# Sundry Print Reports 01/25/2024

U.S. Department of the Interior BUREAU OF LAND MANAGEMENT

Well Name: MARWARI 21-16 STATE Well Location: T25S / R32E / SEC 21 / County or Parish/State:

FED COM SESW /

Well Number: 522H Type of Well: OIL WELL Allottee or Tribe Name:

Lease Number: NMLC0062300 Unit or CA Name: Unit or CA Number:

**US Well Number:** 3002552373 **Well Status:** Approved Application for **Operator:** DEVON ENERGY

Permit to Drill PRODUCTION COMPANY LP

## **Notice of Intent**

**Sundry ID: 2766950** 

Type of Submission: Notice of Intent

Type of Action: APD Change

Date Sundry Submitted: 01/02/2024 Time Sundry Submitted: 02:40

Date proposed operation will begin: 12/20/2023

**Procedure Description:** Devon Energy Production Co., L.P. (Devon) respectfully requests to change the well name, SHL, BHL, and depth on the subject well. Please see attached revised C102, drill plan (break test variance included), and directional plan. Permitted Well name: VAN DOO DAH 28-33 FED COM 733H Proposed Well name: MARWARI 21-16 STATE FED COM 522H Permitted SHL: SESW 200 FSL, 1570 FWL, 21-25S-32E Proposed SHL: SESW 500 FSL, 1610 FWL, 21-25S-32E Permitted BHL: SESW 20 FSL, 2310 FWL, 33-25S-32E Proposed BHL: NWNW 20 FNL, 990 FWL, 16-25S-32E Permitted TVD/MD: 12359/22601 - [98270] WC-025 G-08 S253216D; UPPER WOLFCAMP Proposed TVD/MD: 8959/19390 - [96715] WC-025 G-05 S253209L; BONE SPRING New leases have been added since approved APD and notification has been given. US Well Number: 30-025-52373

# **NOI Attachments**

## **Procedure Description**

WA017743683\_MARWARI\_21\_16\_STATE\_FED\_COM\_522H\_WL\_R3\_20240102143949.pdf

13.375\_54.50\_J55\_SEAH\_20231220125230.pdf

MARWARI\_21\_16\_STATE\_FED\_COM\_522H\_20231220125230.pdf

break\_test\_variance\_BOP\_20231220125230.pdf

MARWARI\_21\_16\_STATE\_FED\_COM\_522H\_Directional\_Plan\_12\_19\_23\_20231220125230.pdf

9.625\_40lb\_J55\_SeAH\_20231220125230.pdf

 $5.5 in\_x\_17.00 lb\_P110 EC\_DWC\_C\_IS\_PLUS\_\_5\_23\_2023\_20231220125230.pdf$ 

Page 1 of 2

eived by OCD: 1/25/2024 9:23:03 AM. Well Name: MARWARI 21-16 STATE

FED COM

Well Location: T25S / R32E / SEC 21 / SESW /

County or Parish/State:

Well Number: 522H

Type of Well: OIL WELL

**Allottee or Tribe Name:** 

Page 2 of

Lease Number: NMLC0062300

**Unit or CA Name:** 

**Unit or CA Number:** 

**US Well Number: 3002552373** 

Well Status: Approved Application for Permit to Drill

**Operator: DEVON ENERGY** PRODUCTION COMPANY LP

# **Conditions of Approval**

# **Additional**

Sundry\_ID\_2766950\_20240122085626.pdf

Sundry\_ID\_2766948\_COA\_20240122085626.pdf

# **Operator**

I certify that the foregoing is true and correct. Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction. Electronic submission of Sundry Notices through this system satisfies regulations requiring a

Operator Electronic Signature: SHAYDA OMOUMI Signed on: JAN 02, 2024 02:40 PM

Name: DEVON ENERGY PRODUCTION COMPANY LP

Title: Regulatory Compliance Associate 3 Street Address: 333 W SHERIDAN AVE

City: OKLAHOMA CITY State: OK

Phone: (405) 235-3611

Email address: SHAYDA.OMOUMI@DVN.COM

#### **Field**

**Representative Name:** 

**Street Address:** 

City: State: Zip:

Phone:

**Email address:** 

## **BLM Point of Contact**

**BLM POC Name: CHRISTOPHER WALLS BLM POC Title:** Petroleum Engineer

**BLM POC Phone:** 5752342234 BLM POC Email Address: cwalls@blm.gov

**Disposition:** Approved Disposition Date: 01/25/2024

Signature: Chris Walls

Page 2 of 2

<u>District I</u>
1625 N. French Dr., Hobbs, NM 88240
Phone: (575) 393-6161 Fax: (575) 393-0720
<u>District II</u>
811 S. First St., Artesia, NM 88210

Phone: (575) 748-1283 Fax: (575) 748-9720

<u>District III</u> 1000 Rio Brazos Road, Aztec, NM 87410 Phone: (505) 334-6178 Fax: (505) 334-6170 District IV

1220 S. St. Francis Dr., Santa Fe, NM 87505 Phone: (505) 476-3460 Fax: (505) 476-3462 State of New Mexico

Energy, Minerals & Natural Resources Department OIL CONSERVATION DIVISION 1220 South St. Francis Dr.

Santa Fe, NM 87505

Form C-102 Revised August 1, 2011 Submit one copy to appropriate District Office

■ AMENDED REPORT

#### WELL LOCATION AND ACREAGE DEDICATION PLAT

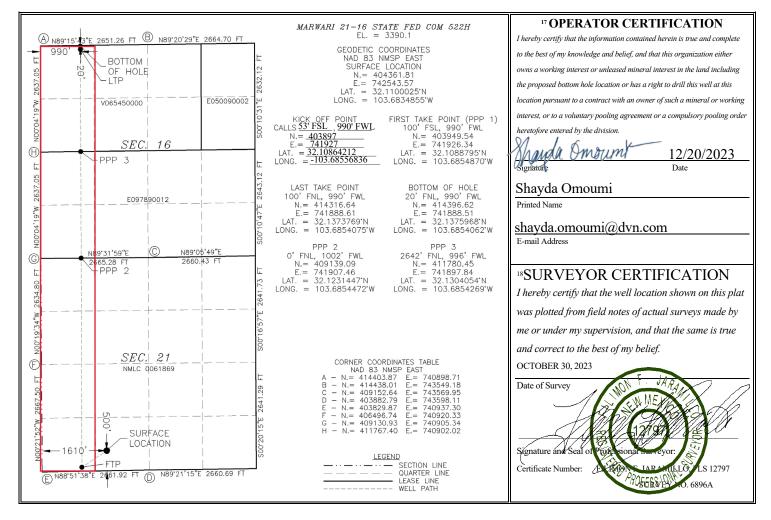
<sup>1</sup> API Numbe	<sup>1</sup> API Number <sup>2</sup> Pool Code <sup>3</sup> Pool Name				
30-025-523	73	96715	WC-025 G-05 S253209L; BO	ONE SPRING	
<sup>4</sup> Property Code		5 Pr	<sup>6</sup> Well Number		
322444		MARWARI 21-16 STATE FED COM			
<sup>7</sup> OGRID No.		<sup>8</sup> Operator Name		<sup>9</sup> Elevation	
6137		DEVON ENERGY PRODUCTION COMPANY, L.P.		3390.1	

<sup>10</sup> Surface Location

UL or lot no.	Section	Township	Range	Lot Idn	Feet from the	North/South line	Feet from the	East/West line	County
N	21	25 S	32 E		500	SOUTH	1610	WEST	LEA
" Bottom Hole Location If Different From Surface									
UL or lot no.	Section	Township	Range	Lot Idn	Feet from the	North/South line	Feet from the	East/West line	County

D	16	25 S		Ew Iun	20	NORTH	990	WEST	LEA
12 Dedicated Acres	13 Joint	or Infill	<sup>14</sup> Consolidatio	n Code			15 Order No.		
320									

No allowable will be assigned to this completion until all interests have been consolidated or a non-standard unit has been approved by the division.



Intent	: Х	As Dril	led											
API#														
DEV	rator Nar 'ON EN MPANY	IERGY P	RODUC	CTION	١		erty N RWAF			STAT	ΈF	ED C	ОМ	Well Number 522H
Kick C	off Point	(KOP)												
UL M	Section 21	Township 25S	Range 32E	Lot	Feet 53		From N	ı/s UTH	Feet 990			i E/W WEST	County LEA	
Latitu					Longitu								NAD 83	
First T	ake Poin	t (FTP)			•									
UL M	Section 21	Township 25S	Range 32E	Lot	Feet 100		From N		Feet 990		From	i E/W ST	County <b>LEA</b>	
Latitu 32.1	de 08879	5			Longitu 103.6		870						NAD 83	
Last T	ake Poin	t (LTP)												
UL D	Section 21	Township 25S	Range 32E	Lot	Feet 100		n N/S RTH	Feet 990		From WES		Count LEA	У	
Latitu 32.1	<sup>de</sup> 37376	9			Longitu 103.6		075					NAD <b>83</b>		
		defining v	vell for th		zontal Sp	oacing	g Unit?		N	]				
s this	well an i	infill well?		Υ										
	l is yes pl ng Unit.	ease provi	ide API if a	availab	ole, Oper	ator I	Name a	and w	ell n	umber	for [	Definir	ng well fo	r Horizontal
API#														
Oper	rator Nar	ne:	1			Prop	erty N	ame:						Well Number
DEVO L.P.	ON ENER	GY PRODU	ICTION CO	MPAN	NY,	MAI	RWARI	21-1	6 ST/	ATE FE	D CO	M 		233Y
	_													

KZ 06/29/2018



# 13-3/8" 54.50# .380 J-55

# **Dimensions (Nominal)**

Outside Diameter	13.375	in.
Wall	0.380	in.
Inside Diameter	12.615	in.
Drift	12.459	in.
Weight, T&C	54.500	lbs/ft
Weight, PE	52.790	lbs/ft

# **Performance Ratings, Minimum**

Collapse, PE	1130	psi
Internal Yields Pressure		
PE	2730	psi
STC	2730	PSI
ВТС	2730	psi
Yield Strength, Pipe Body	853	1000 lbs
Joint Strength, STC	514	1000 lbs
Joint Strength, BTC	909	1000 lbs

Note: SeAH Steel has produced this specification sheet for general information only. SeAH does not assume liability or responsibility for any loss or injury resulting from the use of information or data contained herein. All applications for the material described are at the customer's own risk and responsibility.

d by OCD: 1/25/2024 9:23:03 AM



# **Connection Data Sheet**

OD (in.)	WEIGHT (lbs./ft.)	WALL (in.)	GRADE	DRIFT (in.)	RBW%	CONNECTION
5.500	Nominal: 17.00 Plain End: 16.89	0.304	VST P110 EC	4.767	87.5	DWC/C-IS PLUS

5.500	in.
4.892	in.
4.962	sq.in.
API 5CT	
125	ksi
140	ksi
135	ksi
620	klb
670	klb
12,090	psi
8,840	psi
	4.892 4.962 API 5CT 125 140 135 620 670 12,090

CONNECTION PROPERTIES		
Connection Type	Semi-Premium T&	С
Connection OD (nom)	6.300	in.
Connection ID (nom)	4.892	in.
Make-Up Loss	4.125	in.
Coupling Length	9.250	in.
Critical Cross Section	4.962	sq.in.
Tension Efficiency	100.0%	of pipe
Compression Efficiency	100.0%	of pipe
Internal Pressure Efficiency	100.0%	of pipe
External Pressure Efficiency	100.0%	of pipe

CONNECTION PERFORMANCES		
Yield Strength	620	klb
Parting Load	670	klb
Compression Rating	620	klb
Min. Internal Yield	12,090	psi
*High Collapse*	8,840	psi
Maximum Uniaxial Bend Rating	104.2	°/100 ft
Ref String Length w 1.4 Design Factor	26,050	ft

FIELD TORQUE VALUES		
Min. Make-up Torque	13,400	ft.lbs
Opti. Make-up Torque	14,350	ft.lbs
Max. Make-up Torque	15,300	ft.lbs
Min. Shoulder Torque	1,340	ft.lbs
Max. Shoulder Torque	10,720	ft.lbs
Max. Delta Turn	0.200	Turns
Max Operational Torque	17,200	ft.lbs
Maximum Torsional Value (MTV)	18,920	ft.lbs

For detailed information on performance properties, refer to DWC Connection Data Notes on following page(s).

Connection specifications within the control of VAM USA were correct as of the date printed. Specifications are subject to change without notice. Certain connection specifications are dependent on the mechanical properties of the pipe. Mechanical properties of mill proprietary pipe grades were obtained from mill publications and are subject to change. Properties of mill proprietary grades should be confirmed with the mill. Users are advised to obtain current connection specifications and verify pipe mechanical properties for each application.

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05/23/2023 4:15 PM



VAM USA 2107 CityWest Boulevard Suite 1300 Houston, TX 77042 Phone: 713-479-3200

Fax: 713-479-3234

VAM USA Sales E-mail: <a href="mailto:VAMUSAsales@vam-usa.com">VAMUSAsales@vam-usa.com</a> Tech Support E-mail: tech.support@vam-usa.com

#### **DWC Connection Data Notes:**

- DWC connections are available with a seal ring (SR) option.
- All standard DWC/C connections are interchangeable for a given pipe OD. DWC connections are interchangeable with DWC/C-SR connections of the same OD and wall.
- Connection performance properties are based on nominal pipe body and connection dimensions.
- DWC connection internal and external pressure resistance is calculated using the API rating for buttress connections. API Internal pressure resistance is calculated from formulas 31, 32, and 35 in the API Bulletin 5C3.
- DWC joint strength is the minimum pipe body yield strength multiplied by the connection critical area.
- API joint strength is for reference only. It is calculated from formulas 42 and 43 in the API Bulletin 5C3.
- 7. Bending efficiency is equal to the compression efficiency.
- The torque values listed are recommended. The actual torque required may be affected by field 8. conditions such as temperature, thread compound, speed of make-up, weather conditions, etc.
- Connection yield torque is not to be exceeded.
- 10. Reference string length is calculated by dividing the joint strength by both the nominal weight in air and a design factor (DF) of 1.4. These values are offered for reference only and do not include load factors such as bending, buoyancy, temperature, load dynamics, etc.
- 11. DWC connections will accommodate API standard drift diameters.
- 12. DWC/C family of connections are compatible with API Buttress BTC connections. Please contact tech.support@vam-usa.com for details on connection ratings and make-up.

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All information is provided by VAM USA or its affiliates at user's sole risk, without liability for loss, damage or injury resulting from the use thereof; and on an "AS IS" basis without warranty or representation of any kind, whether express or implied, including without limitation any warranty of merchantability, fitness for purpose or completeness. This document and its contents are subject to change without notice. In no event shall VAM USA or its affiliates be responsible for any indirect, special, incidental, punitive, exemplary or consequential loss or damage (including without limitation, loss of use, loss of bargain, loss of revenue, profit or anticipated profit) however caused or arising, and whether such losses or damages were foreseeable or VAM USA or its affiliates was advised of the possibility of such damages.

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9.625" 40# .395" J-55

# **Dimensions (Nominal)**

Outside Diameter	9.625	in.
Wall	0.395	in.
Inside Diameter	8.835	in.
Drift	8.750	in.
Weight, T&C	40.000	lbs./ft.
Weight, PE	38.970	lbs./ft.
Performance Properties		
<u> </u>		
Collapse, PE	2570	psi
Internal Yield Pressure at Minimum Yield		
PE	3950	psi
LTC	3950	psi
ВТС	3950	psi
Yield Strength, Pipe Body	630	1000 lbs.
Joint Strength		
STC	452	1000 lbs.
LTC	520	1000 lbs.
ВТС	714	1000 lbs.

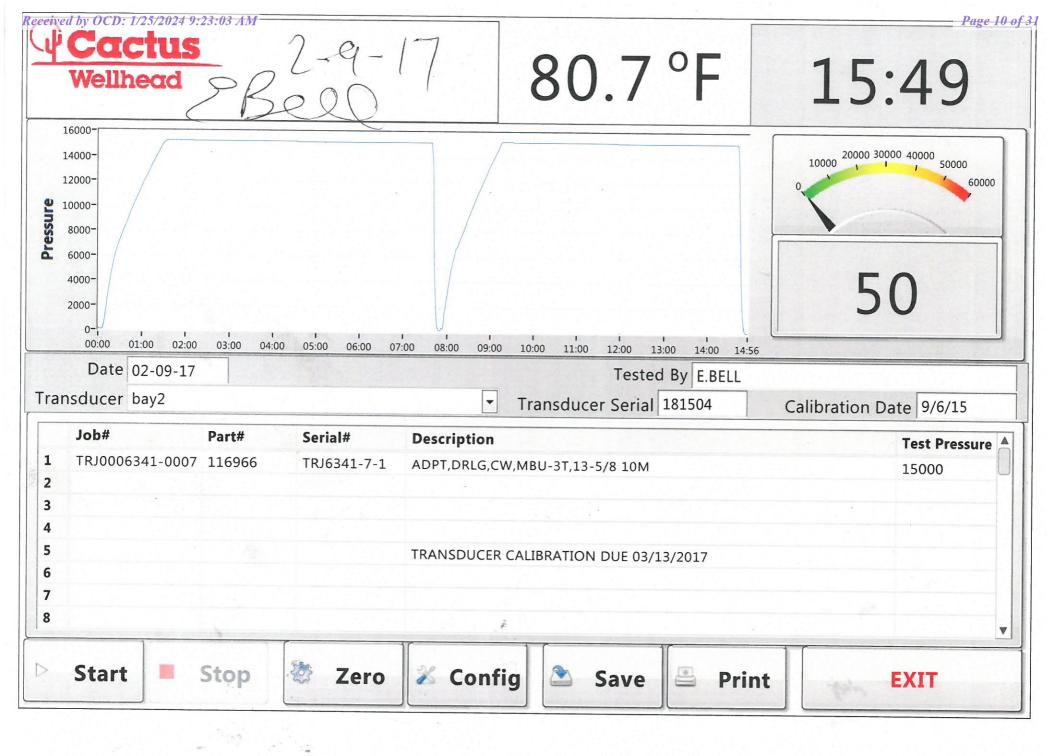
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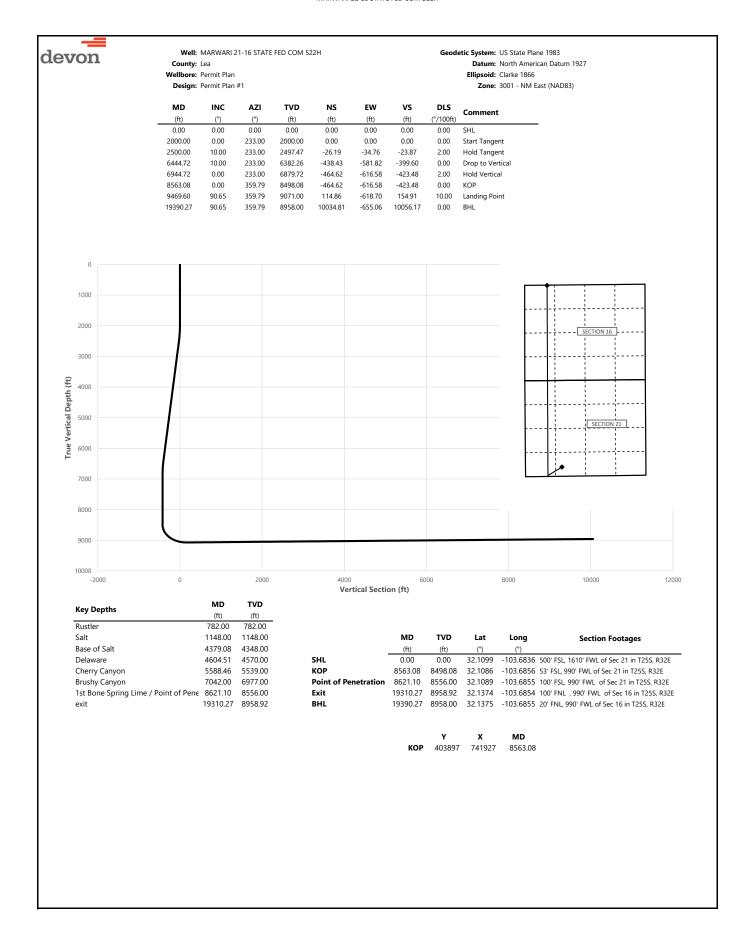
#### **Section 2 - Blowout Preventer Testing Procedure**

Variance Request

Devon Energy requests to only test BOP connection breaks after drilling out of surface casing and while skidding between wells which conforms to API Standard 53 and industry standards. This test will include the Top Pipe Rams, HCR, Kill Line Check Valve, QDC (quick disconnect to wellhead) and Shell of the 10M BOPE to 5M for 10 minutes. If a break to the flex hose that runs to the choke manifold is required due to repositioning from a skid, the HCR will remain open during the shell test to include that additional break. The variance only pertains to intermediate hole-sections and no deeper than the Bone Springs Formation where 5M BOP tests are required. The initial BOP test will follow OOGO2.III.A.2.i, and subsequent tests following a skid will only test connections that are broken. The annular preventer will be tested to 100% working pressure. This variance will meet or exceed OOGO2.III.A.2.i per the following: Devon Energy will perform a full BOP test per OOGO2.III.A.2.i before drilling out of the intermediate casing string(s) and starting the production hole, before starting any hole section that requires a 10M test, before the expiration of the allotted 14-days for 5M intermediate batch drilling or when the drilling rig is fully mobilized to a new well pad, whichever is sooner. We will utilize a 200' TVD tolerance between intermediate shoes as the cutoff for a full BOP test. The BLM will be contacted 4hrs prior to a BOPE test. The BLM will be notified if and when a well control event is encountered. Break test will be a 14 day interval and not a 30 day full BOPE test interval. If in the event break testing is not utilized, then a full BOPE test would be conducted.

- 1. Well Control Response:
- 1. Primary barrier remains fluid
- 2. In the event of an influx due to being underbalanced and after a realized gain or flow, the order of closing BOPE is as follows:
  - a) Annular first
  - b) If annular were to not hold, Upper pipe rams second (which were tested on the skid BOP test)
  - c) If the Upper Pipe Rams were to not hold, Lower Pipe Rams would be third





devon

Well: MARWARI 21-16 STATE FED COM 522H

County: Lea
Wellbore: Permit Plan
Design: Permit Plan #1

Geodetic System: US State Plane 1983

**Datum:** North American Datum 1927 **Ellipsoid:** Clarke 1866

Zone: 3001 - NM East (NAD83)

	Design:	Permit Plan	#1					<b>Zone:</b> 3001 - NM East (NAD83)
MD	INC	AZI	TVD	NS	EW	vs	DLS	Command
(ft)	(°)	(°)	(ft)	(ft)	(ft)	(ft)	(°/100ft)	Comment
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	SHL
100.00	0.00	233.00	100.00	0.00	0.00	0.00	0.00	
200.00	0.00	233.00	200.00	0.00	0.00	0.00	0.00	
300.00 400.00	0.00	233.00 233.00	300.00 400.00	0.00	0.00	0.00 0.00	0.00	
500.00	0.00	233.00	500.00	0.00	0.00	0.00	0.00	
600.00	0.00	233.00	600.00	0.00	0.00	0.00	0.00	
700.00	0.00	233.00	700.00	0.00	0.00	0.00	0.00	
782.00	0.00	233.00	782.00	0.00	0.00	0.00	0.00	Rustler
800.00	0.00	233.00	800.00	0.00	0.00	0.00	0.00	
900.00	0.00	233.00	900.00	0.00	0.00	0.00	0.00	
1000.00	0.00	233.00	1000.00	0.00	0.00	0.00	0.00	
1100.00	0.00	233.00	1100.00	0.00	0.00	0.00	0.00	Call
1148.00 1200.00	0.00	233.00 233.00	1148.00 1200.00	0.00	0.00	0.00 0.00	0.00	Salt
1300.00	0.00	233.00	1300.00	0.00	0.00	0.00	0.00	
1400.00	0.00	233.00	1400.00	0.00	0.00	0.00	0.00	
1500.00	0.00	233.00	1500.00	0.00	0.00	0.00	0.00	
1600.00	0.00	233.00	1600.00	0.00	0.00	0.00	0.00	
1700.00	0.00	233.00	1700.00	0.00	0.00	0.00	0.00	
1800.00	0.00	233.00	1800.00	0.00	0.00	0.00	0.00	
1900.00	0.00	233.00	1900.00	0.00	0.00	0.00	0.00	
2000.00	0.00	233.00	2000.00	0.00	0.00	0.00	0.00	Start Tangent
2100.00	2.00	233.00	2099.98	-1.05	-1.39	-0.96	2.00	
2200.00 2300.00	4.00 6.00	233.00 233.00	2199.84 2299.45	-4.20 -9.44	-5.57 -12.53	-3.83 -8.61	2.00 2.00	
2400.00	8.00	233.00	2398.70	-9.44 -16.78	-12.33	-15.29	2.00	
2500.00	10.00	233.00	2497.47	-26.19	-34.76	-23.87	2.00	Hold Tangent
2600.00	10.00	233.00	2595.95	-36.64	-48.63	-33.40	0.00	
2700.00	10.00	233.00	2694.43	-47.09	-62.49	-42.92	0.00	
2800.00	10.00	233.00	2792.91	-57.54	-76.36	-52.45	0.00	
2900.00	10.00	233.00	2891.39	-67.99	-90.23	-61.97	0.00	
3000.00	10.00	233.00	2989.87	-78.44	-104.10	-71.50	0.00	
3100.00	10.00	233.00	3088.35	-88.90	-117.97	-81.02	0.00	
3200.00 3300.00	10.00 10.00	233.00 233.00	3186.83	-99.35 -109.80	-131.84 145.70	-90.55 -100.07	0.00	
3400.00	10.00	233.00	3285.31 3383.79	-109.80	-145.70 -159.57	-100.07	0.00	
3500.00	10.00	233.00	3482.27	-120.23	-173.44	-119.12	0.00	
3600.00	10.00	233.00	3580.75	-141.15	-187.31	-128.65	0.00	
3700.00	10.00	233.00	3679.23	-151.60	-201.18	-138.17	0.00	
3800.00	10.00	233.00	3777.72	-162.05	-215.04	-147.70	0.00	
3900.00	10.00	233.00	3876.20	-172.50	-228.91	-157.22	0.00	
4000.00	10.00	233.00	3974.68	-182.95	-242.78	-166.75	0.00	
4100.00	10.00	233.00	4073.16	-193.40	-256.65	-176.27	0.00	
4200.00	10.00	233.00	4171.64	-203.85	-270.52	-185.80	0.00	
4300.00 4379.08	10.00 10.00	233.00 233.00	4270.12 4348.00	-214.30 -222.57	-284.38 -295.35	-195.32 -202.85	0.00	Base of Salt
4400.00	10.00	233.00	4368.60	-224.75	-298.25	-204.85	0.00	base of Sait
4500.00	10.00	233.00	4467.08	-235.20	-312.12	-214.37	0.00	
4600.00	10.00	233.00	4565.56	-245.65	-325.99	-223.89	0.00	
4604.51	10.00	233.00	4570.00	-246.12	-326.61	-224.32	0.00	Delaware
4700.00	10.00	233.00	4664.04	-256.10	-339.86	-233.42	0.00	
4800.00	10.00	233.00	4762.52	-266.55	-353.73	-242.94	0.00	
4900.00	10.00	233.00	4861.00	-277.00	-367.59	-252.47	0.00	
5000.00 5100.00	10.00	233.00 233.00	4959.48	-287.45	-381.46	-261.99 271.52	0.00	
5100.00	10.00 10.00	233.00	5057.97 5156.45	-297.90 -308.35	-395.33 -409.20	-271.52 -281.04	0.00	
5300.00	10.00	233.00	5254.93	-318.81	-423.07	-290.57	0.00	
5400.00	10.00	233.00	5353.41	-329.26	-436.93	-300.09	0.00	
5500.00	10.00	233.00	5451.89	-339.71	-450.80	-309.62	0.00	
5588.46	10.00	233.00	5539.00	-348.95	-463.07	-318.04	0.00	Cherry Canyon
5600.00	10.00	233.00	5550.37	-350.16	-464.67	-319.14	0.00	
5700.00	10.00	233.00	5648.85	-360.61	-478.54	-328.67	0.00	
5800.00	10.00	233.00	5747.33	-371.06	-492.41	-338.19	0.00	
5900.00	10.00	233.00	5845.81	-381.51	-506.27	-347.72	0.00	
6000.00	10.00	233.00	5944.29	-391.96	-520.14	-357.24	0.00	
6100.00 6200.00	10.00 10.00	233.00 233.00	6042.77 6141.25	-402.41 -412.86	-534.01 -547.88	-366.77 -376.29	0.00	
6300.00	10.00	233.00	6239.73	-412.00	-561.75	-385.82	0.00	
6400.00	10.00	233.00	6338.22	-433.76	-575.62	-395.34	0.00	



Well: MARWARI 21-16 STATE FED COM 522H

County: Lea
Wellbore: Permit Plan
Design: Permit Plan #1

Geodetic System: US State Plane 1983

**Datum:** North American Datum 1927 **Ellipsoid:** Clarke 1866

**Zone:** 3001 - NM East (NAD83)

	Design: Permit Plan #1					<b>Zone:</b> 3001 - NM East (NAD83)			
MD (ft)	INC (°)	AZI (°)	TVD (ft)	NS (ft)	<b>EW</b> (ft)	VS (ft)	<b>DLS</b> (°/100ft)	Comment	
6444.72	10.00	233.00	6382.26	-438.43	-581.82	-399.60	0.00	Drop to Vertical	
6500.00	8.89	233.00	6436.79	-443.89	-589.07	-404.58	2.00		
6600.00	6.89	233.00	6535.83	-452.16	-600.03	-412.11	2.00		
6700.00	4.89	233.00	6635.30	-458.34	-608.23	-417.74	2.00		
6800.00 6900.00	2.89 0.89	233.00 233.00	6735.06 6835.00	-462.43 -464.41	-613.66 -616.30	-421.47 -423.28	2.00 2.00		
6944.72	0.00	233.00	6879.72	-464.62	-616.58	-423.48	2.00	Hold Vertical	
7000.00	0.00	359.79	6935.00	-464.62	-616.58	-423.47	0.00	Tiold Vertical	
7042.00	0.00	359.79	6977.00	-464.62	-616.58	-423.47	0.00	Brushy Canyon	
7100.00	0.00	359.79	7035.00	-464.62	-616.58	-423.47	0.00	•	
7200.00	0.00	359.79	7135.00	-464.62	-616.58	-423.47	0.00		
7300.00	0.00	359.79	7235.00	-464.62	-616.58	-423.47	0.00		
7400.00	0.00	359.79	7335.00	-464.62	-616.58	-423.47	0.00		
7500.00	0.00	359.79	7435.00	-464.62	-616.58	-423.47	0.00		
7600.00 7700.00	0.00	359.79	7535.00 7635.00	-464.62 -464.62	-616.58	-423.47	0.00		
7800.00	0.00	359.79 359.79	7735.00	-464.62	-616.58 -616.58	-423.47 -423.47	0.00		
7900.00	0.00	359.79	7835.00	-464.62	-616.58	-423.47	0.00		
8000.00	0.00	359.79	7935.00	-464.62	-616.58	-423.47	0.00		
8100.00	0.00	359.79	8035.00	-464.62	-616.58	-423.47	0.00		
8200.00	0.00	359.79	8135.00	-464.62	-616.58	-423.47	0.00		
8300.00	0.00	359.79	8235.00	-464.62	-616.58	-423.47	0.00		
8400.00	0.00	359.79	8335.00	-464.62	-616.58	-423.47	0.00		
8500.00	0.00	359.79	8435.00	-464.62	-616.58	-423.47	0.00		
8563.08	0.00	359.79	8498.08	-464.62	-616.58	-423.48	0.00	KOP	
8600.00 8621.10	3.69 5.80	359.79 359.79	8534.98 8556.00	-463.44 -461.69	-616.58 -616.59	-422.29 -420.54	10.00 10.00	1st Bone Spring Lime / Point of Penetration	
8700.00	13.69	359.79	8633.70	-448.34	-616.64	-420.34	10.00	ist bone spring time / Form of Fenetration	
8800.00	23.69	359.79	8728.31	-416.33	-616.75	-375.27	10.00		
8900.00	33.69	359.79	8815.92	-368.38	-616.93	-327.41	10.00		
9000.00	43.69	359.79	8893.87	-305.95	-617.16	-265.10	10.00		
9100.00	53.69	359.79	8959.80	-230.93	-617.44	-190.22	10.00		
9200.00	63.69	359.79	9011.69	-145.60	-617.75	-105.05	10.00		
9300.00	73.69	359.79	9047.99	-52.55	-618.09	-12.18	10.00		
9400.00	83.69	359.79	9067.57	45.38	-618.45	85.57	10.00		
9469.60	90.65	359.79	9071.00	114.86	-618.70	154.91	10.00	Landing Point	
9500.00 9600.00	90.65 90.65	359.79 359.79	9070.65 9069.51	145.25 245.24	-618.81 -619.18	185.25 285.06	0.00		
9700.00	90.65	359.79	9068.38	345.24	-619.55	384.86	0.00		
9800.00	90.65	359.79	9067.24	445.23	-619.91	484.66	0.00		
9900.00	90.65	359.79	9066.10	545.22	-620.28	584.47	0.00		
10000.00	90.65	359.79	9064.96	645.21	-620.65	684.27	0.00		
10100.00	90.65	359.79	9063.82	745.21	-621.02	784.08	0.00		
10200.00	90.65	359.79	9062.68	845.20	-621.38	883.88	0.00		
10300.00	90.65	359.79	9061.54	945.19	-621.75	983.69	0.00		
10400.00	90.65	359.79	9060.40	1045.19	-622.12	1083.49	0.00		
10500.00 10600.00	90.65 90.65	359.79 359.79	9059.26 9058.13	1145.18 1245.17	-622.48 -622.85	1183.30 1283.10	0.00		
10700.00	90.65	359.79	9056.13	1345.17	-623.22	1382.90	0.00		
10800.00	90.65	359.79	9055.85	1445.16	-623.58	1482.71	0.00		
10900.00	90.65	359.79	9054.71	1545.15	-623.95	1582.51	0.00		
11000.00	90.65	359.79	9053.57	1645.14	-624.32	1682.32	0.00		
11100.00	90.65	359.79	9052.43	1745.14	-624.69	1782.12	0.00		
11200.00	90.65	359.79	9051.29	1845.13	-625.05	1881.93	0.00		
11300.00	90.65	359.79	9050.15	1945.12	-625.42	1981.73	0.00		
11400.00 11500.00	90.65 90.65	359.79 359.79	9049.01 9047.88	2045.11 2145.11	-625.79 -626.15	2081.53	0.00		
11600.00	90.65	359.79	9047.88	2245.11	-626.13 -626.52	2181.34 2281.14	0.00		
11700.00	90.65	359.79	9045.60	2345.09	-626.89	2380.95	0.00		
11800.00	90.65	359.79	9044.46	2445.09	-627.25	2480.75	0.00		
11900.00	90.65	359.79	9043.32	2545.08	-627.62	2580.56	0.00		
12000.00	90.65	359.79	9042.18	2645.07	-627.99	2680.36	0.00		
12100.00	90.65	359.79	9041.04	2745.06	-628.36	2780.17	0.00		
12200.00	90.65	359.79	9039.90	2845.06	-628.72	2879.97	0.00		
12300.00	90.65	359.79	9038.76	2945.05	-629.09	2979.77	0.00		
12400.00	90.65	359.79	9037.63	3045.04	-629.46	3079.58	0.00		
12500.00 12600.00	90.65 90.65	359.79 359.79	9036.49 9035.35	3145.04 3245.03	-629.82 -630.19	3179.38 3279.19	0.00		
12700.00	90.65	359.79 359.79	9035.35	3245.03 3345.02	-630.19 -630.56	3279.19	0.00		
12800.00	90.65	359.79	9033.07	3445.01	-630.92	3478.80	0.00		



Well: MARWARI 21-16 STATE FED COM 522H

County: Lea Wellbore: Permit Plan Design: Permit Plan #1 Geodetic System: US State Plane 1983

**Datum:** North American Datum 1927 **Ellipsoid:** Clarke 1866

Zone: 3001 - NM East (NAD83)

MD	INC	AZI	TVD	NS	EW	vs	DLS	_
(ft)	(°)	(°)	(ft)	(ft)	(ft)	(ft)	(°/100ft)	Comment
12900.00	90.65	359.79	9031.93	3545.01	-631.29	3578.60	0.00	
13000.00	90.65	359.79	9030.79	3645.00	-631.66	3678.40	0.00	
13100.00	90.65	359.79	9029.65	3744.99	-632.03	3778.21	0.00	
13200.00	90.65	359.79	9028.51	3844.98	-632.39	3878.01	0.00	
13300.00	90.65	359.79	9027.38	3944.98	-632.76	3977.82	0.00	
13400.00	90.65	359.79	9026.24	4044.97	-633.13	4077.62	0.00	
3500.00	90.65	359.79	9025.10	4144.96	-633.49	4177.43	0.00	
3600.00	90.65	359.79	9023.96	4244.96	-633.86	4277.23	0.00	
13700.00	90.65	359.79	9022.82	4344.95	-634.23	4377.04	0.00	
13800.00	90.65	359.79	9021.68	4444.94	-634.59	4476.84	0.00	
13900.00	90.65	359.79	9020.54	4544.93	-634.96	4576.64	0.00	
14000.00	90.65	359.79	9019.40	4644.93	-635.33	4676.45	0.00	
14100.00	90.65	359.79	9018.26	4744.92	-635.70	4776.25	0.00	
4200.00	90.65	359.79	9017.13	4844.91	-636.06	4876.06	0.00	
4300.00	90.65	359.79	9015.99	4944.91	-636.43	4975.86	0.00	
4400.00	90.65	359.79	9014.85	5044.90	-636.80	5075.67	0.00	
4500.00	90.65	359.79	9013.71	5144.89	-637.16	5175.47	0.00	
1600.00	90.65	359.79	9012.57	5244.88	-637.53	5275.27	0.00	
700.00	90.65	359.79	9011.43	5344.88	-637.90	5375.08	0.00	
4800.00	90.65	359.79	9010.29	5444.87	-638.27	5474.88	0.00	
4900.00	90.65	359.79	9009.15	5544.86	-638.63	5574.69	0.00	
5000.00	90.65	359.79	9008.01	5644.86	-639.00	5674.49	0.00	
5100.00	90.65	359.79	9006.88	5744.85	-639.37	5774.30	0.00	
5200.00	90.65	359.79	9005.74	5844.84	-639.73	5874.10	0.00	
5300.00	90.65	359.79	9004.60	5944.83	-640.10	5973.91	0.00	
5400.00	90.65	359.79	9003.46	6044.83	-640.47	6073.71	0.00	
5500.00	90.65	359.79	9002.32	6144.82	-640.83	6173.51	0.00	
5600.00	90.65	359.79	9001.18	6244.81	-641.20	6273.32	0.00	
5700.00	90.65	359.79	9000.04	6344.81	-641.57	6373.12	0.00	
5800.00	90.65	359.79	8998.90	6444.80	-641.94	6472.93	0.00	
5900.00	90.65	359.79	8997.76	6544.79	-642.30	6572.73	0.00	
6000.00	90.65	359.79	8996.63	6644.78	-642.67	6672.54	0.00	
6100.00	90.65	359.79	8995.49	6744.78	-643.04	6772.34	0.00	
6200.00	90.65	359.79	8994.35	6844.77	-643.40	6872.14	0.00	
6300.00	90.65	359.79	8993.21	6944.76	-643.77	6971.95	0.00	
6400.00	90.65	359.79	8992.07	7044.76	-644.14	7071.75	0.00	
6500.00	90.65	359.79	8990.93	7144.75	-644.50	7171.56	0.00	
6600.00 6700.00	90.65	359.79 359.79	8989.79	7244.74	-644.87	7271.36	0.00	
6800.00	90.65	359.79	8988.65	7344.73 7444.73	-645.24	7371.17 7470.97	0.00	
6900.00	90.65 90.65	359.79	8987.51 8986.37		-645.61	7570.77	0.00	
7000.00	90.65	359.79	8985.24	7544.72	-645.97	7670.58	0.00	
7100.00	90.65	359.79	8984.10	7644.71 7744.71	-646.34 -646.71	7770.38	0.00	
7200.00		359.79	8982.96		-647.07		0.00	
7300.00	90.65 90.65	359.79	8981.82	7844.70 7944.69	-647.07 -647.44	7870.19 7969.99	0.00	
7400.00	90.65	359.79	8980.68	8044.68	-647. <del>44</del> -647.81	8069.80	0.00	
7500.00	90.65	359.79	8979.54	8144.68	-648.17	8169.60	0.00	
7600.00	90.65	359.79	8978.40	8244.67	-648.54	8269.41	0.00	
7700.00	90.65	359.79	8977.26	8344.66	-648.91	8369.21	0.00	
7800.00	90.65	359.79	8976.12	8444.66	-649.28	8469.01	0.00	
7900.00	90.65	359.79	8974.99	8544.65	-649.64	8568.82	0.00	
8000.00	90.65	359.79	8973.85	8644.64	-650.01	8668.62	0.00	
8100.00	90.65	359.79	8972.71	8744.63	-650.38	8768.43	0.00	
8200.00	90.65	359.79	8971.57	8844.63	-650.74	8868.23	0.00	
8300.00	90.65	359.79	8970.43	8944.62	-651.11	8968.04	0.00	
8400.00	90.65	359.79	8969.29	9044.61	-651.48	9067.84	0.00	
8500.00	90.65	359.79	8968.15	9144.61	-651.85	9167.64	0.00	
8600.00	90.65	359.79	8967.01	9244.60	-652.21	9267.45	0.00	
8700.00	90.65	359.79	8965.87	9344.59	-652.58	9367.25	0.00	
8800.00	90.65	359.79	8964.74	9444.58	-652.95	9467.06	0.00	
8900.00	90.65	359.79	8963.60	9544.58	-653.31	9566.86	0.00	
9000.00	90.65	359.79	8962.46	9644.57	-653.68	9666.67	0.00	
19100.00	90.65	359.79	8961.32	9744.56	-654.05	9766.47	0.00	
9200.00	90.65	359.79	8960.18	9844.56	-654.41	9866.28	0.00	
9300.00	90.65	359.79	8959.04	9944.55	-654.78	9966.08	0.00	
	90.65	359.79	8958.92	9954.82	-654.82	9976.33	0.00	exit
19310.27							0.00	BHL
19310.27 19390.27	90.65	359.79	8958.00	10034.81	-655.06	10056.17	0.00	DIL

## MARWARI 21-16 STATE FED COM 522H

# 1. Geologic Formations

TVD of target	8959	Pilot hole depth	N/A
MD at TD:	19390	Deepest expected fresh water	

## Basin

Dasin	_		
	Depth	Water/Mineral	
Formation	(TVD)	Bearing/Target	Hazards*
	from KB	Zone?	
Rustler	782		
Salt	1148		
Base of Salt	4348		
Delaware	4570		
Cherry Canyon	5539		
Brushy Canyon	6977		
1st Bone Spring Lime	8556		

<sup>\*</sup>H2S, water flows, loss of circulation, abnormal pressures, etc.

2. Casing Program (Primary Design)

	wt Wt				Casing	Interval	Casing Interval	
Hole Size	Csg. Size	(PPF)	Grade	Conn	From (MD)	To (MD)	From (TVD)	To (TVD)
17 1/2	13 3/8	54 1/2	J-55	ВТС	0	807	0	807
12 1/4	9 5/8	40	J-55	ВТС	0	8463	0	8463
8 3/4	5 1/2	17	P110	DWC/C-IS PLUS	0	19390	0	8959

<sup>•</sup>All casing strings will be tested in accordance with 43 CFR 3172. Must have table for contingency casing.

#### 3. Cementing Program (Primary Design)

Assuming no returns are established while drilling, Devon requests to pump a two stage cement job on the intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brushy Canyon and the second stage performed as a bradenhead squeeze with planned cement from the Brushy Canyon to surface. The final cement top will be verified by Echo-meter. Devon will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program. Devon will report to the BLM the volume of fluid (limited to 1 bbls) used to flush intermediate casing valves following backside cementing procedures.

Casing	# Sks	TOC	Wt. ppg	Yld (ft3/sack)	Slurry Description
Surface	Surf 13.2 1.44 Lead: Class C Cement + ad		Lead: Class C Cement + additives		
Int 1	1236	Surf	13.0	2.3	2nd State: Bradenhead Squeeze - Lead: Class C Cement + additives
Int I	414	7041	13.2	1.44	Tail: Class H / C + additives
Production	44	8063	9	3.27	Lead: Class H /C + additives
Froduction	2089	8563	13.2	1.44	Tail: Class H / C + additives

Casing String	% Excess
Surface	50%
Intermediate 1	30%
Prod	10%

**4. Pressure Control Equipment (Three String Design)** 

BOP installed and tested before drilling which hole?	Size?	Min. Required WP	Туре		✓	Tested to:
			Anı	Annular		50% of rated working pressure
Int 1	13-5/8"	5M	Bline	d Ram	X	
IIIt 1	13-3/6	3101	_	Ram		5M
			Doub	le Ram	X	JIVI
			Other*			
			Annular (5M)		X	50% of rated working pressure
Production	13-5/8"	5M	M Blind Ram		X	
Production			Pipe Ram			5M
			Double Ram		X	5M
			Other*			
			Annul	ar (5M)		
			Blind Ram Pipe Ram			
						]
			Doub	le Ram		]
			Other*			
N A variance is requested for	the use of a	diverter or	the surface	casing. See a	attached for s	chematic.
Y A variance is requested to r	un a 5 M ai	nnular on a	10M system			_

5. Mud Program (Three String Design)

Section	Туре	Weight (ppg)
Surface	FW Gel	8.5-9
Intermediate	DBE / Cut Brine	10-10.5
Production	OBM	10-10.5

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times.

What will be used to monitor the loss or gain of fluid?	PVT/Pason/Visual Monitoring

6. Logging and Testing Procedures

Logging, C	Logging, Coring and Testing						
	Will run GR/CNL from TD to surface (horizontal well - vertical portion of hole). Stated logs run will be in the						
X	Completion Report and sbumitted to the BLM.						
	No logs are planned based on well control or offset log information.						
	Drill stem test? If yes, explain.						
	Coring? If yes, explain.						

Additional logs planned		Interval		
	Resistivity	Int. shoe to KOP		
	Density	Int. shoe to KOP		
X	CBL	Production casing		
X	Mud log	Intermediate shoe to TD		
	PEX			

7. Drilling Conditions

Condition	Specfiy what type and where?
BH pressure at deepest TVD	4892
Abnormal temperature	No

Mitigation measure for abnormal conditions. Describe. Lost circulation material/sweeps/mud scavengers.

Hydrogren Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the operator will comply with the provisions of 43 CFR 3176. If Hydrogen Sulfide is encountered measured values and formations will be provided to the BLM.

measured va	measured values and formations will be provided to the BEN.				
N	H2S is present				
Y	H2S plan attached.				

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#### 8. Other facets of operation

Is this a walking operation? Potentially

- 1 If operator elects, drilling rig will batch drill the surface holes and run/cement surface casing; walking the rig to next wells on the pad.
- 2 The drilling rig will then batch drill the intermediate sections and run/cement intermediate casing; the wellbore will be isolated with a blind flange and pressure gauge installed for monitoring the well before walking to the next well.
- 3 The drilling rig will then batch drill the production hole sections on the wells with OBM, run/cement production casing, and install TA caps or tubing heads for completions.

NOTE: During batch operations the drilling rig will be moved from well to well however, it will not be removed from the pad until all wells have production casing run/cemented.

## Will be pre-setting casing? Potentially

- 1 Spudder rig will move in and batch drill surface hole.
  - a. Rig will utilize fresh water based mud to drill surface hole to TD. Solids control will be handled entirely on a closed loop basis.,
- 2 After drilling the surface hole section, the spudder rig will run casing and cement following all of the applicable rules and regulations (43 CFR 3172, all COAs and NMOCD regulations).
- $^{3}$  The wellhead will be installed and tested once the surface casing is cut off and the WOC time has been reached.
- 4 A blind flange with the same pressure rating as the wellhead will be installed to seal the wellbore. Pressure will be monitored with a pressure gauge installed on the wellhead.
- 5 Spudder rig operations is expected to take 4-5 days per well on a multi-well pa.
- 6 The NMOCD will be contacted and notified 24 hours prior to commencing spudder rig operations.
- 7 Drilling operations will be performed with drilling rig. A that time an approved BOP stack will be nippled up and tested on the wellhead before drilling operations commences on each well.
  - a. The NMOCD will be contacted / notified 24 hours before the drilling rig moves back on to the pad with the pre-set surface casing.

Attachment	ts
X	Directional Plan
	Other, describe

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Segment	13 3/8		surface csg in a	17 1/2 i	nch hole.		Design I	actors			Surface		
Pg	Segment	#/ft	Grade		Coupling	Body	Collapse	Burst	Length	B@s	a-B	a-C	Weight
Mark	"A"	54.50		j 55	btc	17.02	2.63	0.59	920	7	0.99	4.96	50,140
	"B"				btc				0				0
Size   Volume   Cmt Sx   CuFr Cmt   Cu Ft   Vision   CuFr Cmt   Vision   CuFr Cmt   Cu Ft   Vision   CuFr Cmt   Cu		w	/8.4#/g mud, 30min Sfc Csg Test	psig: 1,500	Tail Cmt	does not	circ to sfc.	Totals:	920				50,140
Size   Volume   Cmt Sx   CuFr Cmt   Cu Ft   % Excess   Min   1 Stage   1 Stage   Min   1 Stage   1 Stage   Min	comparison o	of Proposed	to Minimum Required Ceme	ent Volumes									
1.56					Min	1 Stage	Drilling	Calc	Reg'd				Min Dis
1.56	Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cp
Segment		0.6946			639		9.00	2754	3M				
Segment	urst Frac Grac	dient(s) for Se	egment(s) A, B = , b All > 0.7	70, OK.									
Segment	0.5/0			42.2/0			Danism				lmt 1		
"A" 40.00 j 55 btc 1.86 0.56 0.81 8.463 1 1.35 0.93 338.52 "B"				13 3/8	Carreline	Dadu			l amadh	D@-		- ^	\A/a:a.b
### Wish			Grade	: 55		•	•		_	_			_
The cement volume(s) are intended to achieve a top of the form surface or a surfa		40.00		J 55	DIC	1.86	0.50	0.81		1	1.35	0.93	, .
Hole   Annular   1 Stage   1 Stage   Min   1 Stage   Drilling   Calc   Req'd   Mud W   MASP   BOPE   Hole-Cp   12 1/4   596   2696   7-78   10.50   2916   3M   0.81   0.81   D V Tool(s):   6977   Sum of sx   \$\(\frac{1}{2}\) \text{CuFL}   \$\(\fra		w,	/8.4#/g mud, 30min Sfc Csg Test	psig: -928				Totals:	8,463				338,52
Hole   Annular   1 Stage   1 Stage   Min   1 Stage   Drilling   Calc   Req'd   Min   Display   Masp   BoPE   Hole-Cp   12 1/4   596   2696   -78   10.50   2916   3M   0.81   D V Tool(s):			The cement v	olume(s) are intend	ed to achieve a top of	0	ft from su	rface or a	920				overlap.
12 1/4	Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Req'd				Min Dis
D V Tool(s):   6977	Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cp
Note   10   10   10   10   10   10   10   1	12 1/4	0.3132	414	596	2696	-78	10.50	2916	3M				
28   27   1650   3439   28   28   27   28   28   28   28   28	D V Tool(s):			6977				sum of sx	Σ CuFt				
Tail cmt   Style   Segment   Style			28										28
Segment	urst Frac Grac		egment(s): A, B, C, D = 0.47, b,	, c, d <0.70 a Proble	em!!								
"A" 17.00 p 110 dwc/c is+ 3.58 1.53 2.18 19,390 2 3.65 2.57 329,631 "B"	Burst Frac Grac	dient(s) for Se			em!!		Design Fac	etors			Prod 1		
"B"  "C"    W/8.4#/g mud, 30min Sfc Csg Test psig: 1,971   Totals: 19,390   329,63     The cement volume(s) are intended to achieve a top of Size   Volume   Size   Volume   Cmt Sx   CuFt Cmt   Cu Ft   K Excess   Mud Wt   MASP   BOPE   Hole-Cp     8 3/4   0.2526   2133   3152   2812   12   10.50   BOPE   Hole-Cp     8 3/4   0.2526   2133   3152   2812   12   10.50   Cmt Sx   Cupit Cmt   Cu Ft	Burst Frac Grac Tail cmt 5 1/2	dient(s) for Se	casing inside the			Joint			Length	B@s		а-С	Weigh
"C"	Burst Frac Grac Tail cmt 5 1/2 Segment	dient(s) for Se	casing inside the	9 5/8	Coupling		Collapse	Burst	_		а-В	-	_
#N/A  #N/A #/g mud, 30min Sfc Csg Test psig: 1,971  #N/A  #N/A #/g mud, 30min Sfc Csg Test psig: 1,971  #N/A  #N/A  #N/B ##/g mud, 30min Sfc Csg Test psig: 1,971  The cement volume(s) are intended to achieve a top of second principle of the cement volume(s) are intended to achieve a top of second principle of the cement volume(s) are intended to achieve a top of second principle of the cement volume(s) are intended to achieve a top of second principle of the cement volume(s) are intended to achieve a top of second principle of the cement volume(s) are intended to achieve a top of second principle of the cement volume(s) are intended to achieve a top of second principle of the cement volume(s) are intended to achieve a top of second principle or second prin	Tail cmt 5 1/2 Segment "A"	dient(s) for Se	casing inside the	9 5/8	Coupling		Collapse	Burst	19,390		а-В	-	329,63
W/8.4#/g mud, 30min Sfc Csg Test psig: 1,971	Tail cmt 5 1/2 Segment "A" "B"	dient(s) for Se	casing inside the	9 5/8	Coupling		Collapse	Burst	19,390 <b>0</b>		а-В	-	329,63 <b>0</b>
The cement volume(s) are intended to achieve a top of   8263   ft from surface or a   200     200	Tail cmt 5 1/2 Segment "A" "B" "C"	dient(s) for Se	casing inside the	9 5/8	Coupling dwc/c is+		Collapse	Burst	19,390 <b>0</b> 0		а-В	-	329,63 <b>0</b> 0
Hole	Tail cmt 5 1/2 Segment "A" "B" "C"	#/ft 17.00	casing inside the Grade	<b>95/8</b> p 110	Coupling dwc/c is+		Collapse	Burst 2.18	19,390 0 0 0		а-В	-	329,63 <b>0</b> 0
Size   Volume   Cmt Sx   CuFt Cmt   Cu Ft   % Excess   Mud Wt   MASP   BOPE   Hole-Cp	Tail cmt 5 1/2 Segment "A" "B" "C"	#/ft 17.00	casing inside the Grade /8.4#/g mud, 30min Sfc Csg Test	<b>95/8</b> p 110 psig: 1,971	Coupling dwc/c is+	3.58	Collapse 1.53	Burst 2.18 Totals:	19,390 0 0 0 19,390		а-В	-	329,63 0 0 0 329,63
8 3/4	Tail cmt 5 1/2 Segment "A" "B" "C" "D"	#/ft 17.00	casing inside the Grade /8.4#/g mud, 30min Sfc Csg Test   The cement vi	9 5/8 p 110 psig: 1,971 olume(s) are intend	Coupling dwc/c is+	3.58 8263	Collapse 1.53	Burst 2.18  Totals:	19,390 0 0 0 19,390 200		а-В	-	329,63 0 0 0 329,63 overlap.
#N/A	Tail cmt 5 1/2 Segment "A" "B" "C" "D"	#/ft 17.00	casing inside the Grade /8.4#/g mud, 30min Sfc Csg Test The cement vo 1 Stage	9 5/8 p 110 psig: 1,971 olume(s) are intend 1 Stage	Coupling dwc/c is+  0  ed to achieve a top of	3.58 8263 1 Stage	Collapse 1.53  ft from su Drilling	Burst 2.18  Totals: rface or a Calc	19,390 0 0 0 19,390 200 Req'd		а-В	-	329,63 0 0 0 329,63 overlap. Min Dis
#N/A	Tail cmt 5 1/2 Segment "A" "B" "C" "D"	#/ft 17.00	casing inside the Grade  /8.4#/g mud, 30min Sfc Csg Test The cement vo 1 Stage Cmt Sx	9 5/8 p 110 psig: 1,971 olume(s) are intend 1 Stage CuFt Cmt	Coupling dwc/c is+  0 ed to achieve a top of Min Cu Ft	3.58 8263 1 Stage % Excess	ft from su Drilling Mud Wt	Burst 2.18  Totals: rface or a Calc	19,390 0 0 0 19,390 200 Req'd		а-В	-	329,63 0 0 329,63 overlap. Min Dis
0	Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 8 3/4	#/ft 17.00 Annular Volume 0.2526	casing inside the Grade  /8.4#/g mud, 30min Sfc Csg Test The cement vo 1 Stage Cmt Sx	9 5/8 p 110 psig: 1,971 olume(s) are intend 1 Stage CuFt Cmt	Coupling dwc/c is+  0 ed to achieve a top of Min Cu Ft	3.58 8263 1 Stage % Excess	ft from su Drilling Mud Wt	Burst 2.18  Totals: rface or a Calc	19,390 0 0 0 19,390 200 Req'd		а-В	-	329,63 0 0 329,63 overlap. Min Dis Hole-Cp
Segment         #/ft         Grade         Coupling         #N/A         Collapse         Burst         Length         B@s         a-B         a-C         Weight           "A"         0.00         0	Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 8 3/4	#/ft 17.00 Annular Volume 0.2526	casing inside the Grade  Grade  /8.4#/g mud, 30min Sfc Csg Test The cement vo 1 Stage Cmt Sx	9 5/8 p 110 psig: 1,971 olume(s) are intend 1 Stage CuFt Cmt	Coupling dwc/c is+  0 ed to achieve a top of Min Cu Ft	3.58 8263 1 Stage % Excess	ft from su Drilling Mud Wt	Burst 2.18  Totals: rface or a Calc	19,390 0 0 0 19,390 200 Req'd		а-В	-	329,63 0 0 0 329,63 overlap. Min Dis Hole-Cp
"A" 0.00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 8 3/4 Class 'C' tail cm	#/ft 17.00 Annular Volume 0.2526	casing inside the Grade  Grade  /8.4#/g mud, 30min Sfc Csg Test The cement vo 1 Stage Cmt Sx	9 5/8 p 110 psig: 1,971 olume(s) are intend 1 Stage CuFt Cmt	Coupling dwc/c is+  0 ed to achieve a top of Min Cu Ft	3.58 8263 1 Stage % Excess	ft from su Drilling Mud Wt	Burst 2.18  Totals: rface or a Calc	19,390 0 0 0 19,390 200 Req'd		а-В	-	329,63 0 0 0 329,63 overlap. Min Dis Hole-Cp
"B"         0.00         0         0           w/8.4#/g mud, 30min Sfc Csg Test psig:         Totals: 0         0           Cmt vol calc below includes this csg, TOC intended         #N/A         ft from surface or a #N/A         overlap.           Hole         Annular         1 Stage         1 Stage         Drilling         Calc         Req'd         Min Dis	Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 8 3/4 Class 'C' tail cm	#/ft 17.00 Annular Volume 0.2526 at yld > 1.35	/8.4#/g mud, 30min Sfc Csg Test In The cement vol. 1 Stage Cmt Sx. 2133	9 5/8 p 110  psig: 1,971 olume(s) are intend 1 Stage CuFt Cmt 3152	Coupling dwc/c is+  0  ed to achieve a top of Min Cu Ft 2812	3.58 8263 1 Stage % Excess 12	ft from su Drilling Mud Wt 10.50	Burst 2.18  Totals: rface or a Calc MASP	19,390 0 0 0 19,390 200 Req'd	2	a-B 3.65	2.57	329,63 0 0 329,63 overlap. Min Dis Hole-Cpi
w/8.4#/g mud, 30min 5fc Csg Test psig:  Cmt vol calc below includes this csg, TOC intended Hole Annular 1 Stage 1 Stage Min 1 Stage Drilling Calc Req'd Min Dis	Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 8 3/4 Llass 'C' tail cm  #N/A 0 Segment	#/ft 17.00 Annular Volume 0.2526 at yld > 1.35	/8.4#/g mud, 30min Sfc Csg Test In The cement vol. 1 Stage Cmt Sx. 2133	9 5/8 p 110  psig: 1,971 olume(s) are intend 1 Stage CuFt Cmt 3152	Coupling dwc/c is+  0  ed to achieve a top of Min Cu Ft 2812  Coupling	3.58 8263 1 Stage % Excess 12	ft from su Drilling Mud Wt 10.50	Burst 2.18  Totals: rface or a Calc MASP	19,390 0 0 0 19,390 200 Req'd BOPE	2	a-B 3.65	2.57	329,63 0 0 0 329,63 overlap. Min Dis Hole-Cp 1.35
Cmt vol calc below includes this csg, TOC intended #N/A ft from surface or a #N/A overlap.  Hole Annular 1 Stage 1 Stage Min 1 Stage Drilling Calc Req'd Min Dis	Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 8 3/4 Class 'C' tail cm  #N/A 0 Segment "A"	#/ft 17.00 Annular Volume 0.2526 at yld > 1.35	/8.4#/g mud, 30min Sfc Csg Test In The cement vol. 1 Stage Cmt Sx. 2133	9 5/8 p 110  psig: 1,971 olume(s) are intend 1 Stage CuFt Cmt 3152	Coupling dwc/c is+  0  ed to achieve a top of Min Cu Ft 2812  Coupling 0.00	3.58 8263 1 Stage % Excess 12	ft from su Drilling Mud Wt 10.50	Burst 2.18  Totals: rface or a Calc MASP	19,390 0 0 0 19,390 200 Req'd BOPE	2	a-B 3.65	2.57	329,63 0 0 329,63 overlap. Min Dis Hole-Cp 1.35
Hole Annular 1 Stage 1 Stage Min 1 Stage Drilling Calc Req'd Min Dis	Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 8 3/4 £lass 'C' tail cm  #N/A 0 Segment "A"	#/ft 17.00 Annular Volume 0.2526 at yld > 1.35	/8.4#/g mud, 30min Sfc Csg Test In The cement vol. 1 Stage Cmt Sx. 2133	9 5/8 p 110  psig: 1,971 olume(s) are intend 1 Stage CuFt Cmt 3152	Coupling dwc/c is+  0  ed to achieve a top of Min Cu Ft 2812  Coupling 0.00	3.58 8263 1 Stage % Excess 12	ft from su Drilling Mud Wt 10.50	Totals: rface or a Calc MASP  Factors Burst	19,390 0 0 0 19,390 200 Req'd BOPE	2	a-B 3.65	2.57	329,63 0 0 329,63 overlap. Min Dis Hole-Cp 1.35
	Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 8 3/4 £lass 'C' tail cm  #N/A 0 Segment "A"	#/ft 17.00  Annular Volume 0.2526 at yld > 1.35	Casing inside the Grade  /8.4#/g mud, 30min Sfc Csg Test   The cement vi 1 Stage Cmt Sx 2133  Grade	9 5/8 p 110  psig: 1,971 olume(s) are intend 1 Stage CuFt Cmt 3152	Coupling dwc/c is+  0  ed to achieve a top of Min Cu Ft 2812  Coupling 0.00 0.00	3.58 8263 1 Stage % Excess 12 #N/A	ft from su Drilling Mud Wt 10.50	Totals:  Totals:  rface or a  Calc  MASP  Factors  Burst  Totals:	19,390 0 0 19,390 200 Req'd BOPE Length 0 0	2	a-B 3.65	2.57	329,63 0 0 329,63 overlap. Min Dis Hole-Cp 1.35
Size Volume Cmt Sx CuFt Cmt Cu Ft % Excess Mud Wt MASP BOPE Hole-Cp	Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 8 3/4 class 'C' tail cm #N/A 0 Segment "A" "B"	#/ft 17.00  Annular Volume 0.2526 at yld > 1.35  #/ft	Casing inside the Grade  (8.4#/g mud, 30min Sfc Csg Test   The cement vi 1 Stage Cmt Sx 2133  Grade  (8.4#/g mud, 30min Sfc Csg Test   Cmt vol cal	9 5/8 p 110  psig: 1,971 olume(s) are intend 1 Stage CuFt Cmt 3152  5 1/2  psig: Ic below includes the	Coupling dwc/c is+  0  ed to achieve a top of Min Cu Ft 2812  Coupling 0.00 0.00 nis csg, TOC intended	3.58  8263 1 Stage % Excess 12  #N/A	ft from su Drilling Mud Wt 10.50  Design I Collapse	Totals: rface or a Calc MASP  Factors Burst  Totals: rface or a	19,390 0 0 19,390 200 Req'd BOPE Length 0 0 #N/A	2	a-B 3.65	2.57	329,63 0 0 329,63 overlap. Min Dis Hole-Cp 1.35 Weigh 0 0 overlap.
	Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 8 3/4 class 'C' tail cm  #N/A 0 Segment "A" "B"	Annular Volume 0.2526 at yld > 1.35	Casing inside the Grade  (8.4#/g mud, 30min Sfc Csg Test   The cement vides to the comment of th	9 5/8  p 110  psig: 1,971 olume(s) are intend 1 Stage CuFt Cmt 3152  5 1/2  psig: Ic below includes th	Coupling dwc/c is+  0  ed to achieve a top of Min Cu Ft 2812  Coupling 0.00 0.00  is csg, TOC intended Min	3.58  8263 1 Stage % Excess 12  #N/A  #N/A 1 Stage	ft from su Drilling Mud Wt 10.50  Design I Collapse	Totals: rface or a Calc MASP  Factors Burst  Totals: rface or a Calc	19,390 0 0 19,390 200 Req'd BOPE Length 0 0 #N/A Req'd	2	a-B 3.65	2.57	329,63 0 0 329,63 overlap. Min Dis Hole-Cp 1.35  Weigh 0 0 overlap. Min Dis
0 #N/A #N/A 0 #N/A	Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 8 3/4 class 'C' tail cm  #N/A 0 Segment "A" "B"	Annular Volume 0.2526 at yld > 1.35	Casing inside the Grade  (8.4#/g mud, 30min Sfc Csg Test   The cement vides to the comment of th	9 5/8  p 110  psig: 1,971 olume(s) are intend 1 Stage CuFt Cmt 3152  5 1/2  psig: Ic below includes th	Coupling dwc/c is+  0  ed to achieve a top of Min Cu Ft 2812  Coupling 0.00 0.00  is csg, TOC intended Min	3.58  8263 1 Stage % Excess 12  #N/A  #N/A 1 Stage	ft from su Drilling Mud Wt 10.50  Design I Collapse	Totals: rface or a Calc MASP  Factors Burst  Totals: rface or a Calc	19,390 0 0 19,390 200 Req'd BOPE Length 0 0 #N/A Req'd	2	a-B 3.65	2.57	329,63 0 0 329,63 overlap. Min Dis Hole-Cp 1.35  Weigh 0 0 overlap. Min Dis
N/A Capitan Reef est top XXXX.	Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 8 3/4 lass 'C' tail cm  #N/A 0 Segment "A" "B"	Annular Volume 0.2526 at yld > 1.35	/8.4#/g mud, 30min Sfc Csg Test The cement vi 1 Stage Cmt Sx 2133  Grade  /8.4#/g mud, 30min Sfc Csg Test Cmt vol cal 1 Stage Cmt Sx	9 5/8 p 110  psig: 1,971 olume(s) are intend 1 Stage CuFt Cmt 3152  5 1/2  psig: Ic below includes th 1 Stage CuFt Cmt	Coupling dwc/c is+  0  ed to achieve a top of Min Cu Ft 2812  Coupling 0.00 0.00  nis csg, TOC intended Min Cu Ft	3.58  8263 1 Stage % Excess 12  #N/A  #N/A  1 Stage % Excess	ft from su Drilling Mud Wt 10.50  Design I Collapse	Totals: rface or a Calc MASP  Factors Burst  Totals: rface or a Calc	19,390 0 0 19,390 200 Req'd BOPE Length 0 0 #N/A Req'd	2	a-B 3.65	2.57	329,63 0 0 329,63 overlap. Min Di: Hole-Cr 1.35  Weigl 0 0 overlap. Min Di:

Carlsbad Field Office 1/19/2024

# PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

**OPERATOR'S NAME:** Devon Energy Production Company LP

LEASE NO.: NMLC0062300

LOCATION: Section 21, T.25 S., R.32 E., NMPM COUNTY: Lea County, New Mexico

WELL NAME & NO.: | Marwari 21-16 State Fed Com 522H

**SURFACE HOLE FOOTAGE:** 500'/S & 1610'/W **BOTTOM HOLE FOOTAGE** 20'/N & 990'/W **ATS/API ID:** 3002552373

APD ID: | 10400065107 Sundry ID: | 2766950

COA

H2S	Yes		
Potash	None 🔻		
Cave/Karst	Low		
Potential			
Cave/Karst	☐ Critical		
Potential			
Variance	■ None	Flex Hose	C Other
Wellhead	Conventional and Multibov	/I <u> </u>	
Other	□4 String	Capitan Reef	□WIPP
		None	
		ITOILE	
Other	Pilot Hole	☐ Open Annulus	
	None 🔻		
Cementing	Contingency Squeeze	Echo-Meter	Primary Cement
	None	Int 1	Squeeze
			None -
Special	□ Water	<b>☑</b> COM	□ Unit
Requirements	Disposal/Injection		
Special	☐ Batch Sundry		
Requirements			
Special	✓ Break Testing	□ Offline	☐ Casing
Requirements		Cementing	Clearance
Variance			

#### A. HYDROGEN SULFIDE

A Hydrogen Sulfide (H2S) Drilling Plan shall be activated 500 feet prior to drilling into the **Delaware** formation. As a result, the Hydrogen Sulfide area must meet **43 CFR part 3170 Subpart 3176** requirements, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, please provide measured values and formations to the BLM.

#### B. CASING

- 1. The 13-3/8 inch surface casing shall be set at approximately 920 feet (a minimum of 25 feet (Lea County) into the Rustler Anhydrite, above the salt, and below usable fresh water) and cemented to the surface. The surface hole shall be 17 1/2 inch in diameter.
  - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
  - b. Wait on cement (WOC) time for a primary cement job will be a minimum of **8** hours or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
  - c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
  - d. If cement falls back, remedial cementing will be done prior to drilling out that string.

Intermediate casing must be kept fluid filled to meet BLM minimum collapse requirement.

2. The minimum required fill of cement behind the 9-5/8 inch intermediate casing is:

#### **Option 1 (Single Stage):**

• Cement to surface. If cement does not circulate see B.1.a, c-d above.

#### Option 2:

Operator has proposed to cement in two stages by conventionally cementing the first stage and performing a bradenhead squeeze on the second stage, contingent upon no returns to surface.

- a. First stage: Operator will cement with intent to reach the top of the Brushy Canyon at 6977' (414 sxs Class H/C+ additives).
- b. Second stage:
  - Operator will perform bradenhead squeeze and top-out. Cement to surface. If cement does not reach surface, the appropriate BLM office shall be notified. (Squeeze 1236 sxs Class C)

Operator has proposed to pump down 13-3/8" X 9-5/8" annulus after primary cementing stage. Operator must run Echo-meter to verify Cement Slurry/Fluid top in the annulus Or operator shall run a CBL from TD of the 9-5/8" casing to surface after the second stage BH to verify TOC.

Submit results to the BLM. No displacement fluid/wash out shall be utilized at the top of the cement slurry between second stage BH and top out. Operator must run one CBL per Well Pad.

If cement does not reach surface, the next casing string must come to surface.

Operator must use a limited flush fluid volume of 1 bbl following backside cementing procedures.

- 3. The minimum required fill of cement behind the 5-1/2 inch production casing is:
  - Cement should tie-back at least 200 feet into previous casing string.
     Operator shall provide method of verification.
     Cement excess is less than 25%, more cement is required if washout occurs. Adjust cement volume and excess based on a fluid caliper or similar method that reflects the as-drilled size of the wellbore.

#### C. PRESSURE CONTROL

- 1. Variance approved to use flex line from BOP to choke manifold. Manufacturer's specification to be readily available. No external damage to flex line. Flex line to be installed as straight as possible (no hard bends).'
- 2.

#### Option 1:

a. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be 5000 (5M) psi. Annular which shall be tested to 3500 (70% Working Pressure) psi.

b. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the 9-5/8 inch intermediate casing shoe shall be 5000 (5M) psi.

#### **Option 2:**

Operator has proposed a multi-bowl wellhead assembly. This assembly will only be tested when installed on the 13-3/8 inch surface casing. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be 5000 (5M) psi.

- a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
- b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
- c. Manufacturer representative shall install the test plug for the initial BOP test.
- d. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- e. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR 3172.6(b)(9) must be followed.

#### D. SPECIAL REQUIREMENT (S)

#### **Communitization Agreement**

- The operator will submit a Communitization Agreement to the Santa Fe Office, 301 Dinosaur Trail Santa Fe, New Mexico 87508, at least 90 days before the anticipated date of first production from a well subject to a spacing order issued by the New Mexico Oil Conservation Division. The Communitization Agreement will include the signatures of all working interest owners in all Federal and Indian leases subject to the Communitization Agreement (i.e., operating rights owners and lessees of record), or certification that the operator has obtained the written signatures of all such owners and will make those signatures available to the BLM immediately upon request.
- The operator will submit an as-drilled survey well plat of the well completion, but are not limited to, those specified in 43 CFR part 3170 Subpart 3171
- If the operator does not comply with this condition of approval, the BLM may take enforcement actions that include, but are not limited to, those specified in 43 CFR 3163.1.
- In addition, the well sign shall include the surface and bottom hole lease numbers. When the Communitization Agreement number is known, it shall also be on the sign.

# **BOPE Break Testing Variance (Approved)**

- BOPE Break Testing is ONLY permitted for 5M BOPE or less. (Annular preventer must be tested to a minimum of 70% of BOPE working pressure and shall be higher than the MASP)
- BOPE Break Testing is NOT permitted to drilling the production hole section.
- Variance only pertains to the intermediate hole-sections and no deeper than the Bone Springs formation.
- While in transfer between wells, the BOPE shall be secured by the hydraulic carrier or cradle.
- Any well control event while drilling require notification to the BLM Petroleum Engineer (575-706-2779) prior to the commencement of any BOPE Break Testing operations.
- A full BOPE test is required prior to drilling the first deep intermediate hole section. If any subsequent hole interval is deeper than the first, a full BOPE test will be required. (200' TVD tolerance between intermediate shoes is allowable).
- The BLM is to be contacted (575-689-5981 Lea County) 4 hours prior to BOPE tests.
- As a minimum, a full BOPE test shall be performed at 21-day intervals.
- In the event any repairs or replacement of the BOPE is required, the BOPE shall test as per 43 CFR part 3170 Subpart 3172.
- If in the event break testing is not utilized, then a full BOPE test would be conducted.

# **GENERAL REQUIREMENTS**

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)

✓ Lea County
Call the Hobbs Field Station, 414 West Taylor, Hobbs NM 88240, (575) 689-5981

- 1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.
  - a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after installing and testing the wellhead, by installing a blind flange of like pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).
  - b. When the operator proposes to set surface casing with Spudder Rig
    - Notify the BLM when moving in and removing the Spudder Rig.
    - Notify the BLM when moving in the 2<sup>nd</sup> Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.
    - BOP/BOPE test to be conducted per **43** CFR part **3170** Subpart **3172** as soon as 2nd Rig is rigged up on well.
- 2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the dog house or stairway area.
- 3. The record of the drilling rate along with the GR/N well log run from TD to surface (horizontal well vertical portion of hole) shall be submitted to the BLM office as well as all other logs run on the borehole 30 days from completion. If available, a digital copy of the logs is to be submitted in addition to the paper copies. The Rustler top and top and bottom of Salt are to be recorded on the Completion Report.

#### A. CASING

1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator

can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.

- 2. Wait on cement (WOC) for Potash Areas: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends, 2) until cement has been in place at least 24 hours. WOC time will be recorded in the driller's log. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 3. Wait on cement (WOC) for Water Basin: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 4. Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.
- 5. No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.
- 6. On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.
- 7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.
- 8. Whenever a casing string is cemented in the R-111-P potash area, the NMOCD requirements shall be followed.
- B. PRESSURE CONTROL

- 1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in 43 CFR part 3170 Subpart 3172 and API STD 53 Sec. 5.3.
- 2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor.
- 3. 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.
- 4. If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:
  - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
  - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
  - c. Manufacturer representative shall install the test plug for the initial BOP
  - d. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR 3172.6(b)(9) must be followed.
  - e. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- 5. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
  - a. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead cement), whichever is greater. However, if the float does not hold, cut-

- off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).
- b. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the cement plug. The BOPE test can be initiated after bumping the cement plug with the casing valve open. (only applies to single stage cement jobs, prior to the cement setting up.)
- c. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer and can be initiated immediately with the casing valve open. The operator also has the option of utilizing an independent tester to test without a plug (i.e. against the casing) pursuant to 43 CFR part 3170 Subpart 3172 with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for water basin (8 hours) or potash (24 hours) or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).
- d. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.
- e. The results of the test shall be reported to the appropriate BLM office.
- f. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
- g. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.
- h. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per 43 CFR part 3170 Subpart 3172.
- C. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

#### D. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area.

Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

LVO 1/19/2024

District I
1625 N. French Dr., Hobbs, NM 88240
Phone: (575) 393-6161 Fax: (575) 393-0720

District II 811 S. First St., Artesia, NM 88210 Phone:(575) 748-1283 Fax:(575) 748-9720

District III 1000 Rio Brazos Rd., Aztec, NM 87410 Phone:(505) 334-6178 Fax:(505) 334-6170

1220 S. St Francis Dr., Santa Fe, NM 87505 Phone:(505) 476-3470 Fax:(505) 476-3462

**State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division** 1220 S. St Francis Dr. **Santa Fe, NM 87505** 

CONDITIONS

Action 307693

#### **CONDITIONS**

Operator:	OGRID:
DEVON ENERGY PRODUCTION COMPANY, LP	6137
333 West Sheridan Ave.	Action Number:
Oklahoma City, OK 73102	307693
	Action Type:
	[C-103] NOI Change of Plans (C-103A)

#### CONDITIONS

Created By		Condition Date
pkautz	None	2/15/2024