closing top of well and date well site conditioned for final inspection looking for approval of the abandonment. If the proposal will involve **hydraulic fracturing operations**, you must comply with 43 CFR 3162.3-3, including providing information about the protection of usable water. Operators should provide the best available information about all formations containing water and their depths. This information could include data and interpretation of resistivity logs run on nearby wells. Information may also be obtained from state or tribal regulatory agencies and from local BLM offices.

## NOTICES

The privacy Act of 1974 and the regulation in 43 CFR 2.48(d) provide that you be furnished the following information in connection with information required by this application.

AUTHORITY: 30 U.S.C. 181 et seq., 351 et seq., 25 U.S.C. 396; 43 CFR 3160.

PRINCIPAL PURPOSE: The information is used to: (1) Evaluate, when appropriate, approve applications, and report completion of subsequent well operations, on a Federal or Indian lease; and (2) document for administrative use, information for the management, disposal and use of National Resource lands and resources, such as: (a) evaluating the equipment and procedures to be used during a proposed subsequent well operation and reviewing the completed well operations for compliance with the approved plan; (b) requesting and granting approval to perform those actions covered by 43 CFR 3162.3-2, 3162.3-3, and 3162.3-4; (c) reporting the beginning or resumption of production, as required by 43 CFR 3162.4-1(c)and (d) analyzing future applications to drill or modify operations in light of data obtained and methods used.

ROUTINE USES: Information from the record and/or the record will be transferred to appropriate Federal, State, local or foreign agencies, when relevant to civil, criminal or regulatory investigations or prosecutions in connection with congressional inquiries or to consumer reporting agencies to facilitate collection of debts owed the Government.

EFFECT OF NOT PROVIDING THE INFORMATION: Filing of this notice and report and disclosure of the information is mandatory for those subsequent well operations specified in 43 CFR 3162.3-2, 3162.3-3, 3162.3-4.

The Paperwork Reduction Act of 1995 requires us to inform you that:

The BLM collects this information to evaluate proposed and/or completed subsequent well operations on Federal or Indian oil and gas leases.

Response to this request is mandatory.

The BLM would like you to know that you do not have to respond to this or any other Federal agency-sponsored information collection unless it displays a currently valid OMB control number.

**BURDEN HOURS STATEMENT:** Public reporting burden for this form is estimated to average 8 hours per response, including the time for reviewing instructions, gathering and maintaining data, and completing and reviewing the form. Direct comments regarding the burden estimate or any other aspect of this form to U.S. Department of the Interior, Bureau of Land Management (1004-0137), Bureau Information Collection Clearance Officer (WO-630), 1849 C St., N.W., Mail Stop 401 LS, Washington, D.C. 20240

## **Additional Information**

#### **Additional Remarks**

LTP: fr/100FNL & 330FEL to 2565FSL & 2535FEL

BHL: fr/50FNL & 330FEL to 2664FSL & 2535FEL, Section 17-T25S-R31E

PPP: 2646 FNL & 2543 FEL

Additionally, XTO Permian Operating, LLC. respectfully requests permission to change production casing weight. Casing/Cement design per the attached drilling program.

Attachments: C102 Drilling Program MBS Directional Plan BOP Variance Spud Variance

## **Location of Well**

0. SHL: NENE / 541 FNL / 272 FEL / TWSP: 25S / RANGE: 31E / SECTION: 30 / LAT: 32.107059 / LONG: -103.80972 (TVD: 0 feet, MD: 0 feet) PPP: NENE / 2310 FNL / 330 FEL / TWSP: 25S / RANGE: 31E / SECTION: 30 / LAT: 32.102196 / LONG: -103.80972 (TVD: 10938 feet, MD: 11250 feet) PPP: SESE / 2310 FNL / 330 FEL / TWSP: 25S / RANGE: 31E / SECTION: 19 / LAT: 32.114036 / LONG: -103.810924 (TVD: 11533 feet, MD: 13900 feet) BHL: NENE / 50 FNL / 330 FEL / TWSP: 25S / RANGE: 31E / SECTION: 19 / LAT: 32.123027 / LONG: -103.809764 (TVD: 11533 feet, MD: 19749 feet)

# PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

<b>OPERATOR'S NAME:</b>	XTO Permian Operating LLC
WELL NAME & NO.:	Poker Lake Unit 30-19 BS 108H
LOCATION:	Sec 28-25S-31E-NMP
COUNTY:	Eddy County, New Mexico

Changes approved through engineering via **Sundry 2770586** on 01/26/2024. Any previous COAs not addressed within the updated COAs still apply.

COA

H <sub>2</sub> S	💽 No	C Yes		
Potash / WIPP	• None	C Secretary	C R-111-P	□ WIPP
Cave / Karst	C Low	Medium	C High	Critical
Wellhead	C Conventional	Multibowl	C Both	C Diverter
Cementing	Primary Squeeze	Cont. Squeeze	EchoMeter	DV Tool
Special Req	Break Testing	Water Disposal	COM	🗹 Unit
Variance	Flex Hose	Casing Clearance	🗖 Pilot Hole	Capitan Reef
Variance	□ Four-String	Offline Cementing	🗆 Fluid-Filled	Open Annulus
		Batch APD / Sundry		

# A. HYDROGEN SULFIDE

Hydrogen Sulfide (H2S) monitors shall be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the Hydrogen Sulfide area shall meet 43 CFR 3176 requirements, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, provide measured values and formations to the BLM.

# **B.** CASING

- 1. The **9-5/8** inch surface casing shall be set at approximately 910 feet (a minimum of 70 feet (Eddy County) into the Rustler Anhydrite, above the salt, and below usable fresh water) and cemented to the surface. **NOTE: This area has a high dissolution of salt, so the operator may need to make adjustments to their surface set depths to find a competent set point.** 
  - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
  - b. Wait on cement (WOC) time for a primary cement job will be a minimum of <u>8 hours</u> or 500 pounds compressive strength, whichever is greater. (This is to include the lead

cement)

- c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
- d. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 2. The minimum required fill of cement behind the **7-5/8** inch intermediate casing is:

Operator has proposed to cement in two stages by conventionally cementing the first stage and performing a bradenhead squeeze on the second stage, contingent upon no returns to surface.

- a. First stage: Operator will cement with intent to reach the top of the **Brushy Canyon** at 6829'
- b. Second stage:
  - Operator will perform bradenhead squeeze and top-out. Cement to surface. If cement does not reach surface, the appropriate BLM office shall be notified. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst, Capitan Reef, or potash.
- In <u>Medium Cave/Karst Areas</u> if cement does not circulate to surface on the first two casing strings, the cement on the 3rd casing string must come to surface.

Operator has proposed to pump down 9-5/8" X 7-5/8" annulus after primary cementing stage. <u>Operator must run Echo-meter to verify Cement Slurry/Fluid top in the annulus OR operator shall run a CBL from TD of the 7-5/8" casing to surface after the second stage BH to verify TOC.</u>

Submit results to the BLM. No displacement fluid/wash out shall be utilized at the top of the cement slurry between second stage BH and top out. Operator must use a limited flush fluid volume of 1 bbl following backside cementing procedures.

- 3. The minimum required fill of cement behind the 5-1/2 inch production casing is:
  - Cement should tie-back at least **300 feet** into previous casing string (due to not meeting the 0.422" clearance requirement.) Operator shall provide method of verification. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst, Capitan Reef, or potash.

# C. PRESSURE CONTROL

1. Variance approved to use flex line from BOP to choke manifold. Manufacturer's specification to be readily available. No external damage to flex line. Flex line to be installed as straight as possible (no hard bends).'

- 2. Operator has proposed a multi-bowl wellhead assembly. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be **5000** (**5M**) psi.
  - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
  - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
  - c. Manufacturer representative shall install the test plug for the initial BOP test.
  - d. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
  - e. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR 3172 must be followed.

# **D. SPECIAL REQUIREMENT (S)**

# Unit Wells

The well sign for a unit well shall include the unit number in addition to the surface and bottom hole lease numbers. This also applies to participating area numbers. If a participating area has not been established, the operator can use the general unit designation, but will replace the unit number with the participating area number when the sign is replaced.

# **Commercial Well Determination**

A commercial well determination shall be submitted after production has been established for at least six months. (This is not necessary for secondary recovery unit wells)

# (Note: For a minimum 5M BOPE or less (Utilizing a 10M BOPE system) BOPE Break Testing Variance

- BOPE Break Testing is ONLY permitted for 5M BOPE or less. (Annular preventer must be tested to a minimum of 70% of BOPE working pressure and shall be higher than the MASP)
- BOPE Break Testing is NOT permitted to drilling the production hole section.
- Variance only pertains to the intermediate hole-sections and no deeper than the Bone Springs formation.
- While in transfer between wells, the BOPE shall be secured by the hydraulic carrier or cradle.
- Any well control event while drilling require notification to the BLM Petroleum Engineer (575-706-2779) prior to the commencement of any BOPE Break Testing operations.
- A full BOPE test is required prior to drilling the first deep intermediate hole section. If any subsequent hole interval is deeper than the first, a full BOPE test will be required. (200' TVD tolerance between intermediate shoes is allowable).
- The BLM is to be contacted (575-361-2822 Eddy County) 4 hours prior to BOPE tests.
- As a minimum, a full BOPE test shall be performed at 21-day intervals.

- In the event any repairs or replacement of the BOPE is required, the BOPE shall test as per Onshore Oil and Gas Order No. 2.
- If in the event break testing is not utilized, then a full BOPE test would be conducted.

## **Offline Cementing**

Contact the BLM prior to the commencement of any offline cementing procedure.

# GENERAL REQUIREMENTS

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)
  - Eddy County (API No. / US Well No. contains 30-015-#####) Email or call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220, BLM\_NM\_CFO\_DrillingNotifications@BLM.GOV (575) 361-2822
  - Lea County (API No. / US Well No. contains 30-025-#####) Call the Hobbs Field Station, 414 West Taylor, Hobbs NM 88240, (575) 689-5981
- 1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.
  - a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after installing and testing the wellhead, by installing a blind flange of like pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).
  - b. When the operator proposes to set surface casing with Spudder Rig
    - Notify the BLM when moving in and removing the Spudder Rig.
    - Notify the BLM when moving in the 2<sup>nd</sup> Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.
    - BOP/BOPE test to be conducted per **43 CFR part 3170 Subpart 3172** as soon as 2nd Rig is rigged up on well.
- 2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the dog house or stairway area.

3. The record of the drilling rate along with the GR/N well log run from TD to surface (horizontal well – vertical portion of hole) shall be submitted to the BLM office as well as all other logs run on the borehole 30 days from completion. If available, a digital copy of the logs is to be submitted in addition to the paper copies. The Rustler top and top and bottom of Salt are to be recorded on the Completion Report.

# A. CASING

- 1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.
- 2. <u>Wait on cement (WOC) for Potash Areas:</u> After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends, 2) until cement has been in place at least <u>24 hours</u>. WOC time will be recorded in the driller's log. The casing intergrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 3. <u>Wait on cement (WOC) for Water Basin:</u> After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least <u>8 hours</u>. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 4. Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.
- 5. No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.
- 6. On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.

- 7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.
- 8. Whenever a casing string is cemented in the R-111-P potash area, the NMOCD requirements shall be followed.
- B. PRESSURE CONTROL
- 1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in **43 CFR part 3170 Subpart 3172** and **API STD 53 Sec. 5.3**.
- 2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor.
- 3. 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.
- 4. If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:
  - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
  - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
  - c. Manufacturer representative shall install the test plug for the initial BOP test.
  - d. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR part 3170 Subpart 3172 must be followed.
  - e. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- 5. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
  - a. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The

casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead cement), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).

- b. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the cement plug. The BOPE test can be initiated after bumping the cement plug with the casing valve open. (only applies to single stage cement jobs, prior to the cement setting up.)
- c. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer and can be initiated immediately with the casing valve open. The operator also has the option of utilizing an independent tester to test without a plug (i.e. against the casing) pursuant to **43 CFR part 3170 Subpart 3172** with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for water basin (8 hours) or potash (24 hours) or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).
- d. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.
- e. The results of the test shall be reported to the appropriate BLM office.
- f. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
- g. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.
- h. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per **43 CFR part 3170 Subpart 3172**.

# C. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

## D. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area.

Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

<u>District I</u> 1625 N. French Dr., Hobbs, NM 88240 Phone: (575) 393-6161 Fax: (575) 393-0720 <u>District II</u> 811 S. First St., Artesia, NM 88210 Phone: (575) 748-1283 Fax: (575) 748-9720 <u>District III</u> 1000 Rio Brazos Road, Aztec, NM 87410 Phone: (505) 334-6178 Fax: (505) 334-6170 <u>District IV</u> 1220 S. St. Francis Dr., Santa Fe, NM 87505 Phone: (505) 476-3460 Fax: (505) 476-3462

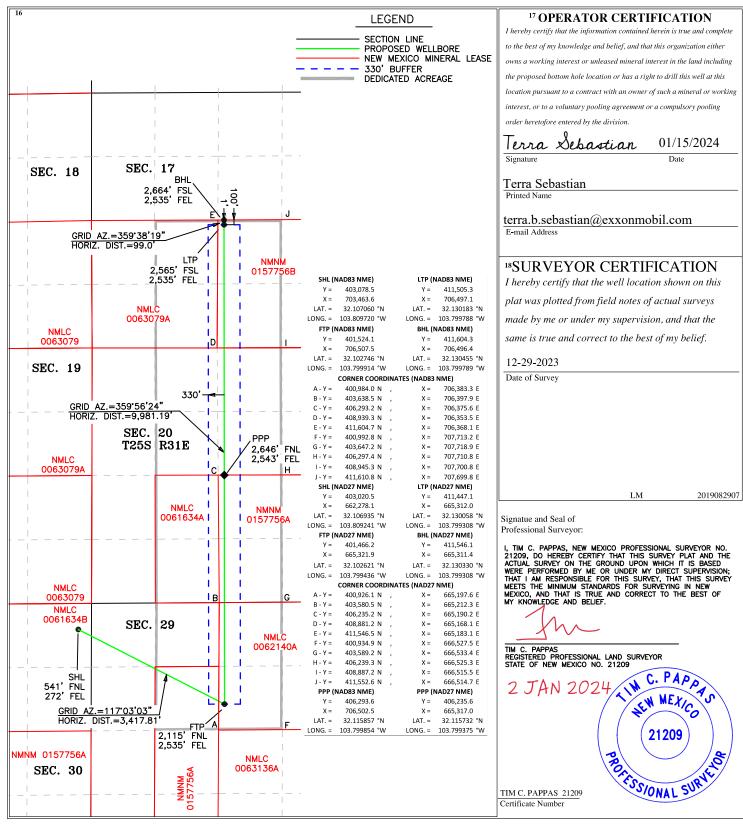
# State of New Mexico Energy, Minerals & Natural Resources Department OIL CONSERVATION DIVISION 1220 South St. Francis Dr. Santa Fe, NM 87505

Form C-102 Revised August 1, 2011 Submit one copy to appropriate District Office

AMENDED REPORT

	API Number 30-015-53			<sup>2</sup> Pool Code 96654		<sup>3</sup> Pool Name WILDCAT BIG SINK; BONE SPRING				
<sup>4</sup> Property C	ode	<sup>5</sup> Property Name <sup>6</sup> Well Number								Well Number
				F	OKER LAKE UN	NIT 30-19 BS				108H
<sup>7</sup> OGRID N	lo.				<sup>8</sup> Operator 1	Name				<sup>9</sup> Elevation
373075		XTO PERMIAN OPERATING, LLC. 3,380'						3,380'		
					<sup>10</sup> Surface I	Location				
UL or lot no.	Section	Township	Range	Lot Idn	Feet from the	North/South line	Feet from the	East	/West line	County
A	30	25 S	31 E		541	NORTH	272	EAS	ST	EDDY
			<sup>11</sup> Bot	tom Hol	e Location If	Different Fron	n Surface			
UL or lot no.	Section	Township	Range	Lot Idn	Feet from the	North/South line	Feet from the	East	/West line	County
J	17	25 S	31 E	31 E 2,664 SOUTH 2,535 EA			ST	EDDY		
<sup>12</sup> Dedicated Acres	<sup>13</sup> Joint o	r Infill <sup>14</sup> C	Consolidation C	Code <sup>15</sup> Order No.						
640										

No allowable will be assigned to this completion until all interests have been consolidated or a non-standard unit has been approved by the division.



Long Lead\_Well Planning

PLU 30-19 BS PLU 30-19 BS PLU 30-19 BS 108H

OH

Plan: Plan 3

# **Standard Planning Report**

15 December, 2023

Page	<i>16</i>	of	36

Plan Sections Measured		Vertic	al		Dogleg	Build	Turn		
, 0.0	22,107.3	r-iaii ט (UH)		_	+ IFR1 + Multi-S				
1 0.0	22,107.3	• •	,		SG MWD+IFR1+				
Depth From (usft)	Depth To (usft)	Survey (Wellb		Tool Name		Remarks			
Plan Survey Tool Pro	oram	Date 12/15	/2023						
			2.0	0.0	0.0	-	3	<b>()</b> 59.94	
Vertical Section:		-	rom (TVD) ısft)	+N/-S (usft)	+E/- (ust		Dir	ection (°)	
Version:			Phase:	PLAN		On Depth:		0.0	
Audit Notes:									
Design	Plan 3								
	IG	RF2020	12/12/2023		6.35		59.68	47,1	41.39672081
Magnetics	Model N	ame	Sample Date	Declina (°)		Dip	Angle (°)		Strength 1T)
Wellbore	ОН								
Grid Convergence:		0.28 °							
Position Uncertainty	+E/-W	0.0 usft 0.0 usft	Easting: Wellhead Elev	vation:	662,278.10 נ ו		ongitude: round Level:		103° 48' 33.266 3,380.0 u
Well Position	+N/-S	0.0 usft	Northing:		403,020.50 u		atitude:		32° 6' 24.966
Well	PLU 30-19 B	S 108H							
Position Uncertainty:		0.0 usft	Slot Radius:		13-3/16 "				
Site Position: From:	Мар		Northing: Easting:			_atitude: _ongitude:			32° 6' 24.964 103° 48' 34.307 '
Site	PLU 30-19 B	S							
Map Zone:									
Geo Datum:		e 1927 (Exact so DCON CONUS)		System Da	tum:	r	Mean Sea Level		
Project	PLU 30-19 B	S							
Design:	Plan 3								
Vell: Vellbore:	PLU 30-19 E OH	35 108H		Survey C	alculation Metho	od:	Minimum Curva	ture	
Site:	PLU 30-19 BS			North Re			Grid		
Project:	PLU 30-19 E			MD Refer			32+3380 @ 341	-	
Company:	Long Lead	Well Planning		TVD Refe	ordinate Refere	lice	Well PLU 30-19 32+3380 @ 341		3)

Measured			Vertical			Dogleg	Build	Turn		
Depth	Inclination	Azimuth	Depth	+N/-S	+E/-W	Rate	Rate	Rate	TFO	
(usft)	(°)	(°)	(usft)	(usft)	(usft)	(°/100usft)	(°/100usft)	(°/100usft)	(°)	Target
0.0	0.00	0.00	0.0	0.0	0.0	0.00	0.00	0.00	0.00	
1,200.0	0.00	0.00	1,200.0	0.0	0.0	0.00	0.00	0.00	0.00	
2,372.5	5 23.45	129.17	2,340.1	-149.5	183.4	2.00	2.00	0.00	129.17	
10,720.2	2 23.45	129.17	9,998.3	-2,247.7	2,758.9	0.00	0.00	0.00	0.00	
12,027.4	90.00	359.94	10,848.0	-1,554.3	3,043.8	8.00	5.09	-9.89	-126.83 I	FTP PLU 30-19 BS 1(
22,008.3	90.00	359.94	10,848.0	8,426.6	3,033.9	0.00	0.00	0.00	0.00	LTP PLU 30-19 BS 10
22,107.3	90.00	359.94	10,848.0	8,525.6	3,033.8	0.00	0.00	0.00	0.00	BHL PLU 30-19 BS 1(

12/15/2023 12:42:11PM

Database:	LMRKPROD3	Local Co-ordinate Reference	Well PLU 30-19 BS 108H
Company:	Long Lead_Well Planning	TVD Reference:	32+3380 @ 3412.0usft (32' KB)
Project:	PLU 30-19 BS	MD Reference:	32+3380 @ 3412.0usft (32' KB)
Site:	PLU 30-19 BS	North Reference:	Grid
Well:	PLU 30-19 BS 108H	Survey Calculation Method:	Minimum Curvature
Wellbore:	OH		
Design:	Plan 3		

Planned Survey

0.0         0.00         0.00         0.00         0.00         0.00         0.00           200.0         0.00         0.00         200.0         0.00         0	Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
1000         0.00 <th< td=""><td>• •</td><td></td><td></td><td></td><td>• •</td><td>• •</td><td>. ,</td><td></td><td>. ,</td><td>(71000311) 0.00</td></th<>	• •				• •	• •	. ,		. ,	(71000311) 0.00
200.0         0.00         0.00         200.0         0.00         <										0.00
300.0         0.00         0.00         300.0         0.00         <										0.00
400.0         0.00         400.0         0.00         0.00         0.00         0.00         0.00           500.0         0.00         0.00         500.0         0.0         0.00 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>0.00</td></td<>										0.00
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$										
660.0         0.00         600.0         0.00         0.00         0.00         0.00           860.0         0.00         0.00         860.0         0.00         0.00         0.00         0.00         0.00           Rustler         U         U         U         U         U         U           900.0         0.00         0.00         900.0         0.00         0.00         0.00         0.00         0.00           100.0         0.00         0.00         100.0         0.00	400.0	0.00	0.00	400.0	0.0	0.0	0.0	0.00	0.00	0.00
70:0         0.00         0.00         70:0         0.0         0.0         0.00         0	500.0	0.00	0.00	500.0	0.0	0.0	0.0	0.00	0.00	0.00
B00.0         0.00         B00.0         0.0         0.0         0.0         0.00         0.00         0.00           Rustler           900.0         0.00         0.00         900.0         0.0         0.0         0.00         0.00         0.00         0.00           1000.0         0.00	600.0	0.00	0.00	600.0	0.0	0.0	0.0	0.00	0.00	0.00
810.0         0.00         810.0         0.0         0.00         0.00         0.00           Rustler           900.0         0.00         0.00         1000.0         0.00 <t< td=""><td>700.0</td><td>0.00</td><td>0.00</td><td>700.0</td><td>0.0</td><td>0.0</td><td>0.0</td><td>0.00</td><td>0.00</td><td>0.00</td></t<>	700.0	0.00	0.00	700.0	0.0	0.0	0.0	0.00	0.00	0.00
Pustler         900.0         0.00         900.0         0.00	800.0	0.00	0.00	800.0		0.0	0.0	0.00		0.00
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	810.0	0.00	0.00	810.0	0.0	0.0	0.0	0.00	0.00	0.00
1,000.0         0.00	Rustler									
1,100.0         0.00         0.00         1,100.0         0.00										0.00
1:180.0       0.00       0.00       0.00       0.00       0.00       0.00         Salado       1       0.00       0.00       0.00       0.00       0.00       0.00       0.00       0.00       0.00         1,200.0       0.00       129.17       1,300.0       -1.1       1.4       -1.1       2.00       2.00       0.00         1,400.0       4.00       129.17       1,499.5       -9.9       12.2       -9.9       2.00       2.00       0.00         1,600.0       8.00       129.17       1,698.7       -17.6       21.6       -17.6       2.00       2.00       0.00         1,700.0       10.00       129.17       1,698.7       -27.5       33.7       -27.5       2.00       2.00       0.00         1,900.0       14.00       129.17       1,988.1       -53.7       66.0       -53.8       2.00       2.00       0.00         2,000.0       16.00       129.17       2,782.3       -186.6       108.7       -88.7       2.00       2.00       0.00         2,200.0       129.17       2,732.2       -131.8       161.7       -131.9       2.00       2.00       0.00       0.00       0.00       0.00 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>0.00</td>										0.00
Salado         1 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>0.00</td>										0.00
1.200.0       0.00       1.20.0       0.0       0.0       0.00       0.00       0.00         1.300.0       2.00       129.17       1.300.0       -1.1       1.4       -1.1       2.00       2.00       0.00         1.400.0       4.00       129.17       1.499.5       -9.9       12.2       -9.9       2.00       2.00       0.00         1.600.0       8.00       129.17       1.598.7       -17.6       21.6       -17.5       2.00       2.00       0.00         1.700.0       10.00       129.17       1.598.7       -27.5       33.7       -27.5       2.00       2.00       0.00         1.800.0       12.00       129.17       1.995.6       -39.5       48.5       -39.6       2.00       2.00       0.00         2.000.0       16.00       129.17       1.998.6       -70.1       86.0       -70.2       2.00       2.00       0.00 <td< td=""><td></td><td>0.00</td><td>0.00</td><td>1,180.0</td><td>0.0</td><td>0.0</td><td>0.0</td><td>0.00</td><td>0.00</td><td>0.00</td></td<>		0.00	0.00	1,180.0	0.0	0.0	0.0	0.00	0.00	0.00
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		0.00	0.00	1 200 0	0.0	0.0	0.0	0.00	0.00	0.00
$\begin{array}{c c c c c c c c c c c c c c c c c c c $										
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1,600.0       8.00       129.17       1,598.7       -17.6       21.6       -17.6       2.00       2.00       0         1,700.0       10.00       129.17       1,697.5       -27.5       33.7       -27.5       2.00       2.00       0         1,800.0       12.00       129.17       1,795.6       -39.5       48.5       -39.6       2.00       2.00       0         2,000.0       16.00       129.17       1,989.6       -70.1       86.0       -70.2       2.00       2.00       0       0         2,100.0       18.00       129.17       2,078.3       -88.6       108.7       -88.7       2.00       2.00       0 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>0.00</td></t<>										0.00
1,700.0       10.00       129.17       1,697.5       -27.5       33.7       -27.5       2.00       2.00       0         1,800.0       12.00       129.17       1,795.6       -39.5       48.5       -39.6       2.00       2.00       0         1,900.0       14.00       129.17       1,893.1       -53.7       66.0       -53.8       2.00       2.00       0         2,000.0       16.00       129.17       2.085.3       -88.6       108.7       -88.7       2.00       2.00       0       0         2,200.0       20.00       129.17       2.193.6       -109.1       133.9       -109.3       2.00       2.00       0       0       2.00       0										0.00
1,800.0       12.00       129.17       1,795.6       -39.5       48.5       -39.6       2.00       2.00       0         1,900.0       14.00       129.17       1,893.1       -53.7       66.0       -53.8       2.00       2.00       0         2,000.0       16.00       129.17       2,085.3       -88.6       108.7       -88.7       2.00       2.00       0       0         2,200.0       20.00       129.17       2,179.8       -109.1       133.9       -109.3       2.00       2.00       0       0         2,300.0       22.00       129.17       2,273.2       -131.8       161.7       -131.9       2.00       2.00       0       0         2,400.0       23.45       129.17       2,365.3       -156.4       191.9       -156.6       0.00       0.00       0       0         2,600.0       23.45       129.17       2,548.7       -266.6       236.6       -206.9       0.00       0.00       0										0.00
1,900.0       14.00       129.17       1,893.1       -53.7       66.0       -53.8       2.00       2.00       0         2,000.0       16.00       129.17       2,085.3       -70.1       86.0       -70.2       2.00       2.00       0         2,200.0       20.00       129.17       2,179.8       -109.1       133.9       -109.3       2.00       2.00       0         2,300.0       22.00       129.17       2,273.2       -131.8       161.7       -131.9       2.00       2.00       0         2,300.0       23.45       129.17       2,365.3       -156.4       191.9       -156.6       0.00       0.00       0         2,400.0       23.45       129.17       2,457.0       -181.5       222.8       -181.7       0.00       0.00       0       0         2,600.0       23.45       129.17       2,548.7       -266.6       235.6       -202.9       0       0       0.00       0.00       0 <td>1,700.0</td> <td>10.00</td> <td>129.17</td> <td>1,697.5</td> <td>-27.5</td> <td>33.7</td> <td>-27.5</td> <td>2.00</td> <td>2.00</td> <td>0.00</td>	1,700.0	10.00	129.17	1,697.5	-27.5	33.7	-27.5	2.00	2.00	0.00
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1,800.0	12.00	129.17	1,795.6	-39.5	48.5	-39.6	2.00	2.00	0.00
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1,900.0	14.00		1,893.1	-53.7	66.0	-53.8	2.00	2.00	0.00
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	2,000.0	16.00		1,989.6	-70.1	86.0	-70.2		2.00	0.00
2,300.0       22.00       129.17       2,273.2       -131.8       161.7       -131.9       2.00       2.00       0         2,372.5       23.45       129.17       2,365.3       -156.4       191.9       -156.6       0.00       0.00       0         2,500.0       23.45       129.17       2,467.0       -181.5       222.8       -181.7       0.00       0.00       0       0         2,600.0       23.45       129.17       2,640.5       -231.8       284.5       -206.9       0.00       0.00       0       0         2,600.0       23.45       129.17       2,640.5       -231.8       284.5       -232.1       0.00       0.00       0       0         2,800.0       23.45       129.17       2,640.5       -231.8       284.5       -232.1       0.00       0.00       0       0         2,900.0       23.45       129.17       2,947.7       -307.2       377.0       -307.6       0.00       0.00       0 <td< td=""><td></td><td></td><td></td><td>2,085.3</td><td></td><td></td><td></td><td></td><td></td><td>0.00</td></td<>				2,085.3						0.00
2,372.5       23.45       129.17       2,340.1       -149.5       183.4       -149.6       2.00       2.00       0         2,400.0       23.45       129.17       2,365.3       -156.4       191.9       -156.6       0.00       0.00       0       0         2,500.0       23.45       129.17       2,467.0       -181.5       222.8       -181.7       0.00       0.00       0       0         2,600.0       23.45       129.17       2,640.5       -231.8       284.5       -232.1       0.00       0.00       0.00       0         2,700.0       23.45       129.17       2,640.5       -231.8       284.5       -232.1       0.00       0.00       0.00       0         2,900.0       23.45       129.17       2,732.2       -256.9       315.3       -257.2       0.00       0.00       0.00       0         3,000.0       23.45       129.17       2,907.4       -332.3       407.9       -332.7       0.00       0.00       0	2,200.0	20.00	129.17	2,179.8	-109.1	133.9	-109.3	2.00	2.00	0.00
2,400.0       23.45       129.17       2,365.3       -156.4       191.9       -156.6       0.00       0.00       0.00         2,500.0       23.45       129.17       2,457.0       -181.5       222.8       -181.7       0.00       0.00       0.00         2,600.0       23.45       129.17       2,548.7       -206.6       253.6       -206.9       0.00       0.00       0.00         2,700.0       23.45       129.17       2,640.5       -231.8       284.5       -232.1       0.00       0.00       0.00       0.00         2,800.0       23.45       129.17       2,626.9       315.3       -257.2       0.00       0.00       0.00       0.00         2,900.0       23.45       129.17       2,915.7       -307.2       377.0       -307.6       0.00       0.00       0.00       0.00         3,000.0       23.45       129.17       3,007.4       -332.3       407.9       -332.7       0.00       0.00       0.00       0.00         3,000.0       23.45       129.17       3,028.7       -407.7       500.5       -408.2       0.00       0.00       0.00       0.00       0.00       0.00       0.00       0.00       0.00										0.00
2,500.0       23.45       129.17       2,457.0       -181.5       222.8       -181.7       0.00       0.00       0.00         2,600.0       23.45       129.17       2,548.7       -206.6       253.6       -206.9       0.00       0.00       0.00       0.00         2,700.0       23.45       129.17       2,732.2       -256.9       315.3       -257.2       0.00       0.00       0.00       0.00         2,800.0       23.45       129.17       2,824.0       -282.0       346.2       -282.4       0.00       0.00       0.00       0.00         3,000.0       23.45       129.17       2,915.7       -307.2       377.0       -307.6       0.00       0.00       0.00         3,100.0       23.45       129.17       3,007.4       -332.3       407.9       -332.7       0.00       0.00       0.00       0.00         3,200.0       23.45       129.17       3,099.2       -357.4       438.7       -357.9       0.00       0.00       0.00       0.00       0.00       0.00       0.00       0.00       0.00       0.00       0.00       0.00       0.00       0.00       0.00       0.00       0.00       0.00       0.00       0.0										0.00
2,600.0       23.45       129.17       2,548.7       -206.6       253.6       -206.9       0.00       0.00       0.00         2,700.0       23.45       129.17       2,640.5       -231.8       284.5       -232.1       0.00       0.00       0.00       0.00         2,800.0       23.45       129.17       2,732.2       -256.9       315.3       -257.2       0.00       0.00       0.00       0.00         3,000.0       23.45       129.17       2,917       -282.0       346.2       -282.4       0.00       0.00       0.00       0.00         3,000.0       23.45       129.17       3,007.4       -332.3       407.9       -332.7       0.00       0.00       0.00       0.00         3,200.0       23.45       129.17       3,099.2       -357.4       438.7       -357.9       0.00 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>0.00</td></t<>										0.00
2,700.0       23.45       129.17       2,640.5       -231.8       284.5       -232.1       0.00       0.00       0.00         2,800.0       23.45       129.17       2,732.2       -256.9       315.3       -257.2       0.00       0.00       0.00         2,900.0       23.45       129.17       2,824.0       -282.0       346.2       -282.4       0.00       0.00       0.00       0.00         3,000.0       23.45       129.17       2,915.7       -307.2       377.0       -307.6       0.00       0.00       0.00       0.00         3,100.0       23.45       129.17       3,099.2       -357.4       438.7       -357.9       0.00       0.00       0.00       0.00         3,200.0       23.45       129.17       3,099.2       -357.4       438.7       -357.9       0.00       0.00       0.00       0.00         3,400.0       23.45       129.17       3,190.9       -826.6       498.6       -383.1       0.00       0.00       0.00       0.00       0.00       0.00       0.00       0.00       0.00       0.00       0.00       0.00       0.00       0.00       0.00       0.00       0.00       0.00       0.00       0.0										0.00
2,800.0       23.45       129.17       2,732.2       -256.9       315.3       -257.2       0.00       0.00       0.00         2,900.0       23.45       129.17       2,824.0       -282.0       346.2       -282.4       0.00       0.00       0.00       0.00         3,000.0       23.45       129.17       2,915.7       -307.2       377.0       -307.6       0.00       0.00       0.00       0.00         3,100.0       23.45       129.17       3,007.4       -332.3       407.9       -332.7       0.00       0.00       0.00       0.00         3,200.0       23.45       129.17       3,190.9       -382.6       469.6       -383.1       0.00       0.00       0.00       0.00         3,400.0       23.45       129.17       3,282.7       -407.7       500.5       -408.2       0.00	2,600.0	23.45	129.17	2,548.7	-206.6	253.6	-206.9	0.00	0.00	0.00
2,900.0       23,45       129.17       2,824.0       -282.0       346.2       -282.4       0.00       0.00       0.00         3,000.0       23,45       129.17       2,915.7       -307.2       377.0       -307.6       0.00       0.00       0.00       0.00         3,100.0       23,45       129.17       3,007.4       -332.3       407.9       -332.7       0.00       0.00       0.00       0.00         3,200.0       23,45       129.17       3,099.2       -357.4       438.7       -357.9       0.00       0.00       0.00       0.00         3,300.0       23,45       129.17       3,190.9       -382.6       469.6       -383.1       0.00       0.00       0.00       0.00         3,400.0       23,45       129.17       3,282.7       -407.7       500.5       -408.2       0.00	2,700.0		129.17	2,640.5	-231.8	284.5	-232.1	0.00	0.00	0.00
3,000.0       23.45       129.17       2,915.7       -307.2       377.0       -307.6       0.00       0.00       0.00         3,100.0       23.45       129.17       3,007.4       -332.3       407.9       -332.7       0.00       0.00       0.00       0.00         3,200.0       23.45       129.17       3,099.2       -357.4       438.7       -357.9       0.00       0.00       0.00       0.00         3,300.0       23.45       129.17       3,190.9       -382.6       469.6       -383.1       0.00       0.00       0.00       0.00         3,400.0       23.45       129.17       3,282.7       -407.7       500.5       -408.2       0.00       0.00       0.00       0.00         3,500.0       23.45       129.17       3,374.4       -432.9       531.3       -433.4       0.00	2,800.0	23.45	129.17	2,732.2	-256.9	315.3	-257.2	0.00	0.00	0.00
3,100.0       23.45       129.17       3,007.4       -332.3       407.9       -332.7       0.00       0.00       0.00         3,200.0       23.45       129.17       3,099.2       -357.4       438.7       -357.9       0.00       0.00       0.00       0.00         3,300.0       23.45       129.17       3,190.9       -382.6       469.6       -383.1       0.00       0.00       0.00       0.00         3,400.0       23.45       129.17       3,282.7       -407.7       500.5       -408.2       0.00       0.	2,900.0	23.45	129.17	2,824.0	-282.0	346.2	-282.4	0.00	0.00	0.00
3,200.0       23.45       129.17       3,099.2       -357.4       438.7       -357.9       0.00       0.00       0.00         3,300.0       23.45       129.17       3,190.9       -382.6       469.6       -383.1       0.00       0.00       0.00       0.00         3,400.0       23.45       129.17       3,282.7       -407.7       500.5       -408.2       0.00       0.00       0.00       0.00         3,500.0       23.45       129.17       3,374.4       -432.9       531.3       -433.4       0.00       0.00       0.00       0.00         3,600.0       23.45       129.17       3,557.9       -483.1       593.0       -483.7       0.00       0.00       0.00       0.00         3,700.0       23.45       129.17       3,557.9       -483.1       593.0       -483.7       0.00										0.00
3,300.0       23.45       129.17       3,190.9       -382.6       469.6       -383.1       0.00       0.00       0.00         3,400.0       23.45       129.17       3,282.7       -407.7       500.5       -408.2       0.00       0.00       0.00       0.00         3,500.0       23.45       129.17       3,374.4       -432.9       531.3       -433.4       0.00       0.00       0.00       0.00         3,600.0       23.45       129.17       3,374.4       -432.9       531.3       -433.4       0.00       0.	3,100.0	23.45	129.17	3,007.4	-332.3	407.9	-332.7	0.00	0.00	0.00
3,400.0       23.45       129.17       3,282.7       -407.7       500.5       -408.2       0.00       0	3,200.0	23.45	129.17	3,099.2	-357.4	438.7	-357.9		0.00	0.00
3,500.0       23.45       129.17       3,374.4       -432.9       531.3       -433.4       0.00       0.00       0.00         3,600.0       23.45       129.17       3,466.2       -458.0       562.2       -458.6       0.00       0.00       0.00       0.00         3,700.0       23.45       129.17       3,557.9       -483.1       593.0       -483.7       0.00										0.00
3,600.0       23.45       129.17       3,466.2       -458.0       562.2       -458.6       0.00       0.00       0         3,700.0       23.45       129.17       3,557.9       -483.1       593.0       -483.7       0.00       0.00       0         3,800.0       23.45       129.17       3,649.6       -508.3       623.9       -508.9       0.00       0.00       0       0         3,900.0       23.45       129.17       3,741.4       -533.4       654.7       -534.1       0.00       0.00       0       0         4,000.0       23.45       129.17       3,741.4       -558.5       685.6       -559.3       0.00       0.00       0.00       0       0         4,100.0       23.45       129.17       3,924.9       -583.7       716.4       -584.4       0.00       0.00       0.00       0       0         4,200.0       23.45       129.17       4,016.6       -608.8       747.3       -609.6       0.00       0.00       0.00       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0										0.00
3,700.0       23.45       129.17       3,557.9       -483.1       593.0       -483.7       0.00       0										0.00
3,800.0       23.45       129.17       3,649.6       -508.3       623.9       -508.9       0.00       0	3,600.0	23.45	129.17	3,466.2	-458.0	562.2	-458.6	0.00	0.00	0.00
3,900.0       23.45       129.17       3,741.4       -533.4       654.7       -534.1       0.00       0										0.00
4,000.0       23.45       129.17       3,833.1       -558.5       685.6       -559.3       0.00       0										0.00
4,100.0       23.45       129.17       3,924.9       -583.7       716.4       -584.4       0.00       0.00       0         4,200.0       23.45       129.17       4,016.6       -608.8       747.3       -609.6       0.00       0.00       0       0         4,202.6       23.45       129.17       4,019.0       -609.5       748.1       -610.3       0.00       0.00       0       0         Base of Sait         4,300.0       23.45       129.17       4,108.3       -633.9       778.1       -634.8       0.00       0.00       0.00       0										0.00
4,200.0       23.45       129.17       4,016.6       -608.8       747.3       -609.6       0.00       0.00       0.00       0.00         4,202.6       23.45       129.17       4,019.0       -609.5       748.1       -610.3       0.00       0.00       0.00       0.00         Base of Salt         4,300.0       23.45       129.17       4,108.3       -633.9       778.1       -634.8       0.00       0.00       0.00       0.00										0.00
4,202.6       23.45       129.17       4,019.0       -609.5       748.1       -610.3       0.00       0.00       0         Base of Salt	4,100.0	23.45	129.17	3,924.9	-583.7	716.4	-584.4	0.00	0.00	0.00
Base of Salt         4,300.0         23.45         129.17         4,108.3         -633.9         778.1         -634.8         0.00         0.00         0										0.00
4,300.0 23.45 129.17 4,108.3 -633.9 778.1 -634.8 0.00 0.00 (			129.17	4,019.0	-609.5	748.1	-610.3	0.00	0.00	0.00
			100.47	4 400 0	600.0	770 4	004.0	0.00	0.00	0.00
						778.1 809.0				0.00
										0.00 0.00

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Database:	LMRKPROD3	Local Co-ordinate Reference	Well PLU 30-19 BS 108H
Company:	Long Lead_Well Planning	TVD Reference:	32+3380 @ 3412.0usft (32' KB)
Project:	PLU 30-19 BS	MD Reference:	32+3380 @ 3412.0usft (32' KB)
Site:	PLU 30-19 BS	North Reference:	Grid
Well:	PLU 30-19 BS 108H	Survey Calculation Method:	Minimum Curvature
Wellbore:	ОН		
Design:	Plan 3		

Planned Survey

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
Delaware									
4,500.0	23.45	129.17	4,291.8	-684.2	839.8	-685.1	0.00	0.00	0.00
4,600.0	23.45	129.17	4,383.6	-709.4	870.7	-710.3	0.00	0.00	0.00
4,700.0	23.45	129.17	4,475.3	-734.5	901.5	-735.4	0.00	0.00	0.00
4,800.0	23.45	129.17	4,567.0	-759.6	932.4	-760.6	0.00	0.00	0.00
4,900.0	23.45	129.17	4,658.8	-784.8	963.2	-785.8	0.00	0.00	0.00
5,000.0	23.45	129.17	4,750.5	-809.9	994.1	-810.9	0.00	0.00	0.00
5,100.0	23.45	129.17	4,842.3	-835.0	1,024.9	-836.1	0.00	0.00	0.00
5,200.0	23.45	129.17	4,934.0	-860.2	1,055.8	-861.3	0.00	0.00	0.00
5,300.0	23.45	129.17	5,025.7	-885.3	1,086.7	-886.4	0.00	0.00	0.00
5,400.0	23.45	129.17	5,117.5	-910.4	1,117.5	-911.6	0.00	0.00	0.00
5,432.2	23.45	129.17	5,147.0	-918.5	1,127.4	-919.7	0.00	0.00	0.00
Cherry Canyo			-,		-,				
5,500.0	23.45	129.17	5,209.2	-935.6	1,148.4	-936.8	0.00	0.00	0.00
5,600.0	23.45	129.17	5,301.0	-960.7	1,179.2	-961.9	0.00	0.00	0.00
5,700.0	23.45	129.17	5,392.7	-985.8	1,210.1	-987.1	0.00	0.00	0.00
5,800.0	23.45	129.17	5,484.4	-1,011.0	1,240.9	-1,012.3	0.00	0.00	0.00
5,900.0	23.45	129.17	5,576.2	-1,036.1	1,271.8	-1,037.5	0.00	0.00	0.00
6,000.0	23.45	129.17	5,667.9	-1,061.3	1,302.6	-1,062.6	0.00	0.00	0.00
6,100.0	23.45	129.17	5,759.7	-1,086.4	1,333.5	-1,087.8	0.00	0.00	0.00
6,200.0	23.45	129.17	5,851.4	-1,111.5	1,364.3	-1,113.0	0.00	0.00	0.00
6,300.0	23.45	129.17	5,943.1	-1,136.7	1,395.2	-1,138.1	0.00	0.00	0.00
6,400.0	23.45	129.17	6,034.9	-1,161.8	1,426.0	-1,163.3	0.00	0.00	0.00
6,500.0	23.45	129.17	6,126.6	-1,186.9	1,456.9	-1,188.5	0.00	0.00	0.00
6,600.0	23.45	129.17	6,218.4	-1,212.1	1,487.7	-1,213.6	0.00	0.00	0.00
6,700.0	23.45	129.17	6,310.1	-1,237.2	1,518.6	-1,238.8	0.00	0.00	0.00
6,800.0	23.45	129.17	6,401.8	-1,262.3	1,549.4	-1,264.0	0.00	0.00	0.00
6,900.0	23.45	129.17	6,493.6	-1,287.5	1,580.3	-1,289.1	0.00	0.00	0.00
7,000.0	23.45	129.17	6,585.3	-1,312.6	1,611.2	-1,314.3	0.00	0.00	0.00
7,100.0	23.45	129.17	6,677.1	-1,337.8	1,642.0	-1,339.5	0.00	0.00	0.00
7,200.0	23.45	129.17	6,768.8	-1,362.9	1,672.9	-1,364.6	0.00	0.00	0.00
7,265.6	23.45	129.17	6,829.0	-1,379.4	1,693.1	-1,381.2	0.00	0.00	0.00
Brushy Canyo		.20.11	0,02010	1,01011	.,	1,00112	0.00	0.00	0.00
7,300.0	23.45	129.17	6,860.5	-1,388.0	1,703.7	-1,389.8	0.00	0.00	0.00
7,300.0	23.45	129.17	6,952.3	-1,300.0 -1,413.2	1,703.7	-1,369.6 -1,415.0	0.00	0.00	0.00
7,400.0 7,500.0	23.45 23.45	129.17	6,952.3 7,044.0	-1,413.2 -1,438.3	1,734.6	-1,415.0 -1,440.1	0.00	0.00	0.00
7,600.0	23.45	129.17	7,044.0 7,135.8	-1,430.3 -1,463.4	1,765.4	-1,440.1	0.00	0.00	0.00
7,800.0	23.45	129.17	7,135.6	-1,463.4 -1,488.6	1,796.3	-1,405.5 -1,490.5	0.00	0.00	0.00
7,800.0	23.45	129.17	7,319.2	-1,513.7	1,858.0	-1,515.6	0.00	0.00	0.00
7,900.0	23.45	129.17	7,411.0	-1,538.8	1,888.8	-1,540.8	0.00	0.00	0.00
8,000.0	23.45	129.17	7,502.7	-1,564.0	1,919.7	-1,566.0	0.00	0.00	0.00
8,100.0	23.45	129.17	7,594.5	-1,589.1	1,950.5	-1,591.2	0.00	0.00	0.00
8,200.0	23.45	129.17	7,686.2	-1,614.2	1,981.4	-1,616.3	0.00	0.00	0.00
8,300.0	23.45	129.17	7,777.9	-1,639.4	2,012.2	-1,641.5	0.00	0.00	0.00
8,400.0	23.45	129.17	7,869.7	-1,664.5	2,043.1	-1,666.7	0.00	0.00	0.00
8,434.1	23.45	129.17	7,901.0	-1,673.1	2,053.6	-1,675.2	0.00	0.00	0.00
Basal Brushy	-	400.47	7.004.4	4 000 7	0.070.0	4 004 0	0.00	0.00	0.00
8,500.0	23.45	129.17	7,961.4	-1,689.7	2,073.9	-1,691.8	0.00	0.00	0.00
8,600.0	23.45	129.17	8,053.2	-1,714.8	2,104.8	-1,717.0	0.00	0.00	0.00
8,689.2	23.45	129.17	8,135.0	-1,737.2	2,132.3	-1,739.4	0.00	0.00	0.00
Bone Spring I									
8.700.0	23.45	129.17	8,144.9	-1,739.9	2,135.7	-1,742.2	0.00	0.00	0.00

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#### Planning Report

Database:	LMRKPROD3	Local Co-ordinate Reference	Well PLU 30-19 BS 108H
Company:	Long Lead_Well Planning	TVD Reference:	32+3380 @ 3412.0usft (32' KB)
Project:	PLU 30-19 BS	MD Reference:	32+3380 @ 3412.0usft (32' KB)
Site:	PLU 30-19 BS	North Reference:	Grid
Well:	PLU 30-19 BS 108H	Survey Calculation Method:	Minimum Curvature
Wellbore:	ОН		
Design:	Plan 3		

Planned Survey

I	Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
	8,800.0	23.45	129.17	8,236.6	-1,765.1	2,166.5	-1,767.3	0.00	0.00	0.00
	8,837.4	23.45	129.17	8,271.0	-1,774.5	2,178.1	-1,776.8	0.00	0.00	0.00
	Avalon Shal	e								
	8,900.0	23.45	129.17	8,328.4	-1,790.2	2,197.4	-1,792.5	0.00	0.00	0.00
	9,000.0	23.45	129.17	8,420.1	-1,815.3	2,228.2	-1,817.7	0.00	0.00	0.00
	9,100.0	23.45	129.17	8,511.9	-1,840.5	2,259.1	-1,842.8	0.00	0.00	0.00
	9,200.0	23.45	129.17	8,603.6	-1,865.6	2,289.9	-1,868.0	0.00	0.00	0.00
	9,300.0	23.45	129.17	8,695.3	-1,890.7	2,320.8	-1,893.2	0.00	0.00	0.00
	9,392.3	23.45	129.17	8,780.0	-1,913.9	2,349.2	-1,916.4	0.00	0.00	0.00
	Lower Avalo	n Shale								
	9,400.0	23.45	129.17	8,787.1	-1,915.9	2,351.6	-1,918.3	0.00	0.00	0.00
	9,500.0	23.45	129.17	8,878.8	-1,941.0	2,382.5	-1,943.5	0.00	0.00	0.00
	9,576.5	23.45	129.17	8,949.0	-1,960.2	2,406.1	-1,962.8	0.00	0.00	0.00
	1st Bone Sp	-	400.47	0.070.0	4 000 0	0.440.0	4 000 7	0.00	0.00	0.00
	9,600.0	23.45	129.17 120.17	8,970.6	-1,966.2	2,413.3	-1,968.7	0.00	0.00 0.00	0.00 0.00
	9,700.0	23.45	129.17	9,062.3	-1,991.3	2,444.2	-1,993.8	0.00		
	9,738.9	23.45	129.17	9,098.0	-2,001.1	2,456.2	-2,003.6	0.00	0.00	0.00
	1st Bone Sp	-								
	9,800.0	23.45	129.17	9,154.0	-2,016.4	2,475.0	-2,019.0	0.00	0.00	0.00
	9,900.0 10,000.0	23.45 23.45	129.17 129.17	9,245.8 9,337.5	-2,041.6 -2,066.7	2,505.9 2,536.7	-2,044.2 -2,069.4	0.00 0.00	0.00 0.00	0.00 0.00
	10,000.0	23.45	129.17	9,337.3	-2,000.7	2,550.7	-2,009.4 -2,094.5	0.00	0.00	0.00
	10,200.0	23.45 23.45	129.17	9,521.0	-2,117.0	2,598.4 2,606.5	-2,119.7	0.00 0.00	0.00 0.00	0.00 0.00
	10,226.1		129.17	9,545.0	-2,123.5	2,000.5	-2,126.3	0.00	0.00	0.00
	2nd Bone Sp 10,300.0	23.45	129.17	9,612.8	-2,142.1	2,629.3	-2,144.9	0.00	0.00	0.00
	10,300.0	23.45	129.17	9,704.5	-2,167.2	2,660.1	-2,170.0	0.00	0.00	0.00
	10,500.0	23.45	129.17	9,796.2	-2,192.4	2,691.0	-2,195.2	0.00	0.00	0.00
	10,555.3	23.45	129.17	9,847.0	-2,206.3	2,708.1	-2,209.1	0.00	0.00	0.00
	2nd Bone Sp		120.11	5,047.0	-2,200.0	2,700.1	-2,200.1	0.00	0.00	0.00
	10,600.0	23.45	129.17	9,888.0	-2,217.5	2,721.9	-2,220.4	0.00	0.00	0.00
	10,700.0	23.45	129.17	9,979.7	-2,242.6	2,752.7	-2,245.5	0.00	0.00	0.00
	10,707.9	23.45	129.17	9,987.0	-2,244.6	2,755.2	-2,247.5	0.00	0.00	0.00
	2nd Bone Sp	oring A Sand								
	10,720.2	23.45	129.17	9,998.3	-2,247.7	2,758.9	-2,250.6	0.00	0.00	0.00
	10,750.0	22.10	124.09	10,025.7	-2,254.6	2,768.2	-2,257.5	8.00	-4.53	-17.04
	10,778.2	20.98	118.74	10,052.0	-2,260.0	2,777.0	-2,262.9	8.00	-3.96	-18.94
	2nd Bone Sp	oring T/B Carb								
	10,800.0	20.24	114.27	10,072.4	-2,263.4	2,783.9	-2,266.4	8.00	-3.39	-20.59
	10,850.0	19.03	102.90	10,119.5	-2,268.8	2,799.7	-2,271.8	8.00	-2.43	-22.72
	10,898.1	18.58	91.03	10,165.0	-2,270.7	2,815.0	-2,273.7	8.00	-0.93	-24.70
	2nd Bone Sp	oring C Sand								
	10,900.0	18.58	90.55	10,166.8	-2,270.7	2,815.6	-2,273.7	8.00	-0.11	-25.11
	10,950.0	18.95	78.14	10,214.2	-2,269.1	2,831.5	-2,272.1	8.00	0.74	-24.81
	10,968.9	19.29	73.66	10,232.0	-2,267.6	2,837.5	-2,270.6	8.00	1.84	-23.77
	3rd Bone Sp	•		10.001.0			0.000			
	11,000.0	20.09	66.65	10,261.3	-2,264.1	2,847.4	-2,267.0	8.00	2.57	-22.50
	11,050.0	21.90	56.67	10,308.0	-2,255.5	2,863.0	-2,258.5	8.00	3.60	-19.97
	11,100.0	24.21	48.31	10,354.0	-2,243.6	2,878.5	-2,246.6	8.00	4.62	-16.71
	11,150.0	26.90	41.43	10,399.2	-2,228.3	2,893.6	-2,231.3	8.00	5.38	-13.76
	11,200.0 11,250.0	29.86	35.77	10,443.1	-2,209.7	2,908.4	-2,212.7	8.00 8.00	5.93 6.33	-11.32
	11,250.0	33.02	31.07	10,485.8	-2,187.9	2,922.7	-2,191.0	8.00	6.33	-9.39

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#### Planning Report

Database:	LMRKPROD3	Local Co-ordinate Reference	Well PLU 30-19 BS 108H
Company:	Long Lead_Well Planning	TVD Reference:	32+3380 @ 3412.0usft (32' KB)
Project:	PLU 30-19 BS	MD Reference:	32+3380 @ 3412.0usft (32' KB)
Site:	PLU 30-19 BS	North Reference:	Grid
Well:	PLU 30-19 BS 108H	Survey Calculation Method:	Minimum Curvature
Wellbore:	ОН		
Design:	Plan 3		

Planned Survey

Measure Depth	1	nclination	Azimuth	Vertical Depth	+N/-S	+E/-W	Vertical Section	Dogleg Rate	Build Rate (°/100usft)	Turn Rate (°/100usft)
(usft)		(°)	(°)	(usft)	(usft)	(usft)	(usft)	(°/100usft)	, ,	. ,
11,30	0.0	36.34	27.13	10,526.9	-2,163.1	2,936.5	-2,166.1	8.00	6.62	-7.89
11,35	50.0	39.76	23.77	10,566.3	-2,135.2	2,949.7	-2,138.3	8.00	6.85	-6.72
11,40		43.27	20.86	10,603.7	-2,104.6	2,962.3	-2,107.7	8.00	7.01	-5.81
11,45	50.0	46.84	18.31	10,639.1	-2,071.2	2,974.1	-2,074.3	8.00	7.14	-5.09
11,46	63.2	47.79	17.69	10,648.0	-2,062.0	2,977.1	-2,065.1	8.00	7.21	-4.72
3rd Bor	ne Sprin	g Shale								
11,50	0.0	50.46	16.05	10,672.1	-2,035.4	2,985.2	-2,038.5	8.00	7.25	-4.46
11,55	50.0	54.12	14.01	10,702.7	-1,997.2	2,995.4	-2,000.3	8.00	7.32	-4.08
11,60		57.81	12.15	10,730.7	-1,956.8	3,004.8	-1,960.0	8.00	7.38	-3.71
11,65		61.53	10.44	10,755.9	-1,914.5	3,013.2	-1,917.7	8.00	7.43	-3.42
11,70		65.27	8.85	10,778.3	-1,870.4	3,020.7	-1,873.6	8.00	7.47	-3.19
11,75	50.0	69.02	7.35	10,797.7	-1,824.8	3,027.2	-1,828.0	8.00	7.51	-3.00
11,80	0.0	72.79	5.92	10,814.1	-1,777.9	3,032.6	-1,781.1	8.00	7.53	-2.86
11,85		76.56	4.55	10,814.1	-1,729.9	3,032.0	-1,733.1	8.00	7.55	-2.74
11,85		80.34	3.22	10,837.3	-1,681.0	3,037.0	-1,684.2	8.00	7.57	-2.66
11,90		84.13	1.92	10,844.0	-1,631.6	3,040.5	-1,634.7	8.00	7.58	-2.60
12,00		87.92	0.64	10,847.5	-1,581.7	3,043.7	-1,584.9	8.00	7.58	-2.56
12,02		89.99	359.95	10,848.0	-1,554.4	3,043.8	-1,557.6	8.00	7.58	-2.55
Landing 12.02		90.00	359.94	10,848.0	-1,554.3	3,043.8	-1,557.5	8.00	7.58	-2.55
12,02		90.00	359.94	10,848.0	-1,481.7	3,043.8	-1,484.9	0.00	0.00	0.00
12,10		90.00	359.94	10,848.0	-1,381.7	3,043.6	-1,384.9	0.00	0.00	0.00
12,20		90.00	359.94	10,848.0	-1,281.7	3,043.5	-1,284.9	0.00	0.00	0.00
12,40		90.00	359.94	10,848.0	-1,181.7	3,043.4	-1,184.9	0.00	0.00	0.00
12,50		90.00	359.94	10,848.0	-1,081.7	3,043.3	-1,084.9	0.00	0.00	0.00
12,60		90.00	359.94	10,848.0	-981.7	3,043.2	-984.9	0.00	0.00	0.00
12,70		90.00	359.94	10,848.0	-881.7	3,043.1	-884.9	0.00	0.00	0.00
12,80	0.0	90.00	359.94	10,848.0	-781.7	3,043.0	-784.9	0.00	0.00	0.00
12,90	0.0	90.00	359.94	10,848.0	-681.7	3,042.9	-684.9	0.00	0.00	0.00
13,00	0.00	90.00	359.94	10,848.0	-581.7	3,042.8	-584.9	0.00	0.00	0.00
13,10	0.00	90.00	359.94	10,848.0	-481.7	3,042.7	-484.9	0.00	0.00	0.00
13,20		90.00	359.94	10,848.0	-381.7	3,042.6	-384.9	0.00	0.00	0.00
13,30	0.0	90.00	359.94	10,848.0	-281.7	3,042.5	-284.9	0.00	0.00	0.00
13,40	0.0	90.00	359.94	10,848.0	-181.7	3,042.4	-184.9	0.00	0.00	0.00
13,50		90.00	359.94	10,848.0	-81.7	3,042.3	-84.9	0.00	0.00	0.00
13,60		90.00	359.94	10,848.0	18.3	3,042.2	15.1	0.00	0.00	0.00
13,70	0.0	90.00	359.94	10,848.0	118.3	3,042.1	115.1	0.00	0.00	0.00
13,80	0.0	90.00	359.94	10,848.0	218.3	3,042.0	215.1	0.00	0.00	0.00
13,90	0.0	90.00	359.94	10,848.0	318.3	3,041.9	315.1	0.00	0.00	0.00
14,00		90.00	359.94	10,848.0	418.3	3,041.8	415.1	0.00	0.00	0.00
14,00		90.00	359.94	10,848.0	518.3	3,041.7	515.1	0.00	0.00	0.00
14,20		90.00	359.94	10,848.0	618.3	3,041.6	615.1	0.00	0.00	0.00
14,30		90.00	359.94	10,848.0	718.3	3,041.5	715.1	0.00	0.00	0.00
14,40		90.00	359.94	10,848.0	818.3	3,041.4	815.1	0.00	0.00	0.00
14,40		90.00 90.00	359.94 359.94	10,848.0	918.3	3,041.4	915.1	0.00	0.00	0.00
14,50		90.00	359.94	10,848.0	1,018.3	3,041.2	1,015.1	0.00	0.00	0.00
14,00		90.00	359.94	10,848.0	1,118.3	3,041.1	1,115.1	0.00	0.00	0.00
14,80		90.00	359.94	10,848.0	1,218.3	3,041.0	1,215.1	0.00	0.00	0.00
14,90 15,00		90.00 90.00	359.94 359.94	10,848.0	1,318.3	3,041.0 3,040.9	1,315.1 1,415.1	0.00	0.00 0.00	0.00 0.00
15,00		90.00 90.00	359.94 359.94	10,848.0 10,848.0	1,418.3 1,518.3	3,040.9 3,040.8	1,415.1	0.00 0.00	0.00	0.00
15,10		90.00 90.00	359.94 359.94	10,848.0	1,518.3	3,040.8 3,040.7	1,615.1	0.00	0.00	0.00
15,20		90.00 90.00	359.94 359.94	10,848.0	1,718.3	3,040.7	1,715.1	0.00	0.00	0.00
10,00	,0.0	50.00	000.04	10,040.0	1,710.0	0,040.0	1,710.1	0.00	0.00	0.00

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#### Planning Report

Database:	LMRKPROD3	Local Co-ordinate Reference	Well PLU 30-19 BS 108H
Company:	Long Lead_Well Planning	TVD Reference:	32+3380 @ 3412.0usft (32' KB)
Project:	PLU 30-19 BS	MD Reference:	32+3380 @ 3412.0usft (32' KB)
Site:	PLU 30-19 BS	North Reference:	Grid
Well:	PLU 30-19 BS 108H	Survey Calculation Method:	Minimum Curvature
Wellbore:	ОН		
Design:	Plan 3		

Planned Survey

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
15,400.0	90.00	359.94	10,848.0	1,818.3	3,040.5	1,815.1	0.00	0.00	0.00
15,500.0	90.00	359.94	10,848.0	1,918.3	3,040.4	1,915.1	0.00	0.00	0.00
15,600.0	90.00	359.94	10,848.0	2,018.3	3,040.3	2,015.1	0.00	0.00	0.00
15,700.0	90.00	359.94	10,848.0	2,118.3	3,040.2	2,115.1	0.00	0.00	0.00
15,800.0	90.00	359.94	10,848.0	2,218.3	3,040.1	2,215.1	0.00	0.00	0.00
15,900.0	90.00	359.94	10,848.0	2,318.3	3,040.0	2,315.1	0.00	0.00	0.00
16,000.0	90.00	359.94	10,848.0	2,418.3	3,039.9	2,415.1	0.00	0.00	0.00
16,100.0	90.00	359.94	10,848.0	2,518.3	3,039.8	2,515.1	0.00	0.00	0.00
16,200.0	90.00	359.94	10,848.0	2,618.3	3,039.7	2,615.1	0.00	0.00	0.00
16,300.0	90.00	359.94	10,848.0	2,718.3	3,039.6	2,715.1	0.00	0.00	0.00
16,400.0	90.00	359.94	10,848.0	2,818.3	3,039.5	2,815.1	0.00	0.00	0.00
16,500.0	90.00	359.94	10,848.0	2,918.3	3,039.4	2,915.1	0.00	0.00	0.00
16,600.0	90.00	359.94	10,848.0	3,018.3	3,039.3	3,015.1	0.00	0.00	0.00
16,700.0	90.00	359.94	10,848.0	3,118.3	3,039.2	3,115.1	0.00	0.00	0.00
16,800.0	90.00	359.94	10,848.0	3,218.3	3,039.1	3,215.1	0.00	0.00	0.00
16,900.0	90.00	359.94	10,848.0	3,318.3	3,039.0	3,315.1	0.00	0.00	0.00
17,000.0	90.00	359.94	10,848.0	3,418.3	3,038.9	3,415.1	0.00	0.00	0.00
17,100.0	90.00	359.94	10,848.0	3,518.3	3,038.8	3,515.1	0.00	0.00	0.00
17,200.0	90.00	359.94	10,848.0	3,618.3	3,038.7	3,615.1	0.00	0.00	0.00
17,300.0	90.00	359.94	10,848.0	3,718.3	3,038.6	3,715.1	0.00	0.00	0.00
17,400.0	90.00	359.94	10,848.0	3,818.3	3,038.5	3,815.1	0.00	0.00	0.00
17,500.0	90.00	359.94	10,848.0	3,918.3	3,038.4	3,915.1	0.00	0.00	0.00
17,600.0	90.00	359.94	10,848.0	4,018.3	3,038.3	4,015.1	0.00	0.00	0.00
17,700.0	90.00	359.94	10,848.0	4,118.3	3,038.2	4,115.1	0.00	0.00	0.00
17,800.0	90.00	359.94	10,848.0	4,218.3	3,038.1	4,215.1	0.00	0.00	0.00
17,900.0	90.00	359.94	10,848.0	4,318.3	3,038.0	4,315.1	0.00	0.00	0.00
18,000.0	90.00	359.94	10,848.0	4,418.3	3,037.9	4,415.1	0.00	0.00	0.00
18,100.0	90.00	359.94	10,848.0	4,518.3	3,037.8	4,515.1	0.00	0.00	0.00
18,200.0	90.00	359.94	10,848.0	4,618.3	3,037.7	4,615.1	0.00	0.00	0.00
18,300.0	90.00	359.94	10,848.0	4,718.3	3,037.6	4,715.1	0.00	0.00	0.00
18,400.0	90.00	359.94	10,848.0	4,818.3	3,037.5	4,815.1	0.00	0.00	0.00
18,500.0	90.00	359.94	10,848.0	4,918.3	3,037.4	4,915.1	0.00	0.00	0.00
18,600.0	90.00	359.94	10,848.0	5,018.3	3,037.3	5,015.1	0.00	0.00	0.00
18,700.0	90.00	359.94	10,848.0	5,118.3	3,037.2	5,115.1	0.00	0.00	0.00
18,800.0	90.00	359.94	10,848.0	5,218.3	3,037.1	5,215.1	0.00	0.00	0.00
18,900.0	90.00	359.94	10,848.0	5,318.3	3,037.0	5,315.1	0.00	0.00	0.00
19,000.0	90.00	359.94	10,848.0	5,418.3	3,036.9	5,415.1	0.00	0.00	0.00
19,100.0	90.00	359.94	10,848.0	5,518.3	3,036.8	5,515.1	0.00	0.00	0.00
19,200.0	90.00	359.94	10,848.0	5,618.3	3,036.7	5,615.1	0.00	0.00	0.00
19,300.0	90.00	359.94	10,848.0	5,718.3	3,036.6	5,715.1	0.00	0.00	0.00
19,400.0	90.00	359.94	10,848.0	5,818.3	3,036.5	5,815.1	0.00	0.00	0.00
19,500.0	90.00	359.94	10,848.0	5,918.3	3,036.4	5,915.1	0.00	0.00	0.00
19,600.0	90.00	359.94	10,848.0	6,018.3	3,036.3	6,015.1	0.00	0.00	0.00
19,700.0	90.00	359.94	10,848.0	6,118.3	3,036.2	6,115.1	0.00	0.00	0.00
19,800.0	90.00	359.94	10,848.0	6,218.3	3,036.1	6,215.1	0.00	0.00	0.00
19,900.0	90.00	359.94	10,848.0	6,318.3	3,036.0	6,315.1	0.00	0.00	0.00
20,000.0	90.00	359.94	10,848.0	6,418.3	3,035.9	6,415.1	0.00	0.00	0.00
20,100.0	90.00	359.94	10,848.0	6,518.3	3,035.8	6,515.1	0.00	0.00	0.00
20,200.0	90.00	359.94	10,848.0	6,618.3	3,035.7	6,615.1	0.00	0.00	0.00
20,300.0	90.00	359.94	10,848.0	6,718.3	3,035.6	6,715.1	0.00	0.00	0.00
20,400.0	90.00	359.94	10,848.0	6,818.3	3,035.5	6,815.1	0.00	0.00	0.00
20,500.0	90.00	359.94	10,848.0	6,918.3	3,035.4	6,915.1	0.00	0.00	0.00
20,600.0	90.00	359.94	10,848.0	7,018.3	3,035.3	7,015.1	0.00	0.00	0.00

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#### Planning Report

Database:	LMRKPROD3	Local Co-ordinate Reference	Well PLU 30-19 BS 108H
Company:	Long Lead_Well Planning	TVD Reference:	32+3380 @ 3412.0usft (32' KB)
Project:	PLU 30-19 BS	MD Reference:	32+3380 @ 3412.0usft (32' KB)
Site:	PLU 30-19 BS	North Reference:	Grid
Well:	PLU 30-19 BS 108H	Survey Calculation Method:	Minimum Curvature
Wellbore:	ОН		
Design:	Plan 3		

Planned Survey

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
20,700.0	90.00	359.94	10,848.0	7,118.3	3,035.2	7,115.1	0.00	0.00	0.00
20,800.0	90.00	359.94	10,848.0	7,218.3	3,035.1	7,215.1	0.00	0.00	0.00
20,900.0	90.00	359.94	10,848.0	7,318.3	3,035.0	7,315.1	0.00	0.00	0.00
21,000.0	90.00	359.94	10,848.0	7,418.3	3,034.9	7,415.1	0.00	0.00	0.00
21,100.0	90.00	359.94	10,848.0	7,518.3	3,034.8	7,515.1	0.00	0.00	0.00
21,200.0	90.00	359.94	10,848.0	7,618.3	3,034.7	7,615.1	0.00	0.00	0.00
21,300.0	90.00	359.94	10,848.0	7,718.3	3,034.6	7,715.1	0.00	0.00	0.00
21,400.0	90.00	359.94	10,848.0	7,818.3	3,034.5	7,815.1	0.00	0.00	0.00
21,500.0	90.00	359.94	10,848.0	7,918.3	3,034.4	7,915.1	0.00	0.00	0.00
21,600.0	90.00	359.94	10,848.0	8,018.3	3,034.3	8,015.1	0.00	0.00	0.00
21,700.0	90.00	359.94	10,848.0	8,118.3	3,034.2	8,115.1	0.00	0.00	0.00
21,800.0	90.00	359.94	10,848.0	8,218.3	3,034.1	8,215.1	0.00	0.00	0.00
21,900.0	90.00	359.94	10,848.0	8,318.3	3,034.0	8,315.1	0.00	0.00	0.00
22,008.3	90.00	359.94	10,848.0	8,426.6	3,033.9	8,423.4	0.00	0.00	0.00
22,107.3	90.00	359.94	10,848.0	8,525.6	3,033.8	8,522.4	0.00	0.00	0.00

Design Targets									
Target Name - hit/miss target - Shape	Dip Angle (°)	Dip Dir. (°)	TVD (usft)	+N/-S (usft)	+E/-W (usft)	Northing (usft)	Easting (usft)	Latitude	Longitude
LTP PLU 30-19 BS 108F - plan hits target cen - Point	0.00 ter	0.00	10,848.0	8,426.6	3,033.9	411,447.10	665,312.00	32° 7' 48.210 N	103° 47' 57.508 W
FTP PLU 30-19 BS 108ł - plan hits target cen - Point	0.00 ter	0.00	10,848.0	-1,554.3	3,043.8	401,466.20	665,321.90	32° 6' 9.437 N	103° 47' 57.968 W
BHL PLU 30-19 BS 108ł - plan misses target - Point	0.00 center by 0.5u	0.00 Isft at 22107	10,848.0 .3usft MD (1	8,525.6 0848.0 TVD, 8	3,033.3 3525.6 N, 3033	411,546.10 3.8 E)	665,311.40	32° 7' 49.189 N	103° 47' 57.510 W

## Planning Report

Database:	LMRKPROD3	Local Co-ordinate Reference	Well PLU 30-19 BS 108H
Company:	Long Lead_Well Planning	TVD Reference:	32+3380 @ 3412.0usft (32' KB)
Project:	PLU 30-19 BS	MD Reference:	32+3380 @ 3412.0usft (32' KB)
Site:	PLU 30-19 BS	North Reference:	Grid
Well:	PLU 30-19 BS 108H	Survey Calculation Method:	Minimum Curvature
Wellbore:	ОН		
Design:	Plan 3		

#### Formations

	Measured Depth (usft)	Vertical Depth (usft)	Name	Lithology	Dip (°)	Dip Direction (°)	
	810.0	810.0	Rustler				
	1,180.0	1,180.0	Salado				
	4,202.6	4,019.0	Base of Salt				
	4,409.7	4,209.0	Delaware				
	5,432.2	5,147.0	Cherry Canyon				
	7,265.6	6,829.0	Brushy Canyon				
	8,434.1	7,901.0	Basal Brushy Canyon				
	8,689.2	8,135.0	Bone Spring Lm.				
	8,837.4	8,271.0	Avalon Shale				
	9,392.3	8,780.0	Lower Avalon Shale				
	9,576.5	8,949.0	1st Bone Spring Lime				
	9,738.9	9,098.0	1st Bone Spring Sand				
	10,226.1	9,545.0	2nd Bone Spring Lime				
	10,555.3	9,847.0	2nd Bone Spring Sand				
	10,707.9	9,987.0	2nd Bone Spring A Sand				
	10,778.2	10,052.0	2nd Bone Spring T/B Carb				
	10,898.1	10,165.0	2nd Bone Spring C Sand				
	10,968.9	10,232.0	3rd Bone Spring Lime				
	11,463.2	10,648.0	3rd Bone Spring Shale				
l	12,027.3	10,848.0	Landing				

#### DRILLING PLAN: BLM COMPLIANCE (Supplement to BLM 3160-3)

XTO Energy Inc. POKER LAKE UNIT 30-19 BS 108H Projected TD: 22107.3' MD / 10848' TVD SHL: 541' FNL & 272' FEL , Section 30, T25S, R31E BHL: 2664' FSL & 2535' FEL , Section 17, T25S, R31E EDDY County, NM

#### 1. Geologic Name of Surface Formation

A. Quaternary

#### 2. Estimated Tops of Geological Markers & Depths of Anticipated Fresh Water, Oil or Gas

Formation	Well Depth (TVD)	Water/Oil/Gas
Rustler	810'	Water
Top of Salt	1180'	Water
Base of Salt	4019'	Water
Delaware	4209'	Water
Brushy Canyon	6829'	Water/Oil/Gas
Bone Spring	8135'	Water
1st Bone Spring	8949'	Water/Oil/Gas
2nd Bone Spring	9545'	Water/Oil/Gas
3rd Bone Spring	10232'	Water/Oil/Gas
Target/Land Curve	10848'	Water/Oil/Gas

\*\*\* Hydrocarbons @ Brushy Canyon

\*\*\* Groundwater depth 40' (per NM State Engineers Office).

No other formations are expected to yield oil, gas or fresh water in measurable volumes. The surface fresh water sands will be protected by setting 9.625 inch casing @ 910' (270' above the salt) and circulating cement back to surface. The intermediate will isolate from the top of salt down to the next casing seat by setting 7.625 inch casing at 10520.2' and cemented to surface. A 6.75 inch curve and 6.75 inch lateral hole will be drilled to 22107.3 MD/TD and 5.5 inch production casing will be set at TD and cemented back up in the intermediate shoe (estimated TOC 10220.2 feet).

#### 3. Casing Design

Hole Size	Depth	OD Csg	Weight	Grade	Collar	New/Used	SF Burst	SF Collapse	SF Tension
12.25	0' – 910'	9.625	40	J-55	BTC	New	1.21	6.92	17.31
8.75	0' – 4000'	7.625	29.7	RY P-110	Flush Joint	New	2.03	2.52	1.79
8.75	4000' – 10520.2'	7.625	29.7	HC L-80	Flush Joint	New	1.47	1.75	2.10
6.75	0' – 10420.2'	5.5	20	RY P-110	Semi-Premium	New	1.26	1.64	2.06
6.75	10420.2' - 22107.3'	5.5	20	RY P-110	Semi-Flush	New	1.26	1.57	2.06

 $\cdot$  XTO requests the option to utilize a spudder rig (Atlas Copco RD20 or Equivalent) to set and cement

surface casing per this Sundry

 $\cdot$  XTO requests to not utilize centralizers in the curve and lateral

 $\cdot$  7.625 Collapse analyzed using 50% evacuation based on regional experience.

5.5 Tension calculated using vertical hanging weight plus the lateral weight multiplied by a friction factor of 0.35

 $\cdot$  Test on Casing will be limited to 70% burst of the casing or 1500 psi, whichever is less

· XTO requests the option to use 5" BTC Float equipment for the the production casing

#### Wellhead:

- Permanent Wellhead Multibowl System A. Starting Head: 11" 10M top flange x 9-5/8" bottom B. Tubing Head: 11" 10M bottom flange x 7-1/16" 15M top flange · Wellhead will be installed by manufacturer's representatives.
  - · Manufacturer will monitor welding process to ensure appropriate temperature of seal.
  - · Operator will test the 7-5/8" casing per BLM Onshore Order 2
  - $\cdot$  Wellhead Manufacturer representative will not be present for BOP test plug installation

#### Surface Casing: 9.625, 40 New BTC, J-55 casing to be set at +/- 910'

Lead: 200 sxs EconoCem-HLTRRC (mixed at 10.5 ppg, 1.87 ft3/sx, 10.13 gal/sx water) Tail: 130 sxs Class C + 2% CaCl (mixed at 14.8 ppg, 1.35 ft3/sx, 6.39 gal/sx water) Top of Cement: Surface Compressives: 12-hr = 900 psi 24 hr = 1500 psi

2nd Intermediate Casing: 7.625, 29.7 New casing to be set at +/- 10520.2' <u>1st Stage</u> Optional Lead: 370 sxs Class C (mixed at 10.5 ppg, 2.77 ft3/sx, 15.59 gal/sx water)

 TOC: Surface

 Tail: 340 sxs Class C (mixed at 14.8 ppg, 1.35 ft3/sx, 6.39 gal/sx water)

 TOC: Brushy Canyon @ 6829

 Compressives:
 12-hr =
 900 psi
 24 hr = 1150 psi

 2nd Stage

 Lead: 0 sxs Class C (mixed at 12.9 ppg, 2.16 ft3/sx, 9.61 gal/sx water)

 Tail: 770 sxs Class C (mixed at 14.8 ppg, 1.33 ft3/sx, 6.39 gal/sx water)

 Top of Cement: 0

 Compressives:
 12-hr =
 900 psi
 24 hr = 1150 psi

XTO requests to pump a two stage cement job on the 7-5/8" intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brush Canyon (6829') and the second stage performed as a bradenhead squeeze with planned cement from the Brushy Canyon to surface. If cement is not visually confirmed to circulate to surface, the final cement top after the second stage job will be verified by Echo-meter. If necessary, a top out consisting of 1,500 sack of Class C cement + 3% Salt + 1% PreMag-M + 6% Bentonite Gel (2.30 yld, 12.91 ppg) will be executed as a contingency. If cement is still unable to circulate to surface, another Echo-meter run will be performed for cement top verification.

XTO will report to the BLM the volume of fluid (limited to 5 bbls) used to flush intermediate casing valves following backside cementing procedures.

XTO requests to pump an Optional Lead if well conditions dictate in an attempt to bring cement inside the first intermediate casing. If cement reaches the desired height, the BLM will be notified and the second stage bradenhead squeeze and subsequent TOC verification will be negated.

XTO requests the option to conduct the bradenhead squeeze and TOC verification offline as per standard approval from BLM when unplanned remediation is needed and batch drilling is approved. In the event the bradenhead is conducted, we will ensure the first stage cement job is cemented properly and the well is static with floats holding and no pressure on the csg annulus as with all other casing strings where batch drilling operations occur before moving off the rig. The TA cap will also be installed per Cactus procedure and pressure inside the casing will be monitored via the valve on the TA cap as per standard batch drilling ops.

#### Production Casing: 5.5, 20 New Semi-Flush, RY P-110 casing to be set at +/- 22107.3'

Lead: 20 sxs NeoCerr	n (mixed at 11.5 p	opg, 2.69 ft3/sx,	15.00 gal/sx water) Top of Cement:	10220.2 feet
Tail: 810 sxs VersaCe	m (mixed at 13.2	2 ppg, 1.51 ft3/s	k, 8.38 gal/sx water) Top of Cement:	10720.2 feet
Compressives:	12-hr =	800 psi	24 hr = 1500 psi	

XTO requests the option to offline cement and remediate (if needed) surface and intermediate casing strings where batch drilling is approved and if unplanned remediation is needed. XTO will ensure well is static with no pressure on the csg annulus, as with all other casing strings where batch drilling operations occur before moving off the rig. The TA cap will also be installed when applicable per Cactus procedure and pressure inside the casing will be monitored via the valve on the TA cap as per standard batch drilling ops. Offline cement operations will then be conducted after the rig is moved off the current well to the next well in the batch sequence.

#### 5. Pressure Control Equipment

Once the permanent WH is installed on the 9.625 casing, the blow out preventer equipment (BOP) will consist of a 13-5/8" minimum 5M Hydril and a 13-5/8" minimum 5M Double Ram BOP. MASP should not exceed 4665 psi. In any instance where 10M BOP is required by BLM, XTO requests a variance to utilize 5M annular with 10M ram preventers (a common BOP configuration, which allows use of 10M rams in unlikely event that pressures exceed 5M).

All BOP testing will be done by an independent service company. Annular pressure tests will be limited to 50% of the working pressure. When nippling up on the 9.625, 5M bradenhead and flange, the BOP test will be limited to 5000 psi. When nippling up on the 7.625, the BOP will be tested to a minimum of 5000 psi. All BOP tests will include a low pressure test as per BLM regulations. The 5M BOP diagrams are attached. Blind rams will be functioned tested each trip, pipe rams will be functioned tested each day.

A variance is requested to allow use of a flex hose as the choke line from the BOP to the Choke Manifold. If this hose is used, a copy of the manufacturer's certification and pressure test chart will be kept on the rig. Attached is an example of a certification and pressure test chart. The manufacturer does not require anchors.

XTO requests a variance to be able to batch drill this well if necessary. In doing so, XTO will set casing and ensure that the well is cemented properly (unless approval is given for offline cementing) and the well is static. With floats holding, no pressure on the csg annulus, and the installation of a 10K TA cap as per Cactus recommendations, XTO will contact the BLM to skid the rig to drill the remaining wells on the pad. Once surface and both intermediate strings are all completed, XTO will begin drilling the production

hole on each of the wells.

A variance is requested to **ONLY** test broken pressure seals on the BOP equipment when moving from wellhead to wellhead which is in compliance with API Standard 53. API standard 53 states, that for pad drilling operation, moving from one wellhead to another within 21 days, pressure testing is required for pressure-containing and pressure-controlling connections when the integrity of a pressure seal is broken. Based on discussions with the BLM on February 27th 2020, we will request permission to **ONLY** retest broken pressure seals if the following conditions are met: 1. After a full BOP test is conducted on the first well on the pad 2. When skidding to drill an intermediate section that does not penetrate into the Wolfcamp.

#### 6. Proposed Mud Circulation System

INTERVAL	Hole Size	Mud Type	MW	Viscosity	Fluid Loss
	TIDIE SIZE		(ppg)	(sec/qt)	(cc)
0' - 910'	12.25	FW/Native	8.4-8.9	35-40	NC
910' - 10520.2'	8.75	FW / Cut Brine / Direct Emulsion	10.2-10.7	30-32	NC
10520.2' - 22107.3'	6.75	ОВМ	12.5-13	50-60	NC - 20

The necessary mud products for weight addition and fluid loss control will be on location at all times.

Spud with fresh water/native mud. Drill out from under 9-5/8" surface casing with brine solution. A 9.7 ppg - 10.2 ppg cut brine mud will be used while drilling through the salt formation. Use fibrous materials as needed to control seepage and lost circulation. Pump viscous sweeps as needed for hole cleaning. Pump speed will be recorded on a daily drilling report after mudding up. A Pason or Totco will be used to detect changes in loss or gain of mud volume. A mud test will be performed every 24 hours to determine: density, viscosity, strength, filtration and pH as necessary. Use available solids controls equipment to help keep mud weight down after mud up. Rig up solids control equipment to operate as a closed loop system.

#### 7. Auxiliary Well Control and Monitoring Equipment

- A. A Kelly cock will be in the drill string at all times.
- B. A full opening drill pipe stabbing valve having appropriate connections will be on the rig floor at all times.
- C. H2S monitors will be on location when drilling below the 9.625 casing.

#### 8. Logging, Coring and Testing Program

Mud Logger: Mud Logging Unit (2 man) below intermediate casing.

Open hole logging will not be done on this well.

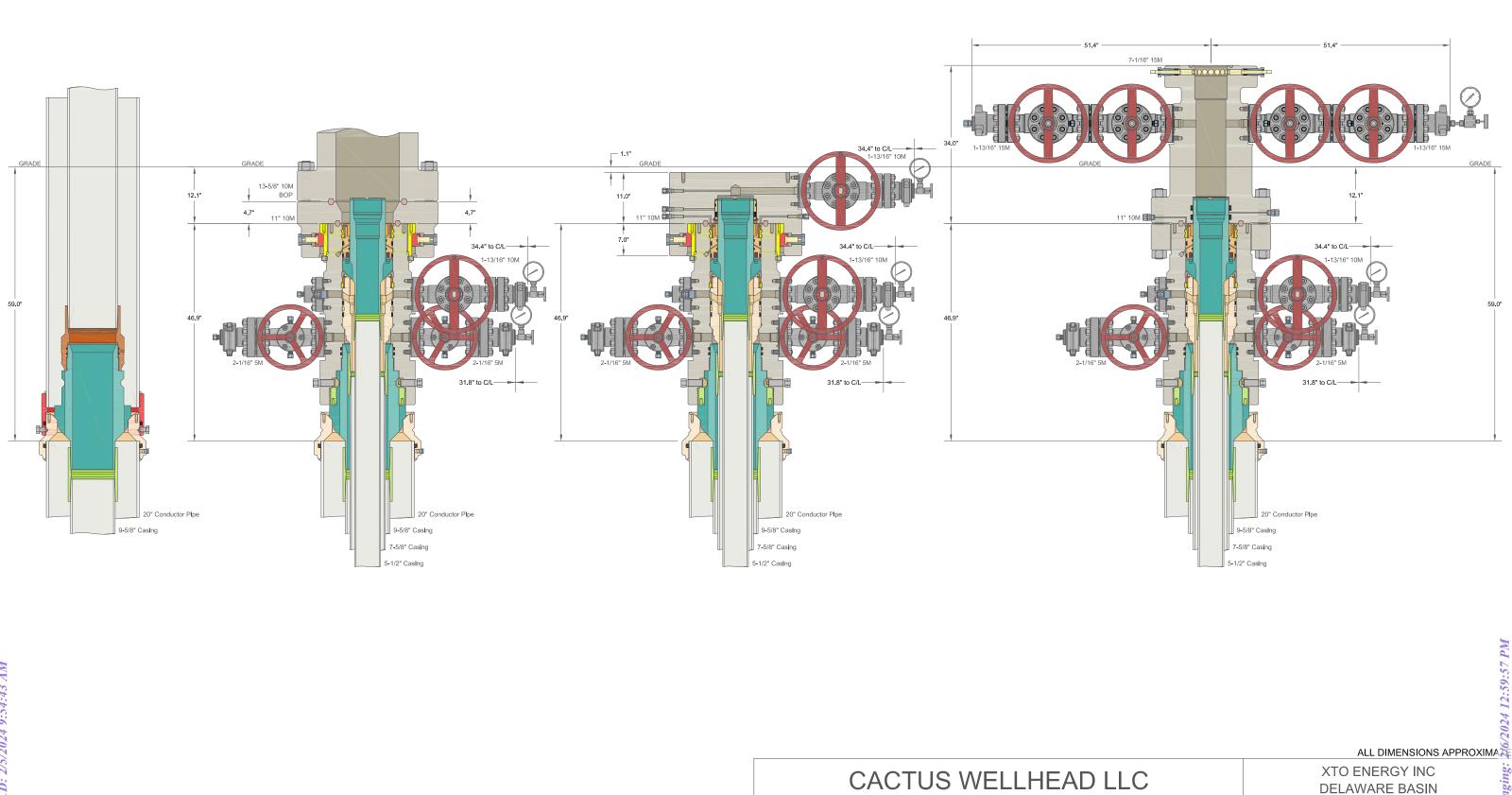
#### 9. Abnormal Pressures and Temperatures / Potential Hazards

None Anticipated. BHT of 175 to 195 F is anticipated. No H2S is expected but monitors will be in place to detect any H2S occurrences. Should these circumstances be encountered the operator and drilling contractor are prepared to take all necessary steps to ensure safety of all personnel and environment. Lost circulation could occur but is not expected to be a serious problem in this area and hole seepage will be compensated for by additions of small amounts of LCM in the drilling fluid. The maximum anticipated bottom hole pressure for this well is 7051 psi.

#### 10. Anticipated Starting Date and Duration of Operations

Anticipated spud date will be after BLM approval. Move in operations and drilling is expected to take 40 days.





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20" x 9-5/8" x 7-5/8" x 5-1/2" MBU-T-CFL-R-DBLO We With 11" 10M x 7-1/16" 15M CTH-DBLHPS Tubing H And 9-5/8", 7-5/8" & 5-1/2" Pin Bottom Mandrel Casing H

ellhead	DRAWN	VJK
	APPRV	
Head		
Hangers	DRAWING N	D. <b>HB</b>

HBE0000479

31MAR22

**Subject:** Request for a Variance Allowing break Testing of the Blowout Preventer Equipment (BOPE)

XTO Energy requests a variance to ONLY test broken pressure seals on the BOPE and function test BOP when skidding a drilling rig between multiple wells on a pad.

#### Background

Onshore Oil and Gas Order CFR Title 43 Part 3170, Drilling Operations, Sections III.A.2.i.iv.B states that the BOP test must be performed whenever any seal subject to test pressure is broken. The current interpretation of the Bureau of Land Management (BLM) requires a complete BOP test and not just a test of the affected component. CFR Title 43 Part 3170 states, "Some situation may exist either on a well-by- well basis or field-wide basis whereby it is commonly accepted practice to vary a particular minimum standard(s) established in this order. This situation can be resolved by requesting a variance...". XTO Energy feels the break testing the BOPE is such a situation. Therefore, as per CFR Title 43 Part 3170, XTO Energy submits this request for the variance.

#### **Supporting Documentation**

CFR Title 43 Part 3170 became effective on December 19, 1988 and has remained the standard for regulating BLM onshore drilling operations for over 30 years. During this time there have been significant changes in drilling technology. BLM continues to use the variance request process to allow for the use of modern technology and acceptable engineering practices that have arisen since CFR Title 43 Part 3170 was originally released. The XTO Energy drilling rig fleet has many modern upgrades that allow the intact BOP stack to be moved between well slots on a multi-well pad, as well as, wellhead designs that incorporate quick connects facilitating release of the BOP from the wellhead without breaking any BOP stack components apart. These technologies have been used extensively offshore, and other regulators, API, and many operators around the world have endorsed break testing as safe and reliable.



Figure 1: Winch System attached to BOP Stack



Figure 2: BOP Winch System

American Petroleum Institute (API) standards, specification and recommended practices are considered the industry standard and are consistently utilized and referenced by the industry. CFR Title 43 Part 3170recognizes API recommended Practices (RP) 53 in its original development. API Standard 53, *Well Control Equipment Systems for Drilling Wells* (Fifth Edition, December 2018, Annex C, Table C.4) recognizes break testing as an acceptable practice. Specifically, API Standard 53, Section 5.3.7.1 states "A pressure test of the pressure containing component shall be performed following the disconnection or repair, limited to the affected component." See Table C.4 below for reference.

1. The state of th		Pressure Test-	-High Pressure <sup>ac</sup>
Component to be Pressure Tested	Pressure Test—Low Pressure <sup>ac</sup> psig (MPa)	Change Out of Component, Elastomer, or Ring Gasket	No Change Out of Component, Elastomer, or Ring Gasket
Annular preventer <sup>b</sup>	250 to 350 (1.72 to 2.41)	RWP of annular preventer	MASP or 70% annular RWP, whichever is lower.
Fixed pipe, variable bore, blind, and BSR preventers <sup>bd</sup>	250 to 350 (1.72 to 2.41)	RWP of ram preventer or wellhead system, whichever is lower	ITP
Choke and kill line and BOP side outlet valves below ram preventers (both sides)	250 to 350 (1.72 to 2.41)	RWP of side outlet valve or wellhead system, whichever is lower	ITP
Choke manifold—upstream of chokes <sup>e</sup>	250 to 350 (1.72 to 2.41)	RWP of ram preventers or wellhead system, whichever is lower	ITP
Choke manifold—downstream of chokes <sup>e</sup>	250 to 350 (1.72 to 2.41)	RWP of valve(s), line(s), or M whichever is lower	MASP for the well program,
Kelly, kelly valves, drill pipe safety valves, IBOPs	250 to 350 (1.72 to 2.41)	MASP for the well program	
	during the evaluation period. The p	h pressure shall not decrease below the allest OD drill pipe to be used in well	
	from one wellhead to another withi when the integrity of a pressure se	n the 21 days, pressure testing is req al is broken.	uired for pressure-containing ar
<sup>d</sup> For surface offshore operations, th	he ram BOPs shall be pressure tes land operations, the ram BOPs sha	al is broken. ted with the ram locks engaged and all be pressure tested with the ram lo	

The Bureau of Safety and Environmental Enforcement (BSEE), Department of Interior, has also utilized the API standards, specification and best practices in the development of its offshore oil and gas regulations and incorporates them by reference within its regulations.

Break testing has been approved by the BLM in the past with other operators based on the detailed information provided in this document.

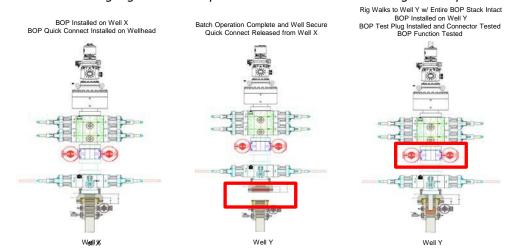
XTO Energy feels break testing and our current procedures meet the intent of CFR Title 43 Part 317 0and often exceed it. There has been no evidence that break testing results in more components failing than seen on full BOP tests. XTO Energy's internal standards requires complete BOPE tests more often than that of CFR Title 43 Part 3170 (Every 21 days). In addition to function testing the annular, pipe rams and blind rams after

each BOP nipple up, XTO Energy performs a choke drill with the rig crew prior to drilling out every casing shoe. This is additional training for the rig crew that exceeds the requirements of the CFR Title 43 Part 3170.

## **Procedures**

- 1. XTO Energy will use this document for our break testing plan for New Mexico Delaware basin. The summary below will be referenced in the APD or Sundry Notice and receive approval prior to implementing this variance.
- 2. XTO Energy will perform BOP break testing on multi-wells pads where multiple intermediate sections can be drilled and cased within the 21-day BOP test window.
  - a. A full BOP test will be conducted on the first well on the pad.
  - b. The first intermediate hole section drilled on the pad will be the deepest. All of the remaining hole sections will be the same depth or shallower.
    - i. Our Lower WC targets set the intermediate casing shoe no deeper than the Wolfcamp B.
    - ii. Our Upper WC targets set the intermediate casing shoe shallower than the Wolfcamp B.
  - c. A Full BOP test will be required if the intermediate hole section being drilled has a MASP over 5M.
  - d. A full BOP test will be required prior to drilling any production hole.
- 3. After performing a complete BOP test on the first well, the intermediate hole section will be drilled and cased, two breaks would be made on the BOP equipment.
  - a. Between the HCV valve and choke line connection
  - b. Between the BOP quick connect and the wellhead
- 4. The BOP is then lifted and removed from the wellhead by a hydraulic system.
- 5. After skidding to the next well, the BOP is moved to the wellhead by the same hydraulic system and installed.
- 6. The connections mentioned in 3a and 3b will then be reconnected.
- 7. Install test plug into the wellhead using test joint or drill pipe.
- 8. A shell test is performed against the upper pipe rams testing the two breaks.
- 9. The shell test will consist of a 250 psi low test and a high test to the value submitted in the APD or Sundry (e.g. 5,000 psi or 10,000psi).
- 10. Function test will be performed on the following components: lower pipe rams, blind rams, and annular.

- 11. For a multi-well pad the same two breaks on the BOP would be made and on the next wells and steps 4 through 10 would be repeated.
- 12. A second break test would only be done if the intermediate hole section being drilled could not be completed within the 21 day BOP test window.



*Note: Picture below highlights BOP components that will be tested during batch operations* 

#### **Summary**

A variance is requested to **ONLY** test broken pressure seals on the BOP equipment when moving from wellhead to wellhead which is in compliance with API Standard 53. API Standard 53 states, that for pad drilling operation, moving from one wellhead to another within 21 days, pressure testing is required for pressure-containing and pressure-controlling connections when the integrity of a pressure seal is broken.

The BOP will be secured by a hydraulic carrier or cradle. The BLM will be contacted if a Well Control event occurs prior to the commencement of a BOPE Break Testing operation.

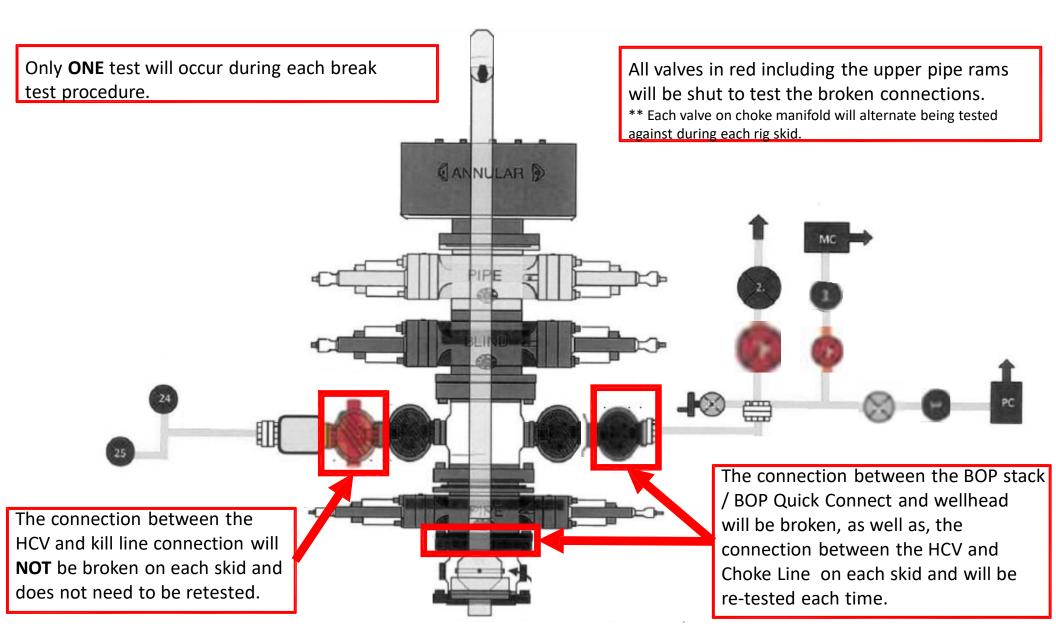
Based on discussions with the BLM on February 27th 2020 and the supporting documentation submitted to the BLM, we will request permission to ONLY retest broken pressure seals if the following conditions are met:

1. After a full BOP test is conducted on the first well on the pad.

2. The first intermediate hole section drilled on the pad will be the deepest. All of the remaining hole sections will be the same depth or shallower.

3. Full BOP test will be required if the intermediate hole section being drilled has a MASP over 5M.

4. Full BOP test will be required prior to drilling the production hole.



XTO respectfully requests approval to utilize a spudder rig to pre-set surface casing.

Description of Operations:

- 1. Spudder rig will move in to drill the surface hole and pre-set surface casing on the well.
  - a. After drilling the surface hole section, the spudder rig will run casing and cement following all of the applicable rules and regulations (OnShore Order 2, all COAs and NMOCD regulations).
  - b. The spudder rig will utilize fresh water-based mud to drill the surface hole to TD. Solids control will be handled entirely on a closed loop basis. No earth pits will be used.
- 2. The wellhead will be installed and tested as soon as the surface casing is cut off and WOC time has been reached.
- 3. A blind flange at the same pressure rating as the wellhead will be installed to seal the wellbore. Pressure will be monitored with needle valves installed on two wing valves.
  - a. A means for intervention will be maintained while the drilling rig is not over the well.
- 4. Spudder rig operations are expected to take 2-3 days per well on the pad.
- 5. The BLM will be contacted and notified 24 hours prior to commencing spudder rig operations.
- 6. Drilling Operations will begin with a larger rig and a BOP stack equal to or greater than the pressure rating that was permitted will be nippled up and tested on the wellhead before drilling operations resume on each well.
  - a. The larger rig will move back onto the location within 180 days from the point at which the wells are secured and the spudder rig is moved off location.
  - b. The BLM will be notified 24 hours before the larger rig moves back on the pre-set locations
- 7. XTO will have supervision on the rig to ensure compliance with all BLM and NMOCD regulations and to oversee operations.
- 8. Once the rig is removed, XTO will secure the wellhead area by placing a guard rail around the cellar area.

District I 1625 N. French Dr., Hobbs, NM 88240 Phone:(575) 393-6161 Fax:(575) 393-0720 District II

811 S. First St., Artesia, NM 88210 Phone:(575) 748-1283 Fax:(575) 748-9720

District III

1000 Rio Brazos Rd., Aztec, NM 87410 Phone:(505) 334-6178 Fax:(505) 334-6170

District IV

1220 S. St Francis Dr., Santa Fe, NM 87505 Phone: (505) 476-3470 Fax: (505) 476-3462

# **State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division** 1220 S. St Francis Dr. Santa Fe, NM 87505

CONDITIONS

Operator:	OGRID:
XTO PERMIAN OPERATING LLC.	373075
6401 HOLIDAY HILL ROAD	Action Number:
MIDLAND, TX 79707	311169
	Action Type:
	[C-103] NOI Change of Plans (C-103A)

#### CONDITIONS

Created By	Condition	Condition Date
ward.rikala	All original COA's still apply. Additionally, if cement is not circulated to surface during any cementing, then a CBL is required.	2/6/2024

CONDITIONS

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Action 311169

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