Form 3160-3 FORM APPROVED OMB No. 1004-0137 (June 2015) Expires: January 31, 2018 **UNITED STATES** DEPARTMENT OF THE INTERIOR 5. Lease Serial No. NMNM0501759 **BUREAU OF LAND MANAGEMENT** APPLICATION FOR PERMIT TO DRILL OR REENTER 6. If Indian, Allotee or Tribe Name 7. If Unit or CA Agreement, Name and No. **✓** DRILL REENTER 1a. Type of work: Oil Well 1b. Type of Well: Gas Well Other 8. Lease Name and Well No. 1c. Type of Completion: Hydraulic Fracturing ✓ Single Zone Multiple Zone TOUGH OMBRES 6/5 FED COM 715H 2. Name of Operator 9. API Well No. MEWBOURNE OIL COMPANY 30-01**5-**55536 3a. Address 3b. Phone No. (include area code) 10. Field and Pool, or Exploratory ALACRAN HILLS/UPPER WOLFCAMP O P O BOX 5270, HOBBS, NM 88241 (575) 393-5905 4. Location of Well (Report location clearly and in accordance with any State requirements.\*) 11. Sec., T. R. M. or Blk. and Survey or Area SEC 7/T21S/R27E/NMP At surface LOT 1 / 300 FNL / 1200 FWL / LAT 32.5007827 / LONG -104.233511 At proposed prod. zone TR K / 1900 FSL / 2552 FWL / LAT 32.5071732 / LONG -104.2122492 14. Distance in miles and direction from nearest town or post office\* 12. County or Parish 13. State **EDDY** NM 8 miles 15. Distance from proposed\* 16. No of acres in lease 17. Spacing Unit dedicated to this well 100 feet location to nearest property or lease line, ft. 480.0 (Also to nearest drig. unit line, if any) 18. Distance from proposed location\* 19. Proposed Depth 20. BLM/BIA Bond No. in file to nearest well, drilling, completed, 20 feet 8899 feet / 17309 feet FED: NM1693 applied for, on this lease, ft. 21. Elevations (Show whether DF, KDB, RT, GL, etc.) 22. Approximate date work will start\* 23. Estimated duration 3231 feet 05/19/2024 60 days 24. Attachments The following, completed in accordance with the requirements of Onshore Oil and Gas Order No. 1, and the Hydraulic Fracturing rule per 43 CFR 3162.3-3 (as applicable) 1. Well plat certified by a registered surveyor. 4. Bond to cover the operations unless covered by an existing bond on file (see Item 20 above). 2. A Drilling Plan. 3. A Surface Use Plan (if the location is on National Forest System Lands, the 5. Operator certification. SUPO must be filed with the appropriate Forest Service Office). 6. Such other site specific information and/or plans as may be requested by the Name (Printed/Typed) Date 25. Signature BRADLEY BISHOP / Ph: (575) 393-5905 04/17/2024 (Electronic Submission) Title Regulatory Approved by (Signature) Date Name (Printed/Typed) (Electronic Submission) CODY LAYTON / Ph: (575) 234-5959 10/15/2024 Title Office Assistant Field Manager Lands & Minerals Carlsbad Field Office

Application approval does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon.

Conditions of approval, if any, are attached.

Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.



		0/17/2024 7:	50:03 AM		State of Nev	y Mayico		Τ		Page 2
<u>C-10</u>	<u>2</u>		En		nerals & Natura	al Resources Departr	nent		'	Revised July 9, 2024
	Electronical Dermitting	ly		OIL (	CONSERVAT	TION DIVISION			☑ Initial Su	bmittal
Via oci	5 1 cm. cm.g					☐ Amended	☐ Amended Report			
								Type:	☐ As Drille	d
					WELL LOCAT	TION INFORMATION				
API Nu	mber 1 <b>-015-5</b> 5	5536	Pool Code	98314	ļ	Pool Name ALACF	RAN HILI	.; UPPE	ER WOLF	CAMP
	y Code <b>6419</b>		Property N	ame TC	UGH OMB	RES 6/5 FED C	СОМ		Well Numbe	er 715H
OGRII	<sup>No.</sup> 14	744	Operator N	ame M	EWBOURN	IE OIL COMPA	NY		Ground Level 32	el Elevation <b>31</b>
Surface	Owner:	State □ Fee □	Tribal 🛚 Fed	deral		Mineral Owner:	State □ Fee	□ Tribal 🛚	Federal	
					Surf	ace Location				
UL	Section	Township	Range	Lot	Ft. from N/S	Ft. from E/W	Latitude	I	Longitude	County
Α	7	21S	27E		300 FNL	1200 FWL	32.500	7827 -1	04.2335110	EDDY
					Bottom	Hole Location				
UL	Section	Township	Range	Lot	Ft. from N/S	Ft. from E/W	Latitude	I	Longitude	County
K	5	21S	27E		1900 FSL	2552 FWL	32.507	1732  -1	104.2122492	EDDY
Dadiaa	ted Acres	Infill or Def	ining Wall	Defining	Well API	Overlapping Spacing	TInit (V/N)	Consolida	tion Codo	
	20	DEFIN	•	Defining	, Well AFI	Overlapping Spacing	g Ollit (1/N)	Collsolida	tion Code	
Order l	Numbers.					Well setbacks are un	der Common (	Ownership:	□Yes □No	
					Kick O	ff Point (KOP)				
UL	Section	Township	Range	Lot	Ft. from N/S	Ft. from E/W	Latitude	I	Longitude	County
ı	1	21	26	33	1973 FSL	473 FEL	32.506	9997 -	104.2389272	EDDY
		1	1		First Ta	nke Point (FTP)	1			
UL <b>A</b>	Section 6	Township 21	Range 27	Lot 1	Ft. from N/S 1998 FSL	Ft. from E/W 100 FWL	Latitude 32.5070		Longitude 04.2370685	County EDDY
						ike Point (LTP)				
UL	Section	Township	Range	Lot	Ft. from N/S	Ft. from E/W	Latitude	1	Longitude	County
K	5	21	27	19						
1	1	1		1	1	1		•		
Unitize	d Area or Ar	rea of Uniform	Interest	Spacing	Unit Type 🛚 Horiz	zontal 🗆 Vertical	Grou	nd Floor Ele	evation: 32	31
OPER/	ATOR CERT	TFICATIONS				SURVEYOR CERTIFI	CATIONS			
			stained herein is	true and com	plete to the best of			um on this ml	at was plotted for	m fold notes of setua
my knov	ledge and beli	ief, and, if the we ins a working inte	ll is a vertical or	directional v	vell, that this	I hereby certify that the w surveys made by me or und				
includin	g the proposed	l bottom hole loca	ation or has a rig	ght to drill thi	s well at this	my belief.				
interest,		ary pooling agree			r unleased mineral g order heretofore					
					has received the					
in each	tract (in the tai		ation) in which a	any part of the	sed mineral interest e well's completed the division					
_		lcDani		-0 0. 401 JI OM	10/16/24					
Signatur			Date			Signature and Seal of Profes	ssional Surveyor			
R`	YAN MO	DANIEL								
					_	-	-			

Note: No allowable will be assigned to this completion until all interests have been consolidated or a non-standard unit has been approved by the division.

RYANMCDANIEL@MEWBOURNE.COM

District I 1625 N. French Dr., Hobbs, NM 88240 Phone: (575) 393-6161 Fax: (575) 393-0720 District II 811 S. First St., Artesia, NM 88210 Phone: (575) 748-1283 Fax: (575) 748-9720 District III 1000 Rio Brazos Road, Aztec, NM 87410 Phone: (505) 334-6178 Fax: (505) 334-6170 District IV 1220 S. St. Francis Dr., Santa Fe, NM 87505 Phone: (505) 476-3460 Fax: (505) 476-3462 State of New Mexico
Energy, Minerals & Natural Resources Department
OIL CONSERVATION DIVISION
1220 South St. Francis Dr.
Santa Fe, NM 87505

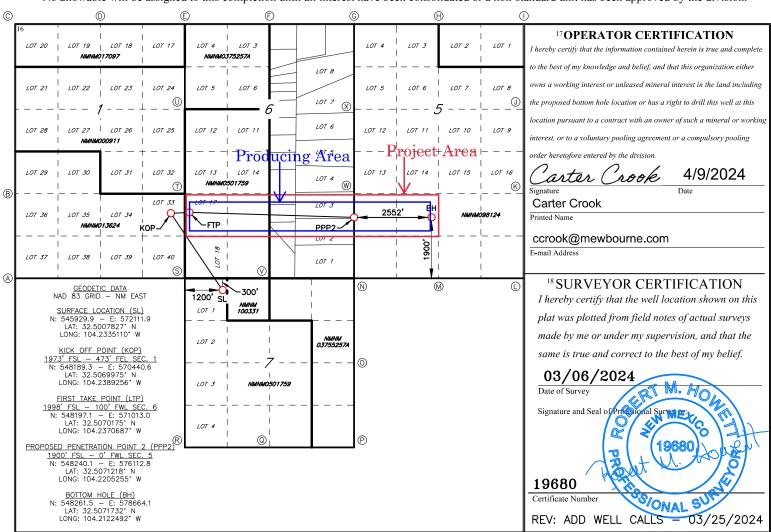
Form C-102 Revised August 1, 2011 Submit one copy to appropriate District Office

☐ AMENDED REPORT

#### WELL LOCATION AND ACREAGE DEDICATION PLAT

1	API Number	г	98	<sup>2</sup> Pool Code 3314	A	ALACRAN HILLS; UPPER WOLFCAMP OIL							
<sup>4</sup> Property Co	4Property Code  TOUGH OMBRES 6/5 FED COM												
70GRID 1 14744		Elevation <b>3231'</b>											
	<sup>10</sup> Surface Location												
UL or lot no.	Section	Township	Range	Lot Idn	Feet from the	ne North/South line	Feet From the	East/We	est line	County			
1	7	21S	27E		300	NORTH	1200	WES	ST	EDDY			
			11 ]	Bottom H	ole Locati	ion If Different Fro	om Surface						
UL or lot no.	Section	Township	Range	Lot Idn	Feet from the	ne North/South line	Feet from the	East/We	est line	County			
K 5 21S 27E 1900 SOUTH 2552 WEST										EDDY			
12 Dedicated Acres	s 13 Joint	or Infill 14 (	Consolidation	Code 15 C	order No.								
320													

No allowable will be assigned to this completion until all interest have been consolidated or a non-standard unit has been approved by the division.



Job No: LS24030192D

District I 1625 N. French Dr., Hobbs, NM 88240 Phone: (575) 393-6161 Fax: (575) 393-0720 District II 811 S. First St., Artesia, NM 88210 Phone: (575) 748-1283 Fax: (575) 748-9720 District III 1000 Rio Brazos Road, Aztec, NM 87410 Phone: (505) 334-6178 Fax: (505) 334-6170 District IV 1220 S. St. Francis Dr., Santa Fe, NM 87505 Phone: (505) 476-3460 Fax: (505) 476-3462

# State of New Mexico Energy, Minerals & Natural Resources Department OIL CONSERVATION DIVISION 1220 South St. Francis Dr. Santa Fe, NM 87505

Form C-102 Revised August 1, 2011 Submit one copy to appropriate District Office

☐ AMENDED REPORT

#### WELL LOCATION AND ACREAGE DEDICATION PLAT

	API Number	r	98	<sup>2</sup> Pool Code 8314	A	ALACRAN HILLS; UPPER WOLFCAMP OIL							
<sup>4</sup> Property Co	ode			TOUGH	<sup>5</sup> Property  OMBRES	Name <b>6/5 FED CO</b>	M		(	Well Number 715H			
$^{70\mathrm{GRID}}$	NO.			MEWB	8 Operator	r Name OIL COMPANY			9]	Elevation 3231'			
	<sup>10</sup> Surface Location												
UL or lot no.	Section	Township	Range	Lot Idn	Feet from the	North/South line	Feet From the	East/Wo	est line	County			
1	7	21S	27E		300	NORTH	1200	WE	ST	EDDY			
	•		<sup>11</sup> ]	Bottom H	ole Locatio	on If Different Fro	om Surface						
UL or lot no.	Section	Township	Range	Lot Idn	Feet from the	North/South line	Feet from the	East/Wo	est line	County			
K	K 5 21S 27E 1900 SOUTH 2552 WE												
12 Dedicated Acre	s 13 Joint	or Infill 14 (	Consolidation	Code 15 O	order No.								

No allowable will be assigned to this completion until all interest have been consolidated or a non-standard unit has been approved by the division.

16		<sup>17</sup> OPERATOR CERTIFICATION
		I hereby certify that the information contained herein is true and complete
		to the best of my knowledge and belief, and that this organization either
		owns a working interest or unleased mineral interest in the land including
		the proposed bottom hole location or has a right to drill this well at this
CORNEF	P DATA	location pursuant to a contract with an owner of such a mineral or working
NAD 83 GRID	- NM EAST	interest, or to a voluntary pooling agreement or a compulsory pooling
A: CALCULATED CORNER N: 546424.7 – E: 565512.6	M: FOUND BRASS CAP "1943" N: 546362.9 — E: 578749.0	order heretofore entered by the division.
B: FOUND BRASS CAP "1976" N: 549073.2 — E: 565577.9	N: FOUND BRASS CAP "1943" N: 546339.7 – E: 576102.5	Carter Crook 4/9/2024 Signature Date
C: FOUND BRASS CAP "1976"	O: FOUND BRASS CAP "1943"	Carter Crook
N: 553856.8 - E: 565611.1 D: FOUND BRASS CAP "1976"	N: 543722.2 - E: 576064.6 P: FOUND BRASS CAP "1943"	Printed Name
N: 553855.4 – E: 568261.8	N: 541084.6 - E: 576111.8	ccrook@mewbourne.com
E: FOUND BRASS CAP "1942" N: 553857.5 – E: 570912.7	Q: FOUND BRASS CAP "1976" N: 540985.9 — E: 573459.2	E-mail Address
F: FOUND BRASS CAP "1943" N: 553862.6 — E: 573486.6	R: FOUND BRASS CAP "1976" N: 540889.6 — E: 570906.8	18 SURVEYOR CERTIFICATION
G: FOUND BRASS CAP "1942" N: 553870.6 — E: 576153.7	S: FOUND BRASS CAP "1943" N: 546196.8 — E: 570913.0	I hereby certify that the well location shown on this
H: FOUND BRASS CAP "1942" N: 553879.0 — E: 578817.7	T: FOUND BRASS CAP "1943" N: 548859.7 – E: 570913.1	plat was plotted from field notes of actual surveys made by me or under my supervision, and that the
l: FOUND BRASS CAP "1942" N: 553889.2 – E: 581479.6	U: FOUND BRASS CAP "1943" N: 551510.0 — E: 570913.8	same is true and correct to the best of my belief.
J: FOUND BRASS CAP "1943" N: 551608.3 — E: 581452.9	V: FOUND BRASS CAP "1943" N: 546266.9 – E: 573460.4	03/06/2024
K: FOUND BRASS CAP "1943" N: 548994.9 — E: 581422.2	W: FOUND BRASS CAP "1943" N: 548955.5 — E: 576116.6	Date of Survey
L: FOUND BRASS CAP "1943" N: 546385.9 - E: 581390.6	X: FOUND BRASS CAP "1943" N: 551574.1 — E: 576132.4	Signature and Seal of Pressional Survey 19680
		19680
		Certificate Number
		REV: ADD WELL CALLS - 03/25/2024

Job No: LS24030192D

# State of New Mexico Energy, Minerals and Natural Resources Department

Submit Electronically Via E-permitting

Oil Conservation Division 1220 South St. Francis Dr. Santa Fe, NM 87505

		N.	ATURAL G	AS MANA	GEMENT P	LAN		
This Natural Gas	Managemen	t Plan m	ust be submitted w	ith each Applica	tion for Permit to I	Orill (APD) for	a new o	r recompleted well.
				1 – Plan D ffective May 25				
I. Operator:	Mewbou	urne C	Oil Co.	OGRID:	14744	Date	: <u>4/2</u>	2/24
II. Type: 💢 Ori	ginal □ Ame	endment	due to □ 19.15.27	7.9.D(6)(a) NMA	C □ 19.15.27.9.D(	(6)(b) NMAC [	Other.	
If Other, please of	lescribe:							
			ormation for each or connected to a			wells proposed	to be dr	illed or proposed to
Well Name	e /	API	ULSTR	Footages	Anticipated Oil BBL/D	Anticipated Gas MCF/D	F	Anticipated Produced Water BBL/D
TOUGH OMBRES 6/5 FE	D COM 716H		A 7 21S 27E	300' FNL x 1220' F	=wL 2000	3500		3500
	Schedule: Pro	ovide the			w or recompleted w			27.9(D)(1) NMAC] osed to be drilled or
Well Name	e /	API	Spud Date	TD Reached Date	Completion Commencement		l Flow Date	First Production Date
TOUGH OMBRES 6/5 FE	ED COM 716H		7/2/24	8/2/24	9/2/24	9/17	/24	9/17/24
VII. Operational Subsection A thr	al Practices: ough F of 19.	Attac     15.27.8	h a complete desc NMAC.	cription of the ac	ctions Operator wil	I take to comp	ly with	otimize gas capture. The requirements of or minimize venting

# Section 2 – Enhanced Plan EFFECTIVE APRIL 1, 2022

Beginning April 1, 2022, an operator that is not in compliance with its statewide natural gas capture requirement for the applicable reporting area must complete this section.

🛮 Operator certifies that it is not required to complete this section because Operator is in compliance with its statewide natural gas capture requirement for the applicable reporting area.

#### IX. Anticipated Natural Gas Production:

Well	API	Anticipated Average Natural Gas Rate MCF/D	Anticipated Volume of Natural Gas for the First Year MCF

#### X. Natural Gas Gathering System (NGGS):

Operator	System	ULSTR of Tie-in	Anticipated Gathering Start Date	Available Maximum Daily Capacity of System Segment Tie-in
				,

**XI.** Map.  $\square$  Attach an accurate and legible map depicting the location of the well(s), the anticipated pipeline route(s) connecting the production operations to the existing or planned interconnect of the natural gas gathering system(s), and the maximum daily capacity of the segment or portion of the natural gas gathering system(s) to which the well(s) will be connected.

**XII.** Line Capacity. The natural gas gathering system  $\square$  will  $\square$  will not have capacity to gather 100% of the anticipated natural gas production volume from the well prior to the date of first production.

**XIII.** Line Pressure. Operator  $\square$  does  $\square$  does not anticipate that its existing well(s) connected to the same segment, or portion, of the natural gas gathering system(s) described above will continue to meet anticipated increases in line pressure caused by the new well(s).

☐ Attach Operator's plan to manage production in response to the increased line pressure.

**XIV. Confidentiality:** □ Operator asserts confidentiality pursuant to Section 71-2-8 NMSA 1978 for the information provided in Section 2 as provided in Paragraph (2) of Subsection D of 19.15.27.9 NMAC, and attaches a full description of the specific information for which confidentiality is asserted and the basis for such assertion.

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# Section 3 - Certifications <u>Effective May</u> 25, 2021

Operator certifies that, after reasonable inquiry and based on the available information at the time of submittal: 🖾 Operator will be able to connect the well(s) to a natural gas gathering system in the general area with sufficient capacity to transport one hundred percent of the anticipated volume of natural gas produced from the well(s) commencing on the date of first production, taking into account the current and anticipated volumes of produced natural gas from other wells connected to the pipeline gathering system; or ☐ Operator will not be able to connect to a natural gas gathering system in the general area with sufficient capacity to transport one hundred percent of the anticipated volume of natural gas produced from the well(s) commencing on the date of first production, taking into account the current and anticipated volumes of produced natural gas from other wells connected to the pipeline gathering system. If Operator checks this box, Operator will select one of the following: Well Shut-In. ☐ Operator will shut-in and not produce the well until it submits the certification required by Paragraph (4) of Subsection D of 19.15.27.9 NMAC; or Venting and Flaring Plan. 

Operator has attached a venting and flaring plan that evaluates and selects one or more of the potential alternative beneficial uses for the natural gas until a natural gas gathering system is available, including: power generation on lease; (a) (b) power generation for grid; compression on lease; (c) liquids removal on lease; (d) reinjection for underground storage; (e) reinjection for temporary storage; **(f)** 

- reinjection for enhanced oil recovery; **(g)**
- fuel cell production; and (h)
- other alternative beneficial uses approved by the division.

# **Section 4 - Notices**

- 1. If, at any time after Operator submits this Natural Gas Management Plan and before the well is spud:
- Operator becomes aware that the natural gas gathering system it planned to connect the well(s) to has become unavailable or will not have capacity to transport one hundred percent of the production from the well(s), no later than 20 days after becoming aware of such information, Operator shall submit for OCD's approval a new or revised venting and flaring plan containing the information specified in Paragraph (5) of Subsection D of 19.15.27.9 NMAC; or
- Operator becomes aware that it has, cumulatively for the year, become out of compliance with its baseline natural gas capture rate or natural gas capture requirement, no later than 20 days after becoming aware of such information, Operator shall submit for OCD's approval a new or revised Natural Gas Management Plan for each well it plans to spud during the next 90 days containing the information specified in Paragraph (2) of Subsection D of 19.15.27.9 NMAC, and shall file an update for each Natural Gas Management Plan until Operator is back in compliance with its baseline natural gas capture rate or natural gas capture requirement.
- 2. OCD may deny or conditionally approve an APD if Operator does not make a certification, fails to submit an adequate venting and flaring plan which includes alternative beneficial uses for the anticipated volume of natural gas produced, or if OCD determines that Operator will not have adequate natural gas takeaway capacity at the time a well will be spud.

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I certify that, after reasonable inquiry, the statements in and attached to this Natural Gas Management Plan are true and correct to the best of my knowledge and acknowledge that a false statement may be subject to civil and criminal penalties under the Oil and Gas Act.

Signature:	Bradley Bishop
	BRADLEY BISHOP
Title:	REGULATORY MANAGER
E-mail Address:	BBISHOP@MEWBOURNE.COM
Date:	4/2/24
Phone:	575-393-5905
-	OIL CONSERVATION DIVISION
	(Only applicable when submitted as a standalone form)
Approved By:	
Title:	
Approval Date:	
Conditions of Appr	oval:

# Mewbourne Oil Company

#### Natural Gas Management Plan – Attachment

- VI. Separation equipment will be sized by construction engineering staff based on stated manufacturer daily throughput capacities and anticipated daily production rates to ensure adequate capacity. Closed vent system piping, compression needs, and VRUs will be sized utilizing ProMax modelling software to ensure adequate capacity for anticipated production volumes and conditions.
- VII. Mewbourne Oil Company (MOC) will take following actions to comply with the regulations listed in 19.15.27.8:
  - A. MOC will maximize the recovery of natural gas by minimizing the waste, as defined by 19.15.2 NMAC, of natural gas through venting and flaring. MOC will ensure that well(s) will be connected to a natural gas gathering system with sufficient capacity to transport natural gas. If there is no adequate takeaway for the gas, well(s) will be shut in until the natural gas gathering system is available.
  - B. All drilling operations will be equipped with a rig flare located at least 100 ft from the nearest surface hole. Rig flare will be utilized to combust any natural gas that is brought to surface during normal drilling operations. In the case of emergency venting or flaring the volumes will be estimated and reported appropriately.
  - C. During completion operations any natural gas brought to surface will be flared. Immediately following the finish of completion operations, all well flow will be directed to permanent separation equipment. Produced natural gas from separation equipment will be sent to sales. It is not anticipated that gas will not meet pipeline standards. However, if natural gas does not meet gathering pipeline quality specifications, MOC will flare the natural gas for 60 days or until the natural gas meets the pipeline quality specifications, whichever is sooner. MOC will ensure that the flare is sized properly and is equipped with automatic igniter or continuous pilot. The gas sample will analyzed twice per week and the gas will be routed into a gathering system as soon as pipeline specifications are met.
  - D. Natural gas will not be flared with the exceptions and provisions listed in the 19.15.27.8 D.(1) through (4). If there is no adequate takeaway for the separator gas, well(s) will be shut in until the natural gas gathering system is available with exception of emergency or malfunction situations. Venting and/or flaring volumes will be estimated and reported appropriately.
  - E. MOC will comply with the performance standards requirements and provisions listed in 19.15.27.8 E.(1) through (8). All equipment will be designed and sized to handle maximum anticipated pressures and throughputs in order to minimize the waste. Production storage tanks constructed after May 25, 2021 will be equipped with automatic gauging system. Flares constructed after May 25, 2021 will be equipped with automatic igniter or continuous pilot. Flares will be located at least 100' from the well and storage tanks unless otherwise approved by the division. MOC will conduct AVO inspections as described in 19.15.27.8 E (5) (a) with frequencies specified in 19.15.27.8 E (5) (b) and (c). All emergencies will be resolved as quickly and safely as feasible to minimize waste.
  - F. The volume of natural gas that is vented or flared as the result of malfunction or emergency during drilling and completions operations will be estimated. The volume of natural gas that is vented, flared or beneficially used during production operations, will be measured or estimated. MOC will install equipment to measure

the volume of natural gas flared from existing process piping or a flowline piped from equipment such as high pressure separators, heater treaters, or vapor recovery units associated with a well or facility associated with a well authorized by an APD issued after May 25, 2021 that has an average daily production greater than 60 Mcf/day. If metering is not practicable due to circumstances such as low flow rate or low pressure venting and flaring, MOC will estimate the volume of vented or flared natural gas. Measuring equipment will conform to industry standards and will not be designed or equipped with a manifold that allows the diversion of natural gas around the metering element except for the sole purpose of inspecting and servicing the measurement equipment.

VIII. For maintenance activities involving production equipment and compression, venting will be limited to the depressurization of the subject equipment to ensure safe working conditions. For maintenance of production and compression equipment the associated producing wells will be shut in to eliminate venting. For maintenance of VRUs all gas normally routed to the VRU will be routed to flare to eliminate venting.



#### U.S. Department of the Interior BUREAU OF LAND MANAGEMENT

# **Drilling Plan Data Report** 10/16/2024

**APD ID:** 10400097990

Submission Date: 04/17/2024

Highlighted data reflects the most recent changes

Well Type: OIL WELL

**Operator Name: MEWBOURNE OIL COMPANY** 

Well Number: 715H

Well Name: TOUGH OMBRES 6/5 FED COM

Well Work Type: Drill

**Show Final Text** 

# **Section 1 - Geologic Formations**

Formation ID	Formation Name	Elevation	True Vertical	Measured Depth	Lithologies	Mineral Resources	Producing Formatio
14317744	UNKNOWN	3267	28	28	OTHER : Topsoil	NONE	N
14317745	TOP SALT	2922	345	345	SALT	NONE	N
14317737	BOTTOM SALT	2717	550	550	SALT	NONE	N
14317739	YATES	2622	645	645	SANDSTONE	NATURAL GAS, OIL	N
14317740	CAPITAN REEF	2250	1017	1017	DOLOMITE, LIMESTONE	USEABLE WATER	N
14317741	LAMAR	822	2445	2445	DOLOMITE, SANDSTONE	NATURAL GAS, OIL	N
14317742	BONE SPRING	-1440	4707	4707	LIMESTONE	NATURAL GAS, OIL	N
14317743	BONE SPRING 1ST	-2953	6220	6220	SANDSTONE	NATURAL GAS, OIL	N
14317749	BONE SPRING 2ND	-3705	6972	6972	SANDSTONE	NATURAL GAS, OIL	N
14317752	BONE SPRING 3RD	-5073	8340	8340	SANDSTONE	NATURAL GAS, OIL	N
14317753	WOLFCAMP	-5430	8697	8697	LIMESTONE, SANDSTONE, SHALE	NATURAL GAS, OIL	Y

# **Section 2 - Blowout Prevention**

Pressure Rating (PSI): 5M Rating Depth: 17309

Equipment: Annular, Pipe Rams, Blind Rams, Other accessories to the BOP equipment will include a Kelly cock and floor safety valve (inside BOP) and choke lines and choke manifold. See attached schematics.

Requesting Variance? YES

Variance request: A variance is requested for the use of a variable choke line from the BOP to the choke manifold. See attached for hydrostatic test chart. Anchors are not required by manufacturer. Variance is requested to use a multi bowl wellhead. Variance is requested to perform break testing according to attached procedure.

Testing Procedure: BOP/BOPE will be tested by an independent service company to 250 psi low and the high pressure indicated above per 43 CFR Part 3172 requirements. The System may be upgraded to a higher

Well Name: TOUGH OMBRES 6/5 FED COM Well Number: 715H

pressure but still tested to the working pressure listed in the table above. If the system is upgraded all the components installed will be functional and tested. Pipe rams will be operationally checked each 24 hour period. Blind rams will be operationally checked on each trip out of the hole. These checks will be noted on the daily tour sheets.

#### **Choke Diagram Attachment:**

Tough\_Ombres\_6\_5\_Fed\_Com\_715H\_5M\_BOPE\_Choke\_Diagram\_20240410100657.pdf
Flex\_Line\_Specs\_API\_16C\_20240808141248.pdf
Multibowl\_5K\_WH\_Schematic\_20240808141311.pdf

#### **BOP Diagram Attachment:**

Tough\_Ombres\_6\_5\_Fed\_Com\_715H\_MOC\_Break\_Testing\_Variance\_20240410100726.pdf
Tough Ombres 6 5 Fed Com 715H 5M BOPE Schematic 20240410100808.pdf

# **Section 3 - Casing**

Casing ID	String Type	Hole Size	Csg Size	Condition	Standard	Tapered String	Top Set MD	Bottom Set MD	Top Set TVD	Bottom Set TVD	Top Set MSL	Bottom Set MSL	Calculated casing length MD	Grade	Weight	Joint Type	Collapse SF	Burst SF	Joint SF Type	Joint SF	Body SF Type	Body SF
1	SURFACE	26	18.625	NEW	API	N	0	275	0	275	3231	2956	275	J-55	87.5	OTHER - BTC	5.12	18.3	DRY	55.2 3	DRY	56.8 1
2	INTERMED IATE	17.5	13.375	NEW	API	N	0	950	0	950	2982	2281	950	H-40	48	ST&C	1.53	3.43	DRY	7.06	DRY	11.8 6
3	INTERMED IATE	12 <b>.</b> 2 5	9.625	NEW	API	N	0	2370	0	2370	3192	861	2370	J-55	36	LT&C	1.91	3.32	DRY	5.31	DRY	6.61
4	PRODUCTI ON	8.75	7.0	NEW	API	N	0	8756	0	8204	3267	-4973	8756	P- 110	26	LT&C	1.54	2.46	DRY	3.04	DRY	3.65
5	LINER	6.12 5	4.5	NEW	API	N	8556	17309	8499	8899	-5268	-5668	8753	P- 110	13.5	LT&C	1.92	2.23	DRY	2.86	DRY	3.57

# **Casing Attachments**

Well Name: TOUGH OMBRES 6/5 FED COM Well Number: 715H

Casing ID: 1

String

SURFACE

**Inspection Document:** 

**Spec Document:** 

**Tapered String Spec:** 

Casing Design Assumptions and Worksheet(s):

Tough\_Ombres\_6\_5\_Fed\_Com\_\_\_715H\_CsgAssumptions\_20240808150000.pdf

Casing ID: 2

String

**INTERMEDIATE** 

**Inspection Document:** 

**Spec Document:** 

**Tapered String Spec:** 

Casing Design Assumptions and Worksheet(s):

Tough\_Ombres\_6\_5\_Fed\_Com\_\_\_715H\_CsgAssumptions\_20240808150009.pdf

Casing ID: 3

String

INTERMEDIATE

**Inspection Document:** 

**Spec Document:** 

**Tapered String Spec:** 

Casing Design Assumptions and Worksheet(s):

Tough\_Ombres\_6\_5\_Fed\_Com\_\_\_715H\_CsgAssumptions\_20240808150019.pdf

Well Name: TOUGH OMBRES 6/5 FED COM Well Number: 715H

# **Casing Attachments**

Casing ID: 4

String

**PRODUCTION** 

**Inspection Document:** 

**Spec Document:** 

**Tapered String Spec:** 

Casing Design Assumptions and Worksheet(s):

Tough\_Ombres\_6\_5\_Fed\_Com\_\_\_715H\_CsgAssumptions\_20240808150029.pdf

Casing ID: 5

String

**LINER** 

**Inspection Document:** 

**Spec Document:** 

**Tapered String Spec:** 

Casing Design Assumptions and Worksheet(s):

Tough\_Ombres\_6\_5\_Fed\_Com\_\_\_715H\_CsgAssumptions\_20240808150038.pdf

# **Section 4 - Cement**

String Type	Lead/Tail	Stage Tool Depth	Top MD	Bottom MD	Quantity(sx)	Yield	Density	Cu Ft	Excess%	Cement type	Additives
SURFACE	Lead		0	186	270	2.12	12.5	580	100	Class C	Salt, Gel, Extender, LCM
SURFACE	Tail		186	275	200	1.34	14.8	268	100	Class C	Retarder
INTERMEDIATE	Lead	992	0	655	120	2.12	12.5	260	25	Class C	Salt, Gel, Extender, LCM
INTERMEDIATE	Tail		655	992	100	1.34	14.8	134	25	Class C	Retarder
INTERMEDIATE	Lead	992	992	1696	130	2.12	12.5	280	25	Class C	Salt, Gel, Extender, LCM

Well Name: TOUGH OMBRES 6/5 FED COM Well Number: 715H

String Type	Lead/Tail	Stage Tool Depth	Top MD	Bottom MD	Quantity(sx)	Yield	Density	Cu Ft	Excess%	Cement type	Additives
INTERMEDIATE	Tail		1696	2370	200	1.34	14.8	268	25	Class C	Retarder
PRODUCTION	Lead	6200	960	5472	390	2.12	12.5	830	25	Class C	Salt, Gel, Extender, LCM, Defoamer
PRODUCTION	Tail		5472	6200	100	1.34	14.8	134	25	Class C	Retarder, Fluid Loss, Defoamer
PRODUCTION	Lead	6200	6200	6683	50	2.12	12.5	110	25	CALSS C	SALT GEL EXTENDER LCM DEFOAMER
PRODUCTION	Tail		6683	8756	400	1.18	15.6	472	25	CLASS H	RETARDER FLUID LOSS DEFOAMER
LINER	Lead		8556	1730 8	560	1.85	13.5	1040	25	Class H	Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer, Anti-settling Agent

# **Section 5 - Circulating Medium**

Mud System Type: Closed

Will an air or gas system be Used? NO

Description of the equipment for the circulating system in accordance with Onshore Order #2:

Diagram of the equipment for the circulating system in accordance with Onshore Order #2:

**Describe what will be on location to control well or mitigate other conditions:** Formation integrity test will be performed per 43 CFR Part 3172. On Exploratory wells or on that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Will be tested in accordance with 43 CFR Part 3172.

Describe the mud monitoring system utilized: Pason/PVT/Visual Monitoring

# **Circulating Medium Table**

Top Depth	Bottom Depth	Mud Type	Min Weight (lbs/gal)	Max Weight (lbs/gal)	Density (lbs/cu ft)	Gel Strength (lbs/100 sqft)	Hd	Viscosity (CP)	Salinity (ppm)	Filtration (cc)	Additional Characteristics
2370	8756	SALT SATURATED	8.6	9.5							

Well Name: TOUGH OMBRES 6/5 FED COM Well Number: 715H

Top Depth	Bottom Depth	Mud Type	Min Weight (lbs/gal)	Max Weight (lbs/gal)	Density (lbs/cu ft)	Gel Strength (lbs/100 sqft)	ЬН	Viscosity (CP)	Salinity (ppm)	Filtration (cc)	Additional Characteristics
0	275	SPUD MUD	8.4	8.6							
275	950	SALT SATURATED	9.5	10.2						9	
950	2370	WATER-BASED MUD	8.4	8.6					1		
8756	1730 8	OIL-BASED MUD	10	12							

# **Section 6 - Test, Logging, Coring**

List of production tests including testing procedures, equipment and safety measures:

No logs are planned based on well control or offset log information. Offset Well: Tough Ombres 6/4 Fed Com #851H

List of open and cased hole logs run in the well:

MEASUREMENT WHILE DRILLING, MUD LOG/GEOLOGIC LITHOLOGY LOG, DIRECTIONAL SURVEY,

Coring operation description for the well:

None

# **Section 7 - Pressure**

Anticipated Bottom Hole Pressure: 5553 Anticipated Surface Pressure: 3595

**Anticipated Bottom Hole Temperature(F): 165** 

Anticipated abnormal pressures, temperatures, or potential geologic hazards? NO

Describe:

Contingency Plans geoharzards description:

Contingency Plans geohazards

Hydrogen Sulfide drilling operations plan required? YES

Hydrogen sulfide drilling operations

Tough\_Ombres\_6\_5\_Fed\_Com\_715H\_H2S\_Plan\_20240410102229.pdf

Well Name: TOUGH OMBRES 6/5 FED COM Well Number: 715H

# **Section 8 - Other Information**

#### Proposed horizontal/directional/multi-lateral plan submission:

```
Tough\_Ombres\_6\_5\_Fed\_Com\_715H\_MOC\_Dir\_Plan\_20240410102415.pdf\\ Tough\_Ombres\_6\_5\_Fed\_Com\_715H\_MOC\_Dir\_Plot\_20240410102420.pdf\\
```

#### Other proposed operations facets description:

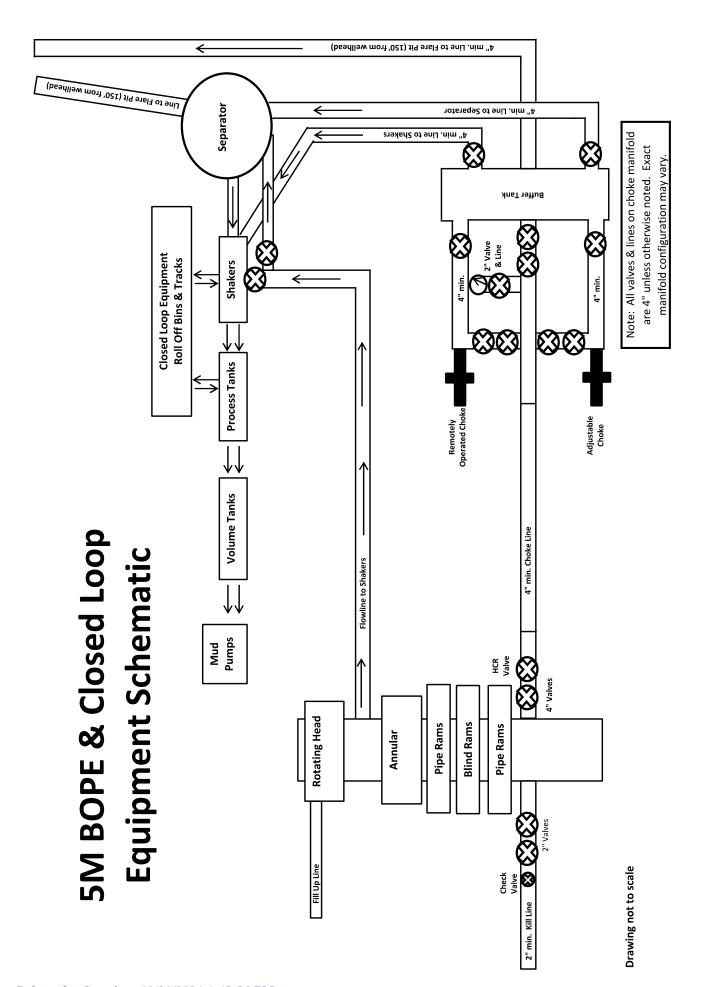
Mewbourne Oil Company also requests approval to implement Design B as described below. BLM will be notified of elected design.

#### Other proposed operations facets attachment:

```
Tough_Ombres_6_5_Fed_Com___715H_AddInfo_20240808145917.pdf
Tough_Ombres_6_5_Fed_Com___715H_Drlg_Program_20240808145924.pdf
```

#### Other Variance attachment:

Tough\_Ombres\_6\_5\_Fed\_Com\_715H\_MOC\_Break\_Testing\_Variance\_20240410102500.pdf
Tough\_Ombres\_6\_5\_Fed\_Com\_715H\_Offline\_Cementing\_Variance\_20240410102505.pdf





# LUOHE LETONE HYDRAULICS TECHNOLOGY CO.,LTD

# HYDROSTATIC TESTING REPORT

LTYY/QR-5.7.1-28

№: 230826015

Product Name	Cho	ke And Kill Hose		Standard	I AP	I Spec 16C 3 <sup>rd</sup> edition
Product Specification	3"×1000	0psi×60ft (18.29m	1)	Serial Num	ber	7660144
Inspection Equipment	MTU	J-BS-1600-3200-E		Test mediu	ım	Water
Inspection Department	(	C. Department		Inspection I	Date	2023.08.26
		Rate of le	ength chang	ge	1	
Standard requirements	At working pro	essure, the rate of le	ength chang	e should not m	nore than $\pm 2$	%
Testing result	10000psi (69.0	MPa) ,Rate of leng	th change (	).7%		
		Hydrosta	atic testing			
Standard requirements		orking pressure, the ssure-holding period				ess than three minutes,
Testing result	15000psi (103	.5MPa), 3 min for th	he first tim	e, 60 min for th	ne second time	e, no leakage
Graph of pressure testin	g:					And the section of th
100 90 90 90 90 90 90 90 90 90 90 90 90 9			100 90 80 70 60 60 10 10			
	भक्तम भक्तम भक्तम भक्तम भ	211 22621 22621 22621 22621226 eted items meet stan	07 21:29:54 21:	rements of API	art (100000000) (2000000)	ac periode sections (1988)
Approver	Jian long Chen	Auditor	Higi	ng Dong	Inspector	Zhansheng War



# LUOHE LETONE HYDRAULICS TECHNOLOGY CO.,LTD

# **CERTIFICATE OF QUALITY**

# LTYY/QR-5.7.1-19B

№: LT2023-126-002

Customer Name	Austin Hose							
Product Name	Choke And Kill Hose							
Product Specification	3"×10000psi×60ft (18.29m)	Quantity	2PCS					
Serial Number	7660143~7660144	FSL	FSL3					
Temperature Range	-29℃~+121℃	Standard	API Spec 16C 3 <sup>rd</sup> edition					
Inspection Department	Q.C. Department	Inspection date	2023.08.26					

	Inspection	Items			Inspection results					
	Appearance Ch	necking			In accordance with API Spec 16C 3 <sup>rd</sup> edition					
	Size and Len	ngths			In accordance with API Spec 16C 3 <sup>rd</sup> edition					
Γ	Dimensions and Tolerances					In accordance with API Spec 16C 3 <sup>rd</sup> edition				
End Connections: 4-	End Connections: 4-1/16"×10000psi Integral flange for sour gas service					In accordance with API Spec 6A 21st edition				
End Connections: 4-	1/16"×10000psi Inte	egral flan	ge for sour gas ser	vice	In accorda	nce with API Spec	17D 3 <sup>rd</sup> edition			
	Hydrostatic To	esting			In accorda	nce with API Spec	16C 3 <sup>rd</sup> edition			
	product Mar	king			In accorda	nce with API Spec	16C 3 <sup>rd</sup> edition			
Inspection con	nclusion	Ti	he inspected ite	ms me	eet standard require	ments of API Spec	16C 3 <sup>rd</sup> edition			
Remark	rs .									
Approver	Jian long Ch	an	Auditor	H	luging Dong Inspector Zhansheng Was					



# LUOHE LETONE HYDRAULICS TECHNOLOGY CO.,LTD

#### CERTIFICATE OF CONFORMANCE

№:LT230826016

Product Name: Choke And Kill Hose

Product Specification: 3"×10000psi×60ft (18.29m)

Serial Number: 7660143~7660144

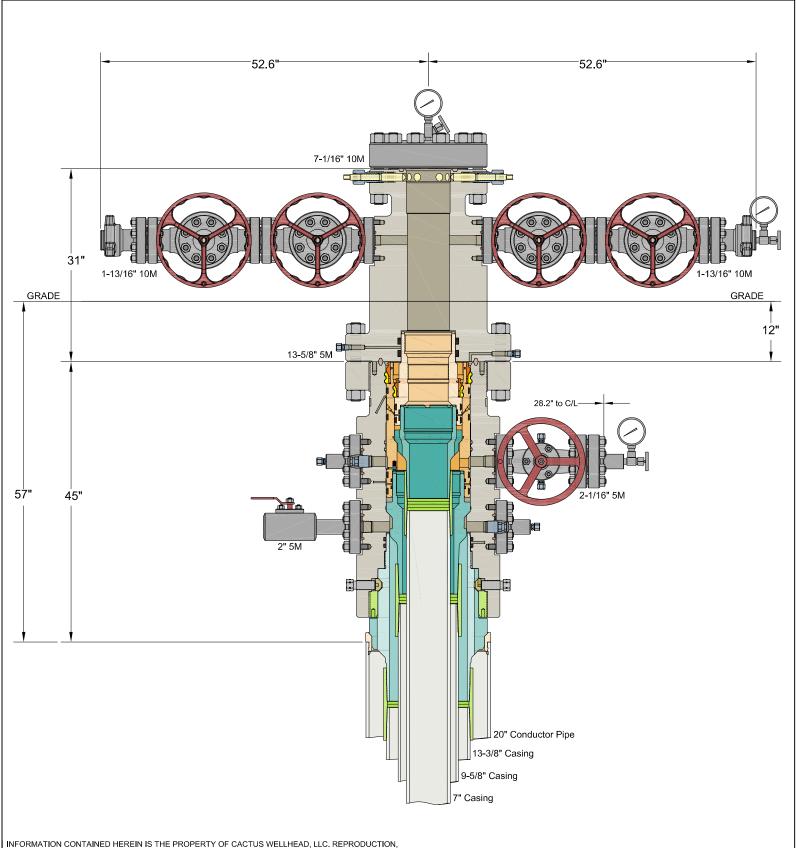
End Connections: 4-1/16"×10000psi Integral flange for sour gas service

The Choke And Kill Hose assembly was produced by LUOHE LETONE HYDRAULICS TECHNOLOGY CO.,LTD. in Aug 2023, and inspected by LUOHE LETONE HYDRAULICS TECHNOLOGY CO.,LTD. according to API Spec 16C 3<sup>rd</sup> edition on Aug 26, 2023. The overall condition is good. This is to certify that the Choke And Kill Hose complies with all current standards and specifications for API Spec 16C 3<sup>rd</sup> edition.

Jiaulong Chen

QC Manager:

Date: Aug 26, 2023



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# CACTUS WELLHEAD LLC

20" x 13-3/8" x 9-5/8" x 7" MBU-3T-CFL-R-DBLO Wellhead System With 9-5/8" & 7" Fluted Mandrel Casing Hangers And 13-5/8" 5M x 7-1/16" 10M CTH-DBLHPS Tubing Head

# ALL DIMENSIONS APPROXIMATE MEWBOURNE OIL COMPANY

DRAWN DLE 18APR22
APPRV

**NEW MEXICO** 

DRAWING NO. HBE0000660



# Mewbourne Oil Co.

# **BOP Break Testing Variance**

Mewbourne Oil Company requests a variance from the minimum standards for well control equipment testing of 43 CFR 3172 to allow a testing schedule of the blow out preventer (BOP) and blow out prevention equipment (BOPE) along with batch drilling & offline cementing operations. Modern rig upgrades which facilitate pad drilling allow the BOP stack to be moved between wells on a multi-well pad without breaking any BOP stack components apart. Widespread use of these technologies has led to break testing BOPE being endorsed as safe and reliable. American Petroleum Institute (API) best practices are frequently used by regulators to develop their regulations. API Standard 53, *Well Control Equipment Systems for Drilling Wells* (5<sup>th</sup> Ed., Dec. 2018) Section 5.3.7.1 states "A pressure test of the pressure containing component shall be performed following the disconnection or repair, limited to the affected component."

# **Procedures**

- 1. Full BOPE test at first installation on the pad.
  - Full BOPE test at least every 21 days.
  - Function test BOP elements per 43 CFR 3172.
  - Contact the BLM if a well control event occurs.
- 2. After the well section is secured and the well is confirmed to be static, the BOP will be disconnected from the wellhead and walked with the rig to another well on the pad. Two breaks on the BOPE will be made (Fig. 1).
  - Connection between the flex line and the HCR valve
  - Connection between the wellhead and the BOP quick connect (Fig. 5 & 6).
- 3. A capping flange will be installed after cementing per wellhead vendor procedure & casing pressure will be monitored via wellhead valve.
- 4. The BOP will be removed and carried by a hydraulic carrier (Fig. 3 & 4).
- 5. The rig will then walk to the next well.
- 6. Confirm that the well is static and remove the capping flange.
- 7. The connection between the flex line and HCR valve and the connection between the wellhead and the BOP guick connect will be reconnected.
- 8. Install a test plug into the wellhead.
- 9. A test will then be conducted against the upper pipe rams and choke, testing both breaks (Fig. 1 & 2).
- 10. The test will be held at 250 psi low and to the high value submitted in the APD, not to exceed 5000 psi.
- 11. The annular, blind rams and lower pipe rams will then be function tested.
- 12. If a pad consists of three or more wells, steps 4 through 11 will be repeated.



13. A break test will only be conducted if the intermediate section can be drilled and cased within 21 days of the last full BOPE test.

# **Barriers**

# **Before Nipple Down:**

- Floats in casing
- Kill weight fluid in casing
- Kill weight fluid in annulus
- Solid body mandrel and/or packoff

#### **After Nipple Down:**

- Floats in casing
- Kill weight fluid in casing
- Kill weight fluid in annulus
- Solid body mandrel and/or packoff
- Offline cementing tool and/or cement head
- Capping flange after cementing

# **Summary**

A variance is requested to only test broken pressure seals on the BOPE when moving between wells on a multi-well pad if the following conditions are met:

- A full BOPE test is conducted on the first well on the pad. API Standard 53 requires testing annular BOP to 70% of RWP or 100% of MASP, whichever is greater.
- If the first well on the pad is not the well with the deepest intermediate section, a full BOPE test will also be performed when moving to a deeper well.
- The hole section being drilled has a MASP under 5000 psi.
- If a well control event occurs, Mewbourne will contact BLM for permission to continue break testing.
- If significant (>50%) losses occur, full BOPE testing will be required going forward.
- Full BOPE test will be required prior to drilling the production hole.

While walking the rig, the BOP stack will be secured via hydraulic winch or hydraulic carrier. A full BOPE test will be performed at least every 21 days.



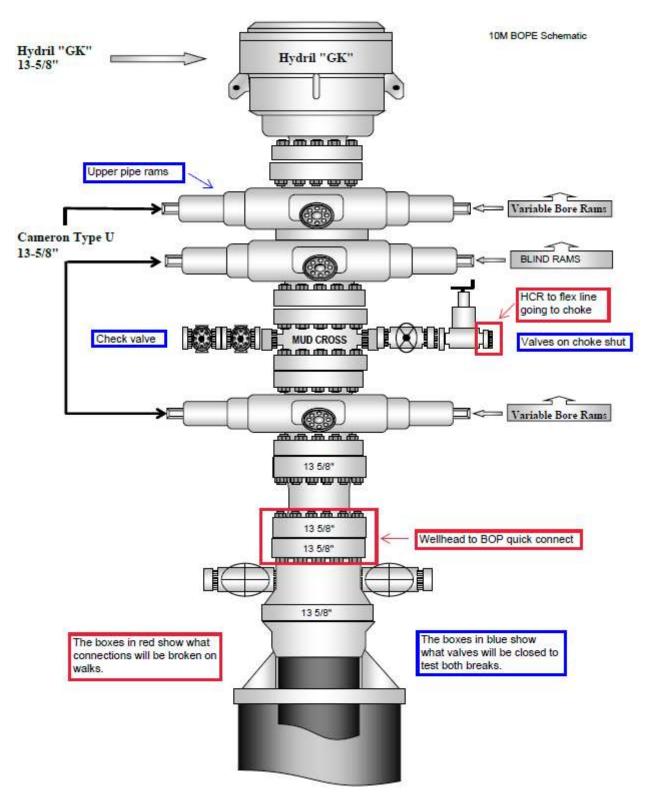


Figure 1. BOP diagram



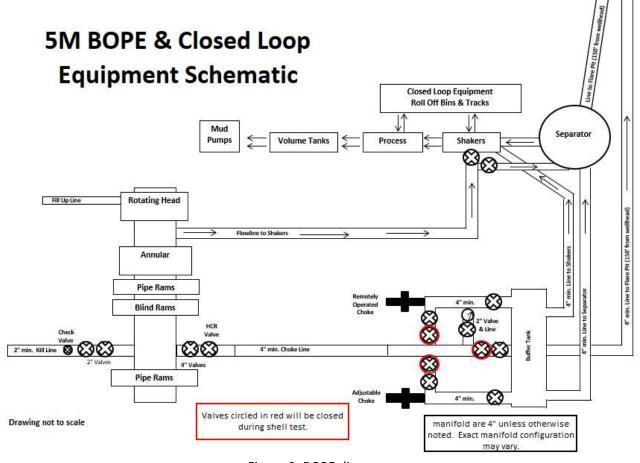


Figure 2. BOPE diagram





Figure 3. BOP handling system





Figure 4. BOP handling system



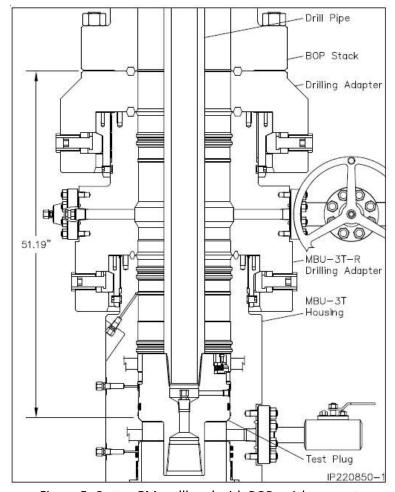


Figure 5. Cactus 5M wellhead with BOP quick connect

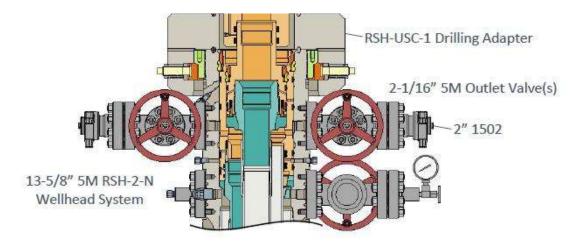
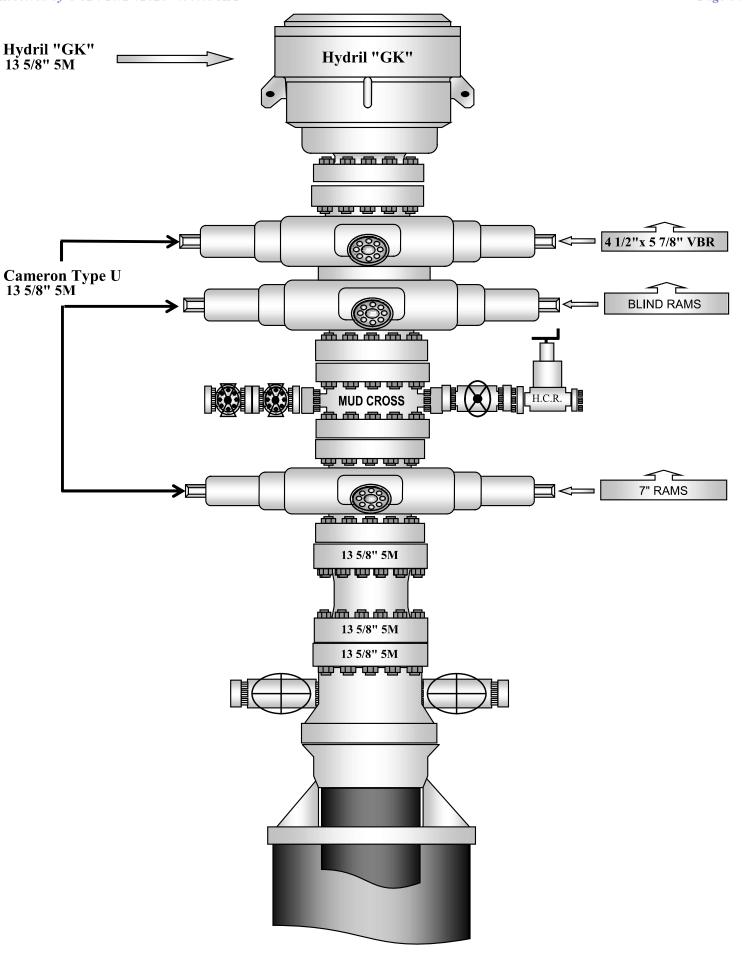


Figure 6. Vault 5M wellhead with BOP quick connect



SHL: 300' FNL 1200' FWL (Sec 7) BHL: 1900' FSL 2552' FWL (Sec 5)

		Casing Prog	ram Design A			BLM Minimum Safety Factors	1.125	1.0	1.6 Dry 1.8 Wet	1.6 Dry 1.8 Wet
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	26'	0'	0'	275'	275'	18 5/8" 87.5# J55 BTC	5.12	18.30	55.23	56.81
Int 1	17.5'	0'	0'	950'	950'	13.375" 48# H40 STC	1.53	3.43	7.06	11.86
Int 2	12.25'	0'	0'	2370'	2370'	9.625" 36# J55 LTC	1.91	3.32	5.31	6.61
Production	8.75'	0'	0'	8756'	8204'	7" 26# P110 LTC	1.54	2.46	3.04	3.65
Liner	6.125'	8556'	8499'	17309'	8899'	4.5" 13.5# P110 LTC	1.92	2.23	2.86	3.57

Cement Program

Casing		# Sacks	Wt. lb/gal	Yield ft <sup>3</sup> /sack	тос/вос	Volume ft <sup>3</sup>	% Excess	Slurry Description		
20,000 in	LEAD	270	12.5	2.12	0' - 186'	580	100%	Class C: Salt, Gel, Extender, LCM		
20.000 111	TAIL	200	14.8	1.34	186' - 275'	268	100%	Class C: Retarder		
13,375 in	LEAD	340	12.5	2.12	0' - 695'	730	50%	Class C: Salt, Gel, Extender, LCM		
13.3/5 III	TAIL	200	14.8	1.34	695' - 950'	268	30%	Class C: Retarder		
1st Stg 9.625 in	LEAD	130	12.5	2.12	992' - 1696'	280	25%	Class C: Salt, Gel, Extender, LCM		
18t Stg 9.025 In	TAIL	200	14.8	1.34	1696' - 2370'	268	25%	Class C: Retarder		
	9 5/8" DV Tool @ 992'									
2nd Stg 9.625 in	LEAD	120	12.5	2.12	0' - 655'	260	25%	Class C: Salt, Gel, Extender, LCM		
2nd Stg 9.025 in	TAIL	100	14.8	1.34	655' - 992'	134	25%	Class C: Retarder		
1.4.04.77	LEAD	50	12.5	2.12	6200' - 6683'	110	250/	Class C: Salt, Gel, Extender, LCM, Defoamer		
1st Stg 7 in	TAIL	400	15.6	1.18	6683' - 8756'	472	25%	Class H: Retarder, Fluid Loss, Defoamer		
					7" DV	Tool @ 6200'				
2-4 04- 71-	LEAD	390	12.5	2.12	960' - 5472'	830	250/	Class C: Salt, Gel, Extender, LCM, Defoamer		
2nd Stg 7 in	TAIL	100	14.8	1.34	5472' - 6200'	134	25%	Class C: Retarder, Fluid Loss, Defoamer		
4.5 in	LEAD	560	13.5	1.85	8556' - 17308.6'	1040	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer, Anti- settling Agent		

Design A - Mud Program

Depth	Mud Wt	Mud Type
0' - 275'	8.4 - 8.6	Fresh Water
275' - 950'	9.5 - 10.2	Brine
950' - 2370'	8.4 - 8.6	Fresh Water
2370' - 8756'	8.6 - 9.5	Cut-Brine
8756' - 17308.6'	10.0 - 12.	OBM

Geology

Formation	Est. Top (TVD)	Mineral Resources	Formation	Est. Top (TVD)	Mineral Resources
Rustler			Yeso		
Castile			Delaware (Lamar)	2445'	Oil/Natural Gas
Salt Top	345'	None	Bell Canyon		
Salt Base	550'	None	Cherry Canyon		
Yates	645'	Oil/Natural Gas	Manzanita Marker		
Seven Rivers			Basal Brushy Canyon		
Queen			Bone Spring	4707'	Oil/Natural Gas
Capitan	1017'	Usable Water	1st Bone Spring	6220'	Oil/Natural Gas
Grayburg			2nd Bone Spring	6972'	Oil/Natural Gas
San Andres			3rd Bone Spring	8340'	Oil/Natural Gas
Glorieta			Wolfcamp	8697'	Oil/Natural Gas

	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Is casing API approved? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	Y
If yes, does production casing cement tie back a minimum of 50' above the Reef?	Y
Is well within the designated 4 string boundary.	Y
Is well located in SOPA but not in R-111-P?	N
If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?	
Is well located in R-111-P and SOPA?	N
If yes, are the first three strings cemented to surface?	
Is 2 <sup>nd</sup> string set 100' to 600' below the base of salt?	
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
Is an engineered weak point used to satisfy R-111-Q?	
If yes, at what depth is the weak point planned?	
Is well located in high Cave/Karst?	N
If yes, are there two strings cemented to surface?	
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there three strings cemented to surface?	

SHL: 300' FNL 1200' FWL (Sec 7) BHL: 1900' FSL 2552' FWL (Sec 5)

		Casing Prog	ram Design B			BLM Minimum Safety Factors	1.125	1.0	1.6 Dry 1.8 Wet	1.6 Dry 1.8 Wet
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	26'	0'	0'	275'	275'	18 5/8" 87.5# J55 BTC	5.12	18.30	55.23	56.81
Int 1	17.5'	0'	0'	950'	950'	13.375" 48# H40 STC	1.53	3.43	7.06	11.86
Int 2	12.25'	0'	0'	2370'	2370'	9.625" 36# J55 LTC	1.91	3.32	5.31	6.61
Production	8.75'	0'	0'	9656'	8777'	7" 26# P110 LTC	1.44	2.29	2.76	3.31
Liner	6.125'	8756'	8204'	17309'	8899'	4.5" 13.5# P110 LTC	1.92	2.23	2.93	3.65

Design B - Cement Program

Design B - Cement I	r og i min								
Casing		# Sacks	Wt. lb/gal	Yield ft <sup>3</sup> /sack	TOC/BOC	Volume ft <sup>3</sup>	% Excess	Slurry Description	
20,000 in	LEAD	270	12.5	2.12	0' - 186'	580	100%	Class C: Salt, Gel, Extender, LCM	
20.000 111	TAIL	200	14.8	1.34	186' - 275'	268	100%	Class C: Retarder	
13.375 in	LEAD	340	12.5	2.12	0' - 695'	730	50%	Class C: Salt, Gel, Extender, LCM	
15.575 111	TAIL	200	14.8	1.34	695' - 950'	268	30%	Class C: Retarder	
1st Stg 9.625 in	LEAD	130	12.5	2.12	992' - 1696'	280	25%	Class C: Salt, Gel, Extender, LCM	
18t Stg 9.025 in	TAIL	200	14.8	1.34	1696' - 2370'	268	25%	Class C: Retarder	
					9 5/8" 1	DV Tool @ 992'			
2nd Stg 9.625 in	LEAD	120	12.5	2.12	0' - 655'	260	25%	Class C: Salt, Gel, Extender, LCM	
2110 Stg 9.025 III	TAIL	100	14.8	1.34	655' - 992'	0	25%	Class C: Retarder	
1st Stg 7 in	LEAD	90	12.5	2.12	6200' - 7229'	200	250/	Class C: Salt, Gel, Extender, LCM, Defoamer	
1st Stg / in	TAIL	400	15.6	1.18	7229' - 9656'	472	25%	Class H: Retarder, Fluid Loss, Defoamer	
	7" DV Tool @ 6200'								
2nd Stg 7 in	LEAD	390	12.5	2.12	960' - 5472'	830	250/	Class C: Salt, Gel, Extender, LCM, Defoamer	
Znu Sig / in	TAIL	100	14.8	1.34	5472' - 6200'	134	25%	Class C: Retarder, Fluid Loss, Defoamer	

Design B - Mud Program

Depth	Mud Wt	Mud Type
0' - 275'	8.4 - 8.6	Fresh Water
275' - 950'	9.5 - 10.2	Brine
950' - 2370'	8.4 - 8.6	Fresh Water
2370' - 9656'	8.6 - 9.5	Cut-Brine
9656' - 17308.6'	10.0 - 12.	OBM

Geology

Geology					
Formation	Est. Top (TVD)	Mineral Resources	Formation	Est. Top (TVD)	Mineral Resources
Rustler			Yeso		
Castile			Delaware (Lamar)	2445'	Oil/Natural Gas
Salt Top	345'	None	Bell Canyon		
Salt Base	550'	None	Cherry Canyon		
Yates	645'	Oil/Natural Gas	Manzanita Marker		
Seven Rivers			Basal Brushy Canyon		
Queen			Bone Spring	4707'	Oil/Natural Gas
Capitan	1017'	Usable Water	1st Bone Spring	6220'	Oil/Natural Gas
Grayburg			2nd Bone Spring	6972'	Oil/Natural Gas
San Andres			3rd Bone Spring	8340'	Oil/Natural Gas
Glorieta			Wolfcamp	8697'	Oil/Natural Gas

	Y or N					
Is casing new? If used, attach certification as required in Onshore Order #1	Y					
Is casing API approved? If no, attach casing specification sheet.						
Is premium or uncommon casing planned? If yes attach casing specification sheet.						
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y					
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y					
Is well located within Capitan Reef?	Y					
If yes, does production casing cement tie back a minimum of 50' above the Reef?	Y					
Is well within the designated 4 string boundary.	Y					
Is well located in SOPA but not in R-111-P?	N					
If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?						
Is well located in R-111-P and SOPA?	N					
If yes, are the first three strings cemented to surface?						
Is 2 <sup>nd</sup> string set 100' to 600' below the base of salt?						
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.						
Is an engineered weak point used to satisfy R-111-Q?						
If yes, at what depth is the weak point planned?						
Is well located in high Cave/Karst?	N					
If yes, are there two strings cemented to surface?						
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?						
Is well located in critical Cave/Karst?	N					
If yes, are there three strings cemented to surface?						

SHL: 300' FNL 1200' FWL (Sec 7) BHL: 1900' FSL 2552' FWL (Sec 5)

Casing Program Design A						BLM Minimum Safety Factors	1.125	1.0	1.6 Dry 1.8 Wet	1.6 Dry 1.8 Wet
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	26'	0'	0'	275'	275'	18 5/8" 87.5# J55 BTC	5.12	18.30	55.23	56.81
Int 1	17.5'	0'	0'	950'	950'	13.375" 48# H40 STC	1.53	3.43	7.06	11.86
Int 2	12.25'	0'	0'	2370'	2370'	9.625" 36# J55 LTC	1.91	3.32	5.31	6.61
Production	8.75'	0'	0'	8756'	8204'	7" 26# P110 LTC	1.54	2.46	3.04	3.65
Liner	6.125'	8556'	8499'	17309'	8899'	4.5" 13.5# P110 LTC	1.92	2.23	2.86	3.57

Cement Program

Casing		# Sacks	Wt. lb/gal	Yield ft <sup>3</sup> /sack	тос/вос	Volume ft <sup>3</sup>	% Excess	Slurry Description		
20,000 in	LEAD	270	12.5	2.12	0' - 186'	580	100%	Class C: Salt, Gel, Extender, LCM		
20.000 III	TAIL	200	14.8	1.34	186' - 275'	268	100%	Class C: Retarder		
13,375 in	LEAD	340	12.5	2.12	0' - 695'	730	50%	Class C: Salt, Gel, Extender, LCM		
15.5/5 III	TAIL	200	14.8	1.34	695' - 950'	268	50%	Class C: Retarder		
1-4 04-0 (25 1-	LEAD	130	12.5	2.12	992' - 1696'	280	25%	Class C: Salt, Gel, Extender, LCM		
1st Stg 9.625 in	TAIL	200	14.8	1.34	1696' - 2370'	268	25%	Class C: Retarder		
	9 5/8" DV Tool @ 992'									
2nd Stg 9.625 in	LEAD	120	12.5	2.12	0' - 655'	260	25%	Class C: Salt, Gel, Extender, LCM		
2nd Stg 9.025 in	TAIL	100	14.8	1.34	655' - 992'	134	25%	Class C: Retarder		
1-1-04-71-	LEAD	50	12.5	2.12	6200' - 6683'	110	25%	Class C: Salt, Gel, Extender, LCM, Defoamer		
1st Stg 7 in	TAIL	400	15.6	1.18	6683' - 8756'	472	25%	Class H: Retarder, Fluid Loss, Defoamer		
					7" DV	Tool @ 6200'				
2nd Stg 7 in	LEAD	390	12.5	2.12	960' - 5472'	830	25%	Class C: Salt, Gel, Extender, LCM, Defoamer		
Ziiu Stg / III	TAIL	100	14.8	1.34	5472' - 6200'	134	1 25%	Class C: Retarder, Fluid Loss, Defoamer		
4.5 in	LEAD	560	13.5	1.85	8556' - 17308.6'	1040	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer, Anti- settling Agent		

Design A - Mud Program

Depth	Mud Wt	Mud Type
0' - 275'	8.4 - 8.6	Fresh Water
275' - 950'	9.5 - 10.2	Brine
950' - 2370'	8.4 - 8.6	Fresh Water
2370' - 8756'	8.6 - 9.5	Cut-Brine
8756' - 17308.6'	10.0 - 12.	OBM

Geology

Formation	Est. Top (TVD)	Mineral Resources	Formation	Est. Top (TVD)	Mineral Resources
Rustler			Yeso		
Castile			Delaware (Lamar)	2445'	Oil/Natural Gas
Salt Top	345'	None	Bell Canyon		
Salt Base	550'	None	Cherry Canyon		
Yates	645'	Oil/Natural Gas	Manzanita Marker		
Seven Rivers			Basal Brushy Canyon		
Queen			Bone Spring	4707'	Oil/Natural Gas
Capitan	1017'	Usable Water	1st Bone Spring	6220'	Oil/Natural Gas
Grayburg			2nd Bone Spring	6972'	Oil/Natural Gas
San Andres			3rd Bone Spring	8340'	Oil/Natural Gas
Glorieta			Wolfcamp	8697'	Oil/Natural Gas

	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Is casing API approved? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	Y
If yes, does production casing cement tie back a minimum of 50' above the Reef?	Y
Is well within the designated 4 string boundary.	Y
Is well located in SOPA but not in R-111-P?	N
If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?	
Is well located in R-111-P and SOPA?	N
If yes, are the first three strings cemented to surface?	
Is 2 <sup>nd</sup> string set 100' to 600' below the base of salt?	
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
Is an engineered weak point used to satisfy R-111-Q?	
If yes, at what depth is the weak point planned?	
Is well located in high Cave/Karst?	N
If yes, are there two strings cemented to surface?	
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there three strings cemented to surface?	

SHL: 300' FNL 1200' FWL (Sec 7) BHL: 1900' FSL 2552' FWL (Sec 5)

		Casing Prog	ram Design B			BLM Minimum Safety Factors	1.125	1.0	1.6 Dry 1.8 Wet	1.6 Dry 1.8 Wet
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	26'	0'	0'	275'	275'	18 5/8" 87.5# J55 BTC	5.12	18.30	55.23	56.81
Int 1	17.5'	0'	0'	950'	950'	13.375" 48# H40 STC	1.53	3.43	7.06	11.86
Int 2	12.25'	0'	0'	2370'	2370'	9.625" 36# J55 LTC	1.91	3.32	5.31	6.61
Production	8.75'	0'	0'	9656'	8777'	7" 26# P110 LTC	1.44	2.29	2.76	3.31
Liner	6.125'	8756'	8204'	17309'	8899'	4.5" 13.5# P110 LTC	1.92	2,23	2.93	3.65

Design B - Cement Program

Design B - Cement I	r og i min								
Casing		# Sacks	Wt. lb/gal	Yield ft <sup>3</sup> /sack	TOC/BOC	Volume ft <sup>3</sup>	% Excess	Slurry Description	
20,000 in	LEAD	270	12.5	2.12	0' - 186'	580	100%	Class C: Salt, Gel, Extender, LCM	
20.000 111	TAIL	200	14.8	1.34	186' - 275'	268	100%	Class C: Retarder	
13.375 in	LEAD	340	12.5	2.12	0' - 695'	730	50%	Class C: Salt, Gel, Extender, LCM	
15.575 111	TAIL	200	14.8	1.34	695' - 950'	268	30%	Class C: Retarder	
1st Stg 9.625 in	LEAD	130	12.5	2.12	992' - 1696'	280	25%	Class C: Salt, Gel, Extender, LCM	
18t Stg 9.025 in	TAIL	200	14.8	1.34	1696' - 2370'	268	25%	Class C: Retarder	
					9 5/8" 1	DV Tool @ 992'			
2nd Stg 9.625 in	LEAD	120	12.5	2.12	0' - 655'	260	25%	Class C: Salt, Gel, Extender, LCM	
2110 Stg 9.025 III	TAIL	100	14.8	1.34	655' - 992'	0	25%	Class C: Retarder	
1st Stg 7 in	LEAD	90	12.5	2.12	6200' - 7229'	200	250/	Class C: Salt, Gel, Extender, LCM, Defoamer	
1st Stg / in	TAIL	400	15.6	1.18	7229' - 9656'	472	25%	Class H: Retarder, Fluid Loss, Defoamer	
	7" DV Tool @ 6200'								
2nd Stg 7 in	LEAD	390	12.5	2.12	960' - 5472'	830	25%	Class C: Salt, Gel, Extender, LCM, Defoamer	
Ziiu Stg / III	TAIL	100	14.8	1.34	5472' - 6200'	134	43%	Class C: Retarder, Fluid Loss, Defoamer	

Design B - Mud Program

Depth	Mud Wt	Mud Type
0' - 275'	8.4 - 8.6	Fresh Water
275' - 950'	9.5 - 10.2	Brine
950' - 2370'	8.4 - 8.6	Fresh Water
2370' - 9656'	8.6 - 9.5	Cut-Brine
9656' - 17308.6'	10.0 - 12.	OBM

Geology

Geology					
Formation	Est. Top (TVD)	Mineral Resources	Formation	Est. Top (TVD)	Mineral Resources
Rustler			Yeso		
Castile			Delaware (Lamar)	2445'	Oil/Natural Gas
Salt Top	345'	None	Bell Canyon		
Salt Base	550'	None	Cherry Canyon		
Yates	645'	Oil/Natural Gas	Manzanita Marker		
Seven Rivers			Basal Brushy Canyon		
Queen			Bone Spring	4707'	Oil/Natural Gas
Capitan	1017'	Usable Water	1st Bone Spring	6220'	Oil/Natural Gas
Grayburg			2nd Bone Spring	6972'	Oil/Natural Gas
San Andres			3rd Bone Spring	8340'	Oil/Natural Gas
Glorieta			Wolfcamp	8697'	Oil/Natural Gas

	Y or N
Is easing new? If used, attach certification as required in Onshore Order #1	Y
Is casing API approved? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	Y
If yes, does production casing cement tie back a minimum of 50' above the Reef?	Y
Is well within the designated 4 string boundary.	Y
Is well located in SOPA but not in R-111-P?	N
If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?	
Is well located in R-111-P and SOPA?	N
If yes, are the first three strings cemented to surface?	
Is 2 <sup>nd</sup> string set 100' to 600' below the base of salt?	
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
Is an engineered weak point used to satisfy R-111-Q?	
If yes, at what depth is the weak point planned?	
Is well located in high Cave/Karst?	N
If yes, are there two strings cemented to surface?	
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there three strings cemented to surface?	IN .

SHL: 300' FNL 1200' FWL (Sec 7) BHL: 1900' FSL 2552' FWL (Sec 5)

Casing Program Design A					BLM Minimum Safety Factors	1.125	1.0	1.6 Dry 1.8 Wet	1.6 Dry 1.8 Wet	
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	26'	0'	0'	275'	275'	18 5/8" 87.5# J55 BTC	5.12	18.30	55.23	56.81
Int 1	17.5'	0'	0'	950'	950'	13.375" 48# H40 STC	1.53	3.43	7.06	11.86
Int 2	12.25'	0'	0'	2370'	2370'	9.625" 36# J55 LTC	1.91	3.32	5.31	6.61
Production	8.75'	0'	0'	8756'	8204'	7" 26# P110 LTC	1.54	2.46	3.04	3.65
Liner	6.125'	8556'	8499'	17309'	8899'	4.5" 13.5# P110 LTC	1.92	2.23	2.86	3.57

**Cement Program** 

Casing		# Sacks	Wt. lb/gal	Yield ft <sup>3</sup> /sack	тос/вос	Volume ft <sup>3</sup>	% Excess	Slurry Description
20,000 in	LEAD	270	12.5	2.12	0' - 186'	580	100%	Class C: Salt, Gel, Extender, LCM
20.000 III	TAIL	200	14.8	1.34	186' - 275'	268	100%	Class C: Retarder
13,375 in	LEAD	340	12.5	2.12	0' - 695'	730	50%	Class C: Salt, Gel, Extender, LCM
15.5/5 III	TAIL	200	14.8	1.34	695' - 950'	268	30%	Class C: Retarder
1st Stg 9.625 in	LEAD	130	12.5	2.12	992' - 1696'	280	25%	Class C: Salt, Gel, Extender, LCM
18t Stg 9.025 III	TAIL	200	14.8	1.34	1696' - 2370'	268	2370	Class C: Retarder
					9 5/8'' 1	OV Tool @ 992'		
2nd Stg 9,625 in	LEAD	120	12.5	2.12	0' - 655'	260	25%	Class C: Salt, Gel, Extender, LCM
2110 Stg 9.025 III	TAIL	100	14.8	1.34	655' - 992'	134	2370	Class C: Retarder
1st Stg 7 in	LEAD	50	12.5	2.12	6200' - 6683'	110	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
ist Stg / iii	TAIL	400	15.6	1.18	6683' - 8756'	472	23%	Class H: Retarder, Fluid Loss, Defoamer
					7" DV	Tool @ 6200'		
2nd Stg 7 in	LEAD	390	12.5	2.12	960' - 5472'	830	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
Ziiu Sig / iii	TAIL	100	14.8	1.34	5472' - 6200'	134	23%	Class C: Retarder, Fluid Loss, Defoamer
4.5 in	LEAD	560	13.5	1.85	8556' - 17308.6'	1040	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer, Anti- settling Agent

Design A - Mud Program

Depth	Mud Wt	Mud Type
0' - 275'	8.4 - 8.6	Fresh Water
275' - 950'	9.5 - 10.2	Brine
950' - 2370'	8.4 - 8.6	Fresh Water
2370' - 8756'	8.6 - 9.5	Cut-Brine
8756' - 17308.6'	10.0 - 12.	OBM

Geology

Formation	Est. Top (TVD)	Mineral Resources	Formation	Est. Top (TVD)	Mineral Resources
Rustler			Yeso		
Castile			Delaware (Lamar)	2445'	Oil/Natural Gas
Salt Top	345'	None	Bell Canyon		
Salt Base	550'	None	Cherry Canyon		
Yates	645'	Oil/Natural Gas	Manzanita Marker		
Seven Rivers			Basal Brushy Canyon		
Queen			Bone Spring	4707'	Oil/Natural Gas
Capitan	1017'	Usable Water	1st Bone Spring	6220'	Oil/Natural Gas
Grayburg			2nd Bone Spring	6972'	Oil/Natural Gas
San Andres			3rd Bone Spring	8340'	Oil/Natural Gas
Glorieta			Wolfcamp	8697'	Oil/Natural Gas

	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Is casing API approved? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	Y
If yes, does production casing cement tie back a minimum of 50' above the Reef?	Y
Is well within the designated 4 string boundary.	Y
Is well located in SOPA but not in R-111-P?	N
If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?	
Is well located in R-111-P and SOPA?	N
If yes, are the first three strings cemented to surface?	
Is 2 <sup>nd</sup> string set 100' to 600' below the base of salt?	
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
Is an engineered weak point used to satisfy R-111-Q?	
If yes, at what depth is the weak point planned?	
Is well located in high Cave/Karst?	N
If yes, are there two strings cemented to surface?	
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there three strings cemented to surface?	

SHL: 300' FNL 1200' FWL (Sec 7) BHL: 1900' FSL 2552' FWL (Sec 5)

Casing Program Design B						BLM Minimum Safety Factors	1.125	1.0	1.6 Dry 1.8 Wet	1.6 Dry 1.8 Wet
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	26'	0'	0'	275'	275'	18 5/8" 87.5# J55 BTC	5.12	18.30	55.23	56.81
Int 1	17.5'	0'	0'	950'	950'	13.375" 48# H40 STC	1.53	3.43	7.06	11.86
Int 2	12.25'	0'	0'	2370'	2370'	9.625" 36# J55 LTC	1.91	3.32	5.31	6.61
Production	8.75'	0'	0'	9656'	8777'	7" 26# P110 LTC	1.44	2.29	2.76	3.31
Liner	6.125'	8756'	8204'	17309'	8899'	4.5" 13.5# P110 LTC	1.92	2.23	2.93	3.65

Design B - Cement Program

Design D - Centent I	ľ					à		
Casing		# Sacks	Wt. lb/gal	Yield ft <sup>3</sup> /sack	TOC/BOC	Volume ft <sup>3</sup>	% Excess	Slurry Description
20.000 in	LEAD	270	12.5	2.12	0' - 186'	580	100%	Class C: Salt, Gel, Extender, LCM
20.000 III	TAIL	200	14.8	1.34	186' - 275'	268	100%	Class C: Retarder
13.375 in	LEAD	340	12.5	2.12	0' - 695'	730	50%	Class C: Salt, Gel, Extender, LCM
15.575 III	TAIL	200	14.8	1.34	695' - 950'	268	30%	Class C: Retarder
1st Stg 9.625 in	LEAD	130	12.5	2.12	992' - 1696'	280	25%	Class C: Salt, Gel, Extender, LCM
18t 5tg 9.025 iii	TAIL	200	14.8	1.34	1696' - 2370'	268	2370	Class C: Retarder
					9 5/8" 1	DV Tool @ 992'		
2nd Stg 9.625 in	LEAD	120	12.5	2.12	0' - 655'	260	25%	Class C: Salt, Gel, Extender, LCM
2110 Stg 9.025 III	TAIL	100	14.8	1.34	655' - 992'	0	2370	Class C: Retarder
1st Stg 7 in	LEAD	90	12.5	2.12	6200' - 7229'	200	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
1st Stg / in	TAIL	400	15.6	1.18	7229' - 9656'	472	25%	Class H: Retarder, Fluid Loss, Defoamer
					7" DV	Tool @ 6200'		
2nd Stg 7 in	LEAD	390	12.5	2.12	960' - 5472'	830	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
Ziiu Stg / III	TAIL	100	14.8	1.34	5472' - 6200'	134	43%	Class C: Retarder, Fluid Loss, Defoamer

Design B - Mud Program

Depth	Mud Wt	Mud Type
0' - 275'	8.4 - 8.6	Fresh Water
275' - 950'	9.5 - 10.2	Brine
950' - 2370'	8.4 - 8.6	Fresh Water
2370' - 9656'	8.6 - 9.5	Cut-Brine
9656' - 17308.6'	10.0 - 12.	OBM

Geology

GCology					
Formation	Est. Top (TVD)	Mineral Resources	Formation	Est. Top (TVD)	Mineral Resources
Rustler			Yeso		
Castile			Delaware (Lamar)	2445'	Oil/Natural Gas
Salt Top	345'	None	Bell Canyon		
Salt Base	550'	None	Cherry Canyon		
Yates	645'	Oil/Natural Gas	Manzanita Marker		
Seven Rivers			Basal Brushy Canyon		
Queen			Bone Spring	4707'	Oil/Natural Gas
Capitan	1017'	Usable Water	1st Bone Spring	6220'	Oil/Natural Gas
Grayburg			2nd Bone Spring	6972'	Oil/Natural Gas
San Andres			3rd Bone Spring	8340'	Oil/Natural Gas
Glorieta			Wolfcamp	8697'	Oil/Natural Gas

	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Is casing API approved? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	Y
If yes, does production casing cement tie back a minimum of 50' above the Reef?	Ŷ
Is well within the designated 4 string boundary.	Y
Is well located in SOPA but not in R-111-P?	N
If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?	
Is well located in R-111-P and SOPA?	N
If yes, are the first three strings cemented to surface?	
Is 2 <sup>nd</sup> string set 100' to 600' below the base of salt?	
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
Is an engineered weak point used to satisfy R-111-Q?	
If yes, at what depth is the weak point planned?	
Is well located in high Cave/Karst?	N
If yes, are there two strings cemented to surface?	
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there three strings cemented to surface?	11

SHL: 300' FNL 1200' FWL (Sec 7) BHL: 1900' FSL 2552' FWL (Sec 5)

	Casing Program Design A						1.125	1.0	1.6 Dry 1.8 Wet	1.6 Dry 1.8 Wet
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	26'	0'	0'	275'	275'	18 5/8" 87.5# J55 BTC	5.12	18.30	55.23	56.81
Int 1	17.5'	0'	0'	950'	950'	13.375" 48# H40 STC	1.53	3.43	7.06	11.86
Int 2	12.25'	0'	0'	2370'	2370'	9.625" 36# J55 LTC	1.91	3.32	5.31	6.61
Production	8.75'	0'	0'	8756'	8204'	7" 26# P110 LTC	1.54	2.46	3.04	3.65
Liner	6.125'	8556'	8499'	17309'	8899'	4.5" 13.5# P110 LTC	1.92	2.23	2.86	3.57

Cement Program

Casing		# Sacks	Wt. lb/gal	Yield ft <sup>3</sup> /sack	тос/вос	Volume ft <sup>3</sup>	% Excess	Slurry Description
20,000 in	LEAD	270	12.5	2.12	0' - 186'	580	100%	Class C: Salt, Gel, Extender, LCM
20.000 III	TAIL	200	14.8	1.34	186' - 275'	268	10076	Class C: Retarder
13,375 in	LEAD	340	12.5	2.12	0' - 695'	730	50%	Class C: Salt, Gel, Extender, LCM
15.575 111	TAIL	200	14.8	1.34	695' - 950'	268	30%	Class C: Retarder
1-4 04- 0 (25 1-	LEAD	130	12.5	2.12	992' - 1696'	280	25%	Class C: Salt, Gel, Extender, LCM
1st Stg 9.625 in	TAIL	200	14.8	1.34	1696' - 2370'	268	25%	Class C: Retarder
9 5/8" DV Tool @ 992'								
2nd Stg 9.625 in	LEAD	120	12.5	2.12	0' - 655'	260	25%	Class C: Salt, Gel, Extender, LCM
2nd Stg 9.025 in	TAIL	100	14.8	1.34	655' - 992'	134	25%	Class C: Retarder
1-1-04-71-	LEAD	50	12.5	2.12	6200' - 6683'	110	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
1st Stg 7 in	TAIL	400	15.6	1.18	6683' - 8756'	472	25%	Class H: Retarder, Fluid Loss, Defoamer
					7" DV	Tool @ 6200'		
2nd Stg 7 in	LEAD	390	12.5	2.12	960' - 5472'	830	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
Ziiu Stg / III	TAIL	100	14.8	1.34	5472' - 6200'	134	1 25%	Class C: Retarder, Fluid Loss, Defoamer
4.5 in	LEAD	560	13.5	1.85	8556' - 17308.6'	1040	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer, Anti- settling Agent

Design A - Mud Program

Depth	Mud Wt	Mud Type
0' - 275'	8.4 - 8.6	Fresh Water
275' - 950'	9.5 - 10.2	Brine
950' - 2370'	8.4 - 8.6	Fresh Water
2370' - 8756'	8.6 - 9.5	Cut-Brine
8756' - 17308.6'	10.0 - 12.	OBM

Geology

Formation	Est. Top (TVD)	Mineral Resources	Formation	Est. Top (TVD)	Mineral Resources
Rustler			Yeso		
Castile			Delaware (Lamar)	2445'	Oil/Natural Gas
Salt Top	345'	None	Bell Canyon		
Salt Base	550'	None	Cherry Canyon		
Yates	645'	Oil/Natural Gas	Manzanita Marker		
Seven Rivers			Basal Brushy Canyon		
Queen			Bone Spring	4707'	Oil/Natural Gas
Capitan	1017'	Usable Water	1st Bone Spring	6220'	Oil/Natural Gas
Grayburg			2nd Bone Spring	6972'	Oil/Natural Gas
San Andres			3rd Bone Spring	8340'	Oil/Natural Gas
Glorieta			Wolfcamp	8697'	Oil/Natural Gas

	·
	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Is casing API approved? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	Y
If yes, does production casing cement tie back a minimum of 50' above the Reef?	Y
Is well within the designated 4 string boundary.	Y
Is well located in SOPA but not in R-111-P?	N
If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?	
Is well located in R-111-P and SOPA?	N
If yes, are the first three strings cemented to surface?	
Is 2 <sup>nd</sup> string set 100' to 600' below the base of salt?	
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
Is an engineered weak point used to satisfy R-111-Q?	
If yes, at what depth is the weak point planned?	
Is well located in high Cave/Karst?	N
If yes, are there two strings cemented to surface?	
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there three strings cemented to surface?	

SHL: 300' FNL 1200' FWL (Sec 7) BHL: 1900' FSL 2552' FWL (Sec 5)

		Casing Prog	gram Design B			BLM Minimum Safety Factors	1.125	1.0	1.6 Dry 1.8 Wet	1.6 Dry 1.8 Wet
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	26'	0'	0'	275'	275'	18 5/8" 87.5# J55 BTC	5.12	18.30	55.23	56.81
Int 1	17.5'	0'	0'	950'	950'	13.375" 48# H40 STC	1.53	3.43	7.06	11.86
Int 2	12.25'	0'	0'	2370'	2370'	9.625" 36# J55 LTC	1.91	3.32	5.31	6.61
Production	8.75'	0'	0'	9656'	8777'	7" 26# P110 LTC	1.44	2.29	2.76	3.31
Liner	6.125'	8756'	8204'	17309'	8899'	4.5" 13.5# P110 LTC	1.92	2.23	2.93	3.65

Design B - Cement Program

Design B - Cement I	r og i min							
Casing		# Sacks	Wt. lb/gal	Yield ft <sup>3</sup> /sack	TOC/BOC	Volume ft <sup>3</sup>	% Excess	Slurry Description
20,000 in	LEAD	270	12.5	2.12	0' - 186'	580	100%	Class C: Salt, Gel, Extender, LCM
20.000 111	TAIL	200	14.8	1.34	186' - 275'	268	10078	Class C: Retarder
13.375 in	LEAD	340	12.5	2.12	0' - 695'	730	50%	Class C: Salt, Gel, Extender, LCM
15.575 111	TAIL	200	14.8	1.34	695' - 950'	268	30%	Class C: Retarder
1st Stg 9.625 in	LEAD	130	12.5	2.12	992' - 1696'	280	25%	Class C: Salt, Gel, Extender, LCM
18t Stg 9.025 in	TAIL	200	14.8	1.34	1696' - 2370'	268		Class C: Retarder
					9 5/8" 1	DV Tool @ 992'		
2nd Stg 9.625 in	LEAD	120	12.5	2.12	0' - 655'	260	25%	Class C: Salt, Gel, Extender, LCM
2110 Stg 9.025 III	TAIL	100	14.8	1.34	655' - 992'	0	25%	Class C: Retarder
1st Stg 7 in	LEAD	90	12.5	2.12	6200' - 7229'	200	250/	Class C: Salt, Gel, Extender, LCM, Defoamer
1st Stg / in	TAIL	400	15.6	1.18	7229' - 9656'	472	25%	Class H: Retarder, Fluid Loss, Defoamer
					7" DV	Tool @ 6200'		
2nd Stg 7 in	LEAD	390	12.5	2.12	960' - 5472'	830	250/	Class C: Salt, Gel, Extender, LCM, Defoamer
2nd Stg / in	TAIL	100	14.8	1.34	5472' - 6200'	134	25%	Class C: Retarder, Fluid Loss, Defoamer

Design B - Mud Program

Depth	Mud Wt	Mud Type
0' - 275'	8.4 - 8.6	Fresh Water
275' - 950'	9.5 - 10.2	Brine
950' - 2370'	8.4 - 8.6	Fresh Water
2370' - 9656'	8.6 - 9.5	Cut-Brine
9656' - 17308.6'	10.0 - 12.	OBM

Geology

Geology					
Formation	Est. Top (TVD)	Mineral Resources	Formation	Est. Top (TVD)	Mineral Resources
Rustler			Yeso		
Castile			Delaware (Lamar)	2445'	Oil/Natural Gas
Salt Top	345'	None	Bell Canyon		
Salt Base	550'	None	Cherry Canyon		
Yates	645'	Oil/Natural Gas	Manzanita Marker		
Seven Rivers			Basal Brushy Canyon		
Queen			Bone Spring	4707'	Oil/Natural Gas
Capitan	1017'	Usable Water	1st Bone Spring	6220'	Oil/Natural Gas
Grayburg			2nd Bone Spring	6972'	Oil/Natural Gas
San Andres			3rd Bone Spring	8340'	Oil/Natural Gas
Glorieta			Wolfcamp	8697'	Oil/Natural Gas

	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Is casing API approved? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	Y
If yes, does production easing cement tie back a minimum of 50° above the Reef?	Ÿ
Is well within the designated 4 string boundary.	Y
Is well located in SOPA but not in R-111-P?	N
If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?	
Is well located in R-111-P and SOPA?	N
If yes, are the first three strings cemented to surface?	
Is 2 <sup>nd</sup> string set 100' to 600' below the base of salt?	
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
Is an engineered weak point used to satisfy R-111-Q?	
If yes, at what depth is the weak point planned?	
Is well located in high Cave/Karst?	N
If yes, are there two strings cemented to surface?	
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there three strings cemented to surface?	N
n yes, are there strings comence to surface.	

SHL: 300' FNL 1200' FWL (Sec 7) BHL: 1900' FSL 2552' FWL (Sec 5)

	Casing Program Design A						1.125	1.0	1.6 Dry 1.8 Wet	1.6 Dry 1.8 Wet
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	26'	0'	0'	275'	275'	18 5/8" 87.5# J55 BTC	5.12	18.30	55.23	56.81
Int 1	17.5'	0'	0'	950'	950'	13.375" 48# H40 STC	1.53	3.43	7.06	11.86
Int 2	12.25'	0'	0'	2370'	2370'	9.625" 36# J55 LTC	1.91	3.32	5.31	6.61
Production	8.75'	0'	0'	8756'	8204'	7" 26# P110 LTC	1.54	2.46	3.04	3.65
Liner	6.125'	8556'	8499'	17309'	8899'	4.5" 13.5# P110 LTC	1.92	2.23	2.86	3.57

Cement Program

Casing		# Sacks	Wt. lb/gal	Yield ft <sup>3</sup> /sack	тос/вос	Volume ft <sup>3</sup>	% Excess	Slurry Description
20,000 in	LEAD	270	12.5	2.12	0' - 186'	580	100%	Class C: Salt, Gel, Extender, LCM
20.000 111	TAIL	200	14.8	1.34	186' - 275'	268	10076	Class C: Retarder
13,375 in	LEAD	340	12.5	2.12	0' - 695'	730	50%	Class C: Salt, Gel, Extender, LCM
13.375 III	TAIL	200	14.8	1.34	695' - 950'	268		Class C: Retarder
1st Stg 9.625 in	LEAD	130	12.5	2.12	992' - 1696'	280	25%	Class C: Salt, Gel, Extender, LCM
18t Stg 9.025 in	TAIL	200	14.8	1.34	1696' - 2370'	268	25%	Class C: Retarder
9 5/8" DV Tool @ 992'								
2nd Stg 9.625 in	LEAD	120	12.5	2.12	0' - 655'	260	250/	Class C: Salt, Gel, Extender, LCM
2nd Stg 9.025 in	TAIL	100	14.8	1.34	655' - 992'	134	25%	Class C: Retarder
1st Stg 7 in	LEAD	50	12.5	2.12	6200' - 6683'	110	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
ist stg / iii	TAIL	400	15.6	1.18	6683' - 8756'	472	23%	Class H: Retarder, Fluid Loss, Defoamer
					7" DV	Tool @ 6200'		
2nd Stg 7 in	LEAD	390	12.5	2.12	960' - 5472'	830	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
Ziiu Stg / III	TAIL	100	14.8	1.34	5472' - 6200'	134	25%	Class C: Retarder, Fluid Loss, Defoamer
4.5 in	LEAD	560	13.5	1.85	8556' - 17308.6'	1040	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer, Anti- settling Agent

Design A - Mud Program

Depth	Mud Wt	Mud Type
0' - 275'	8.4 - 8.6	Fresh Water
275' - 950'	9.5 - 10.2	Brine
950' - 2370'	8.4 - 8.6	Fresh Water
2370' - 8756'	8.6 - 9.5	Cut-Brine
8756' - 17308.6'	10.0 - 12.	OBM

Geology

Formation	Est. Top (TVD)	Mineral Resources	Formation	Est. Top (TVD)	Mineral Resources
Rustler			Yeso		
Castile			Delaware (Lamar)	2445'	Oil/Natural Gas
Salt Top	345'	None	Bell Canyon		
Salt Base	550'	None	Cherry Canyon		
Yates	645'	Oil/Natural Gas	Manzanita Marker		
Seven Rivers			Basal Brushy Canyon		
Queen			Bone Spring	4707'	Oil/Natural Gas
Capitan	1017'	Usable Water	1st Bone Spring	6220'	Oil/Natural Gas
Grayburg			2nd Bone Spring	6972'	Oil/Natural Gas
San Andres			3rd Bone Spring	8340'	Oil/Natural Gas
Glorieta			Wolfcamp	8697'	Oil/Natural Gas

s casing new? If used, attach certification as required in Onshore Order #1  s casing API approved? If no, attach casing specification sheet.  y s casing API approved? If no, attach casing specification sheet.  Nose the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).  Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?  y s well located within Capitan Reef?  If yes, does production casing cement tie back a minimum of 50' above the Reef?  If yes, does production casing cement tie back a minimum of 50' above the Reef?  y If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?  s well located in R-111-P and SOPA?  If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?  s well located in R-111-P and SOPA?  If yes, are the first three strings cemented to surface?  Is 2 <sup>rd</sup> string set 100' to 600' below the base of salt?  s an open annulus used to satisfy R-111-Q? If yes, see cement design.  s an engineered weak point used to satisfy R-111-Q?  If yes, at what depth is the weak point planned?		
s casing API approved? If no, attach casing specification sheet.  y spremium or uncommon easing planned? If yes attach casing specification sheet.  No Nocs the above casing design meet or exceede BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).  Yill the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?  y will located within Capitan Reef?  If yes, does production casing cement tie back a minimum of 50' above the Reef?  Is well within the designated 4 string boundary.  y will located in SOPA but not in R-111-P?  If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?  s well located in R-111-P and SOPA?  If yes, are the first three strings cemented to surface?  Is 2 <sup>m</sup> string set 100' to 600' below the base of salt?  s an open annulus used to satisfy R-111-Q? If yes, see cement design.  s an engineered weak point used to satisfy R-111-Q?  If yes, ar what depth is the weak point planned?  s well located in high Cave/Karst?  N  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  s well located in critical Cave/Karst?		Y or N
s premium or uncommon casing planned? If yes attach casing specification sheet.  Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).  Yell the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?  So well located within Capitan Reef?  If yes, does production casing cement tie back a minimum of 50' above the Reef?  If yes, does production casing cement tie back a minimum of 50' above the Reef?  If yes, does production casing cement tie back a minimum of 50' above the Reef?  If yes, are the first 2 strings comented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?  So well located in SOPA but not in R-111-P?  If yes, are the first three strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?  So well located in R-111-P and SOPA?  If yes, are the first three strings cemented to surface?  Is 2 <sup>rd</sup> string set 100' to 600' below the base of salt?  So an open annulus used to satisfy R-111-Q?  If yes, are what depth is the weak point planned?  So well located in high Cave/Karst?  No If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  So well located in critical Cave/Karst?	Is casing new? If used, attach certification as required in Onshore Order #1	Y
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).  Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?  s well located within Capitan Reef?  If yes, does production casing cement tie back a minimum of 50' above the Reef?  y If yes, does production casing cement tie back a minimum of 50' above the Reef?  y If yes, does production casing cement tie back a minimum of 50' above the Reef?  y If yes, does production casing cement tie back a minimum of 50' above the Reef?  y If yes, are the first 2 strings or the first 2 strings cemented to surface and 3'rd string cement tied back 500' into previous casing?  s well located in R-111-P and SOPA?  If yes, are the first three strings cemented to surface?  Is 2"d string set 100' to 600' below the base of salt?  s an open annulus used to satisfy R-111-Q? If yes, see cement design.  s an engineered weak point used to satisfy R-111-Q?  If yes, are what depth is the weak point planned?  s well located in high Cave/Karst?  N  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  s well located in critical Cave/Karst?	Is casing API approved? If no, attach casing specification sheet.	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the easing?  s well located within Capitan Reef?  If yes, does production easing cement tie back a minimum of 50' above the Reef?  Is well within the designated 4 string boundary.  s well located in SOPA but not in R-111-P?  If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?  s well located in R-111-P and SOPA?  If yes, are the first three strings cemented to surface?  Is 2 <sup>rd</sup> string set 100' to 600' below the base of salf?  s an open annulus used to satisfy R-111-Q? If yes, see cement design.  s an engineered weak point used to satisfy R-111-Q?  If yes, at what depth is the weak point planned?  s well located in high Cave/Karst?  N  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  s well located in critical Cave/Karst?	Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
s well located within Capitan Reef?  If yes, does production casing cement tie back a minimum of 50° above the Reef?  If well within the designated 4 string boundary.  s well located in SOPA but not in R-111-P?  If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500° into previous casing?  s well located in R-111-P and SOPA?  If yes, are the first three strings cemented to surface?  Is 2 <sup>nd</sup> string set 100° to 600° below the base of salt?  s an open annulus used to satisfy R-111-Q? If yes, see cement design.  s an engineered weak point used to satisfy R-111-Q?  If yes, at what depth is the weak point planned?  s well located in high Cave/Karst?  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  s well located in critical Cave/Karst?	Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y
If yes, does production easing cement tie back a minimum of 50' above the Reef?  Is well within the designated 4 string boundary.  **s well located in SOPA but not in R-111-P?  If yes, are the first 2 strings cemented to surface and 3" string cement tied back 500' into previous casing?  **s well located in R-111-P and SOPA?  If yes, are the first three strings cemented to surface?  Is 2" string set 100' to 600' below the base of salt?  **s an open annulus used to satisfy R-111-Q? If yes, see cement design.  **s an open annulus used to satisfy R-111-Q?  If yes, at what depth is the weak point planned?  **s well located in high Cave/Karst?*  N  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  **s well located in critical Cave/Karst?*  N	Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
If yes, does production easing cement tie back a minimum of 50' above the Reef?  Is well within the designated 4 string boundary.  **s well located in SOPA but not in R-111-P?  If yes, are the first 2 strings cemented to surface and 3" string cement tied back 500' into previous casing?  **s well located in R-111-P and SOPA?  If yes, are the first three strings cemented to surface?  Is 2" string set 100' to 600' below the base of salt?  **s an open annulus used to satisfy R-111-Q? If yes, see cement design.  **s an open annulus used to satisfy R-111-Q?  If yes, at what depth is the weak point planned?  **s well located in high Cave/Karst?*  N  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  **s well located in critical Cave/Karst?*  N		
Is well located in SOPA but not in R-111-P?  If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?  If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?  If yes, are the first three strings cemented to surface?  Is 2 <sup>nd</sup> string set 100' to 600' below the base of salt?  Is an open annulus used to satisfy R-111-Q? If yes, see cement design.  If yes, at what depth is the weak point planned?  If yes, at what depth is the weak point planned?  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  N  N  N  N  N  N  N  N  N  N  N  N  N	Is well located within Capitan Reef?	Y
s well located in SOPA but not in R-111-P?  If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?  s well located in R-111-P and SOPA?  If yes, are the first three strings cemented to surface?  Is 2 <sup>nd</sup> string set 100' to 600' below the base of salt?  s an open annulus used to satisfy R-111-Q? If yes, see cement design.  s an engineered weak point used to satisfy R-111-Q?  If yes, at what depth is the weak point planned?  s well located in high Cave/Karst?  N  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?		Y
If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500° into previous casing?  If yes, are the first three strings cemented to surface?  Is 2 <sup>nd</sup> string set 100° to 600° below the base of salt?  s an open annulus used to satisfy R-111-Q? If yes, see cement design.  s an engineered weak point used to satisfy R-111-Q?  If yes, at what depth is the weak point planned?  s well located in high Cave/Karst?  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  N  N  N  N  N  N  N  N  N  N  N  N  N	Is well within the designated 4 string boundary.	Y
If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500° into previous casing?  If yes, are the first three strings cemented to surface?  Is 2 <sup>nd</sup> string set 100° to 600° below the base of salt?  s an open annulus used to satisfy R-111-Q? If yes, see cement design.  s an engineered weak point used to satisfy R-111-Q?  If yes, at what depth is the weak point planned?  s well located in high Cave/Karst?  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  N  N  N  N  N  N  N  N  N  N  N  N  N		
s well located in R-111-P and SOPA?  If yes, are the first three strings cemented to surface?  Is 2 <sup>nd</sup> string set 100' to 600' below the base of salt?  s an open annulus used to satisfy R-111-Q? If yes, see cement design.  s an engineered weak point used to satisfy R-111-Q?  If yes, at what depth is the weak point planned?  s well located in high Cave/Karst?  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  s well located in critical Cave/Karst?	Is well located in SOPA but not in R-111-P?	N
If yes, are the first three strings cemented to surface?  Is 2 <sup>nd</sup> string set 100' to 600' below the base of salt?  s an open annulus used to satisfy R-111-Q? If yes, see cement design.  s an engineered weak point used to satisfy R-111-Q?  If yes, at what depth is the weak point planned?  s well located in high Cave/Karst?  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  s well located in critical Cave/Karst?	If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?	
If yes, are the first three strings cemented to surface?  Is 2 <sup>nd</sup> string set 100' to 600' below the base of salt?  s an open annulus used to satisfy R-111-Q? If yes, see cement design.  s an engineered weak point used to satisfy R-111-Q?  If yes, at what depth is the weak point planned?  s well located in high Cave/Karst?  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  s well located in critical Cave/Karst?		
Is 2 <sup>nd</sup> string set 100' to 600' below the base of salt?  s an open annulus used to satisfy R-111-Q? If yes, see cement design.  s an engineered weak point used to satisfy R-111-Q?  If yes, at what depth is the weak point planned?  s well located in high Cave/Karst?  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  s well located in critical Cave/Karst?	Is well located in R-111-P and SOPA?	N
s an open annulus used to satisfy R-111-Q? If yes, see cement design. s an engineered weak point used to satisfy R-111-Q? If yes, at what depth is the weak point planned? s well located in high Cave/Karst? If yes, are there two strings cemented to surface? (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs? s well located in critical Cave/Karst? N	If yes, are the first three strings cemented to surface?	
s an engineered weak point used to satisfy R-111-Q?  If yes, at what depth is the weak point planned?  s well located in high Cave/Karst?  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  s well located in critical Cave/Karst?  N	Is 2 <sup>nd</sup> string set 100' to 600' below the base of salt?	
If yes, at what depth is the weak point planned?  s well located in high Cave/Karst?  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  s well located in critical Cave/Karst?  N	Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
s well located in high Cave/Karst?  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  s well located in critical Cave/Karst?	Is an engineered weak point used to satisfy R-111-Q?	
If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  s well located in critical Cave/Karst?	If yes, at what depth is the weak point planned?	
If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  s well located in critical Cave/Karst?		
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  s well located in critical Cave/Karst?  N	Is well located in high Cave/Karst?	N
s well located in critical Cave/Karst?		
	(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
If yes, are there three strings cemented to surface?		N
	If yes, are there three strings cemented to surface?	

SHL: 300' FNL 1200' FWL (Sec 7) BHL: 1900' FSL 2552' FWL (Sec 5)

		Casing Prog	ram Design B			BLM Minimum Safety Factors	1.125	1.0	1.6 Dry 1.8 Wet	1.6 Dry 1.8 Wet
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	26'	0'	0'	275'	275'	18 5/8" 87.5# J55 BTC	5.12	18.30	55.23	56.81
Int 1	17.5'	0'	0'	950'	950'	13.375" 48# H40 STC	1.53	3.43	7.06	11.86
Int 2	12.25'	0'	0'	2370'	2370'	9.625" 36# J55 LTC	1.91	3.32	5.31	6.61
Production	8.75'	0'	0'	9656'	8777'	7" 26# P110 LTC	1.44	2.29	2.76	3.31
Liner	6.125'	8756'	8204'	17309'	8899'	4.5" 13.5# P110 LTC	1.92	2.23	2.93	3.65

Design B - Cement Program

Besign B - Cement I								
Casing		# Sacks	Wt. lb/gal	Yield ft <sup>3</sup> /sack	TOC/BOC	Volume ft <sup>3</sup>	% Excess	Slurry Description
20,000 in	LEAD	270	12.5	2.12	0' - 186'	580	100%	Class C: Salt, Gel, Extender, LCM
20.000 111	TAIL	200	14.8	1.34	186' - 275'	268	100%	Class C: Retarder
13.375 in	LEAD	340	12.5	2.12	0' - 695'	730	50%	Class C: Salt, Gel, Extender, LCM
13.575 III	TAIL	200	14.8	1.34	695' - 950'	268	3076	Class C: Retarder
1st Stg 9.625 in	LEAD	130	12.5	2.12	992' - 1696'	280	25%	Class C: Salt, Gel, Extender, LCM
18t Stg 9.025 in	TAIL	200	14.8	1.34	1696' - 2370'	268	25%	Class C: Retarder
					9 5/8" 1	DV Tool @ 992'		
2nd Stg 9.625 in	LEAD	120	12.5	2.12	0' - 655'	260	25%	Class C: Salt, Gel, Extender, LCM
2110 Stg 9.025 III	TAIL	100	14.8	1.34	655' - 992'	0	25%	Class C: Retarder
1st Stg 7 in	LEAD	90	12.5	2.12	6200' - 7229'	200	250/	Class C: Salt, Gel, Extender, LCM, Defoamer
1st Stg / in	TAIL	400	15.6	1.18	7229' - 9656'	472	25%	Class H: Retarder, Fluid Loss, Defoamer
		-			7" DV	Tool @ 6200'		
2nd Stg 7 in	LEAD	390	12.5	2.12	960' - 5472'	830	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
Ziiu Stg / III	TAIL	100	14.8	1.34	5472' - 6200'	134	43%	Class C: Retarder, Fluid Loss, Defoamer

Design B - Mud Program

Depth	Mud Wt	Mud Type
0' - 275'	8.4 - 8.6	Fresh Water
275' - 950'	9.5 - 10.2	Brine
950' - 2370'	8.4 - 8.6	Fresh Water
2370' - 9656'	8.6 - 9.5	Cut-Brine
9656' - 17308.6'	10.0 - 12.	OBM

Geology

GCology					
Formation	Est. Top (TVD)	Mineral Resources	Formation	Est. Top (TVD)	Mineral Resources
Rustler			Yeso		
Castile			Delaware (Lamar)	2445'	Oil/Natural Gas
Salt Top	345'	None	Bell Canyon		
Salt Base	550'	None	Cherry Canyon		
Yates	645'	Oil/Natural Gas	Manzanita Marker		
Seven Rivers			Basal Brushy Canyon		
Queen			Bone Spring	4707'	Oil/Natural Gas
Capitan	1017'	Usable Water	1st Bone Spring	6220'	Oil/Natural Gas
Grayburg			2nd Bone Spring	6972'	Oil/Natural Gas
San Andres			3rd Bone Spring	8340'	Oil/Natural Gas
Glorieta			Wolfcamp	8697'	Oil/Natural Gas

	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Is casing API approved? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	Y
If yes, does production casing cement tie back a minimum of 50' above the Reef?	Ŷ
Is well within the designated 4 string boundary.	Y
Is well located in SOPA but not in R-111-P?	N
If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?	
Is well located in R-111-P and SOPA?	N
If yes, are the first three strings cemented to surface?	
Is 2 <sup>nd</sup> string set 100' to 600' below the base of salt?	
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
Is an engineered weak point used to satisfy R-111-Q?	
If yes, at what depth is the weak point planned?	
Is well located in high Cave/Karst?	N
If yes, are there two strings cemented to surface?	
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there three strings cemented to surface?	IN .

# **Mewbourne Oil Company**

Eddy County, New Mexico NAD 83 Tough Ombres 6/5 Fed Com #715H Sec 07, T21S, R27E

SHL: 300' FNL & 1200' FWL (Sec 7) BHL: 1900' FSL & 2552' FWL (Sec 5)

Plan: Design #1

# **Standard Planning Report**

26 March, 2024

Database: Hobbs

Company: Mewbourne Oil Company

Project: Eddy County, New Mexico NAD 83
Site: Tough Ombres 6/5 Fed Com #715H

Well: Sec 07, T21S, R27E

**Wellbore:** BHL: 1900' FSL & 2552' FWL (Sec 5)

Design: Design #1

Local Co-ordinate Reference:

TVD Reference:
MD Reference:
North Reference:

Survey Calculation Method:

Site Tough Ombres 6/5 Fed Com #715H

Well @ 3259.0usft (Original well) Well @ 3259.0usft (Original well)

Grid

Minimum Curvature

Project Eddy County, New Mexico NAD 83

Map System: US State Plane 1983
Geo Datum: North American Datum 1983

Map Zone: North American Datum 198
New Mexico Eastern Zone

System Datum: Ground Level

Site Tough Ombres 6/5 Fed Com #715H

 Site Position:
 Northing:
 545,929.70 usft
 Latitude:
 32.5007821

 From:
 Map
 Easting:
 572,112.70 usft
 Longitude:
 -104.2335083

Position Uncertainty: 0.0 usft Slot Radius: 13-3/16 "

**Well** Sec 07, T21S, R27E

 Well Position
 +N/-S
 0.0 usft
 Northing:
 545,929.70 usft
 Latitude:
 32.5007821

 +E/-W
 0.0 usft
 Easting:
 572,112.70 usft
 Longitude:
 -104.2335083

Position Uncertainty0.0 usftWellhead Elevation:3,259.0 usftGround Level:3,231.0 usft

Grid Convergence: 0.05 °

**Wellbore** BHL: 1900' FSL & 2552' FWL (Sec 5)

 Magnetics
 Model Name
 Sample Date
 Declination (°)
 Dip Angle (°)
 Field Strength (nT)

 IGRF2010
 12/31/2014
 7.47
 60.24
 48,332.65249057

Design #1

Audit Notes:

Version:Phase:PROTOTYPETie On Depth:0.0

 Vertical Section:
 Depth From (TVD) (usft)
 +N/-S (usft)
 +E/-W (usft)
 Direction (°)

 0.0
 0.0
 0.0
 70.40

Plan Survey Tool Program Date 3/26/2024

Depth From Depth To

(usft) (usft) Survey (Wellbore) Tool Name Remarks

1 0.0 17,308.6 Design #1 (BHL: 1900' FSL & 255

Plan Sections										
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)	TFO (°)	Target
0.0	0.00	0.00	0.0	0.0	0.0	0.00	0.00	0.00	0.00	
550.0	0.00	0.00	550.0	0.0	0.0	0.00	0.00	0.00	0,00	
1,725.9	23.52	323.50	1,693.2	191.3	-141.6	2.00	2.00	0.00	323.50	
7,579.8	23.52	323.50	7,060.8	2,069.1	-1,531.0	0.00	0.00	0.00	0.00	
8,755.8	0.00	0.00	8,204.0	2,260.4	-1,672.6	2.00	-2.00	0.00	180.00 K	OP: 1973' FSL & 47
9,646.8	89.09	89.50	8,777.0	2,265.3	-1,108.7	10.00	10.00	0.00	89.50	
17,308.6	89.09	89.50	8,899.0	2,332.5	6,551.8	0.00	0.00	0.00	0.00 BI	HL: 1900' FSL & 25

Database: Hobbs

Company: Mewbourne Oil Company

Project: Eddy County, New Mexico NAD 83
Site: Tough Ombres 6/5 Fed Com #715H

Well: Sec 07, T21S, R27E

**Wellbore:** BHL: 1900' FSL & 2552' FWL (Sec 5)

Design: Design #1

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Site Tough Ombres 6/5 Fed Com #715H

Well @ 3259.0usft (Original well) Well @ 3259.0usft (Original well)

Grid

ed Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
0.0	0.00	0.00	0.0	0.0	0.0	0.0	0.00	0.00	0.00
	NL & 1200' FWL								
100.0	0.00	0.00	100.0	0.0	0.0	0.0	0.00	0.00	0.00
200.0	0.00	0.00	200.0	0.0	0.0	0.0	0.00	0.00	0.00
300.0	0.00	0.00	300.0	0.0	0.0	0.0	0.00	0.00	0.00
400.0	0.00	0.00	400.0	0.0	0.0	0.0	0.00	0.00	0.00
500.0	0.00	0.00	500.0	0.0	0.0	0.0	0.00	0.00	0.00
550.0	0.00	0.00	550.0	0.0	0.0	0.0	0.00	0.00	0.00
600.0	1.00	323.50	600.0	0.4	<b>-</b> 0.3	-0.1	2.00	2.00	0.00
700.0	3.00	323.50	699.9	3.2	<b>-</b> 2.3	-1.1	2.00	2.00	0.00
800.0	5.00	323.50	799.7	8.8	<b>-</b> 6.5	<b>-</b> 3.2	2.00	2.00	0.00
900.0	7.00	323.50	899.1	17.2	-12.7	-6.2	2.00	2.00	0.00
1,000.0	9.00	323.50	998.2	28.4	-21.0	-10.3	2.00	2.00	0.00
1,100.0	11.00	323.50	1,096.6	42.3	-31.3	-15.3	2.00	2.00	0.00
1,200.0	13.00	323.50	1,194.4	59.0	-43.7	-21.3	2.00	2.00	0.00
1,300.0	15.00	323.50	1,291.5	78.5	-58.1	-28.4	2.00	2.00	0.00
1,400.0	17.00	323.50	1,387.6	100.6	-74.5	-36.4	2.00	2.00	0.00
1,500.0	19.00	323.50	1,482.7	125.5	<b>-</b> 92.8	-45.4	2.00	2.00	0.00
1,600.0	21.00	323.50	1,576.6	153.0	-113.2	-55.3	2.00	2.00	0.00
1,700.0	23.00	323.50	1,669.4	183.1	-1135.5	-66.2	2.00	2.00	0.00
1,725.9	23.52	323.50	1,693.2	191.3	-141.6	-69.2	2.00	2.00	0.00
1,800,0	23,52	323,50	1,761,1	215,1	-159.1	-77.8	0,00	0,00	0,00
1,900.0	23.52	323,50	1,852,8	247.1	-182.9	-89.4	0.00	0.00	0,00
2,000.0	23.52	323,50	1,944.5	279.2	-102.9	-03.4 -101.0	0,00	0.00	0,00
2,100,0 2,200,0	23.52 23.52	323,50 323,50	2,036,2 2,127,9	311.3 343.4	-230.3 -254.1	-112,6 -124,2	0.00 0.00	0.00 0.00	0,00 0,00
2,300.0	23.52	323.50	2,219.6	375.4	<b>-</b> 277.8	-135.8	0.00	0.00	0.00
			2,311.3		-277.6 -301.6	-133.6 -147.4	0.00	0.00	0.00
2,400.0	23.52	323.50	,	407.5					
2,500.0	23.52	323.50	2,403.0	439.6	-325.3	<b>-</b> 159.0	0.00	0.00	0.00
2,600.0	23.52	323.50	2,494.6	471.7	-349.0	-170.6	0.00	0.00	0.00
2,700.0	23.52	323.50	2,586.3	503.8	-372.8	-182.2	0.00	0.00	0.00
2,800.0	23.52	323.50	2,678.0	535.8	-396.5	-193.8	0.00	0.00	0.00
2,900.0	23.52	323.50	2,769.7	567.9	-420.2	-205.4	0.00	0.00	0.00
3,000.0	23.52	323.50	2,861.4	600.0	-444.0	-217.0	0.00	0.00	0.00
3,100.0	23.52	323.50	2,953.1	632.1	-467.7	-228.6	0.00	0.00	0.00
3,200.0	23.52	323.50	3,044.8	664.1	-491.4	-240.2	0.00	0.00	0.00
3,300.0	23.52	323.50	3,136.5	696.2	-515.2	-251.8	0.00	0.00	0.00
3,400.0	23.52	323.50	3,228.2	728.3	-538.9	-263.4	0.00	0.00	0.00
3,500.0	23.52	323.50	3,319.9	760.4	-562.6	-275.0	0.00	0.00	0.00
3,600.0	23.52	323.50	3,411.6	792.5	-586.4	-286.6	0.00	0.00	0.00
3,700.0	23.52	323.50	3,503.3	824.5	-610.1	-298.2	0.00	0.00	0.00
3,800.0	23.52	323.50	3,595.0	856.6	-633.9	-309.8	0.00	0.00	0.00
3,900.0	23.52	323.50	3,686.7	888.7	-657.6	-321.4	0.00	0.00	0.00
4,000.0	23.52	323.50	3,778.3	920.8	-681.3	-333.1	0.00	0.00	0.00
4,100.0	23.52	323.50	3,870.0	952.8	-705.1	-344.7	0.00	0.00	0.00
4,200.0	23.52	323.50	3,961.7	984.9	-728.8	-356.3	0.00	0.00	0.00
4,300.0	23.52	323.50	4,053.4	1,017.0	-752.5	-367.9	0.00	0.00	0.00
4,400.0	23.52	323.50	4,145.1	1,049.1	-776.3	-379.5	0.00	0.00	0.00
4,500.0	23.52	323.50	4,236.8	1,081.2	-800.0	-391.1	0.00	0.00	0.00
4,600.0	23.52	323.50	4,328.5	1,113.2	-823.7	-402.7	0.00	0.00	0.00
4,700.0	23.52	323.50	4,420.2	1,145.3	-847.5	-414.3	0.00	0.00	0.00
4,800.0	23.52	323.50	4,511.9	1,177.4	-871.2	-425.9	0.00	0.00	0.00
4,900.0	23.52	323.50	4,603.6	1,209.5	-895.0	-437.5	0.00	0.00	0.00
5,000.0	23.52	323.50	4,695.3	1,241.5	-918.7	-449.1	0.00	0.00	0.00

Hobbs Database: Company:

Project:

Site:

Mewbourne Oil Company

Eddy County, New Mexico NAD 83 Tough Ombres 6/5 Fed Com #715H

Well: Sec 07, T21S, R27E

BHL: 1900' FSL & 2552' FWL (Sec 5) Wellbore:

Design: Design #1 Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

**Survey Calculation Method:** 

Site Tough Ombres 6/5 Fed Com #715H

Well @ 3259.0usft (Original well) Well @ 3259.0usft (Original well)

anned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
5,100.0 5,200.0	23.52 23.52	323,50 323,50	4,787.0 4,878.7	1,273.6 1,305.7	<b>-</b> 942.4 <b>-</b> 966.2	-460.7 -472.3	0.00 0.00	0.00 0.00	0.00 0.00
5,300.0	23.52	323.50	4,970.4	1,337.8	-989.9	-483.9	0.00	0.00	0.00
5,400.0	23.52	323,50	5,062.1	1,369.9	-1,013.6	-495.5	0.00	0.00	0.00
5,500.0	23.52	323.50	5,153.7	1,401.9	-1,037.4	-507.1	0.00	0.00	0.00
5,600.0 5,700.0	23.52 23.52	323.50 323.50	5,245.4 5,337.1	1,434.0 1,466.1	-1,061.1 -1,084.8	-518.7 -530.3	0.00 0.00	0.00 0.00	0.00 0.00
5,800.0	23.52	323,50	5,428.8	1,498.2	-1,108.6	-541,9	0.00	0.00	0.00
5,900.0	23.52	323.50	5,520.5	1,530.2	-1,132.3	-553.5	0.00	0.00	0.00
6,000.0	23.52	323.50	5,612.2	1,562.3	-1,156.1	-565.1	0.00	0.00	0.00
6,100.0	23.52	323,50	5,703.9	1,594.4	-1,179.8	-576.7	0.00	0.00	0.00
6,200.0	23.52	323.50	5,795.6	1,626.5	-1,203.5	-588.3	0.00	0.00	0.00
6,300.0	23.52	323.50	5,887.3	1,658.6	-1,227.3	-599.9	0.00	0.00	0.00
6,400.0	23.52	323.50	5,979.0	1,690.6	-1,251.0	-611.5	0.00	0.00	0.00
6,500.0	23.52	323.50	6,070.7	1,722.7	-1,274.7	-623.1	0.00	0.00	0.00
6,600.0	23.52	323.50	6,162.4	1,754.8	-1,298.5	-634.7	0.00	0.00	0.00
6,700.0	23.52	323.50	6,254.1	1,786.9	-1,322.2	-646.3	0.00	0.00	0.00
6,800.0	23,52	323,50	6,345,8	1,818.9	-1,345,9	-657.9	0.00	0.00	0.00
6,900.0	23,52	323,50	6,437.4	1,851.0	-1,369.7	-669.5	0.00	0.00	0.00
7,000.0	23,52	323,50	6,529.1	1,883.1	-1,393.4	-681.1	0.00	0.00	0.00
7,100,0	23,52	323,50	6,620,8	1,915.2	-1,417,2	-692.7	0.00	0,00	0.00
7,200.0	23.52	323.50	6,712.5	1,947.3	-1,440.9	-704.3	0.00	0.00	0.00
7,300.0	23.52	323.50	6,804.2	1,979.3	-1,464.6	-715.9	0.00	0.00	0.00
7,400.0	23.52	323.50	6,895.9	2,011.4	-1,488.4	-727.5	0.00	0.00	0.00
7,500.0	23.52	323.50	6,987.6	2,043.5	-1,512.1	-739.2	0.00	0.00	0.00
7,579.8	23.52	323.50	7,060.8	2,069.1	-1,531.0	-748.4	0.00	0.00	0.00
7,600.0	23.12	323.50	7,079.3	2,075.5	-1,535.8	-750.7	2.00	<del>-</del> 2.00	0.00
7,700,0	21,12	323,50	7,172,0	2,105,8	-1,558.2	-761,7	2,00	-2,00	0,00
7,800.0	19.12	323,50	7,265.9	2,133.4	-1,578.6	-771.7	2.00	-2.00	0.00
7,900.0	17,12	323,50	7,360.9	2,158.4	-1,597.1	-780.7	2.00	-2.00	0.00
8,000.0	15.12	323,50	7,457.0	2,180.7	-1,613.6	-788.8	2.00	-2.00	0.00
8,100.0	13.12	323,50	7,553.9	2,200.3	-1,628.1	-795.9	2.00	-2.00	0.00
8,200.0	11.12	323.50	7,651.7	2,217.2	-1,640.6	-802.0	2.00	<del>-</del> 2.00	0.00
8,300.0	9.12	323.50	7,750.1	2,231.3	-1,651.1	-807.1	2.00	-2.00	0.00
8,400.0	7.12	323.50	7,849.1	2,242.7	-1,659.5	-811.2	2.00	-2.00	0.00
8,500.0	5.12	323.50	7,948.6	2,251.2	-1,665.8	-814.3	2.00	-2.00	0.00
8,600.0	3.12	323.50	8,048.3	2,257.0	-1,670.1	-816.4	2.00	-2.00	0.00
8,700.0	1.12	323,50	8,148.2	2,260.0	-1,672.3	-817.5	2,00	-2.00	0.00
8,755.8	0.00	0.00	8,204.0	2,260.4	-1,672.6	-817.6	2,00	-2.00	0.00
	FSL & 473' FEL (	•							
8,800.0	4.42	89.50	8,248.2	2,260.4	-1,670.9	-816.0	10.00	10.00	0.00
8,850.0	9.42	89.50	8,297.8	2,260.5	-1,664.9	-810.3	10.00	10.00	0.00
8,900.0	14.42	89.50	8,346.7	2,260.6	-1,654.5	-800.5	10.00	10.00	0.00
8,950.0	19.42	89.50	8,394.5	2,260.7	-1,640.0	<del>-</del> 786.8	10.00	10.00	0.00
9,000.0	24.42	89.50	8,440.9	2,260.8	<b>-</b> 1,621.3	<del>-</del> 769.2	10.00	10.00	0.00
9,050.0	29.42	89.50	8,485.5	2,261.0	<b>-</b> 1,598.7	<b>-</b> 747.8	10.00	10.00	0.00
9,100.0	34.42	89.50	8,527.9	2,261.3	<b>-</b> 1,572.3	<del>-</del> 722.8	10.00	10.00	0.00
9,150.0	39.41	89.50	8,567.9	2,261.5	<b>-</b> 1,542.3	<b>-</b> 694.4	10.00	10.00	0.00
9,200.0	44.41	89.50	8,605.1	2,261.8	-1,508.9	-662.9	10.00	10.00	0.00
9,250.0	49.41	89,50	8,639.2	2,262.2	-1,472.4	-628.4	10.00	10,00	0.00
9,300.0	54.41	89,50	8,670.0	2,262.5	-1,433.0	-591.2	10,00	10,00	0.00
9,350.0	59.41	89,50	8,697.3	2,262.9	-1,391.2	-551.6	10.00	10.00	0.00
9,400.0	64.41	89.50	8,720,9	2,263,3	-1,347,1	-510.0	10.00	10.00	0.00

Database: Hobbs

Company: Mewbourne Oil Company

Project: Eddy County, New Mexico NAD 83
Site: Tough Ombres 6/5 Fed Com #715H

Well: Sec 07, T21S, R27E

**Wellbore:** BHL: 1900' FSL & 2552' FWL (Sec 5)

Design: Design #1

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Site Tough Ombres 6/5 Fed Com #715H

Well @ 3259.0usft (Original well) Well @ 3259.0usft (Original well)

Grid

ned Survey									
inea Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
9,450.0	69.41	89.50	8,740.5	2,263,7	-1,301.1	<b>-</b> 466.5	10,00	10.00	0.00
9,500.0	74.41	89.50	8,756.0	2,264.1	<b>-</b> 1,253.6	<del>-</del> 421.6	10.00	10,00	0.00
9,550.0	79.41	89.50	8,767.3	2,264.5	<b>-</b> 1,204.9	<b>-</b> 375.6	10.00	10.00	0.00
9,600.0	84.41	89,50	8,774.3	2,264.9	<b>-</b> 1,155.4	<b>-</b> 328.9	10.00	10.00	0.00
9,646.8	89.09	89.50	8,777.0	2,265.3	<b>-</b> 1,108.7	<b>-</b> 284.7	10.00	10.00	0.00
9,655.9	89.09	89.50	8,777.1	2,265.4	-1,099.6	-276.1	0.00	0.00	0.00
FTP/LP: 19	98' FSL & 100' FV	VL (Sec 6)							
9,700.0	89.09	89.50	8,777.8	2,265.8	-1,055.5	-234.4	0.00	0.00	0.00
9,800.0	89.09	89.50	8,779.4	2,266.7	-955.5	-140.0	0.00	0.00	0.00
9,900.0	89.09	89.50	8,781.0	2,267.6	-855.5	-45.5	0.00	0.00	0.00
10,000.0	89.09	89.50	8,782.6	2,268.4	-755.6	49.0	0.00	0.00	0.00
10,100.0	89.09	89.50	8,784.2	2,269.3	-655.6	143.5	0.00	0.00	0.00
10,100.0	89.09	89.50	8,785.8	2,270.2	-555.6	238.0	0.00	0.00	0.00
10,300.0	89.09	89.50	8,787.4	2,271.1	-455.6	332.5	0.00	0.00	0.00
10,400.0	89.09	89.50	8,789.0	2,271.9	-355.6	427.0	0.00	0.00	0.00
10,500.0	89.09	89.50	8,790.6	2,272.8	-255.6	521.4	0.00	0.00	0.00
10,600.0	89.09	89.50	8,792.2	2,273.7	-155.7	615.9	0.00	0.00	0.00
10,700.0	89.09	89.50	8,793.8	2,274.6	-55.7	710.4	0.00	0.00	0.00
10,800.0	89.09	89.50	8,795.4 8,707.0	2,275.5	44.3	804.9	0.00	0.00	0.00
10,900.0 11,000.0	89.09 89.09	89.50 89.50	8,797.0 8,798.5	2,276.3 2,277.2	144.3 244.3	899.4 993.9	0.00 0.00	0.00 0.00	0.00 0.00
11,100.0	89.09	89.50	8,800.1	2,278.1	344.3	1,088.4	0.00	0.00	0,00
11,200,0	89.09	89,50	8,801.7	2,279.0	444.2	1,182.8	0.00	0.00	0.00
11,300.0	89.09	89,50	8,803.3	2,279.8	544.2	1,277.3	0.00	0.00	0.00
11,400.0	89.09	89,50	8,804.9	2,280.7	644.2	1,371,8	0.00	0.00	0.00
11,500.0	89.09	89.50	8,806.5	2,281.6	744.2	1,466.3	0.00	0.00	0.00
11,600.0	89.09	89.50	8,808.1	2,282.5	844.2	1,560.8	0.00	0.00	0.00
11,700.0	89.09	89.50	8,809.7	2,283.3	944.2	1,655.3	0.00	0.00	0.00
11,800.0	89.09	89.50	8,811.3	2,284.2	1,044.1	1,749.8	0.00	0.00	0.00
11,900.0	89.09	89.50	8,812.9	2,285.1	1,144.1	1,844.3	0.00	0.00	0.00
12,000.0	89.09	89.50	8,814.5	2,286.0	1,244.1	1,938.7	0.00	0.00	0.00
12,100.0	89.09	89.50	8,816.1	2,286.8	1,344.1	2,033.2	0.00	0.00	0.00
12,200.0	89.09	89.50	8,817.7	2,287.7	1,444.1	2,127.7	0.00	0.00	0.00
12,300.0	89.09	89.50	8,819.2	2,288.6	1,544.1	2,222.2	0.00	0.00	0.00
12,400.0	89.09	89.50	8,820.8	2,289.5	1,644.0	2,316.7	0.00	0.00	0.00
12,500.0	89.09	89.50	8,822.4	2,290.4	1,744.0	2,411.2	0.00	0.00	0.00
12,600.0	89.09	89.50	8,824.0	2,291.2	1,844.0	2,505.7	0.00	0.00	0.00
12,700.0	89.09 89.09	89.50	8,825.6	2,291.2	1,044.0	2,505.7 2,600.1	0.00	0.00	0.00
12,700.0	89.09	89.50	8,827.2	2,293.0	2.044.0	2,694.6	0.00	0.00	0.00
12,900.0	89.09	89.50	8,828.8	2,293.9	2,044.0	2,789.1	0.00	0.00	0.00
13,000.0	89.09	89.50	8,830.4	2,294.7	2,243.9	2,883.6	0.00	0.00	0.00
				,					
13,100.0	89.09	89.50	8,832.0	2,295.6	2,343.9	2,978.1	0.00	0.00	0.00
13,200.0	89.09	89.50	8,833.6	2,296.5	2,443.9	3,072.6	0.00	0.00	0.00
13,300.0	89.09	89.50	8,835.2	2,297.4	2,543.9	3,167.1	0.00	0.00	0.00
13,400.0	89.09	89.50 89.50	8,836.8 8,838.4	2,298.2	2,643.9	3,261.5	0.00	0.00	0.00
13,500.0	89.09	89.50	8,838.4	2,299.1	2,743.9	3,356.0	0.00	0.00	0.00
13,600.0	89.09	89.50	8,839.9	2,300.0	2,843.8	3,450.5	0.00	0.00	0.00
13,700.0	89.09	89.50	8,841.5	2,300.9	2,943.8	3,545.0	0.00	0.00	0.00
13,800.0	89.09	89.50	8,843.1	2,301.7	3,043.8	3,639.5	0.00	0.00	0.00
13,900.0	89.09	89.50	8,844.7	2,302.6	3,143.8	3,734.0	0.00	0.00	0.00
14,000.0	89.09	89.50	8,846.3	2,303.5	3,243.8	3,828.5	0.00	0.00	0.00
14,100.0	89.09	89.50	8,847.9	2,304.4	3,343.8	3,923.0	0.00	0.00	0.00
14,200.0	89.09	89.50	8,849.5	2,305.3	3,443.7	4,017.4	0.00	0,00	0.00
14,300.0	89.09	89.50	8,851.1	2,306.1	3,543.7	4,111.9	0.00	0.00	0.00

Database: Hobbs

Company: Mewbourne Oil Company

Project: Eddy County, New Mexico NAD 83
Site: Tough Ombres 6/5 Fed Com #715H

Well: Sec 07, T21S, R27E

**Wellbore:** BHL: 1900' FSL & 2552' FWL (Sec 5)

Design: Design #1

Local Co-ordinate Reference:

TVD Reference:
MD Reference:
North Reference:

Survey Calculation Method:

Site Tough Ombres 6/5 Fed Com #715H

Well @ 3259.0usft (Original well) Well @ 3259.0usft (Original well)

Grid

ed Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
14,400.0	89.09	89.50	8,852.7	2,307.0	3,643.7	4,206.4	0.00	0.00	0.00
14,500.0	89.09	89.50	8,854.3	2,307.9	3,743.7	4,300.9	0.00	0.00	0.00
14,600.0	89.09	89.50	8,855.9	2,308.8	3,843.7	4,395.4	0.00	0.00	0.00
14,700.0	89.09	89.50	8,857.5	2,309.6	3,943.7	4,489.9	0.00	0.00	0.00
14,756.4	89.09	89.50	8,858.4	2,310.1	4,000.1	4,543.2	0.00	0.00	0.00
	-SL & 0' FWL (S	iec 5)		,	,	,			
14,800.0	89.09	89.50	8,859.1	2,310.5	4,043.6	4,584.4	0.00	0.00	0.00
14,900.0	89.09	89.50	8,860.6	2,311.4	4,143.6	4,678.8	0.00	0.00	0.00
15,000.0	89.09	89.50	8,862.2	2,312.3	4,243.6	4,773.3	0.00	0.00	0.00
15,100.0	89.09	89.50	8,863.8	2,313.1	4,343.6	4,867.8	0.00	0.00	0.00
15,200.0	89.09	89.50	8,865.4	2,314.0	4,443.6	4,962.3	0.00	0.00	0.00
15,300.0	89.09	89.50	8,867.0	2,314.9	4,543.6	5,056.8	0.00	0.00	0.00
15,400.0	89.09	89.50	8,868.6	2,315.8	4,643.5	5,151.3	0.00	0.00	0.00
15,500.0	89.09	89.50	8,870.2	2,316.6	4,743.5	5,245.8	0.00	0.00	0.00
15,600.0	89.09	89.50	8,871.8	2,317.5	4,843.5	5,340.2	0.00	0.00	0.00
15,700.0	89.09	89.50	8,873.4	2,318.4	4,943.5	5,434.7	0.00	0.00	0.00
15,800.0	89.09	89.50	8,875.0	2,319.3	5,043.5	5,529.2	0.00	0.00	0.00
15,900.0	89.09	89.50	8,876.6	2,320.2	5,143.5	5,623.7	0.00	0.00	0.00
16,000.0	89.09	89.50	8,878.2	2,321.0	5,243.4	5,718.2	0.00	0.00	0,00
16,100.0	89.09	89.50	8,879.8	2,321.9	5,343.4	5,812.7	0.00	0.00	0,00
16,200.0	89.09	89.50	8,881.3	2,322.8	5,443.4	5,907.2	0.00	0.00	0,00
16,300.0	89.09	89.50	8,882.9	2,323.7	5,543.4	6,001.7	0.00	0.00	0,00
16,400.0	89.09	89.50	8,884.5	2,324.5	5,643.4	6,096.1	0.00	0.00	0,00
16,500.0	89.09	89.50	8,886.1	2,325.4	5,743.4	6,190.6	0.00		0.00
16,600.0 16,700.0 16,800.0 16,900.0	89.09 89.09 89.09 89.09	89.50 89.50 89.50 89.50	8,887.7 8,889.3 8,890.9 8,892.5	2,325.4 2,326.3 2,327.2 2,328.0 2,328.9	5,843.3 5,943.3 6,043.3 6,143.3	6,285.1 6,379.6 6,474.1 6,568.6	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00
17,000.0	89.09	89.50	8,894.1	2,329.8	6,243.3	6,663.1	0.00	0.00	0.00
17,100.0	89.09	89.50	8,895.7	2,330.7	6,343.3	6,757.5	0.00	0.00	0.00
17,200.0	89.09	89.50	8,897.3	2,331.5	6,443.3	6,852.0	0.00	0.00	0.00
17,308.6	89.09	89.50	8,899.0	2,332.5	6,551.8	6,954.6	0.00	0.00	0.00

Hobbs Database: Company:

Project:

Site:

Mewbourne Oil Company

Eddy County, New Mexico NAD 83 Tough Ombres 6/5 Fed Com #715H

Well: Sec 07, T21S, R27E

BHL: 1900' FSL & 2552' FWL (Sec 5) Wellbore:

Design: Design #1 Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

**Survey Calculation Method:** 

Site Tough Ombres 6/5 Fed Com #715H

Well @ 3259.0usft (Original well)

Well @ 3259.0usft (Original well)

Design Targets									
Target Name - hit/miss target - Shape	Dip Angle (°)	Dip Dir. (°)	TVD (usft)	+N/-S (usft)	+E/-W (usft)	Northing (usft)	Easting (usft)	Latitude	Longitude
SHL: 300' FNL & 1200' F - plan hits target cent - Point	0.00 er	0.00	0.0	0.0	0.0	545,929.70	572,112.70	32.5007821	-104.2335083
KOP: 1973' FSL & 473' F - plan hits target cent - Point	0,00 er	0,00	8,204.0	2,260.4	-1,672 <u>.</u> 6	548,190.10	570,440.10	32,5069997	-104,2389272
FTP/LP: 1998' FSL & 10 - plan misses target c - Point	0.00 enter by 0.1u	0.00 usft at 9655.9	8,777.1 usft MD (87	2,265.4 77.1 TVD, 226	-1,099.6 65.4 <b>N</b> , -1099.	548,195.10 6 E)	571,013.09	32,5070120	-104,2370685
PPP2: 1900' FSL & 0' F\ - plan hits target cent - Point	0.00 er	0.00	8,858.4	2,310.1	4,000.1	548,239.83	576,112.76	32.5071212	-104.2205255
BHL: 1900' FSL & 2552' - plan hits target cent - Point	0.00 er	0.00	8,899.0	2,332.5	6,551.8	548,262.20	578,664.50	32.5071750	-104.2122478



SHL: 300' FNL 1200' FWL (Sec 7) BHL: 1900' FSL 2552' FWL (Sec 5)

Operator Name:	Property Name:	Well Number
Mewbourne Oil Company	Tough Ombres 6/5 Fed Com	#715H

Viole	Off Point	(VOD)
KICK	OTT Point	(KUP)

UL	Section	Township	Range	Lot	Feet	From N/S	Feet	From E/W	County
Lot 33	1	21	26	33	1973'	FSL	473'	FEL	Eddy
Latitude			Longitude					NAD	
32.5069997				-104.23892	272			83	

First Take Point (FTP)

UL	Section	Township	Range	Lot	Feet	From N/S	Feet	From E/W	County
Lot 17	6	21	27	17	1998'	FSL	100'	FWL	Eddy
	Latitude			Longitude				NAD	
				-104.23706	85			83	

Last Take Point (LTP)

	Lust Tune 1	Ome (E11	,							
	UL	Section	Township	Range	Lot	Feet	From N/S	Feet	From E/W	County
	K	5	21	27	19	1900'	FSL	2552'	FWL	Eddy
ı	Latitude			Longitude					NAD	
ı					-104.21224	178			83	

Is this well the defining well for the Horizontal  Is this well an infill well?  N	Spacing Unit? Y	
If infill is yes please provide API if available, C Spacing Unit.	Operator Name and well number for Defining well for Horizontal	
API#		
Operator Name:	Property Name:	Well Number

# PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

**OPERATOR'S NAME:** MEWBOURNE OIL COMPANY

**WELL NAME & NO.:** TOUGH OMBRES 6/5 FED COM 715H

**APD ID:** 10400097990

**LOCATION:** Section 7, T21S, R27E. NMP.

**COUNTY:** Eddy County, New Mexico

COA

H <sub>2</sub> S	0	No	•	Yes
Potash /	None	O Secretary	O R-111-Q	☐ Open Annulus
WIPP				□ WIPP
Cave / Karst	O Low	<ul><li>Medium</li></ul>	• High	<ul><li>Critical</li></ul>
Wellhead	Conventional	<ul><li>Multibowl</li></ul>	O Both	<ul><li>Diverter</li></ul>
Cementing	☐ Primary Squeeze	☐ Cont. Squeeze	☐ EchoMeter	DV Tool
Special Req	Capitan Reef	☐ Water Disposal	✓ COM	☐ Unit
Waste Prev.	Self-Certification	O Waste Min. Plan	• APD Submitted p	prior to 06/10/2024
Additional	✓ Flex Hose	☐ Casing Clearance	☐ Pilot Hole	Break Testing
Language	Four-String	Offline Cementing	☐ Fluid-Filled	

### A. HYDROGEN SULFIDE

A Hydrogen Sulfide (H<sub>2</sub>S) Drilling Plan shall be activated **AT SPUD**. As a result, the Hydrogen Sulfide area must meet **43 CFR 3176** requirements, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, please provide measured values and formations to the BLM.

### **B. CASING DESIGN**

### **Primary Casing Program**

- 1. The 18-5/8-inch surface casing shall be set at approximately 275 ft. (a minimum of 70 feet (Eddy County) into the Rustler Anhydrite and above the salt) and cemented to the surface. If salt is encountered set casing at least 25 ft. above the salt.
  - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after

- completing the cement job.
- b. Wait on cement (WOC) time for a primary cement job will be a minimum of **8** hours or **500** psi compressive strength, whichever is greater. (This is to include the lead cement)
- c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 psi compressive strength, whichever is greater.
- d. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 2. The 13-3/8 inch 1<sup>st</sup> intermediate casing shall be set in a competent bed at approximately 950 ft. The minimum required fill of cement behind the 13-3/8 inch intermediate casing is:

Option 1 (Single Stage): Cement to surface. If cement does not circulate, see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to Cave/Karst and Capitan reef.

**Option 2 (Two-stage):** Operator has proposed a DV tool, the depth may be adjusted as long as the cement is changed proportionally. The DV tool may be cancelled if cement circulates to surface on the first stage.

- a. First stage to DV tool: Cement to circulate. If cement does not circulate off the DV tool, contact the appropriate BLM office before proceeding with second stage cement job.
- b. Second stage above DV tool: Cement to surface. If cement does not circulate, contact the appropriate BLM office. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to Cave/Karst and Capitan reef.
- ❖ In <u>Capitan Reef Areas</u> if cement does not circulate to surface on the first two casing strings, the cement on the 3<sup>rd</sup> casing string must come to surface.
- ❖ In <u>High Cave/Karst Areas</u> if cement does not circulate to surface on the first two casing strings, the cement on the 3<sup>rd</sup> casing string must come to surface.
- ❖ Special Capitan Reef requirements. If lost circulation (50% or greater) occurs below the Base of the Salt, the operator shall do the following:
  (Use this for 3 string wells in the Capitan Reef, if 4 string well ensure FW based mud used across the Capitan interval)
  - Switch to freshwater mud to protect the Capitan Reef and use freshwater mud until setting the intermediate casing. The appropriate BLM office is to be notified for a PET to witness the switch to fresh water.
  - Daily drilling reports from the Base of the Salt to the setting of the intermediate casing are to be submitted to the BLM CFO engineering staff via e-mail by

0800 hours each morning. Any lost circulation encountered is to be recorded on these drilling reports. The daily drilling report should show mud volume per shift/tour. Failure to submit these reports will result in an Incidence of Non-Compliance being issued for failure to comply with the Conditions of Approval. If not already planned, the operator shall run a caliper survey for the intermediate well bore and submit to the appropriate BLM office.

**Note:** The 2<sup>nd</sup> intermediate casing set depth was adjusted per BLM geologist's recommendation.

- 3. The 9-5/8 inch 2<sup>nd</sup> intermediate casing shall be set at approximately 2,300 ft. in the base of Capitan reef. The minimum required fill of cement behind the 9-5/8 inch intermediate casing is:
  - Option 1 (Single Stage): Cement should tie-back at least 200 feet into previous casing string or 50 ft. above Capitan reef top, whichever is greater. Operator shall provide method of verification. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to Cave/Karst and Capitan reef.
  - <u>Option 2 (Two-stage):</u> Operator has proposed a DV tool, the depth may be adjusted as long as the cement is changed proportionally. The DV tool may be cancelled if cement circulates to surface on the first stage.
    - a. **First stage to DV tool:** Cement to circulate. If cement does not circulate off the DV tool, contact the appropriate BLM office before proceeding with second stage cement job.
    - b. Second stage above DV tool: Cement should tie-back at least 200 feet into previous casing string or 50 ft. above Capitan reef top, whichever is greater. Operator shall provide method of verification. If cement does not circulate, contact the appropriate BLM office. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to Cave/Karst and Capitan reef.
- **4.** Operator has proposed to set **7 in.** production casing at approximately **8,756 ft.** (8,204 ft. TVD). The minimum required fill of cement behind the **7 in.** production casing is:
  - Option 1 (Single Stage): Cement should tie-back at least 200 feet into previous casing string. Operator shall provide method of verification. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to Cave/Karst and Capitan reef.
  - **Option 2 (Two-stage):** Operator has proposed a DV tool, the depth may be adjusted as long as the cement is changed proportionally. The DV tool may be cancelled if cement circulates to surface on the first stage.
    - a. **First stage to DV tool:** Cement to circulate. If cement does not circulate off the DV tool, contact the appropriate BLM office before proceeding with second stage cement job.

- b. Second stage above DV tool: Cement should tie-back at least 200 feet into previous casing string. Operator shall provide method of verification. If cement does not circulate, contact the appropriate BLM office. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to Cave/Karst and Capitan reef.
- 5. The minimum required fill of cement behind the 4-1/2 in. production liner is:
  - Cement should tie-back at least 100 feet into previous casing string. Operator shall provide method of verification.

### **Alternate Casing Program**

- 1. The 18-5/8-inch surface casing shall be set at approximately 275 ft. (a minimum of 70 feet (Eddy County) into the Rustler Anhydrite and above the salt) and cemented to the surface. If salt is encountered set casing at least 25 ft. above the salt.
  - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
  - b. Wait on cement (WOC) time for a primary cement job will be a minimum of <u>8</u> hours or 500 psi compressive strength, whichever is greater. (This is to include the lead cement)
  - c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 psi compressive strength, whichever is greater.
  - d. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 2. The 13-3/8 inch 1<sup>st</sup> intermediate casing shall be set in a competent bed at approximately 950 ft. The minimum required fill of cement behind the 13-3/8 inch intermediate casing is:
  - <u>Option 1 (Single Stage):</u> Cement to surface. If cement does not circulate, see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to Cave/Karst and Capitan reef.
  - <u>Option 2 (Two-stage):</u> Operator has proposed a DV tool, the depth may be adjusted as long as the cement is changed proportionally. The DV tool may be cancelled if cement circulates to surface on the first stage.
    - a. First stage to DV tool: Cement to circulate. If cement does not circulate off the DV tool, contact the appropriate BLM office before proceeding with second stage cement job.
    - b. Second stage above DV tool: Cement to surface. If cement does not circulate, contact the appropriate BLM office. Wait on cement (WOC) time

for a primary cement job is to include the lead cement slurry due to Cave/Karst and Capitan reef.

- ❖ In <u>Capitan Reef Areas</u> if cement does not circulate to surface on the first two casing strings, the cement on the 3<sup>rd</sup> casing string must come to surface.
- ❖ In <u>High Cave/Karst Areas</u> if cement does not circulate to surface on the first two casing strings, the cement on the 3<sup>rd</sup> casing string must come to surface.
- ❖ Special Capitan Reef requirements. If lost circulation (50% or greater) occurs below the Base of the Salt, the operator shall do the following:
   (Use this for 3 string wells in the Capitan Reef, if 4 string well ensure FW based mud used across the Capitan interval)
  - Switch to freshwater mud to protect the Capitan Reef and use freshwater mud until setting the intermediate casing. The appropriate BLM office is to be notified for a PET to witness the switch to fresh water.
  - Daily drilling reports from the Base of the Salt to the setting of the intermediate casing are to be submitted to the BLM CFO engineering staff via e-mail by 0800 hours each morning. Any lost circulation encountered is to be recorded on these drilling reports. The daily drilling report should show mud volume per shift/tour. Failure to submit these reports will result in an Incidence of Non-Compliance being issued for failure to comply with the Conditions of Approval. If not already planned, the operator shall run a caliper survey for the intermediate well bore and submit to the appropriate BLM office.

**Note:** The 2<sup>nd</sup> intermediate casing set depth was adjusted per BLM geologist's recommendation.

- 3. The 9-5/8 inch 2<sup>nd</sup> intermediate casing shall be set at approximately 2,300 ft. in the base of Capitan reef. The minimum required fill of cement behind the 9-5/8 inch intermediate casing is:
  - Option 1 (Single Stage): Cement should tie-back at least 200 feet into previous casing string or 50 ft. above Capitan reef top, whichever is greater. Operator shall provide method of verification. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to Cave/Karst and Capitan reef.
  - <u>Option 2 (Two-stage):</u> Operator has proposed a DV tool, the depth may be adjusted as long as the cement is changed proportionally. The DV tool may be cancelled if cement circulates to surface on the first stage.
    - a. **First stage to DV tool:** Cement to circulate. If cement does not circulate off the DV tool, contact the appropriate BLM office before proceeding with second stage cement job.

- b. Second stage above DV tool: Cement should tie-back at least 200 feet into previous casing string or 50 ft. above Capitan reef top, whichever is greater. Operator shall provide method of verification. If cement does not circulate, contact the appropriate BLM office. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to Cave/Karst and Capitan reef.
- **4.** Operator has proposed to set **7 in.** production casing at approximately **9,656 ft.** (8,777 ft. TVD). The minimum required fill of cement behind the **7 in.** production casing is:

<u>Option 1 (Single Stage):</u> Cement should tie-back at least 200 feet into previous casing string. Operator shall provide method of verification.

<u>Option 2 (Two-stage):</u> Operator has proposed a DV tool, the depth may be adjusted as long as the cement is changed proportionally. The DV tool may be cancelled if cement circulates to surface on the first stage.

- c. **First stage to DV tool:** Cement to circulate. If cement does not circulate off the DV tool, contact the appropriate BLM office before proceeding with second stage cement job.
- d. **Second stage above DV tool:** Cement should tie-back **at least 200 feet** into previous casing string. Operator shall provide method of verification. If cement does not circulate, contact the appropriate BLM office.
- 5. The minimum required fill of cement behind the 4-1/2 in. production liner is:
  - Cement should tie-back at least 100 feet into previous casing string. Operator shall provide method of verification.

**Note:** Excess cement is below the BLM's recommendation of 25%. More cement might be needed.

### **Offline Cementing**

Operator has been (**Approved**) to pump the proposed cement program offline in the **Surface and intermediate(s) intervals**. Offline cementing should commence within 24 hours of landing the casing for the interval. Notify the BLM 4hrs prior to cementing offline at **Eddy County:** 575-361-2822.

### C. PRESSURE CONTROL

- 1. Variance approved to use **flex line** from BOP to choke manifold. Manufacturer's specification to be readily available. No external damage to flex line. Flex line to be installed as straight as possible (no hard bends).
- 2. Operator has proposed a **multi-bowl wellhead** assembly. This assembly will only be tested when installed on the surface casing. Minimum working pressure of the blowout

preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be **5000 (5M)** psi. The BOP/BOPE and annular preventer shall be pressure-tested in accordance with **title 43 CFR 3172 and API Standard 53.** 

- a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
- b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
- c. Manufacturer representative shall install the test plug for the initial BOP test.
- d. If the cement does not circulate and one-inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- e. Whenever any seal subject to test pressure is broken, all the tests in the title 43 CFR 3172.6(b)(9) must be followed.

### **BOPE Break Testing Variance (Approved)**

(Note: For a minimum 5M BOPE or less (Utilizing a 10M BOPE system)

- BOPE Break Testing is ONLY permitted for 5M BOPE or less. (Annular preventer must be tested to a minimum of 70% of BOPE working pressure and shall be higher than the MASP)
- BOPE Break Testing is NOT permitted to drilling the production hole section.
- Variance only pertains to the intermediate hole-sections and no deeper than the Bone Springs formation.
- While in transfer between wells, the BOPE shall be secured by the hydraulic carrier or cradle.
- Any well control event while drilling require notification to the BLM Petroleum Engineer (575-706-2779) prior to the commencement of any BOPE Break Testing operations.
- A full BOPE test is required prior to drilling the first deep intermediate hole section. If any subsequent hole interval is deeper than the first, a full BOPE test will be required. (200' TVD tolerance between intermediate shoes is allowable).
- The BLM is to be contacted (575-361-2822 Eddy County) 4 hours prior to BOPE tests
- As a minimum, a full BOPE test shall be performed at 21-day intervals.
- In the event any repairs or replacement of the BOPE is required, the BOPE shall test as per 43 CFR part 3170 Subpart 3172.
- If in the event break testing is not utilized, then a full BOPE test would be conducted.

### D. SPECIAL REQUIREMENT (S)

### **Communitization Agreement**

• The operator will submit a Communitization Agreement to the Santa Fe Office, 301 Dinosaur Trail Santa Fe, New Mexico 87508, at least 90 days before the anticipated

date of first production from a well subject to a spacing order issued by the New Mexico Oil Conservation Division. The Communitization Agreement will include the signatures of all working interest owners in all Federal and Indian leases subject to the Communitization Agreement (i.e., operating rights owners and lessees of record), or certification that the operator has obtained the written signatures of all such owners and will make those signatures available to the BLM immediately upon request.

- If the operator does not comply with this condition of approval, the BLM may take enforcement actions that include, but are not limited to, those specified in 43 CFR 3163.1.
- In addition, the well sign shall include the surface and bottom hole lease numbers. When the Communitization Agreement number is known, it shall also be on the sign.

### **GENERAL REQUIREMENTS**

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)

### **Contact Eddy County Petroleum Engineering Inspection Staff:**

Email or call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220; **BLM\_NM\_CFO\_DrillingNotifications@BLM.GOV**; (575) 361-2822.

- 1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.
  - a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after installing and testing the wellhead, by installing a blind flange of like pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).
  - b. When the operator proposes to set surface casing with Spudder Rig
    - i. Notify the BLM when moving in and removing the Spudder Rig.
    - ii. Notify the BLM when moving in the 2<sup>nd</sup> Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.
    - iii. BOP/BOPE test to be conducted per **43 CFR 3172** as soon as 2<sup>nd</sup> Rig is rigged up on well.
- 2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all

- times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the doghouse or stairway area.
- 3. For intervals in which cement to surface is required, cement to surface should be verified with a visual check and density or pH check to differentiate cement from spacer and drilling mud. The results should be documented in the driller's log and daily reports.

#### A. CASING

- 1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.
- 2. Wait on cement (WOC) for Potash Areas: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends of both lead and tail cement, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 3. Wait on cement (WOC) for Water Basin: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 4. Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.
- 5. No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.
- **6.** On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the

- shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.
- 7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.
- **8.** Whenever a casing string is cemented in the R-111-Q potash area, the NMOCD requirements shall be followed.

### **B. PRESSURE CONTROL**

- 1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in 43 CFR 3172.
- 2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor.
- **3.** 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.
- **4.** If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:
  - i. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
  - ii. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
  - iii. Manufacturer representative shall install the test plug for the initial BOP test.
  - iv. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR 3172.6(b)(9) must be followed.
  - v. If the cement does not circulate and one-inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.

- **5.** The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
  - i. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead cement), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).
  - ii. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the cement plug. The BOPE test can be initiated after bumping the cement plug with the casing valve open. (Only applies to single stage cement jobs, prior to the cement setting up.)
  - iii. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer and can be initiated immediately with the casing valve open. The operator also has the option of utilizing an independent tester to test without a plug (i.e. against the casing) pursuant to **43 CFR 3172** with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for 8 hours or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).
  - iv. The test shall be run on a 5000-psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one-hour chart. A circular chart shall have a maximum 2-hour clock. If a twelve hour or twenty-four-hour chart is used, tester shall make a notation that it is run with a two hour clock.
  - v. The results of the test shall be reported to the appropriate BLM office.
  - vi. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
  - vii. The BOP/BOPE test shall include a low-pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.

viii. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per 43 CFR 3172.

### C. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

### D. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area. Porto-johns and trash containers will be on-location during fracturing operations or any other crewintensive operations.

SA 09/27/2024

### Hydrogen Sulfide Drilling Operations Plan Mewbourne Oil Company

### 1. General Requirements

Rule 118 does not apply to this well because MOC has researched this area and no high concentrations of H2S were found. MOC will have on location and working all H2S safety equipment before the Delaware formation for purposes of safety and insurance requirements.

### 2. Hydrogen Sulfide Training

All personnel, whether regularly assigned, contracted, or employed on an unscheduled basis, will have received training from a qualified instructor in the following areas prior to entering the drilling pad area of the well:

- 1. The hazards and characteristics of hydrogen sulfide gas.
- 2. The proper use of personal protective equipment and life support systems.
- 3. The proper use of hydrogen sulfide detectors, alarms, warning systems, briefing areas, evacuation procedures.
- 4. The proper techniques for first aid and rescue operations.

Additionally, supervisory personnel will be trained in the following areas:

- The effects of hydrogen sulfide on metal components. If high tensile tubular systems are utilized, supervisory personnel will be trained in their special maintenance requirements.
- 2 Corrective action and shut in procedures, blowout prevention, and well control procedures while drilling a well.
- The contents of the Hydrogen Sulfide Drilling Operations Plan.

There will be an initial training session prior to encountering a know hydrogen sulfide source. The initial training session shall include a review of the site specific Hydrogen Sulfide Drilling Operations Plan.

### 3. Hydrogen Sulfide Safety Equipment and Systems

All hydrogen sulfide safety equipment and systems will be installed, tested, and operational prior to drilling below the 9 5/8" intermediate casing.

### 1. Well Control Equipment

- A. Choke manifold with minimum of one adjustable choke/remote choke.
- B. Blowout preventers equipped with blind rams and pipe rams to accommodate all pipe sizes with properly sized closing unit
- C. Auxiliary equipment including annular type blowout preventer.
- 2. <u>Protective Equipment for Essential Personnel</u>

Thirty minute self contained work unit located in the dog house and at briefing areas.

Additionally: If H2S is encountered in concentrations less than 10 ppm, fans will be placed in work areas to prevent the accumulation of hazardous amounts of poisonous gas. If higher concentrations of H2S are detected the well will be shut in and a rotating head, mud/gas separator, remote choke and flare line with igniter will be installed.

### 3. <u>Hydrogen Sulfide Protection and Monitoring Equipment</u>

Two portable hydrogen sulfide monitors positioned on location for optimum coverage and detection. The units shall have audible sirens to notify personnel when hydrogen sulfide levels exceed 20 PPM.

### 4. Visual Warning Systems

- A. Wind direction indicators as indicated on the wellsite diagram.
- B. Caution signs shall be posted on roads providing access to location. Signs shall be painted a high visibility color with lettering of sufficient size to be readable at reasonable distances from potentially contaminated areas.

### 4. Mud Program

The mud program has been designed to minimize the amount of hydrogen sulfide entrained in the mud system. Proper mud weight, safe drilling practices, and the use of hydrogen sulfide scavengers will minimize hazards while drilling the well.

### 5. Metallurgy

All tubular systems, wellheads, blowout preventers, drilling spools, kill lines, choke manifolds, and valves shall be suitable for service in a hydrogen sulfide environment when chemically treated.

### 6. Communications

State & County Officials phone numbers are posted on rig floor and supervisors trailer. Communications in company vehicles and toolpushers are either two way radios or cellular phones.

### 7. Well Testing

Drill stem testing is not an anticipated requirement for evaluation of this well. If a drill stem test is required, it will be conducted with a minimum number of personnel in the immediate vicinity. The test will be conducted during daylight hours only.

### 8. Emergency Phone Numbers

<b>Eddy County Sheriff's Office</b>	911 or 575-887-7551
Ambulance Service	911 or 575-885-2111
Carlsbad Fire Dept	911 or 575-885-2111
Loco Hills Volunteer Fire Dept.	911 or 575-677-3266
<b>Closest Medical Facility - Columbia Medical Center</b>	of Carlsbad 575-492-5000

Mewbourne Oil Company	Hobbs District Office Fax 2 <sup>nd</sup> Fax	575-393-5905 575-397-6252 575-393-7259
District Manager	Robin Terrell	575-390-4816
<b>Drilling Superintendent</b>	Frosty Lathan	575-390-4103
	<b>Bradley Bishop</b>	575-390-6838
<b>Drilling Foreman</b>	Wesley Noseff	575-441-0729

**Operator Name: MEWBOURNE OIL COMPANY** 

Well Name: TOUGH OMBRES 6/5 FED COM Well Number: 715H

Waste type: GARBAGE

Waste content description: Garbage & trash from all drilling & completion procedures

Amount of waste: 1500 pounds

Waste disposal frequency: One Time Only

Safe containment description: Enclosed trash trailers

Safe containmant attachment:

Waste disposal type: HAUL TO COMMERCIAL Disposal location ownership: PRIVATE

**FACILITY** 

Disposal type description:

Disposal location description: County of Eddy waste management

### **Reserve Pit**

Reserve Pit being used? NO

Temporary disposal of produced water into reserve pit? NO

Reserve pit length (ft.) Reserve pit width (ft.)

Reserve pit depth (ft.) Reserve pit volume (cu. yd.)

Is at least 50% of the reserve pit in cut?

Reserve pit liner

Reserve pit liner specifications and installation description

### **Cuttings Area**

Cuttings Area being used? NO

Are you storing cuttings on location? Y

**Description of cuttings location** Drill cuttings will be properly contained in steel tanks (20 yard roll off bins.) and taken to an NMOCD approved disposal facility listed below. After drilling and completion operations, trash, chemicals, salts, frac sand and other waste material will be removed and disposed of properly at the said facilities. NMOCD approved waste disposal locations are CRI or Lea Land, both facilities are located on HWY 62/180, Sec. 27 T20S R32E.

Cuttings area length (ft.) Cuttings area width (ft.)

Cuttings area depth (ft.) Cuttings area volume (cu. yd.)

Is at least 50% of the cuttings area in cut?

**WCuttings** area liner

Cuttings area liner specifications and installation description

**Operator Name: MEWBOURNE OIL COMPANY** 

Well Name: TOUGH OMBRES 6/5 FED COM Well Number: 715H

### **Section 8 - Ancillary**

Are you requesting any Ancillary Facilities?: N

**Ancillary Facilities** 

Comments:

**Section 9 - Well Site** 

Well Site Layout Diagram:

TOUGH\_OMBRES\_6\_5\_FED\_COM\_715H\_WellSiteLayout\_20240410102744.pdf

Comments: NONE

**Section 10 - Plans for Surface Reclamation** 

Type of disturbance: New Surface Disturbance Multiple Well Pad Name: Tough Ombres 6/5 715 & 716

Multiple Well Pad Number: 2

Recontouring

**Drainage/Erosion control construction:** None required **Drainage/Erosion control reclamation:** None required

Well pad proposed disturbance Well pad interim reclamation (acres): Well pad long term disturbance

(acres): 5.5 0.8 (acres): 5.5

Road proposed disturbance (acres): Road interim reclamation (acres): 0 Road long term disturbance (acres): 0

0.101

Powerline proposed disturbance Powerline interim reclamation (acres): Powerline long term disturbance

(acres): 0 (acres): 0

Pipeline proposed disturbance Pipeline interim reclamation (acres): 0 Pipeline long term disturbance

(acres): 0

Other proposed disturbance (acres): 0 Other interim reclamation (acres): 0 Other long term disturbance (acres): 0

Total proposed disturbance: 5.601 Total interim reclamation: 0.8 Total long term disturbance: 5.5

**Disturbance Comments:** The length of the pipeline is unknown. A sundry notice will be filed for approval of said pipeline.

**Reconstruction method:** Remove caliche, redistribute topsoil over reclaimed area & reseed.

**Topsoil redistribution:** Use backhoe/loader to spread material.

Soil treatment: None

Existing Vegetation at the well pad: Various brush & grasses.

**Existing Vegetation at the well pad** 

District I
1625 N. French Dr., Hobbs, NM 88240
Phone: (575) 393-6161 Fax: (575) 393-0720 District II

811 S. First St., Artesia, NM 88210 Phone:(575) 748-1283 Fax:(575) 748-9720 District III

1000 Rio Brazos Rd., Aztec, NM 87410 Phone:(505) 334-6178 Fax:(505) 334-6170

1220 S. St Francis Dr., Santa Fe, NM 87505 Phone:(505) 476-3470 Fax:(505) 476-3462

**State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division** 1220 S. St Francis Dr. **Santa Fe, NM 87505** 

CONDITIONS

Action 393319

### **CONDITIONS**

Operator:	OGRID:
MEWBOURNE OIL CO	14744
P.O. Box 5270	Action Number:
Hobbs, NM 88241	393319
	Action Type:
	[C-101] BLM - Federal/Indian Land Lease (Form 3160-3)

#### CONDITIONS

Created By	Condition	Condition Date
ward.rikala	Notify OCD 24 hours prior to casing & cement	10/21/2024
ward.rikala	Will require a File As Drilled C-102 and a Directional Survey with the C-104	10/21/2024
ward.rikala	Once the well is spud, to prevent ground water contamination through whole or partial conduits from the surface, the operator shall drill without interruption through the fresh water zone or zones and shall immediately set in cement the water protection string	10/21/2024
ward.rikala	Cement is required to circulate on both surface and intermediate1 strings of casing	10/21/2024
ward.rikala	If cement does not circulate on any string, a CBL is required for that string of casing	10/21/2024
ward.rikala	Oil base muds are not to be used until fresh water zones are cased and cemented providing isolation from the oil or diesel. This includes synthetic oils. Oil based mud, drilling fluids and solids must be contained in a steel closed loop system	10/21/2024
ward.rikala	This well is within the Capitan Reef. The 1st intermediate string shall be sat and cemented immediately above the top of the Capitan Reef. The 2nd intermediate string shall be sat and cemented immediately below the base of the Capitan Reef.	10/21/2024