U.S. Department of the Interior
BUREAU OF LAND MANAGEMENT

# Sundry Print Report

04/30/2025

**Well Name:** TUNA NUT 24-13 FEDERAL COM

**Well Location:** T22S / R32E / SEC 24 / SESW / 32.370807 / -103.632289

**County or Parish/State:** LEA / NM

**Well Number:** 23H

**Type of Well:** OIL WELL

**Allottee or Tribe Name:**

**Lease Number:** NMNM81633

**Unit or CA Name:**

**Unit or CA Number:**

**US Well Number:** 3002554090

**Operator:** OXY USA INCORPORATED

## Notice of Intent

**Sundry ID:** 2843838

**Type of Submission:** Notice of Intent

**Type of Action:** APD Change

**Date Sundry Submitted:** 03/27/2025

**Time Sundry Submitted:** 08:52

**Date proposed operation will begin:** 07/01/2025

**Procedure Description:** OXY USA Inc., respectfully requests to amend the subject AAPD to revise the SHL, BHL, HSU, TVD and Drill Plan. Old SHL: 275' FSL 1425' FWL New SHL: 390' FSL 1155' FWL Old BHL: 20' FNL 2250' FWL New BHL: 20' FNL 1400' FWL Old HSU: 640 acres New HSU: 1280 acres Old TVD: 10933' New TVD: 10874' *THERE IS NO ADDITIONAL SURFACE DISTURBANCE RELATED TO THIS SUNDRY" Attached is the updated C102, drill plan, contingency plan, directional, Blanket Design and APD Change Worksheet.

## NOI Attachments

**Procedure Description**

TUNANUT24_13FEDCOM23H_API_BTC_SC_10.750in_45.50ppf_L80IC_20250327085217.pdf

Blanket_Design_B_Pad_Review_Document_REDTNK_T22SR32E_24_01_20250327085209.pdf

TUNANUT24_13FEDCOM23H_DrillPlan_4S_20250327085200.pdf

TUNANUT24_13FEDCOM23H_VAM_SPRINT_SF_5.5in_20ppf_P110RY_20250327085142.pdf

TUNANUT24_13FEDCOM23H_13inADAPT_4S_10x15_20250327085135.pdf

TUNANUT24_13FEDCOM23H_DirectPlan_20250327085125.pdf

Blanket_Design_A_Pad_Review_Document_REDTNK_T22SR32E_24_01_20250327085116.pdf

Combined_Blanket_Design___A1___A2__B___OXY___3S_Slim_v7.2_and_4S_Slim_Contingency_v3.2_20250327085107.pdf

**Well Name:** TUNA NUT 24-13 FEDERAL COM

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**County or Parish/State:** LEA / NM

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**Operator:** OXY USA INCORPORATED

TUNANUT24_13FEDCOM23H_DrillPlan_20250327085058.pdf

TUNANUT24_13FEDCOM23H_C102_20250327085049.pdf

TUNANUT24_13FEDCOM23H_APDCHGSUNDRYWORKSHEET_20250327085036.pdf

## Conditions of Approval

**Additional**

TUNA_NUT_24_13_FED_COM_23H___SUNDRY_COA_20250410112646.pdf

## Operator

*I certify that the foregoing is true and correct. Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction. Electronic submission of Sundry Notices through this system satisfies regulations requiring a*

**Operator Electronic Signature:** MELISSA GUIDRY

**Signed on:** MAR 27, 2025 08:52 AM

**Name:** OXY USA INCORPORATED

**Title:** Advisor Regulatory Sr.

**Street Address:** 5 GREENWAY PLAZA SUITE 110

**City:** HOUSTON **State:** TX

**Phone:** (713) 497-2481

**Email address:** MELISSA_GUIDRY@OXY.COM

## Field

**Representative Name:**

**Street Address:**

**City:** **State:** **Zip:**

**Phone:**

**Email address:**

## BLM Point of Contact

**BLM POC Name:** CHRISTOPHER WALLS

**BLM POC Title:** Petroleum Engineer

**BLM POC Phone:** 5752342234

**BLM POC Email Address:** cwalls@blm.gov

**Disposition:** Approved

**Disposition Date:** 04/30/2025

**Signature:** Chris Walls

Form 3160-5
(June 2019)

UNITED STATES
DEPARTMENT OF THE INTERIOR
BUREAU OF LAND MANAGEMENT

FORM APPROVED
OMB No. 1004-0137
Expires: October 31, 2021

**SUNDRY NOTICES AND REPORTS ON WELLS**

***Do not use this form for proposals to drill or to re-enter an abandoned well. Use Form 3160-3 (APD) for such proposals.***

***SUBMIT IN TRIPLICATE*** *- Other instructions on page 2*

5. Lease Serial No. NMNM81633

6. If Indian, Allottee or Tribe Name

7. If Unit of CA/Agreement, Name and/or No.

1. Type of Well
☑ Oil Well ☐ Gas Well ☐ Other

8. Well Name and No.
TUNA NUT 24-13 FEDERAL COM/23H

2. Name of Operator OXY USA INCORPORATED

9. API Well No. 3002554090

3a. Address P.O. BOX 1002, TUPMAN, CA 93276-1002

3b. Phone No. *(include area code)* (661) 763-6046

10. Field and Pool or Exploratory Area
RED TANK/BONE SPRING

4. Location of Well *(Footage, Sec., T.,R.,M., or Survey Description)*
SEC 24/T22S/R32E/NMP

11. Country or Parish, State
LEA/NM

12. CHECK THE APPROPRIATE BOX(ES) TO INDICATE NATURE OF NOTICE, REPORT OR OTHER DATA

| TYPE OF SUBMISSION | TYPE OF ACTION | | | |
|---|---|---|---|---|
| ☑ Notice of Intent | ☐ Acidize | ☐ Deepen | ☐ Production (Start/Resume) | ☐ Water Shut-Off |
| ☐ Subsequent Report | ☐ Alter Casing | ☐ Hydraulic Fracturing | ☐ Reclamation | ☐ Well Integrity |
| ☐ Final Abandonment Notice | ☐ Casing Repair | ☐ New Construction | ☐ Recomplete | ☐ Other |
| | ☑ Change Plans | ☐ Plug and Abandon | ☐ Temporarily Abandon | |
| | ☐ Convert to Injection | ☐ Plug Back | ☐ Water Disposal | |

13. Describe Proposed or Completed Operation: Clearly state all pertinent details, including estimated starting date of any proposed work and approximate duration thereof. If the proposal is to deepen directionally or recomplete horizontally, give subsurface locations and measured and true vertical depths of all pertinent markers and zones. Attach the Bond under which the work will be perfonned or provide the Bond No. on file with BLM/BIA. Required subsequent reports must be filed within 30 days following completion of the involved operations. If the operation results in a multiple completion or recompletion in a new interval, a Form 3160-4 must be filed once testing has been completed. Final Abandonment Notices must be filed only after all requirements, including reclamation, have been completed and the operator has detennined that the site is ready for final inspection.)

OXY USA Inc., respectfully requests to amend the subject AAPD to revise the SHL, BHL, HSU, TVD and Drill Plan.

Old SHL: 275' FSL 1425' FWL
New SHL: 390' FSL 1155' FWL

Old BHL: 20' FNL 2250' FWL
New BHL: 20' FNL 1400' FWL

Old HSU: 640 acres
New HSU: 1280 acres

Old TVD: 10933'

Continued on page 3 additional information

14. I hereby certify that the foregoing is true and correct. Name *(Printed/Typed)*
MELISSA GUIDRY / Ph: (713) 497-2481

Title Advisor Regulatory Sr.

Signature (Electronic Submission)

Date 03/27/2025

**THE SPACE FOR FEDERAL OR STATE OFICE USE**

Approved by
CHRISTOPHER WALLS / Ph: (575) 234-2234 / Approved

Title Petroleum Engineer

Date 04/30/2025

Conditions of approval, if any, are attached. Approval of this notice does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon.

Office CARLSBAD

Title 18 U.S.C Section 1001 and Title 43 U.S.C Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

(Instructions on page 2)

## GENERAL INSTRUCTIONS

This form is designed for submitting proposals to perform certain well operations and reports of such operations when completed as indicated on Federal and Indian lands pursuant to applicable Federal law and regulations. Any necessary special instructions concerning the use of this form and the number of copies to be submitted, particularly with regard to local area or regional procedures and practices, are either shown below, will be issued by or may be obtained from the local Federal office.

## SPECIFIC INSTRUCTIONS

*Item 4* - Locations on Federal or Indian land should be described in accordance with Federal requirements. Consult the local Federal office for specific instructions.

*Item 13:* Proposals to abandon a well and subsequent reports of abandonment should include such special information as is required by the local Federal office. In addition, such proposals and reports should include reasons for the abandonment; data on any former or present productive zones or other zones with present significant fluid contents not sealed off by cement or otherwise; depths (top and bottom) and method of placement of cement plugs; mud or other material placed below, between and above plugs; amount, size, method of parting of any casing, liner or tubing pulled and the depth to the top of any tubing left in the hole; method of closing top of well and date well site conditioned for final inspection looking for approval of the abandonment. If the proposal will involve **hydraulic fracturing operations**, you must comply with 43 CFR 3162.3-3, including providing information about the protection of usable water. Operators should provide the best available information about all formations containing water and their depths. This information could include data and interpretation of resistivity logs run on nearby wells. Information may also be obtained from state or tribal regulatory agencies and from local BLM offices.

## NOTICES

The privacy Act of 1974 and the regulation in 43 CFR 2.48(d) provide that you be furnished the following information in connection with information required by this application.
AUTHORITY: 30 U.S.C. 181 et seq., 351 et seq., 25 U.S.C. 396; 43 CFR 3160.
PRINCIPAL PURPOSE: The information is used to: (1) Evaluate, when appropriate, approve applications, and report completion of subsequent well operations, on a Federal or Indian lease; and (2) document for administrative use, information for the management, disposal and use of National Resource lands and resources, such as: (a) evaluating the equipment and procedures to be used during a proposed subsequent well operation and reviewing the completed well operations for compliance with the approved plan; (b) requesting and granting approval to perform those actions covered by 43 CFR 3162.3-2, 3162.3-3, and 3162.3-4; (c) reporting the beginning or resumption of production, as required by 43 CFR 3162.4-1(c)and (d) analyzing future applications to drill or modify operations in light of data obtained and methods used.
ROUTINE USES: Information from the record and/or the record will be transferred to appropriate Federal, State, local or foreign agencies, when relevant to civil, criminal or regulatory investigations or prosecutions in connection with congressional inquiries or to consumer reporting agencies to facilitate collection of debts owed the Government.
EFFECT OF NOT PROVIDING THE INFORMATION: Filing of this notice and report and disclosure of the information is mandatory for those subsequent well operations specified in 43 CFR 3162.3-2, 3162.3-3, 3162.3-4.

The Paperwork Reduction Act of 1995 requires us to inform you that:
The BLM collects this information to evaluate proposed and/or completed subsequent well operations on Federal or Indian oil and gas leases.
Response to this request is mandatory.
The BLM would like you to know that you do not have to respond to this or any other Federal agency-sponsored information collection unless it displays a currently valid OMB control number.

**BURDEN HOURS STATEMENT:** Public reporting burden for this form is estimated to average 8 hours per response, including the time for reviewing instructions, gathering and maintaining data, and completing and reviewing the form. Direct comments regarding the burden estimate or any other aspect ofthis form to U.S. Department ofthe Interior, Bureau ofLand Management (1004-0137), Bureau Information Collection Clearance Officer (WO-630), 1849 C St., N.W., Mail Stop 401 LS, Washington, D.C. 20240

## Additional Information

### Additional Remarks

New TVD: 10874'

*THERE IS NO ADDITIONAL SURFACE DISTURBANCE RELATED TO THIS SUNDRY"

Attached is the updated C102, drill plan, contingency plan, directional, Blanket Design and APD Change Worksheet.

### Location of Well

0. SHL: SESW / 275 FSL / 1425 FWL / TWSP: 22S / RANGE: 32E / SECTION: 24 / LAT: 32.370807 / LONG: -103.632289 ( TVD: 0 feet, MD: 0 feet )

PPP: SESW / 100 FSL / 2250 FWL / TWSP: 22S / RANGE: 32E / SECTION: 24 / LAT: 32.370336 / LONG: -103.629618 ( TVD: 10833 feet, MD: 11246 feet )

PPP: SESW / 1 FSL / 2250 FWL / TWSP: 22S / RANGE: 32E / SECTION: 24 / LAT: 32.370061 / LONG: -103.629618 ( TVD: 10835 feet, MD: 11484 feet )

PPP: SENW / 2639 FNL / 2248 FWL / TWSP: 22S / RANGE: 32E / SECTION: 24 / LAT: 32.377322 / LONG: -103.629624 ( TVD: 10855 feet, MD: 13593 feet )

PPP: SESW / 3 FSL / 2245 FWL / TWSP: 22S / RANGE: 32E / SECTION: 13 / LAT: 32.384581 / LONG: -103.62963 ( TVD: 10881 feet, MD: 16236 feet )

BHL: NENW / 20 FNL / 2250 FWL / TWSP: 22S / RANGE: 32E / SECTION: 13 / LAT: 32.399039 / LONG: -103.629642 ( TVD: 10933 feet, MD: 21496 feet )

# PECOS DISTRICT
# DRILLING CONDITIONS OF APPROVAL

| | |
|---|---|
| OPERATOR'S NAME: | OXY USA INCORPORATED |
| WELL NAME & NO.: | TUNA NUT 24 13 FED COM 23H |
| LOCATION: | Section 24, T.22 S., R.32 E. |
| COUNTY: | Lea County, New Mexico |

**ALL PREVIOUS COAs STILL APPLY**

COA

| | | | |
|---|---|---|---|
| H2S | (•) Yes | ( ) No | |
| Potash | ( ) None | (•) Secretary | ( ) R-111-P |
| Cave/Karst Potential | (•) Low | ( ) Medium | ( ) High |
| Cave/Karst Potential | ( ) Critical | | |
| Variance | ( ) None | (•) Flex Hose | ( ) Other |
| Wellhead | ( ) Conventional | (•) Multibowl | ( ) Both |
| Wellhead Variance | ( ) Diverter | | |
| Other | [ ] 4 String | [ ] Capitan Reef | [ ] WIPP |
| Other | [ ] Fluid Filled | [ ] Pilot Hole | [ ] Open Annulus |
| Cementing | [ ] Contingency Cement Squeeze | [ ] EchoMeter | [x] Primary Cement Squeeze |
| Special Requirements | [ ] Water Disposal | [x] COM | [ ] Unit |
| Special Requirements | [ ] Batch Sundry | | |
| Special Requirements Variance | [x] Break Testing | [x] Offline Cementing | [ ] Casing Clearance |

## A. HYDROGEN SULFIDE

A Hydrogen Sulfide (H2S) Drilling Plan shall be activated AT SPUD. As a result, the Hydrogen Sulfide area must meet Onshore Order 6 requirements, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, please provide measured values and formations to the BLM.

## B. CASING

**NOTE: WELL APPROVED FOR DESIGNS A1, A2 AND B. REVIEW CEMENT VOLUMES TO ACHIEVE TIE BACKS LISTED BELOW.**

**A1:**

1. The **10-3/4** inch surface casing shall be set at approximately **1090** feet **TVD** (a minimum of 25 feet (Lea County) into the Rustler Anhydrite, above the salt, and below usable fresh water) and cemented to the surface.

a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
b. Wait on cement (WOC) time for a primary cement job will be a minimum of **24 hours in the Potash Area** or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
d. If cement falls back, remedial cementing will be done prior to drilling out that string.

2. The **7-5/8** inch intermediate casing shall be set at approximately **10,148** feet. **KEEP CASING 1/2 FULL FOR COLLAPSE SF. PRESSURE TEST NEEDS EXTERNAL PRESSURE REVIEW AS WELL.** The minimum required fill of cement behind the **7-5/8** inch intermediate casing is:

**Option 1 (Single Stage):**

- Cement to surface. If cement does not circulate see B.1.a, c-d above.

Operator has proposed to cement in two stages by conventionally cementing the first stage and performing a bradenhead squeeze on the second stage, contingent upon no returns to surface.

a. First stage: Operator will cement with intent to reach the top of the **Brushy Canyon**

b. Second stage:

- Operator will perform bradenhead squeeze and top-out. Cement to surface. If cement does not reach surface, the appropriate BLM office shall be notified

❖ In Secretary Potash Areas if cement does not circulate to surface on the first two casing strings, the cement on the 3rd casing string must come to surface.

**Operator has proposed to pump down 10-3/4" X 7-5/8" annulus. Operator must top out cement after the bradenhead squeeze and verify cement to surface. Operator can also check TOC with Echo-meter. CBL must be run from TD of the 7-5/8"**

**casing to surface if confidence is lacking on the quality of the bradenhead squeeze cement job. Submit results to BLM.**

**If cement does not tie-back into the previous casing shoe, a third stage remediation BH may be performed. The appropriate BLM office shall be notified.**

**Bradenhead squeeze in the production interval is only as an edge case remediation measure and is NOT approved in this COA. If production cement job experiences losses and a bradenhead squeeze is needed for tie-back, BLM Engineering should be notified prior to job with volumes and planned wellbore schematic. CBL will be needed when this occurs.**

3. The **5-1/2** inch production casing shall be set at approximately **21,155** feet. The minimum required fill of cement behind the **5-1/2** inch production casing is:

   **Option 1 (Single Stage):**

   - Cement should tie-back at least **500 feet** into previous casing string. Operator shall provide method of verification.

**A2:**

1. The **13-3/8** inch surface casing shall be set at approximately **1090** feet **TVD** (a minimum of 25 feet (Lea County) into the Rustler Anhydrite, above the salt, and below usable fresh water) and cemented to the surface.

   e. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
   f. Wait on cement (WOC) time for a primary cement job will be a minimum of **24 hours in the Potash Area** or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
   g. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
   h. If cement falls back, remedial cementing will be done prior to drilling out that string.

2. The **7-5/8** inch intermediate casing shall be set at approximately **10,148** feet. **KEEP CASING 1/2 FULL FOR COLLAPSE SF. PRESSURE TEST NEEDS EXTERNAL PRESSURE REVIEW AS WELL.** The minimum required fill of cement behind the **7-5/8** inch intermediate casing is:

**Option 1 (Single Stage):**

- Cement to surface. If cement does not circulate see B.1.a, c-d above.

**Option 2 (Bradenhead):**

Operator has proposed to cement in two stages by conventionally cementing the first stage and performing a bradenhead squeeze on the second stage, contingent upon no returns to surface.

c. First stage: Operator will cement with intent to reach the top of the **Brushy Canyon**

d. Second stage:

- Operator will perform bradenhead squeeze and top-out. Cement to surface. If cement does not reach surface, the appropriate BLM office shall be notified

3. The **5-1/2** inch production casing shall be set at approximately **21,155** feet. The minimum required fill of cement behind the **5-1/2** inch production casing is:

**Option 1 (Single Stage):**

- Cement should tie-back at least **500 feet** into previous casing string. Operator shall provide method of verification.

**B (Contingency: )**

1. The **13-3/8** inch surface casing shall be set at approximately **1090** feet **TVD** (a minimum of 25 feet (Lea County) into the Rustler Anhydrite, above the salt, and below usable fresh water) and cemented to the surface.

i. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.

j. Wait on cement (WOC) time for a primary cement job will be a minimum of **24 hours in the Potash Area** or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)

k. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.

l. If cement falls back, remedial cementing will be done prior to drilling out that

string.

2. The **10-3/4** inch intermediate casing shall be set at approximately **4898** feet. **KEEP CASING 1/2 FULL FOR COLLAPSE SF. PRESSURE TEST NEEDS EXTERNAL PRESSURE REVIEW AS WELL.** The minimum required fill of cement behind the **7-5/8** inch intermediate casing is:

   **Option 1 (Single Stage):**

   - Cement to surface. If cement does not circulate see B.1.a, c-d above.

3. The **7-5/8** inch intermediate casing shall be set at approximately **10,148** feet. **KEEP CASING 1/2 FULL FOR COLLAPSE SF. PRESSURE TEST NEEDS EXTERNAL PRESSURE REVIEW AS WELL.** The minimum required fill of cement behind the **7-5/8** inch intermediate casing is:

   **Option 1 (Single Stage):**

   - Cement to surface. If cement does not circulate see B.1.a, c-d above.

   **Option 2 (Bradenhead):**

   Operator has proposed to cement in two stages by conventionally cementing the first stage and performing a bradenhead squeeze on the second stage, contingent upon no returns to surface.

   e. First stage: Operator will cement with intent to reach the top of the **Brushy Canyon**

   f. Second stage:

   - Operator will perform bradenhead squeeze and top-out. Cement to surface. If cement does not reach surface, the appropriate BLM office shall be notified

4. The **5-1/2** inch production casing shall be set at approximately **21,155** feet. The minimum required fill of cement behind the **5-1/2** inch production casing is:

   **Option 1 (Single Stage):**

   - Cement should tie-back at least **500 feet** into previous casing string. Operator shall provide method of verification.

## C. PRESSURE CONTROL

1. Variance approved to use flex line from BOP to choke manifold. Manufacturer's specification to be readily available. No external damage to flex line. Flex line to be installed as straight as possible (no hard bends).'

2. Operator has proposed a multi-bowl wellhead assembly. This assembly will only be tested when installed on surface casing. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be **5000 (5M)** psi and the intermediate casing shoe shall be **10,000 (10M)** psi. **Variance is approved to use a 5000 (5M) Annular which shall be tested to 3500 (70% Working Pressure) psi.**

    a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
    b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
    c. Manufacturer representative shall install the test plug for the initial BOP test.
    d. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
    e. Whenever any seal subject to test pressure is broken, all the tests in OOGO2.III.A.2.i must be followed.

## D. SPECIAL REQUIREMENT (S)

**Communitization Agreement**

- The operator will submit a Communitization Agreement to the Santa Fe Office, 301 Dinosaur Trail Santa Fe, New Mexico 87508, at least 90 days before the anticipated date of first production from a well subject to a spacing order issued by the New Mexico Oil Conservation Division. The Communitization Agreement will include the signatures of all working interest owners in all Federal and Indian leases subject to the Communitization Agreement (i.e., operating rights owners and lessees of record), or certification that the operator has obtained the written signatures of all such owners and will make those signatures available to the BLM immediately upon request.
- The operator will submit an as-drilled survey well plat of the well completion, but are not limited to, those specified in Onshore Order 1 and 2.
- If the operator does not comply with this condition of approval, the BLM may take enforcement actions that include, but are not limited to, those specified in 43 CFR 3163.1.
- In addition, the well sign shall include the surface and bottom hole lease numbers. When the Communitization Agreement number is known, it shall also be on the sign.

**(Note: For a minimum 5M BOPE or less (Utilizing a 10M BOPE system)**

**BOPE Break Testing Variance**

- BOPE Break Testing is ONLY permitted for 5M BOPE or less. **(Annular preventer must be tested to a minimum of 70% of BOPE working pressure and shall be higher than the MASP)**
- BOPE Break Testing is NOT permitted to drilling the production hole section.
- Variance only pertains to the intermediate hole-sections and no deeper than the Bone Springs formation.
- While in transfer between wells, the BOPE shall be secured by the hydraulic carrier or cradle.
- Any well control event while drilling require notification to the BLM Petroleum Engineer **(575-706-2779)** prior to the commencement of any BOPE Break Testing operations.
- A full BOPE test is required prior to drilling the first deep intermediate hole section. If any subsequent hole interval is deeper than the first, a full BOPE test will be required. (200' TVD tolerance between intermediate shoes is allowable).
- The BLM is to be contacted (575-361-2822 Eddy County) 4 hours prior to BOPE tests.
- As a minimum, a full BOPE test shall be performed at 21-day intervals.
- In the event any repairs or replacement of the BOPE is required, the BOPE shall test as per Onshore Oil and Gas Order No. 2.
- If in the event break testing is not utilized, then a full BOPE test would be conducted.

**Offline Cementing**

Offline cementing OK for surface and intermediate intervals. Notify the BLM prior to the commencement of any offline cementing procedure.

# GENERAL REQUIREMENTS

The BLM is to be notified in advance for a representative to witness:

a. Spudding well (minimum of 24 hours)
b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
c. BOPE tests (minimum of 4 hours)

**Contact Eddy County Petroleum Engineering Inspection Staff:**

Email or call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220; **BLM_NM_CFO_DrillingNotifications@BLM.GOV**; (575) 361-2822

**Contact Lea County Petroleum Engineering Inspection Staff:**

Call the Hobbs Field Station, 414 West Taylor, Hobbs NM 88240, (575) 689-5981

1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.
    a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after

installing and testing the wellhead, by installing a blind flange of like pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).

b. When the operator proposes to set surface casing with Spudder Rig

i. Notify the BLM when moving in and removing the Spudder Rig.

ii. Notify the BLM when moving in the 2nd Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.

iii. BOP/BOPE test to be conducted per **43 CFR 3172** as soon as 2nd Rig is rigged up on well.

2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the dog house or stairway area.

3. For intervals in which cement to surface is required, cement to surface should be verified with a visual check and density or pH check to differentiate cement from spacer and drilling mud. The results should be documented in the driller's log and daily reports.

A. **CASING**

1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.

2. Wait on cement (WOC) for Potash Areas: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends of both lead and tail cement, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.

3. Wait on cement (WOC) for Water Basin: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.

4. Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.

5. No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.

6. On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe

shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.

7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.

8. Whenever a casing string is cemented in the R-111-Q potash area, the NMOCD requirements shall be followed.

B. **PRESSURE CONTROL**

1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in **43 CFR 3172**.

2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor.

3. 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.

4. If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:

i. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.

ii. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.

iii. Manufacturer representative shall install the test plug for the initial BOP test.

iv. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR 3172.6(b)(9) must be followed.

v. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.

5. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.

i. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead cement), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).

ii. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation

has been done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the cement plug. The BOPE test can be initiated after bumping the cement plug with the casing valve open. (only applies to single stage cement jobs, prior to the cement setting up.)

iii. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer and can be initiated immediately with the casing valve open. The operator also has the option of utilizing an independent tester to test without a plug (i.e. against the casing) pursuant to **43 CFR 3172** with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for 8 hours or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).

iv. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.

v. The results of the test shall be reported to the appropriate BLM office.

vi. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.

vii. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.

viii. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per **43 CFR 3172**.

C. **DRILLING MUD**

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

D. **WASTE MATERIAL AND FLUIDS**

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area. Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

**KPI** 4/10/2025

Tenaris

# API BTC -Special Clearance

| Coupling | Pipe Body |
|---|---|
| Grade: **L80-IC** | Grade: **L80-IC** |
| Body: **Red** | 1st Band: **Red** |
| 1st Band: **Brown** | 2nd Band: **Brown** |
| 2nd Band: **-** | 3rd Band: **Pale Green** |
| 3rd Band: **-** | 4th Band: **-** |

| | | | | | |
|---|---|---|---|---|---|
| **Outside Diameter** | 10.750 in. | **Wall Thickness** | 0.400 in. | **Grade** | L80-IC |
| **Min. Wall Thickness** | 87.50 % | **Pipe Body Drift** | Alternative Drift | **Type** | Casing |
| **Connection OD Option** | Special Clearance | | | | |

## Pipe Body Data

| Geometry | | | | Performance | |
|---|---|---|---|---|---|
| **Nominal OD** | 10.750 in. | **Drift** | 9.875 in. | **SMYS** | 80,000 psi |
| **Wall Thickness** | 0.400 in. | **Plain End Weight** | 44.26 lb/ft | **Min UTS** | 95,000 psi |
| **Nominal Weight** | 45.500 lb/ft | **OD Tolerance** | API | **Body Yield Strength** | 1040 x1000 lb |
| **Nominal ID** | 9.950 in. | | | **Min. Internal Yield Pressure** | 5210 psi |
| | | | | **Collapse Pressure** | 2950 psi |
| | | | | **Max. Allowed Bending** | 34 °/100 ft |

## Connection Data

| Geometry | | Performance | |
|---|---|---|---|
| **Thread per In** | 5 | **Joint Strength** | 1041 x1000 lb |
| **Connection OD** | 11.250 in. | **Coupling Face Load** | 478 x1000 lb |
| **Hand Tight Stand Off** | 1 in. | **Internal Pressure Capacity** | 4150 psi |

## Notes

For products according to API Standards 5CT & 5B; Performance calculated considering API Technical Report 5C3 (Sections 9 & 10) equations.
For geometrical and steel grades combinations not considered in the API Standards 5CT and/or 5B; Performance calculations indirectly derived from API Technical Report 5C3 (Sections 9 & 10) equations.
Couplings OD are shown according to current API 5CT 10th Edition.

# Oxy USA Inc. - Blanket Design Pad Document

## OXY - Blanket Design B

**Pad Name:** REDTNK_T22SR32E_24_01

**SHL:** 390' FSL 1095' FWL, Sec 24, T22S-R32E

Oxy requests for the bellow wells to be approved for the two designs listed in the Blanket Design document **(Blanket Design B –OXY –4S Slim v3.2.)** The MDs and TVDs for all intervals are within the boundary conditions. The max inclination and DLS are also within the boundary conditions (directional plans attached separately for review.)

## 1. Blanket Design - Wells

| Well Name | APD # | Surface | | Salt | | Intermediate | | Production | |
|---|---|---|---|---|---|---|---|---|---|
| | | MD | TVD | MD | TVD | MD | TVD | MD | TVD |
| TUNA NUT 24_13 FED COM 22H | 10400093225 | 1090 | 1090 | 4875 | 4875 | 10226 | 10163 | 21193 | 10874 |
| TUNA NUT 24_13 FED COM 23H | 10400093266 | 1087 | 1087 | 4898 | 4898 | 10148 | 10117 | 21155 | 10874 |
| TUNA NUT 24_13 FED COM 171H | 10400097316 | 1090 | 1090 | 4884 | 4884 | 10631 | 10592 | 21621 | 11330 |
| TUNA NUT 24_13 FED COM 172H | 10400097320 | 1085 | 1085 | 4920 | 4920 | 10676 | 10617 | 21644 | 11330 |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |

## 2. Review Criteria Table

| | Y or N |
|---|---|
| Is casing new? If used, attach certification as required in 43 CFR 3160 | Y |
| Does casing meet API specifications? If no, attach casing specification sheet. | Y |
| Is premium or uncommon casing planned? If yes attach casing specification sheet. | Y |
| Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria). | Y |
| Will the intermediate pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing? | Y |
| | |
| Is well located within Capitan Reef? | N |
| If yes, does production casing cement tie back a minimum of 50' above the Reef? | |
| Is well within the designated 4 string boundary. | |
| | |
| Is well located in SOPA but not in R-111-Q? | N |
| If yes, are the first 2 strings cemented to surface and 3rd string cement tied back 500' into previous casing? | |
| | |
| Is well located in R-111-Q and SOPA? | N |
| If yes, are the first three strings cemented to surface? | |
| Is 2nd string set 100' to 600' below the base of salt? | |
| | |
| Is well located in high Cave/Karst? | N |
| If yes, are there two strings cemented to surface? | |
| (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs? | |
| | |
| Is well located in critical Cave/Karst? | N |
| If yes, are there three strings cemented to surface? | |

## 3. Geologic Formations

| Formation | MD-RKB (ft) | TVD-RKB (ft) | Expected Fluids |
|---|---|---|---|
| Rustler | 1030 | 1030 | |
| Salado | 1665 | 1665 | Salt |
| Castile | 3438 | 3438 | Salt |
| Delaware | 4875 | 4875 | Oil/Gas/Brine |
| Bell Canyon | 4969 | 4969 | Oil/Gas/Brine |
| Cherry Canyon | 5781 | 5781 | Oil/Gas/Brine |
| Brushy Canyon | 7094 | 7080 | Losses |
| Bone Spring | 8756 | 8717 | Oil/Gas |
| Bone Spring 1st | 9879 | 9823 | Oil/Gas |
| Bone Spring 2nd | 10580 | 10509 | Oil/Gas |
| Bone Spring 3rd | | | Oil/Gas |
| Wolfcamp | | | Oil/Gas |
| Penn | | | Oil/Gas |
| Strawn | | | Oil/Gas |

## 4. Cementing Program

| Section | Stage | Slurry: | Sacks | Yield (ft^3/ft) | Density (lb/gal) | Excess: | TOC | Placement | Description |
|---|---|---|---|---|---|---|---|---|---|
| Surface | 1 | Surface - Tail | 1139 | 1.33 | 14.8 | 100% | - | Circulate | Class C+Accel. |
| Int.1 | 1 | Intermediate - Tail | 85 | 1.33 | 14.8 | 20% | 4,375 | Circulate | Class C+Accel. |
| Int.1 | 1 | Intermediate - Lead | 686 | 1.73 | 12.9 | 50% | - | Circulate | Class Pozz+Ret. |
| Int. 2 | 1 | Intermediate 1S - Tail | 387 | 1.68 | 13.2 | 5% | 7,344 | Circulate | Class C+Ret., Disper. |
| Int. 2 | 2 | Intermediate 2S - Tail BH | 1023 | 1.71 | 13.3 | 25% | - | Bradenhead | Class C+Accel. |
| Prod. | 1 | Production - Tail | 649 | 1.84 | 13.3 | 25% | 9,726 | Circulate | Class C+Ret. |

# Oxy USA Inc. - TUNA NUT 24_13 FED COM 23H
## Drill Plan

### 1. Geologic Formations

| | | | |
|---|---|---|---|
| TVD of Target (ft): | 10874 | Pilot Hole Depth (ft): | |
| Total Measured Depth (ft): | 21155 | Deepest Expected Fresh Water (ft): | 1027 |

### Delaware Basin

| Formation | MD-RKB (ft) | TVD-RKB (ft) | Expected Fluids |
|---|---|---|---|
| Rustler | 1027 | 1027 | |
| Salado | 1686 | 1686 | Salt |
| Castile | 3478 | 3478 | Salt |
| Delaware | 4898 | 4898 | Oil/Gas/Brine |
| Bell Canyon | 4989 | 4989 | Oil/Gas/Brine |
| Cherry Canyon | 5786 | 5786 | Oil/Gas/Brine |
| Brushy Canyon | 7093 | 7093 | Losses |
| Bone Spring | 8741 | 8733 | Oil/Gas |
| Bone Spring 1st | 9863 | 9838 | Oil/Gas |
| Bone Spring 2nd | 10562 | 10524 | Oil/Gas |
| Bone Spring 3rd | | | Oil/Gas |
| Wolfcamp | | | Oil/Gas |
| Penn | | | Oil/Gas |
| Strawn | | | Oil/Gas |

*H2S, water flows, loss of circulation, abnormal pressures, etc.

### 2. Casing Program

| | | MD | | TVD | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| Section | Hole Size (in) | From (ft) | To (ft) | From (ft) | To (ft) | Csg. OD (in) | Csg Wt. (ppf) | Grade | Conn. |
| Surface | 17.5 | 0 | 1087 | 0 | 1087 | 13.375 | 54.5 | J-55 | BTC |
| Salt | 12.25 | 0 | 4898 | 0 | 4898 | 10.75 | 45.5 | L-80 HC | BTC-SC |
| Intermediate | 9.875 | 0 | 10148 | 0 | 10117 | 7.625 | 26.4 | L-80 HC | BTC |
| Production | 6.75 | 0 | 21155 | 0 | 10874 | 5.5 | 20 | P-110 | Sprint-SF |

All casing strings will be tested in accordance with 43 CFR part 3170 Subpart 3172

| *All Casing SF Values will meet or exceed those below* | | | |
|---|---|---|---|
| **SF Collapse** | **SF Burst** | **Body SF Tension** | **Joint SF Tension** |
| 1.00 | 1.100 | 1.4 | 1.4 |

| | Y or N |
|---|---|
| Is casing new? If used, attach certification as required in 43 CFR 3160 | Y |
| Does casing meet API specifications? If no, attach casing specification sheet. | Y |
| Is premium or uncommon casing planned? If yes attach casing specification sheet. | Y |
| Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria). | Y |
| Will the intermediate pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing? | Y |
| | |
| Is well located within Capitan Reef? | N |
| If yes, does production casing cement tie back a minimum of 50' above the Reef? | |
| Is well within the designated 4 string boundary. | |
| | |
| Is well located in SOPA but not in R-111-Q? | N |
| If yes, are the first 2 strings cemented to surface and 3rd string cement tied back 500' into previous casing? | |
| | |
| Is well located in R-111-Q and SOPA? | N |
| If yes, are the first three strings cemented to surface? | |
| Is 2nd string set 100' to 600' below the base of salt? | |
| | |
| Is well located in high Cave/Karst? | N |
| If yes, are there two strings cemented to surface? | |
| (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs? | |
| | |
| Is well located in critical Cave/Karst? | N |
| If yes, are there three strings cemented to surface? | |

## 3. Cementing Program

| Section | Stage | Slurry: | Sacks | Yield (ft^3/ft) | Density (lb/gal) | Excess: | TOC | Placement | Description |
|---|---|---|---|---|---|---|---|---|---|
| Surface | 1 | Surface - Tail | 1135 | 1.33 | 14.8 | 100% | - | Circulate | Class C+Accel. |
| Int.1 | 1 | Intermediate - Tail | 85 | 1.33 | 14.8 | 20% | 4,398 | Circulate | Class C+Accel. |
| Int.1 | 1 | Intermediate - Lead | 690 | 1.73 | 12.9 | 50% | - | Circulate | Class Pozz+Ret. |
| Int. 2 | 1 | Intermediate 1S - Tail | 377 | 1.68 | 13.2 | 5% | 7,343 | Circulate | Class C+Ret., Disper. |
| Int. 2 | 2 | Intermediate 2S - Tail BH | 1022 | 1.71 | 13.3 | 25% | - | Bradenhead | Class C+Accel. |
| Prod. | 1 | Production - Tail | 652 | 1.84 | 13.3 | 25% | 9,648 | Circulate | Class C+Ret. |

**Offline Cementing Request**

Oxy requests a variance to cement the 9.625” and/or 7.625” intermediate casing strings offline in accordance to the approved variance, EC Tran 461365. Please see Offline Cementing Variance attachment for further details.

**Bradenhead CBL Request**

Oxy requests permission to adjust the CBL requirement after bradenhead cement jobs, on 7-5/8” intermediate casings, as per the agreement reached in the OXY/BLM meeting on September 5, 2019. Please see Bradenhead CBL Variance attachment for further details.

## 4. Pressure Control Equipment

| BOP installed and tested before drilling which hole? | Size? | Min. Required WP | Type | ✓ | Tested to: | TVD Depth (ft) per Section: |
|---|---|---|---|---|---|---|
| 12.25" Hole | 13-5/8” | 5M | Annular | ✓ | 70% of working pressure | 4898 |
| | | 5M | Blind Ram | ✓ | 250 psi / 5000 psi | |
| | | | Pipe Ram | | | |
| | | | Double Ram | ✓ | | |
| | | | Other* | | | |
| 9.875" Hole | 13-5/8” | 5M | Annular | ✓ | 70% of working pressure | 10117 |
| | | 5M | Blind Ram | ✓ | 250 psi / 5000 psi | |
| | | | Pipe Ram | | | |
| | | | Double Ram | ✓ | | |
| | | | Other* | | | |
| 6.75" Hole | 13-5/8” | 5M | Annular | ✓ | 70% of working pressure | 10874 |
| | | 5M | Blind Ram | ✓ | 250 psi / 5000 psi | |
| | | | Pipe Ram | | | |
| | | | Double Ram | ✓ | | |
| | | | Other* | | | |

*Specify if additional ram is utilized

BOP/BOPE will be tested by an independent service company to 250 psi low and the high pressure indicated above per 43 CFR part 3170 Subpart 3172 requirements. The System may be upgraded to a higher pressure but still tested to the working pressure listed in the table above. If the system is upgraded all the components installed will be functional and tested.

Pipe rams will be operationally checked each 24 hour period. Blind rams will be operationally checked on each trip out of the hole. These checks will be noted on the daily tour sheets. Other accessories to the BOP equipment will include a Kelly cock and floor safety valve (inside BOP) and choke lines and choke

| | | |
|---|---|---|
| | Formation integrity test will be performed per 43 CFR part 3170 Subpart 3172. | |
| | On Exploratory wells or on that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Will be tested in accordance with 43 CFR part 3170 Subpart 3172. | |
| | | |
| | A variance is requested for the use of a flexible choke line from the BOP to Choke Manifold. See attached for specs and hydrostatic test chart. | |
| | Y | Are anchors required by manufacturer? |
| | A multibowl or a unionized multibowl wellhead system will be employed. The wellhead and connection to the BOPE will meet all API 6A requirements. The BOP will be tested per 43 CFR part 3170 Subpart 3172 after installation on the surface casing which will cover testing requirements for a maximum of 30 days. If any seal subject to test pressure is broken the system must be tested. We will test the flange connection of the wellhead with a test port that is directly in the flange. We are proposing that we will run the wellhead through the rotary prior to cementing surface casing as discussed with the BLM on October 8, 2015.<br><br>See attached schematics. | |

**BOP Break Testing Request**

Oxy requests permission to adjust the BOP break testing requirements as per the agreement reached in the OXY/BLM meeting on September 5, 2019. Please see BOP Break Testing Variance attachment for further details.

**Oxy will use Cameron ADAPT wellhead system that uses an OEC top flange connection. This connection has been fully vetted and verified by API to Spec 6A and carries an API monogram.**

## 5. Mud Program

| Section | Depth | | Depth - TVD | | Type | Weight (ppg) | Viscosity | Water Loss |
|---|---|---|---|---|---|---|---|---|
| | From (ft) | To (ft) | From (ft) | To (ft) | | | | |
| Surface | 0 | 1087 | 0 | 1087 | Water-Based Mud | 8.6 - 8.8 | 40-60 | N/C |
| Intermediate 1 | 1087 | 4898 | 1087 | 4898 | Saturated Brine-Based or Oil-Based Mud | 8.0 - 10.0 | 35-45 | N/C |
| Intermediate 2 | 4898 | 10148 | 4898 | 10117 | Water-Based or Oil-Based Mud | 8.0 - 10.0 | 38-50 | N/C |
| Production | 10148 | 21155 | 10117 | 10874 | Water-Based or Oil-Based Mud | 8.0 - 9.6 | 38-50 | N/C |

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times. The following is a general list of products: Barite, Bentonite, Gypsum, Lime, Soda Ash, Caustic Soda, Nut Plug, Cedar Fiber, Cotton Seed Hulls,

| | |
|---|---|
| What will be used to monitor the loss or gain of fluid? | PVT/MD Totco/Visual Monitoring |

## 6. Logging and Testing Procedures

| Logging, Coring and Testing. | |
|---|---|
| Yes | Will run GR from TD to surface (horizontal well – vertical portion of hole). |
| | Stated logs run will be in the Completion Report and submitted to the BLM. |
| No | Logs are planned based on well control or offset log information. |
| No | Drill stem test? If yes, explain |
| No | Coring? If yes, explain |

| Additional logs planned | | Interval |
|---|---|---|
| No | Resistivity | |
| No | Density | |
| Yes | CBL | Production string |
| Yes | Mud log | Bone Spring – TD |
| No | PEX | |

## 7. Drilling Conditions

| Condition | Specify what type and where? |
|---|---|
| BH Pressure at deepest TVD | 5429 psi |
| Abnormal Temperature | No |
| BH Temperature at deepest TVD | 167°F |

Pump high viscosity sweeps as needed for hole cleaning. The mud system will be monitored visually/manually as well as with an electronic PVT. The necessary mud products for additional weight and fluid loss control will be on location at all times. Appropriately weighted mud will be used to isolate potential gas, oil, and water zones until such time as casing can be cemented into place for

| Hydrogen Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the operator will comply with the provisions of 43 CFR part 3170 Subpart 3172. If Hydrogen Sulfide is encountered, measured values and formations will be provided to the BLM. | |
|---|---|
| N | H2S is present |
| Y | H2S Plan attached |

## 8. Other facets of operation

| | Yes/No |
|---|---|
| Will the well be drilled with a walking/skidding operation? If yes, describe.<br>We plan to drill the 4 well pad in batch by section: all surface sections, intermediate sections and production sections. The wellhead will be secured with a night cap whenever the rig is not over the well. | Yes |
| Will more than one drilling rig be used for drilling operations? If yes, describe.<br>Oxy requests the option to contract a Surface Rig to drill, set surface casing, and cement for this well. If the timing between rigs is such that Oxy would not be able to preset surface, the Primary Rig will MIRU and drill the well in its entirety per the APD. Please see the attached document for information on the spudder rig. | Yes |

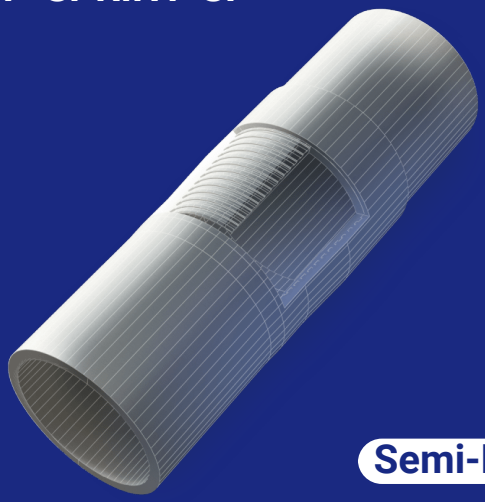
**Total Estimated Cuttings Volume:** 1864 bbls

Generated on April 25, 2024

# CONNECTION DATA SHEET

OD: **5.500 in.** Grade: **P110 RY**
Weight: **20.00 lb/ft** Drift: **4.653 in. (API)**
Wall Th.: **0.361 in.**

## VAM® SPRINT-SF



**Semi-Flush**

### Field Torque Values

**Make-up Torque (ft-lb)**
20,000 **MIN**
22,500 **OPTI**
25,000 **MAX**

**Torque with Sealability (ft-lb)**
36,000 **MTS**

**Locked Flank Torque (ft-lb)**
4,500 **MIN**
15,750 **MAX**

*(2) MTS: Maximum Torque with Sealability.*

## PIPE BODY PROPERTIES

| | | |
|---|---|---|
| **Nominal OD** | 5.500 | *in.* |
| **Nominal ID** | 4.778 | *in.* |
| **Nominal Wall Thickness** | 0.361 | *in.* |
| **Minimum Wall Thickness** | 87.5 | *%* |
| **Nominal Weight (API)** | 20.00 | *lb/ft* |
| **Plain End Weight** | 19.83 | *lb/ft* |
| **Drift** | 4.653 | *in.* |
| **Grade Type** | Controlled Yield | |
| **Minimum Yield Strength** | 110 | *ksi* |
| **Maximum Yield Strength** | 125 | *ksi* |
| **Minimum Ultimate Tensile Strength** | 140 | *ksi* |
| **Pipe Body Yield Strength** | 641 | *klb* |
| **Internal Yield Pressure** | 12,640 | *psi* |
| **Collapse Pressure** | 11,110 | *psi* |

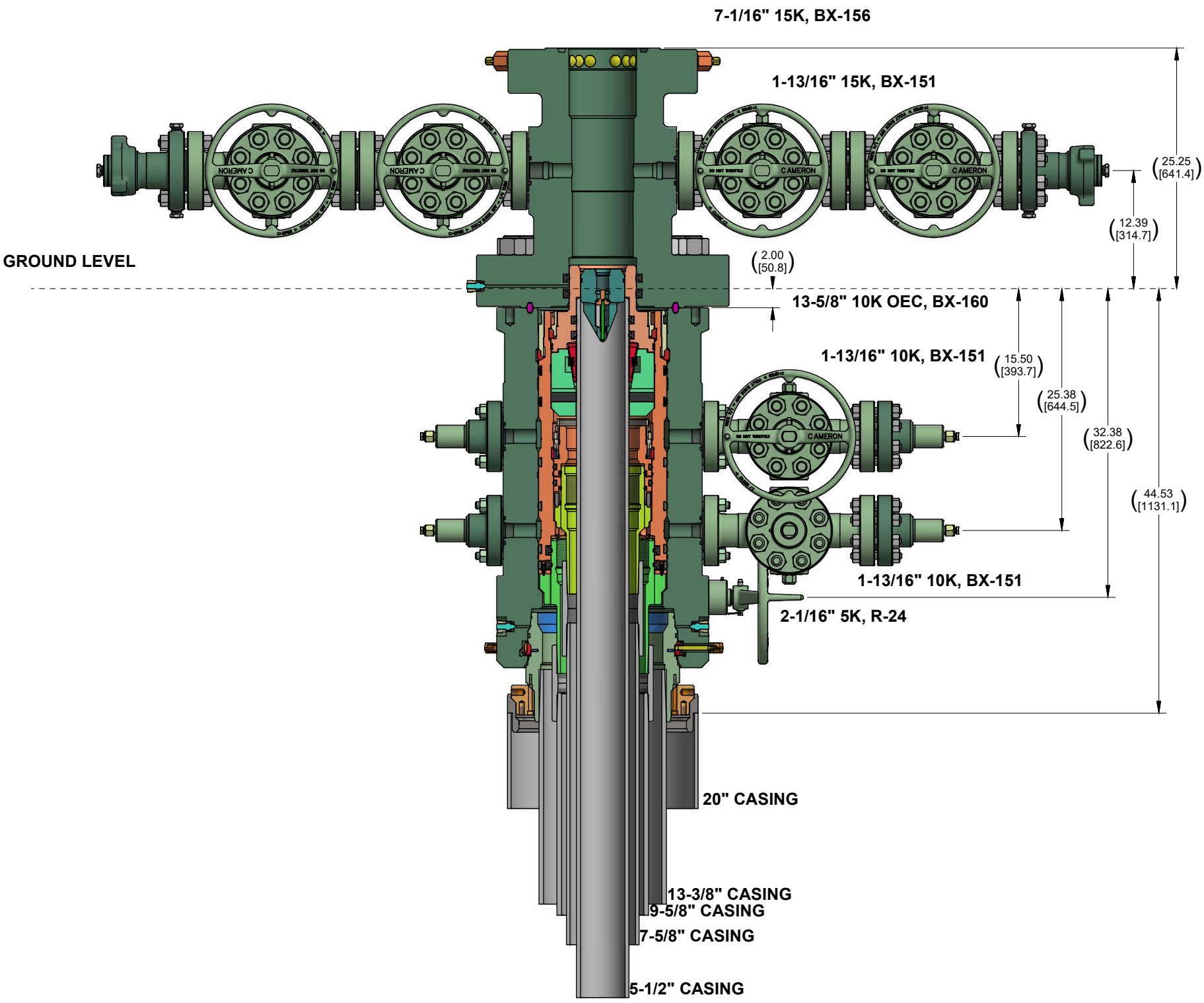
## CONNECTION PROPERTIES

| | | |
|---|---|---|
| **Connection Type** | Semi-Premium Integral Semi-Flu | |
| **Nominal Connection OD** | 5.783 | *in.* |
| **Nominal Connection ID** | 4.718 | *in.* |
| **Make-up Loss** | 5.965 | *in.* |
| **Tension Efficiency** | 90 | *% Pipe Body* |
| **Compression Efficiency** | 90 | *% Pipe Body* |
| **Internal Pressure Efficiency** | 100 | *% Pipe Body* |
| **External Pressure Efficiency** | 100 | *% Pipe Body* |

## JOINT PERFORMANCES

| | | |
|---|---|---|
| **Tension Strength** | 577 | *klb* |
| **Compression Strength** | 577 | *klb* |
| **Internal Pressure Resistance** | 12,640 | *psi* |
| **External Pressure Resistance** | 11,110 | *psi* |
| **Maximum Bending, Structural** | 78 | *°/100 ft* |
| **Maximum Bending, with Sealability(1)** | 30 | *°/100 ft* |

*(1) Sealability rating demonstrated as per API RP 5C5 / ISO 13679*




CONFIDENTIAL

| | | | | |
|---|---|---|---|---|
| SURFACE TREATMENT | DO NOT SCALE | | CAMERON A Schlumberger Company | SURFACE SYSTEMS |
| | DRAWN BY: A. SKLENKA | DATE 26 Apr 22 | | |
| MATERIAL & HEAT TREAT | CHECKED BY: A. SKLENKA | DATE 26 Apr 22 | OXY ADAPT NST 10K 3 STAGE WELLHEAD STANDARD / EMERGENCY SYSTEM | |
| | APPROVED BY: A. SKLENKA | DATE 26 Apr 22 | | |
| ESTIMATED WEIGHT: 7968.4 LBS 3614.4 KG | INITIAL USE B/M: I T# 7836394 | | SHEET 1 OF 1 | LO-096232-62 REV: 01 |

INVENTOR - D

# OXY

**PRD NM DIRECTIONAL PLANS (NAD 1983)**
**Tuna Nut 24_13 Fed Com**
**Tuna Nut 24_13 Fed Com 23H**

**Wellbore #1**

**Plan: Permitting Plan**

# Standard Planning Report

**18 February, 2025**

# OXY
## Planning Report

| | | | |
|---|---|---|---|
| **Database:** | HOPSPP | **Local Co-ordinate Reference:** | Well Tuna Nut 24_13 Fed Com 23H |
| **Company:** | ENGINEERING DESIGNS | **TVD Reference:** | RKB=25' @ 3786.00ft |
| **Project:** | PRD NM DIRECTIONAL PLANS (NAD 1983) | **MD Reference:** | RKB=25' @ 3786.00ft |
| **Site:** | Tuna Nut 24_13 Fed Com | **North Reference:** | Grid |
| **Well:** | Tuna Nut 24_13 Fed Com 23H | **Survey Calculation Method:** | Minimum Curvature |
| **Wellbore:** | Wellbore #1 | | |
| **Design:** | Permitting Plan | | |

**Project** PRD NM DIRECTIONAL PLANS (NAD 1983)

| | | | |
|---|---|---|---|
| **Map System:** | US State Plane 1983 | **System Datum:** | Mean Sea Level |
| **Geo Datum:** | North American Datum 1983 | | |
| **Map Zone:** | New Mexico Eastern Zone | | Using geodetic scale factor |

**Site** Tuna Nut 24_13 Fed Com

| | | | | | |
|---|---|---|---|---|---|
| **Site Position:** | | **Northing:** | 497,414.86 usft | **Latitude:** | 32.365515 |
| **From:** | Map | **Easting:** | 757,769.29 usft | **Longitude:** | -103.632352 |
| **Position Uncertainty:** | 1.79 ft | **Slot Radius:** | 13.200 in | | |

**Well** Tuna Nut 24_13 Fed Com 23H

| | | | | | | |
|---|---|---|---|---|---|---|
| **Well Position** | **+N/-S** | 0.00 ft | **Northing:** | 499,451.71 usf | **Latitude:** | 32.371119 |
| | **+E/-W** | 0.00 ft | **Easting:** | 757,504.51 usf | **Longitude:** | -103.633166 |
| **Position Uncertainty** | | 2.00 ft | **Wellhead Elevation:** | ft | **Ground Level:** | 3,761.00 ft |
| **Grid Convergence:** | | 0.37 ° | | | | |

**Wellbore** Wellbore #1

| Magnetics | Model Name | Sample Date | Declination (°) | Dip Angle (°) | Field Strength (nT) |
|---|---|---|---|---|---|
| | HDGM_FILE | 11/22/2022 | 6.33 | 59.98 | 47,681.60000000 |

**Design** Permitting Plan

**Audit Notes:**

| | | | | |
|---|---|---|---|---|
| **Version:** | **Phase:** | PROTOTYPE | **Tie On Depth:** | 0.00 |

| Vertical Section: | Depth From (TVD) (ft) | +N/-S (ft) | +E/-W (ft) | Direction (°) |
|---|---|---|---|---|
| | 3.00 | 0.00 | 0.00 | 0.97 |

**Plan Survey Tool Program** **Date** 2/18/2025

| | Depth From (ft) | Depth To (ft) | Survey (Wellbore) | Tool Name | Remarks |
|---|---|---|---|---|---|
| 1 | 0.00 | 21,153.89 | Permitting Plan (Wellbore #1) | B001Mc_MWD+HRGM_R5 | |
| | | | | MWD+HRGM | |

**Plan Sections**

| Measured Depth (ft) | Inclination (°) | Azimuth (°) | Vertical Depth (ft) | +N/-S (ft) | +E/-W (ft) | Dogleg Rate (°/100ft) | Build Rate (°/100ft) | Turn Rate (°/100ft) | TFO (°) | Target |
|---|---|---|---|---|---|---|---|---|---|---|
| 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 7,554.00 | 0.00 | 0.00 | 7,554.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 8,554.45 | 10.00 | 150.03 | 8,549.38 | -75.47 | 43.53 | 1.00 | 1.00 | 0.00 | 150.03 | |
| 10,247.77 | 10.00 | 150.03 | 10,216.94 | -330.30 | 190.50 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 11,234.68 | 90.00 | 359.58 | 10,874.00 | 236.48 | 243.57 | 10.00 | 8.11 | -15.24 | -150.06 | |
| 21,154.68 | 90.00 | 359.58 | 10,874.00 | 10,156.22 | 171.49 | 0.00 | 0.00 | 0.00 | 0.00 | PBHL (Tuna Nut |

# OXY

## Planning Report

| | | | |
|---|---|---|---|
| **Database:** | HOPSPP | **Local Co-ordinate Reference:** | Well Tuna Nut 24_13 Fed Com 23H |
| **Company:** | ENGINEERING DESIGNS | **TVD Reference:** | RKB=25' @ 3786.00ft |
| **Project:** | PRD NM DIRECTIONAL PLANS (NAD 1983) | **MD Reference:** | RKB=25' @ 3786.00ft |
| **Site:** | Tuna Nut 24_13 Fed Com | **North Reference:** | Grid |
| **Well:** | Tuna Nut 24_13 Fed Com 23H | **Survey Calculation Method:** | Minimum Curvature |
| **Wellbore:** | Wellbore #1 | | |
| **Design:** | Permitting Plan | | |

**Planned Survey**

| Measured Depth (ft) | Inclination (°) | Azimuth (°) | Vertical Depth (ft) | +N/-S (ft) | +E/-W (ft) | Vertical Section (ft) | Dogleg Rate (°/100ft) | Build Rate (°/100ft) | Turn Rate (°/100ft) |
|---|---|---|---|---|---|---|---|---|---|
| 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 100.00 | 0.00 | 0.00 | 100.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 200.00 | 0.00 | 0.00 | 200.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 300.00 | 0.00 | 0.00 | 300.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 400.00 | 0.00 | 0.00 | 400.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 500.00 | 0.00 | 0.00 | 500.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 600.00 | 0.00 | 0.00 | 600.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 700.00 | 0.00 | 0.00 | 700.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 800.00 | 0.00 | 0.00 | 800.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 900.00 | 0.00 | 0.00 | 900.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 1,000.00 | 0.00 | 0.00 | 1,000.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 1,100.00 | 0.00 | 0.00 | 1,100.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 1,200.00 | 0.00 | 0.00 | 1,200.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 1,300.00 | 0.00 | 0.00 | 1,300.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 1,400.00 | 0.00 | 0.00 | 1,400.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 1,500.00 | 0.00 | 0.00 | 1,500.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 1,600.00 | 0.00 | 0.00 | 1,600.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 1,700.00 | 0.00 | 0.00 | 1,700.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 1,800.00 | 0.00 | 0.00 | 1,800.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 1,900.00 | 0.00 | 0.00 | 1,900.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2,000.00 | 0.00 | 0.00 | 2,000.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2,100.00 | 0.00 | 0.00 | 2,100.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2,200.00 | 0.00 | 0.00 | 2,200.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2,300.00 | 0.00 | 0.00 | 2,300.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2,400.00 | 0.00 | 0.00 | 2,400.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2,500.00 | 0.00 | 0.00 | 2,500.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2,600.00 | 0.00 | 0.00 | 2,600.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2,700.00 | 0.00 | 0.00 | 2,700.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2,800.00 | 0.00 | 0.00 | 2,800.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2,900.00 | 0.00 | 0.00 | 2,900.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 3,000.00 | 0.00 | 0.00 | 3,000.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 3,100.00 | 0.00 | 0.00 | 3,100.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 3,200.00 | 0.00 | 0.00 | 3,200.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 3,300.00 | 0.00 | 0.00 | 3,300.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 3,400.00 | 0.00 | 0.00 | 3,400.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 3,500.00 | 0.00 | 0.00 | 3,500.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 3,600.00 | 0.00 | 0.00 | 3,600.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 3,700.00 | 0.00 | 0.00 | 3,700.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 3,800.00 | 0.00 | 0.00 | 3,800.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 3,900.00 | 0.00 | 0.00 | 3,900.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 4,000.00 | 0.00 | 0.00 | 4,000.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 4,100.00 | 0.00 | 0.00 | 4,100.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 4,200.00 | 0.00 | 0.00 | 4,200.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 4,300.00 | 0.00 | 0.00 | 4,300.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 4,400.00 | 0.00 | 0.00 | 4,400.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 4,500.00 | 0.00 | 0.00 | 4,500.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 4,600.00 | 0.00 | 0.00 | 4,600.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 4,700.00 | 0.00 | 0.00 | 4,700.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 4,800.00 | 0.00 | 0.00 | 4,800.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 4,900.00 | 0.00 | 0.00 | 4,900.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 5,000.00 | 0.00 | 0.00 | 5,000.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 5,100.00 | 0.00 | 0.00 | 5,100.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 5,200.00 | 0.00 | 0.00 | 5,200.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 5,300.00 | 0.00 | 0.00 | 5,300.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 5,400.00 | 0.00 | 0.00 | 5,400.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

# OXY
## Planning Report

| | | | |
|---|---|---|---|
| **Database:** | HOPSPP | **Local Co-ordinate Reference:** | Well Tuna Nut 24_13 Fed Com 23H |
| **Company:** | ENGINEERING DESIGNS | **TVD Reference:** | RKB=25' @ 3786.00ft |
| **Project:** | PRD NM DIRECTIONAL PLANS (NAD 1983) | **MD Reference:** | RKB=25' @ 3786.00ft |
| **Site:** | Tuna Nut 24_13 Fed Com | **North Reference:** | Grid |
| **Well:** | Tuna Nut 24_13 Fed Com 23H | **Survey Calculation Method:** | Minimum Curvature |
| **Wellbore:** | Wellbore #1 | | |
| **Design:** | Permitting Plan | | |

**Planned Survey**

| Measured Depth (ft) | Inclination (°) | Azimuth (°) | Vertical Depth (ft) | +N/-S (ft) | +E/-W (ft) | Vertical Section (ft) | Dogleg Rate (°/100ft) | Build Rate (°/100ft) | Turn Rate (°/100ft) |
|---|---|---|---|---|---|---|---|---|---|
| 5,500.00 | 0.00 | 0.00 | 5,500.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 5,600.00 | 0.00 | 0.00 | 5,600.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 5,700.00 | 0.00 | 0.00 | 5,700.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 5,800.00 | 0.00 | 0.00 | 5,800.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 5,900.00 | 0.00 | 0.00 | 5,900.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6,000.00 | 0.00 | 0.00 | 6,000.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6,100.00 | 0.00 | 0.00 | 6,100.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6,200.00 | 0.00 | 0.00 | 6,200.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6,300.00 | 0.00 | 0.00 | 6,300.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6,400.00 | 0.00 | 0.00 | 6,400.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6,500.00 | 0.00 | 0.00 | 6,500.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6,600.00 | 0.00 | 0.00 | 6,600.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6,700.00 | 0.00 | 0.00 | 6,700.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6,800.00 | 0.00 | 0.00 | 6,800.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6,900.00 | 0.00 | 0.00 | 6,900.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 7,000.00 | 0.00 | 0.00 | 7,000.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 7,100.00 | 0.00 | 0.00 | 7,100.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 7,200.00 | 0.00 | 0.00 | 7,200.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 7,300.00 | 0.00 | 0.00 | 7,300.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 7,400.00 | 0.00 | 0.00 | 7,400.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 7,500.00 | 0.00 | 0.00 | 7,500.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 7,554.00 | 0.00 | 0.00 | 7,554.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| **Build 1°/100'** | | | | | | | | | |
| 7,600.00 | 0.46 | 150.03 | 7,600.00 | -0.16 | 0.09 | -0.16 | 1.00 | 1.00 | 0.00 |
| 7,700.00 | 1.46 | 150.03 | 7,699.98 | -1.61 | 0.93 | -1.60 | 1.00 | 1.00 | 0.00 |
| 7,800.00 | 2.46 | 150.03 | 7,799.92 | -4.57 | 2.64 | -4.53 | 1.00 | 1.00 | 0.00 |
| 7,900.00 | 3.46 | 150.03 | 7,899.79 | -9.05 | 5.22 | -8.96 | 1.00 | 1.00 | 0.00 |
| 8,000.00 | 4.46 | 150.03 | 7,999.55 | -15.03 | 8.67 | -14.88 | 1.00 | 1.00 | 0.00 |
| 8,100.00 | 5.46 | 150.03 | 8,099.17 | -22.52 | 12.99 | -22.30 | 1.00 | 1.00 | 0.00 |
| 8,200.00 | 6.46 | 150.03 | 8,198.63 | -31.51 | 18.18 | -31.20 | 1.00 | 1.00 | 0.00 |
| 8,300.00 | 7.46 | 150.03 | 8,297.89 | -42.01 | 24.23 | -41.59 | 1.00 | 1.00 | 0.00 |
| 8,400.00 | 8.46 | 150.03 | 8,396.93 | -54.01 | 31.15 | -53.47 | 1.00 | 1.00 | 0.00 |
| 8,500.00 | 9.46 | 150.03 | 8,495.71 | -67.50 | 38.93 | -66.83 | 1.00 | 1.00 | 0.00 |
| 8,554.45 | 10.00 | 150.03 | 8,549.38 | -75.47 | 43.53 | -74.73 | 1.00 | 1.00 | 0.00 |
| **Hold 10° Tangent** | | | | | | | | | |
| 8,600.00 | 10.00 | 150.03 | 8,594.23 | -82.32 | 47.48 | -81.51 | 0.00 | 0.00 | 0.00 |
| 8,700.00 | 10.00 | 150.03 | 8,692.71 | -97.37 | 56.16 | -96.41 | 0.00 | 0.00 | 0.00 |
| 8,800.00 | 10.00 | 150.03 | 8,791.19 | -112.42 | 64.84 | -111.31 | 0.00 | 0.00 | 0.00 |
| 8,900.00 | 10.00 | 150.03 | 8,889.67 | -127.47 | 73.52 | -126.21 | 0.00 | 0.00 | 0.00 |
| 9,000.00 | 10.00 | 150.03 | 8,988.15 | -142.52 | 82.20 | -141.11 | 0.00 | 0.00 | 0.00 |
| 9,100.00 | 10.00 | 150.03 | 9,086.63 | -157.57 | 90.88 | -156.01 | 0.00 | 0.00 | 0.00 |
| 9,200.00 | 10.00 | 150.03 | 9,185.11 | -172.62 | 99.56 | -170.91 | 0.00 | 0.00 | 0.00 |
| 9,300.00 | 10.00 | 150.03 | 9,283.59 | -187.67 | 108.24 | -185.81 | 0.00 | 0.00 | 0.00 |
| 9,400.00 | 10.00 | 150.03 | 9,382.07 | -202.72 | 116.92 | -200.71 | 0.00 | 0.00 | 0.00 |
| 9,500.00 | 10.00 | 150.03 | 9,480.55 | -217.77 | 125.60 | -215.61 | 0.00 | 0.00 | 0.00 |
| 9,600.00 | 10.00 | 150.03 | 9,579.03 | -232.81 | 134.28 | -230.51 | 0.00 | 0.00 | 0.00 |
| 9,700.00 | 10.00 | 150.03 | 9,677.50 | -247.86 | 142.96 | -245.41 | 0.00 | 0.00 | 0.00 |
| 9,800.00 | 10.00 | 150.03 | 9,775.98 | -262.91 | 151.64 | -260.31 | 0.00 | 0.00 | 0.00 |
| 9,900.00 | 10.00 | 150.03 | 9,874.46 | -277.96 | 160.32 | -275.22 | 0.00 | 0.00 | 0.00 |
| 10,000.00 | 10.00 | 150.03 | 9,972.94 | -293.01 | 169.00 | -290.12 | 0.00 | 0.00 | 0.00 |
| 10,100.00 | 10.00 | 150.03 | 10,071.42 | -308.06 | 177.68 | -305.02 | 0.00 | 0.00 | 0.00 |
| 10,200.00 | 10.00 | 150.03 | 10,169.90 | -323.11 | 186.36 | -319.92 | 0.00 | 0.00 | 0.00 |
| 10,247.77 | 10.00 | 150.03 | 10,216.94 | -330.30 | 190.50 | -327.03 | 0.00 | 0.00 | 0.00 |
| **KOP, Build & Turn 10°/100'** | | | | | | | | | |
| 10,300.00 | 6.06 | 124.54 | 10,268.67 | -335.79 | 195.04 | -332.45 | 10.00 | -7.55 | -48.79 |

# OXY

## Planning Report

| | | | |
|---|---|---|---|
| **Database:** | HOPSPP | **Local Co-ordinate Reference:** | Well Tuna Nut 24_13 Fed Com 23H |
| **Company:** | ENGINEERING DESIGNS | **TVD Reference:** | RKB=25' @ 3786.00ft |
| **Project:** | PRD NM DIRECTIONAL PLANS (NAD 1983) | **MD Reference:** | RKB=25' @ 3786.00ft |
| **Site:** | Tuna Nut 24_13 Fed Com | **North Reference:** | Grid |
| **Well:** | Tuna Nut 24_13 Fed Com 23H | **Survey Calculation Method:** | Minimum Curvature |
| **Wellbore:** | Wellbore #1 | | |
| **Design:** | Permitting Plan | | |

**Planned Survey**

| Measured Depth (ft) | Inclination (°) | Azimuth (°) | Vertical Depth (ft) | +N/-S (ft) | +E/-W (ft) | Vertical Section (ft) | Dogleg Rate (°/100ft) | Build Rate (°/100ft) | Turn Rate (°/100ft) |
|---|---|---|---|---|---|---|---|---|---|
| 10,400.00 | 8.20 | 36.72 | 10,368.13 | -333.06 | 203.68 | -329.58 | 10.00 | 2.14 | -87.82 |
| 10,500.00 | 17.24 | 15.87 | 10,465.62 | -313.03 | 212.02 | -309.41 | 10.00 | 9.04 | -20.85 |
| 10,600.00 | 26.96 | 9.43 | 10,558.17 | -276.32 | 219.81 | -272.57 | 10.00 | 9.72 | -6.43 |
| 10,700.00 | 36.82 | 6.26 | 10,642.98 | -224.04 | 226.81 | -220.18 | 10.00 | 9.86 | -3.18 |
| 10,800.00 | 46.74 | 4.28 | 10,717.46 | -157.77 | 232.81 | -153.82 | 10.00 | 9.91 | -1.98 |
| 10,900.00 | 56.67 | 2.86 | 10,779.36 | -79.54 | 237.63 | -75.52 | 10.00 | 9.94 | -1.42 |
| 11,000.00 | 66.63 | 1.74 | 10,826.78 | 8.28 | 241.12 | 12.35 | 10.00 | 9.95 | -1.12 |
| 11,100.00 | 76.58 | 0.77 | 10,858.30 | 103.03 | 243.17 | 107.12 | 10.00 | 9.96 | -0.97 |
| 11,200.00 | 86.54 | 359.88 | 10,872.95 | 201.82 | 243.73 | 205.91 | 10.00 | 9.96 | -0.89 |
| 11,234.68 | 90.00 | 359.58 | 10,874.00 | 236.48 | 243.57 | 240.56 | 10.00 | 9.96 | -0.87 |
| **Landing Point** | | | | | | | | | |
| 11,300.00 | 90.00 | 359.58 | 10,874.00 | 301.80 | 243.09 | 305.86 | 0.00 | 0.00 | 0.00 |
| 11,400.00 | 90.00 | 359.58 | 10,874.00 | 401.79 | 242.37 | 405.83 | 0.00 | 0.00 | 0.00 |
| 11,500.00 | 90.00 | 359.58 | 10,874.00 | 501.79 | 241.64 | 505.80 | 0.00 | 0.00 | 0.00 |
| 11,600.00 | 90.00 | 359.58 | 10,874.00 | 601.79 | 240.91 | 605.77 | 0.00 | 0.00 | 0.00 |
| 11,700.00 | 90.00 | 359.58 | 10,874.00 | 701.79 | 240.19 | 705.74 | 0.00 | 0.00 | 0.00 |
| 11,800.00 | 90.00 | 359.58 | 10,874.00 | 801.78 | 239.46 | 805.71 | 0.00 | 0.00 | 0.00 |
| 11,900.00 | 90.00 | 359.58 | 10,874.00 | 901.78 | 238.73 | 905.68 | 0.00 | 0.00 | 0.00 |
| 12,000.00 | 90.00 | 359.58 | 10,874.00 | 1,001.78 | 238.01 | 1,005.65 | 0.00 | 0.00 | 0.00 |
| 12,100.00 | 90.00 | 359.58 | 10,874.00 | 1,101.78 | 237.28 | 1,105.62 | 0.00 | 0.00 | 0.00 |
| 12,200.00 | 90.00 | 359.58 | 10,874.00 | 1,201.77 | 236.55 | 1,205.60 | 0.00 | 0.00 | 0.00 |
| 12,300.00 | 90.00 | 359.58 | 10,874.00 | 1,301.77 | 235.83 | 1,305.57 | 0.00 | 0.00 | 0.00 |
| 12,400.00 | 90.00 | 359.58 | 10,874.00 | 1,401.77 | 235.10 | 1,405.54 | 0.00 | 0.00 | 0.00 |
| 12,500.00 | 90.00 | 359.58 | 10,874.00 | 1,501.77 | 234.37 | 1,505.51 | 0.00 | 0.00 | 0.00 |
| 12,600.00 | 90.00 | 359.58 | 10,874.00 | 1,601.76 | 233.65 | 1,605.48 | 0.00 | 0.00 | 0.00 |
| 12,700.00 | 90.00 | 359.58 | 10,874.00 | 1,701.76 | 232.92 | 1,705.45 | 0.00 | 0.00 | 0.00 |
| 12,800.00 | 90.00 | 359.58 | 10,874.00 | 1,801.76 | 232.19 | 1,805.42 | 0.00 | 0.00 | 0.00 |
| 12,900.00 | 90.00 | 359.58 | 10,874.00 | 1,901.75 | 231.47 | 1,905.39 | 0.00 | 0.00 | 0.00 |
| 13,000.00 | 90.00 | 359.58 | 10,874.00 | 2,001.75 | 230.74 | 2,005.36 | 0.00 | 0.00 | 0.00 |
| 13,100.00 | 90.00 | 359.58 | 10,874.00 | 2,101.75 | 230.01 | 2,105.33 | 0.00 | 0.00 | 0.00 |
| 13,200.00 | 90.00 | 359.58 | 10,874.00 | 2,201.75 | 229.29 | 2,205.30 | 0.00 | 0.00 | 0.00 |
| 13,251.25 | 90.00 | 359.58 | 10,874.00 | 2,253.00 | 228.91 | 2,256.54 | 0.00 | 0.00 | 0.00 |
| **PPP-1 Cross** | | | | | | | | | |
| 13,300.00 | 90.00 | 359.58 | 10,874.00 | 2,301.74 | 228.56 | 2,305.27 | 0.00 | 0.00 | 0.00 |
| 13,400.00 | 90.00 | 359.58 | 10,874.00 | 2,401.74 | 227.83 | 2,405.25 | 0.00 | 0.00 | 0.00 |
| 13,500.00 | 90.00 | 359.58 | 10,874.00 | 2,501.74 | 227.11 | 2,505.22 | 0.00 | 0.00 | 0.00 |
| 13,600.00 | 90.00 | 359.58 | 10,874.00 | 2,601.74 | 226.38 | 2,605.19 | 0.00 | 0.00 | 0.00 |
| 13,700.00 | 90.00 | 359.58 | 10,874.00 | 2,701.73 | 225.65 | 2,705.16 | 0.00 | 0.00 | 0.00 |
| 13,800.00 | 90.00 | 359.58 | 10,874.00 | 2,801.73 | 224.93 | 2,805.13 | 0.00 | 0.00 | 0.00 |
| 13,900.00 | 90.00 | 359.58 | 10,874.00 | 2,901.73 | 224.20 | 2,905.10 | 0.00 | 0.00 | 0.00 |
| 14,000.00 | 90.00 | 359.58 | 10,874.00 | 3,001.73 | 223.47 | 3,005.07 | 0.00 | 0.00 | 0.00 |
| 14,100.00 | 90.00 | 359.58 | 10,874.00 | 3,101.72 | 222.75 | 3,105.04 | 0.00 | 0.00 | 0.00 |
| 14,200.00 | 90.00 | 359.58 | 10,874.00 | 3,201.72 | 222.02 | 3,205.01 | 0.00 | 0.00 | 0.00 |
| 14,300.00 | 90.00 | 359.58 | 10,874.00 | 3,301.72 | 221.29 | 3,304.98 | 0.00 | 0.00 | 0.00 |
| 14,400.00 | 90.00 | 359.58 | 10,874.00 | 3,401.72 | 220.57 | 3,404.95 | 0.00 | 0.00 | 0.00 |
| 14,500.00 | 90.00 | 359.58 | 10,874.00 | 3,501.71 | 219.84 | 3,504.93 | 0.00 | 0.00 | 0.00 |
| 14,600.00 | 90.00 | 359.58 | 10,874.00 | 3,601.71 | 219.11 | 3,604.90 | 0.00 | 0.00 | 0.00 |
| 14,700.00 | 90.00 | 359.58 | 10,874.00 | 3,701.71 | 218.39 | 3,704.87 | 0.00 | 0.00 | 0.00 |
| 14,800.00 | 90.00 | 359.58 | 10,874.00 | 3,801.70 | 217.66 | 3,804.84 | 0.00 | 0.00 | 0.00 |
| 14,900.00 | 90.00 | 359.58 | 10,874.00 | 3,901.70 | 216.93 | 3,904.81 | 0.00 | 0.00 | 0.00 |
| 15,000.00 | 90.00 | 359.58 | 10,874.00 | 4,001.70 | 216.21 | 4,004.78 | 0.00 | 0.00 | 0.00 |
| 15,100.00 | 90.00 | 359.58 | 10,874.00 | 4,101.70 | 215.48 | 4,104.75 | 0.00 | 0.00 | 0.00 |
| 15,200.00 | 90.00 | 359.58 | 10,874.00 | 4,201.69 | 214.75 | 4,204.72 | 0.00 | 0.00 | 0.00 |
| 15,300.00 | 90.00 | 359.58 | 10,874.00 | 4,301.69 | 214.03 | 4,304.69 | 0.00 | 0.00 | 0.00 |
| 15,400.00 | 90.00 | 359.58 | 10,874.00 | 4,401.69 | 213.30 | 4,404.66 | 0.00 | 0.00 | 0.00 |

# OXY
## Planning Report

| | | | |
|---|---|---|---|
| **Database:** | HOPSPP | **Local Co-ordinate Reference:** | Well Tuna Nut 24_13 Fed Com 23H |
| **Company:** | ENGINEERING DESIGNS | **TVD Reference:** | RKB=25' @ 3786.00ft |
| **Project:** | PRD NM DIRECTIONAL PLANS (NAD 1983) | **MD Reference:** | RKB=25' @ 3786.00ft |
| **Site:** | Tuna Nut 24_13 Fed Com | **North Reference:** | Grid |
| **Well:** | Tuna Nut 24_13 Fed Com 23H | **Survey Calculation Method:** | Minimum Curvature |
| **Wellbore:** | Wellbore #1 | | |
| **Design:** | Permitting Plan | | |

**Planned Survey**

| Measured Depth (ft) | Inclination (°) | Azimuth (°) | Vertical Depth (ft) | +N/-S (ft) | +E/-W (ft) | Vertical Section (ft) | Dogleg Rate (°/100ft) | Build Rate (°/100ft) | Turn Rate (°/100ft) |
|---|---|---|---|---|---|---|---|---|---|
| 15,500.00 | 90.00 | 359.58 | 10,874.00 | 4,501.69 | 212.57 | 4,504.63 | 0.00 | 0.00 | 0.00 |
| 15,600.00 | 90.00 | 359.58 | 10,874.00 | 4,601.68 | 211.85 | 4,604.60 | 0.00 | 0.00 | 0.00 |
| 15,700.00 | 90.00 | 359.58 | 10,874.00 | 4,701.68 | 211.12 | 4,704.58 | 0.00 | 0.00 | 0.00 |
| 15,800.00 | 90.00 | 359.58 | 10,874.00 | 4,801.68 | 210.39 | 4,804.55 | 0.00 | 0.00 | 0.00 |
| 15,891.32 | 90.00 | 359.58 | 10,874.00 | 4,893.00 | 209.73 | 4,895.84 | 0.00 | 0.00 | 0.00 |
| **PPP-2 Cross** | | | | | | | | | |
| 15,900.00 | 90.00 | 359.58 | 10,874.00 | 4,901.68 | 209.67 | 4,904.52 | 0.00 | 0.00 | 0.00 |
| 16,000.00 | 90.00 | 359.58 | 10,874.00 | 5,001.67 | 208.94 | 5,004.49 | 0.00 | 0.00 | 0.00 |
| 16,100.00 | 90.00 | 359.58 | 10,874.00 | 5,101.67 | 208.21 | 5,104.46 | 0.00 | 0.00 | 0.00 |
| 16,200.00 | 90.00 | 359.58 | 10,874.00 | 5,201.67 | 207.49 | 5,204.43 | 0.00 | 0.00 | 0.00 |
| 16,300.00 | 90.00 | 359.58 | 10,874.00 | 5,301.67 | 206.76 | 5,304.40 | 0.00 | 0.00 | 0.00 |
| 16,400.00 | 90.00 | 359.58 | 10,874.00 | 5,401.66 | 206.03 | 5,404.37 | 0.00 | 0.00 | 0.00 |
| 16,500.00 | 90.00 | 359.58 | 10,874.00 | 5,501.66 | 205.31 | 5,504.34 | 0.00 | 0.00 | 0.00 |
| 16,600.00 | 90.00 | 359.58 | 10,874.00 | 5,601.66 | 204.58 | 5,604.31 | 0.00 | 0.00 | 0.00 |
| 16,700.00 | 90.00 | 359.58 | 10,874.00 | 5,701.65 | 203.85 | 5,704.28 | 0.00 | 0.00 | 0.00 |
| 16,800.00 | 90.00 | 359.58 | 10,874.00 | 5,801.65 | 203.13 | 5,804.25 | 0.00 | 0.00 | 0.00 |
| 16,900.00 | 90.00 | 359.58 | 10,874.00 | 5,901.65 | 202.40 | 5,904.23 | 0.00 | 0.00 | 0.00 |
| 17,000.00 | 90.00 | 359.58 | 10,874.00 | 6,001.65 | 201.68 | 6,004.20 | 0.00 | 0.00 | 0.00 |
| 17,100.00 | 90.00 | 359.58 | 10,874.00 | 6,101.64 | 200.95 | 6,104.17 | 0.00 | 0.00 | 0.00 |
| 17,200.00 | 90.00 | 359.58 | 10,874.00 | 6,201.64 | 200.22 | 6,204.14 | 0.00 | 0.00 | 0.00 |
| 17,300.00 | 90.00 | 359.58 | 10,874.00 | 6,301.64 | 199.50 | 6,304.11 | 0.00 | 0.00 | 0.00 |
| 17,400.00 | 90.00 | 359.58 | 10,874.00 | 6,401.64 | 198.77 | 6,404.08 | 0.00 | 0.00 | 0.00 |
| 17,500.00 | 90.00 | 359.58 | 10,874.00 | 6,501.63 | 198.04 | 6,504.05 | 0.00 | 0.00 | 0.00 |
| 17,600.00 | 90.00 | 359.58 | 10,874.00 | 6,601.63 | 197.32 | 6,604.02 | 0.00 | 0.00 | 0.00 |
| 17,700.00 | 90.00 | 359.58 | 10,874.00 | 6,701.63 | 196.59 | 6,703.99 | 0.00 | 0.00 | 0.00 |
| 17,800.00 | 90.00 | 359.58 | 10,874.00 | 6,801.63 | 195.86 | 6,803.96 | 0.00 | 0.00 | 0.00 |
| 17,900.00 | 90.00 | 359.58 | 10,874.00 | 6,901.62 | 195.14 | 6,903.93 | 0.00 | 0.00 | 0.00 |
| 18,000.00 | 90.00 | 359.58 | 10,874.00 | 7,001.62 | 194.41 | 7,003.90 | 0.00 | 0.00 | 0.00 |
| 18,100.00 | 90.00 | 359.58 | 10,874.00 | 7,101.62 | 193.68 | 7,103.88 | 0.00 | 0.00 | 0.00 |
| 18,200.00 | 90.00 | 359.58 | 10,874.00 | 7,201.62 | 192.96 | 7,203.85 | 0.00 | 0.00 | 0.00 |
| 18,300.00 | 90.00 | 359.58 | 10,874.00 | 7,301.61 | 192.23 | 7,303.82 | 0.00 | 0.00 | 0.00 |
| 18,400.00 | 90.00 | 359.58 | 10,874.00 | 7,401.61 | 191.50 | 7,403.79 | 0.00 | 0.00 | 0.00 |
| 18,500.00 | 90.00 | 359.58 | 10,874.00 | 7,501.61 | 190.78 | 7,503.76 | 0.00 | 0.00 | 0.00 |
| 18,600.00 | 90.00 | 359.58 | 10,874.00 | 7,601.60 | 190.05 | 7,603.73 | 0.00 | 0.00 | 0.00 |
| 18,700.00 | 90.00 | 359.58 | 10,874.00 | 7,701.60 | 189.32 | 7,703.70 | 0.00 | 0.00 | 0.00 |
| 18,800.00 | 90.00 | 359.58 | 10,874.00 | 7,801.60 | 188.60 | 7,803.67 | 0.00 | 0.00 | 0.00 |
| 18,900.00 | 90.00 | 359.58 | 10,874.00 | 7,901.60 | 187.87 | 7,903.64 | 0.00 | 0.00 | 0.00 |
| 19,000.00 | 90.00 | 359.58 | 10,874.00 | 8,001.59 | 187.14 | 8,003.61 | 0.00 | 0.00 | 0.00 |
| 19,100.00 | 90.00 | 359.58 | 10,874.00 | 8,101.59 | 186.42 | 8,103.58 | 0.00 | 0.00 | 0.00 |
| 19,200.00 | 90.00 | 359.58 | 10,874.00 | 8,201.59 | 185.69 | 8,203.55 | 0.00 | 0.00 | 0.00 |
| 19,300.00 | 90.00 | 359.58 | 10,874.00 | 8,301.59 | 184.96 | 8,303.53 | 0.00 | 0.00 | 0.00 |
| 19,400.00 | 90.00 | 359.58 | 10,874.00 | 8,401.58 | 184.24 | 8,403.50 | 0.00 | 0.00 | 0.00 |
| 19,500.00 | 90.00 | 359.58 | 10,874.00 | 8,501.58 | 183.51 | 8,503.47 | 0.00 | 0.00 | 0.00 |
| 19,600.00 | 90.00 | 359.58 | 10,874.00 | 8,601.58 | 182.78 | 8,603.44 | 0.00 | 0.00 | 0.00 |
| 19,700.00 | 90.00 | 359.58 | 10,874.00 | 8,701.58 | 182.06 | 8,703.41 | 0.00 | 0.00 | 0.00 |
| 19,800.00 | 90.00 | 359.58 | 10,874.00 | 8,801.57 | 181.33 | 8,803.38 | 0.00 | 0.00 | 0.00 |
| 19,900.00 | 90.00 | 359.58 | 10,874.00 | 8,901.57 | 180.60 | 8,903.35 | 0.00 | 0.00 | 0.00 |
| 20,000.00 | 90.00 | 359.58 | 10,874.00 | 9,001.57 | 179.88 | 9,003.32 | 0.00 | 0.00 | 0.00 |
| 20,100.00 | 90.00 | 359.58 | 10,874.00 | 9,101.56 | 179.15 | 9,103.29 | 0.00 | 0.00 | 0.00 |
| 20,200.00 | 90.00 | 359.58 | 10,874.00 | 9,201.56 | 178.42 | 9,203.26 | 0.00 | 0.00 | 0.00 |
| 20,300.00 | 90.00 | 359.58 | 10,874.00 | 9,301.56 | 177.70 | 9,303.23 | 0.00 | 0.00 | 0.00 |
| 20,400.00 | 90.00 | 359.58 | 10,874.00 | 9,401.56 | 176.97 | 9,403.20 | 0.00 | 0.00 | 0.00 |
| 20,500.00 | 90.00 | 359.58 | 10,874.00 | 9,501.55 | 176.24 | 9,503.18 | 0.00 | 0.00 | 0.00 |
| 20,600.00 | 90.00 | 359.58 | 10,874.00 | 9,601.55 | 175.52 | 9,603.15 | 0.00 | 0.00 | 0.00 |
| 20,700.00 | 90.00 | 359.58 | 10,874.00 | 9,701.55 | 174.79 | 9,703.12 | 0.00 | 0.00 | 0.00 |

# OXY
## Planning Report

| | | | |
|---|---|---|---|
| **Database:** | HOPSPP | **Local Co-ordinate Reference:** | Well Tuna Nut 24_13 Fed Com 23H |
| **Company:** | ENGINEERING DESIGNS | **TVD Reference:** | RKB=25' @ 3786.00ft |
| **Project:** | PRD NM DIRECTIONAL PLANS (NAD 1983) | **MD Reference:** | RKB=25' @ 3786.00ft |
| **Site:** | Tuna Nut 24_13 Fed Com | **North Reference:** | Grid |
| **Well:** | Tuna Nut 24_13 Fed Com 23H | **Survey Calculation Method:** | Minimum Curvature |
| **Wellbore:** | Wellbore #1 | | |
| **Design:** | Permitting Plan | | |

**Planned Survey**

| Measured Depth (ft) | Inclination (°) | Azimuth (°) | Vertical Depth (ft) | +N/-S (ft) | +E/-W (ft) | Vertical Section (ft) | Dogleg Rate (°/100ft) | Build Rate (°/100ft) | Turn Rate (°/100ft) |
|---|---|---|---|---|---|---|---|---|---|
| 20,800.00 | 90.00 | 359.58 | 10,874.00 | 9,801.55 | 174.06 | 9,803.09 | 0.00 | 0.00 | 0.00 |
| 20,900.00 | 90.00 | 359.58 | 10,874.00 | 9,901.54 | 173.34 | 9,903.06 | 0.00 | 0.00 | 0.00 |
| 21,000.00 | 90.00 | 359.58 | 10,874.00 | 10,001.54 | 172.61 | 10,003.03 | 0.00 | 0.00 | 0.00 |
| 21,100.00 | 90.00 | 359.58 | 10,874.00 | 10,101.54 | 171.88 | 10,103.00 | 0.00 | 0.00 | 0.00 |
| 21,154.68 | 90.00 | 359.58 | 10,874.00 | 10,156.22 | 171.49 | 10,157.67 | 0.00 | 0.00 | 0.00 |
| **TD at 21154.68' MD** | | | | | | | | | |

**Design Targets**

| Target Name - hit/miss target - Shape | Dip Angle (°) | Dip Dir. (°) | TVD (ft) | +N/-S (ft) | +E/-W (ft) | Northing (usft) | Easting (usft) | Latitude | Longitude |
|---|---|---|---|---|---|---|---|---|---|
| KOP (Tuna Nut 24_13 | 0.00 | 0.00 | 0.00 | -336.94 | 247.73 | 499,114.78 | 757,752.23 | 32.370188 | -103.632371 |
| - plan misses target center by 418.21ft at 0.00ft MD (0.00 TVD, 0.00 N, 0.00 E) | | | | | | | | | |
| - Point | | | | | | | | | |
| PBHL (Tuna Nut | 0.00 | 0.00 | 10,874.00 | 10,156.22 | 171.49 | 509,607.53 | 757,675.99 | 32.399030 | -103.632395 |
| - plan hits target center | | | | | | | | | |
| - Point | | | | | | | | | |
| FTP (Tuna Nut 24_13 | 0.00 | 0.00 | 10,874.00 | -286.95 | 247.37 | 499,164.77 | 757,751.87 | 32.370325 | -103.632371 |
| - plan misses target center by 203.48ft at 10800.00ft MD (10717.46 TVD, -157.77 N, 232.81 E) | | | | | | | | | |
| - Point | | | | | | | | | |

**Formations**

| Measured Depth (ft) | Vertical Depth (ft) | Name | Lithology | Dip (°) | Dip Direction (°) |
|---|---|---|---|---|---|
| 1,027.00 | 1,027.00 | RUSTLER | | | |
| 1,686.00 | 1,686.00 | SALADO | | | |
| 3,478.00 | 3,478.00 | CASTILE | | | |
| 4,898.00 | 4,898.00 | DELAWARE | | | |
| 4,989.00 | 4,989.00 | BELL CANYON | | | |
| 5,786.00 | 5,786.00 | CHERRY CANYON | | | |
| 7,093.00 | 7,093.00 | BRUSHY CANYON | | | |
| 8,740.91 | 8,733.00 | BONE SPRING | | | |
| 9,862.97 | 9,838.00 | BONE SPRING 1ST | | | |
| 10,562.25 | 10,524.00 | BONE SPRING 2ND | | | |

**Plan Annotations**

| Measured Depth (ft) | Vertical Depth (ft) | Local Coordinates +N/-S (ft) | Local Coordinates +E/-W (ft) | Comment |
|---|---|---|---|---|
| 7,554.00 | 7,554.00 | 0.00 | 0.00 | Build 1°/100' |
| 8,554.45 | 8,549.38 | -75.47 | 43.53 | Hold 10° Tangent |
| 10,247.77 | 10,216.94 | -330.30 | 190.50 | KOP, Build & Turn 10°/100' |
| 11,234.68 | 10,874.00 | 236.48 | 243.57 | Landing Point |
| 13,251.25 | 10,874.00 | 2,253.00 | 228.91 | PPP-1 Cross |
| 15,891.32 | 10,874.00 | 4,893.00 | 209.73 | PPP-2 Cross |
| 21,154.68 | 10,874.00 | 10,156.22 | 171.49 | TD at 21154.68' MD |

# Oxy USA Inc. - Blanket Design Pad Document

## OXY - Blanket Design A

**Pad Name:** REDTNK_T22SR32E_24_01

**SHL:** 390' FSL 1095' FWL, Sec 24, T22S-R32E

Oxy requests for the bellow wells to be approved for the two designs listed in the Blanket Design document **(Blanket Design A –OXY –3S Slim v7.2.)** The MDs and TVDs for all intervals are within the boundary conditions. The max inclination and DLS are also within the boundary conditions (directional plans attached separately for review.)

### 1. Blanket Design - Wells

| Well Name | APD # | Surface | | Intermediate | | Production | |
|---|---|---|---|---|---|---|---|
| | | MD | TVD | MD | TVD | MD | TVD |
| TUNA NUT 24_13 FED COM 22H | 10400093225 | 1090 | 1090 | 10226 | 10163 | 21193 | 10874 |
| TUNA NUT 24_13 FED COM 23H | 10400093266 | 1087 | 1087 | 10148 | 10117 | 21155 | 10874 |
| TUNA NUT 24_13 FED COM 171H | 10400097316 | 1090 | 1090 | 10631 | 10592 | 21621 | 11330 |
| TUNA NUT 24_13 FED COM 172H | 10400097320 | 1085 | 1085 | 10676 | 10617 | 21644 | 11330 |
| | | | | | | | |
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### 2. Review Criteria Table

| | Y or N |
|---|---|
| Is casing new? If used, attach certification as required in 43 CFR 3160 | Y |
| Does casing meet API specifications? If no, attach casing specification sheet. | Y |
| Is premium or uncommon casing planned? If yes attach casing specification sheet. | Y |
| Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria). | Y |
| Will the intermediate pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing? | Y |
| | |
| Is well located within Capitan Reef? | N |
| If yes, does production casing cement tie back a minimum of 50' above the Reef? | |
| Is well within the designated 4 string boundary. | |
| | |
| Is well located in SOPA but not in R-111-Q? | N |
| If yes, are the first 2 strings cemented to surface and 3rd string cement tied back 500' into previous casing? | |
| | |
| Is well located in R-111-Q and SOPA? | N |
| If yes, are the first three strings cemented to surface? | |
| Is 2nd string set 100' to 600' below the base of salt? | |
| | |
| Is well located in high Cave/Karst? | N |
| If yes, are there two strings cemented to surface? | |
| (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs? | |
| | |
| Is well located in critical Cave/Karst? | N |
| If yes, are there three strings cemented to surface? | |

## 3. Geologic Formations

| Formation | MD-RKB (ft) | TVD-RKB (ft) | Expected Fluids |
|---|---|---|---|
| Rustler | 1030 | 1030 | |
| Salado | 1665 | 1665 | Salt |
| Castile | 3438 | 3438 | Salt |
| Delaware | 4875 | 4875 | Oil/Gas/Brine |
| Bell Canyon | 4969 | 4969 | Oil/Gas/Brine |
| Cherry Canyon | 5781 | 5781 | Oil/Gas/Brine |
| Brushy Canyon | 7094 | 7080 | Losses |
| Bone Spring | 8756 | 8717 | Oil/Gas |
| Bone Spring 1st | 9879 | 9823 | Oil/Gas |
| Bone Spring 2nd | 10580 | 10509 | Oil/Gas |
| Bone Spring 3rd | | | Oil/Gas |
| Wolfcamp | | | Oil/Gas |
| Penn | | | Oil/Gas |
| Strawn | | | Oil/Gas |

## 4. Cementing Program

| Section | Stage | Slurry: | Sacks | Yield (ft^3/ft) | Density (lb/gal) | Excess: | TOC | Placement | Description |
|---|---|---|---|---|---|---|---|---|---|
| Surface | 1 | Surface - Tail | 1139 | 1.33 | 14.8 | 100% | - | Circulate | Class C+Accel. |
| Int. | 1 | Intermediate 1S - Tail | 387 | 1.68 | 13.2 | 5% | 7,344 | Circulate | Class C+Ret., Disper. |
| Int. | 2 | Intermediate 2S - Tail BH | 1333 | 1.71 | 13.3 | 25% | - | Bradenhead | Class C+Accel. |
| Prod. | 1 | Production - Tail | 649 | 1.84 | 13.3 | 25% | 9,726 | Circulate | Class C+Ret. |

# Oxy Blanket Design - Casing Design "A"

## 1. Casing Program

**The designs and associated details listed in this document are the "worst case scenario" boundaries for design safety factors.**

**Location and lithology have NOT been accounted for in these designs; however, the designs are NOT valid for wells within KPLA Boundaries or Capitan Reef areas. The specific well details will be based on the APD/Sundry package and the information listed in the COA.**

**The mud program listed below will remain the same between each design variation.**

**Hole will be full during casing run for well control and tensile SF.**

**Casing will be kept at least half full during run for these designs to meet BLM collapse SF requirement.**

### Design Variation "A1"

| | | MD | | TVD | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| Section | Hole Size (in) | From (ft) | To (ft) | From (ft) | To (ft) | Csg. OD (in) | Csg Wt. (ppf) | Grade | Conn. |
| Surface | 14.75 | 0 | 1200 | 0 | 1200 | 10.75 | 45.5 | J-55 | BTC |
| Intermediate | 9.875 | 0 | 13111* | 0 | 12775* | 7.625 | 26.4 | L-80 HC | BTC Axis HT GBCD |
| Production | 6.75 | 0 | 23361 | 0 | 12775 | 5.5 | 20 | P-110 | Wedge 461 Sprint SF DWC/C-HT-IS |

*Curve could be in intermediate or production section

### Design Variation "A2" - Option to Pivot to Design "B" for Contingency 4S

| | | MD | | TVD | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| Section | Hole Size (in) | From (ft) | To (ft) | From (ft) | To (ft) | Csg. OD (in) | Csg Wt. (ppf) | Grade | Conn. |
| Surface | 17.5 | 0 | 1200 | 0 | 1200 | 13.375 | 54.5 | J-55 | BTC |
| Intermediate | 12.25† | 0 | 13111* | 0 | 12775* | 7.625 | 26.4 | L-80 HC | BTC Axis HT GBCD |
| Production | 6.75 | 0 | 23361 | 0 | 12775 | 5.5 | 20 | P-110 | Wedge 461 Sprint SF DWC/C-HT-IS |

*Curve could be in intermediate or production section

†If 4S Contingency is not required, Oxy requests permission to transition from 12.25" to 9.875" Intermediate at some point during the hole section. Cement volumes will be updated on C103 submission.

All casing strings will be tested in accordance with 43 CFR part 3170 Subpart 3172

# Oxy Blanket Design - Casing Design "A"

| *All Casing SF Values will meet or exceed those below* | | | |
|---|---|---|---|
| **SF Collapse** | **SF Burst** | **Body SF Tension** | **Joint SF Tension** |
| 1.00 | 1.100 | 1.4 | 1.4 |

**§Annular Clearance Variance Request**

As per the agreement reached in the Oxy/BLM face-to-face meeting on Feb 22, 2018, Oxy requests permission to allow deviation from the 0.422" annular clearance requirement. Please see Annular Clearance Variance attachment for further details.

§Annular Clearance Variance Request may not apply to all connections used or presented.

## 2. Trajectory / Boundary Conditions

| | MD | | TVD | | | |
|---|---|---|---|---|---|---|
| **Section** | **Deepest KOP (ft)** | **End Build (ft)** | **Deepest KOP (ft)** | **End Build (ft)** | **Max. Angle** | **Max. Planned DLS** |
| Surface | 0 | 1200 | 0 | 1200 | 5° | 1°/100 ft |
| Intermediate | 5000 (inside Cherry Canyon) | 6500 | 4980 | 6390 | 20° | 2°/100 ft |
| | 12211 | 13111 | 12202 | 12775 | 92° ‡ | 12°/100 ft ‡ |
| Production | 12211 (~100' MD past ICP) | 13111 | 12202 | 12775 | 92° ‡ | 12°/100 ft ‡ |

‡ Applies only when intermediate casing depth is deepened to landing point to match TVD of production in some areas where required to accommodate higher MWs in depleted areas.

Oxy has reviewed casing burst, collapse, and axial loadcases in Landmark StressCheck with the boundary conditions in the table above which satisfies Oxy and BLM minimum design criteria. Triaxial plots for each casing string is shown in Section 7 and intermediate load case inputs are shown in Section 8.

# Oxy Blanket Design - Casing Design "A"

## 3. Cementing Program

NOTE: Blanket design is for technical review only. The cement volumes will be adjusted to ensure cement tops meet BLM requirements.

### Design Variation "A1"

| Section | Stage | Slurry: | Sacks | Yield (ft^3/ft) | Density (lb/gal) | Excess: | TOC | Placement | Description |
|---|---|---|---|---|---|---|---|---|---|
| Surface | 1 | Surface - Tail | 819 | 1.33 | 14.8 | 100% | - | Circulate | Class C+Accel. |
| Int. | 1 | Intermediate 1S - Tail | 658 | 1.68 | 13.2 | 5% | 7,206 | Circulate | Class C+Ret., Disper. |
| Int. | 2 | Intermediate 2S - Tail BH | 1111 | 1.71 | 13.3 | 25% | - | Bradenhead | Class C+Accel. |
| Prod. | 1 | Production - Tail | 665 | 1.84 | 13.3 | 25% | 11,611 | Circulate | Class C+Ret. |
| Prod. | 2* | Production - Tail BH* | TBD | 1.84 | 13.3 | 50% | 500' inside prev csg | Circulate | Class C+Ret. |

**Only applies in scenario where planned single stage job TOC is not 500' above previous shoe as designed/programmed requiring bradenhead 2nd stage to meet requirements*

### Design Variation "A2"

| Section | Stage | Slurry: | Sacks | Yield (ft^3/ft) | Density (lb/gal) | Excess: | TOC | Placement | Description |
|---|---|---|---|---|---|---|---|---|---|
| Surface | 1 | Surface - Tail | 1023 | 1.33 | 14.8 | 100% | - | Circulate | Class C+Accel. |
| Int. | 1 | Intermediate 1S - Tail | 658 | 1.68 | 13.2 | 5% | 7,206 | Circulate | Class C+Ret., Disper. |
| Int. | 2 | Intermediate 2S - Tail BH | 1293 | 1.71 | 13.3 | 25% | - | Bradenhead | Class C+Accel. |
| Prod. | 1 | Production - Tail | 665 | 1.84 | 13.3 | 25% | 11,611 | Circulate | Class C+Ret. |
| Prod. | 2* | Production - Tail BH* | TBD | 1.84 | 13.3 | 50% | 500' inside prev csg | Circulate | Class C+Ret. |

**Only applies in scenario where planned single stage job TOC is not 500' above previous shoe as designed/programmed requiring bradenhead 2nd stage to meet requirements*

As Reviewed and Approved by BLM on Feb 8, 2024: Oxy uses a Class C / Pozzolan mix on its production cement slurry, which has the same fluid properties as Class H, and has been pilot and field blend tested to have as good or better compressive strength development at our target densities.

**Offline Cementing Request**

Oxy requests a variance to cement the 9.625" and/or 7.625" intermediate casing strings offline in accordance to the approved variance, EC Tran 461365. Please see Offline Cementing Variance attachment for further details.

**Bradenhead CBL Request**

Oxy requests permission to adjust the CBL requirement after bradenhead cement jobs, on 7-5/8" intermediate casings, as per the agreement reached in the OXY/BLM meeting on September 5, 2019. Please see Bradenhead CBL Variance attachment for further details.

# Oxy Blanket Design - Casing Design "A"

## 4. Pressure Control Equipment

| BOP installed and tested before drilling which hole? | Size? | Min. Required WP | Type | ✓ | Tested to: | Deepest TVD Depth (ft) per Section: |
|---|---|---|---|---|---|---|
| 9.875" Hole | 13-5/8" | 5M | Annular | ✓ | 70% of working pressure | 12775** |
| | | 5M | Blind Ram | ✓ | 250 psi / 5000 psi | |
| | | | Pipe Ram | | | |
| | | | Double Ram | ✓ | | |
| | | | Other* | | | |
| 6.75" Hole | 13-5/8" | 5M | Annular | ✓ | 100% of working pressure | 12775 |
| | | 10M | Blind Ram | ✓ | 250 psi / 10000 psi | |
| | | | Pipe Ram | | | |
| | | | Double Ram | ✓ | | |
| | | | Other* | | | |

*Specify if additional ram is utilized
**Curve could be in intermediate or production section

BOP/BOPE will be tested by an independent service company to 250 psi low and the high pressure indicated above per 43 CFR part 3170 Subpart 3172 requirements. The System may be upgraded to a higher pressure but still tested to the working pressure listed in the table above. If the system is upgraded all the components installed will be functional and tested.

Pipe rams will be operationally checked each 24 hour period. Blind rams will be operationally checked on each trip out of the hole. These checks will be noted on the daily tour sheets. Other accessories to the BOP equipment will include a Kelly cock and floor safety valve (inside BOP) and choke lines and choke manifold. See attached schematics.

**5M Annular BOP Request**

Per BLM's Memorandum No. NM-2017-008: *Decision and Rationale for a Variance Allowing the Use of a 5M Annular Preventer with a 10M BOP Stack*, Oxy requests to employ a 5M annular with a 10M BOPE stack in the pilot and lateral sections of the well and will ensure that two barriers to flow are

# Oxy Blanket Design - Casing Design "A"

| |
|---|
| Formation integrity test will be performed per 43 CFR part 3170 Subpart 3172. |
| On Exploratory wells or on that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Will be tested in accordance with 43 CFR part 3170 Subpart 3172. |

| | |
|---|---|
| A variance is requested for the use of a flexible choke line from the BOP to Choke Manifold. Coflex hoses are in compliance with API 16C and meets inspection and testing requirements. See attached for specs and hydrostatic test chart. | |
| Y | Are anchors required by manufacturer? |

A multibowl or a unionized multibowl wellhead system will be employed. The wellhead and connection to the BOPE will meet all API 6A requirements. The BOP will be tested per 43 CFR part 3170 Subpart 3172 after installation on the surface casing which will cover testing requirements for a maximum of 30 days. If any seal subject to test pressure is broken the system must be tested. We will test the flange connection of the wellhead with a test port that is directly in the flange. We are proposing that we will run the wellhead through the rotary prior to cementing surface casing as discussed with the BLM on October 8, 2015.

See attached Schematics.

**BOP Break Testing Request**

Oxy requests permission to adjust the BOP break testing requirements as per the agreement reached in the OXY/BLM meeting on September 5, 2019. Please see BOP Break Testing Variance attachment for further details.

**Hammer Union Variance**

Oxy requests permission for hammer unions behind the choke to be routed to the gas buster. The hammer unions will not be subject to wellbore pressure in compliance with API STD 53.

**Oxy will use Cameron ADAPT wellhead system that uses an OEC top flange connection. This connection has been fully vetted and verified by API to Spec 6A and carries an API monogram.**

# Oxy Blanket Design - Casing Design "A"

## 5. Mud Program & Drilling Conditions

| Section | Depth - MD | | Depth - TVD | | Type | Weight (ppg) | Viscosity | Water Loss |
|---|---|---|---|---|---|---|---|---|
| | From (ft) | To (ft) | From (ft) | To (ft) | | | | |
| Surface | 0 | 1200 | 0 | 1200 | Water-Based Mud | 8.6 - 8.8 | 40-60 | N/C |
| Intermediate | 1200 | 13111* | 1200 | 12775* | Saturated Brine-Based or Oil-Based Mud | 8.0 - 10.0 | 35-45 | N/C |
| Production | 13111 | 23361 | 12775 | 12775 | Water-Based or Oil-Based Mud | 9.5 - 13.5 | 38-50 | N/C |

*Curve could be in intermediate or production section*

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times. The following is a general list of products: Barite, Bentonite, Gypsum, Lime, Soda Ash, Caustic Soda, Nut Plug, Cedar Fiber, Cotton Seed Hulls, Drilling Paper, Salt Water Clay, CACL2. Oxy will use a closed mud system.

### Drilling Blind Request

In the event total losses are encountered in the intermediate section, Oxy requests permission to drill blind due to depleted formations where risk of hydrocarbon kicks are unlikely.

- Oxy will first attempt to cure losses before proceeding with drilling blind
- Drilling blind will only be allowed in the Castille and formations below
- While drilling blind, will monitor backside by filling-up on connections and utilize gas monitors
- Depths at which losses occurred and attempt to cure losses with relevant details (LCM sweep info, etc.) will be documented in the drillers log and Subsequent Reports to the BLM.
- If a well control event (hydrocarbon kick) occurs while drilling blind, the BLM will be notified after the well is secured and returned to static.

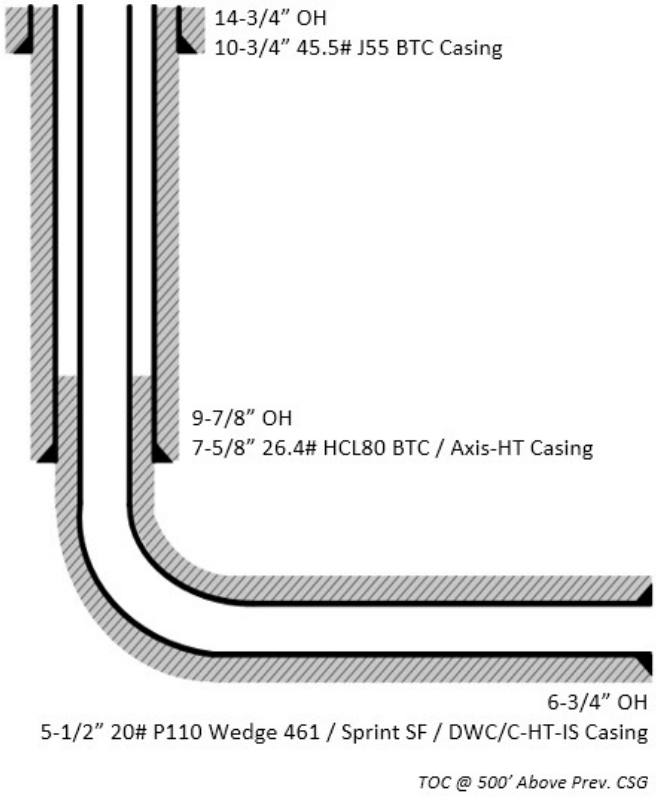
| | |
|---|---|
| What will be used to monitor the loss or gain of fluid? | PVT/MD Totco/Visual Monitoring |

Pump high viscosity sweeps as needed for hole cleaning. The mud system will be monitored visually/manually as well as with an electronic PVT. The necessary mud products for additional weight and fluid loss control will be on location at all times. Appropriately weighted mud will be used to isolate potential gas, oil, and water zones until such time as casing can be cemented into place for zonal isolation.

# Oxy Blanket Design - Casing Design “A”

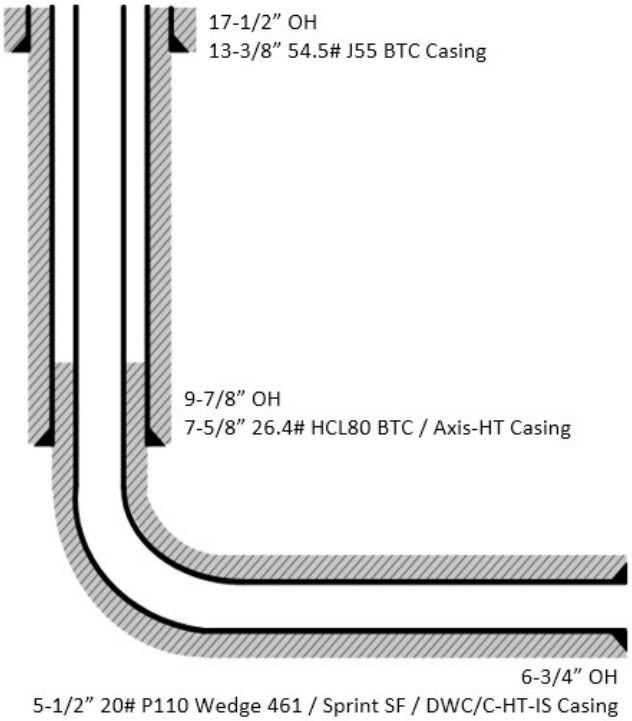
## 6. Wellbore Diagram(s)

### Design Variation “A1”




*TOC @ 500’ Above Prev. CSG*

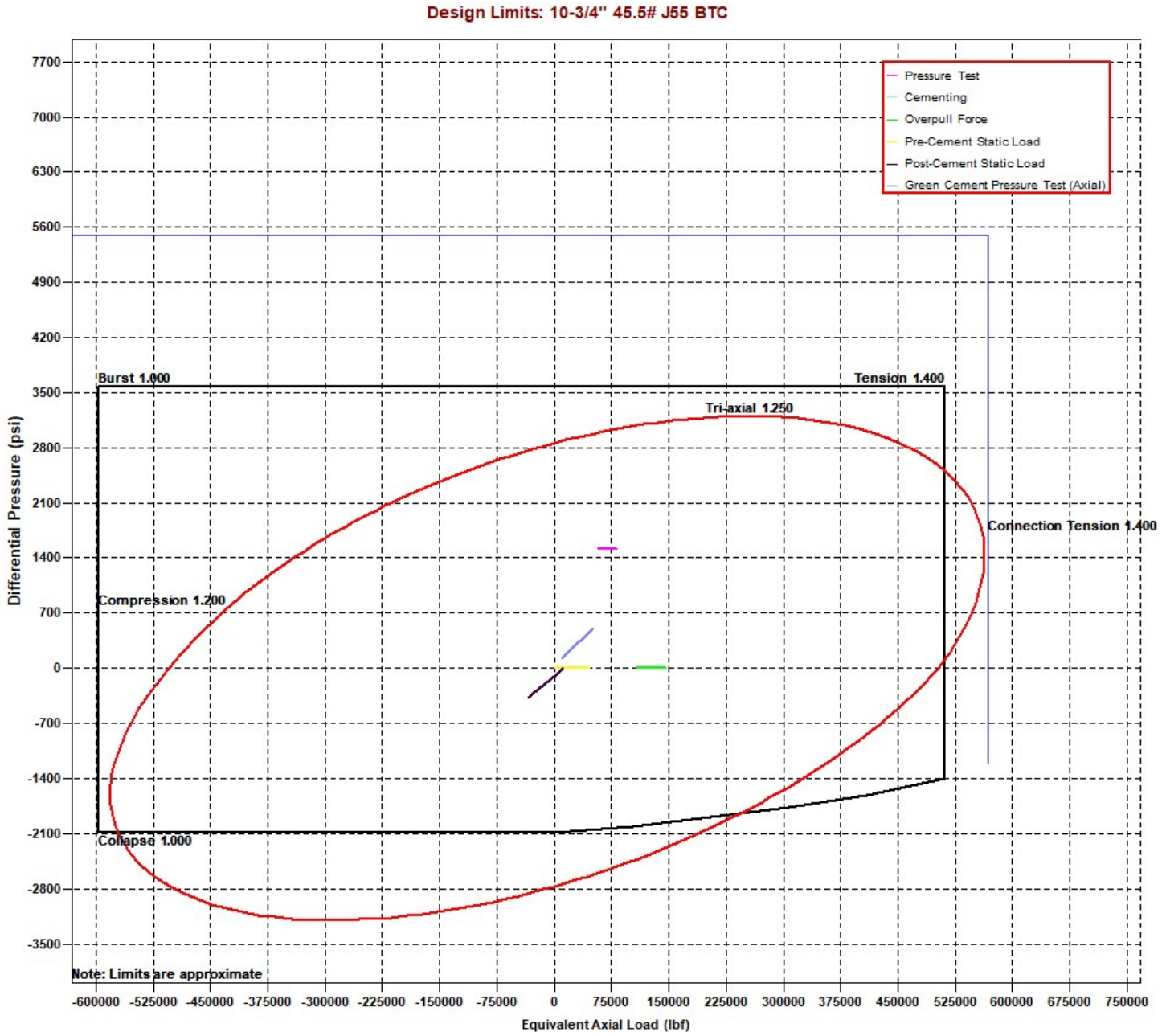
### Design Variation “A2”



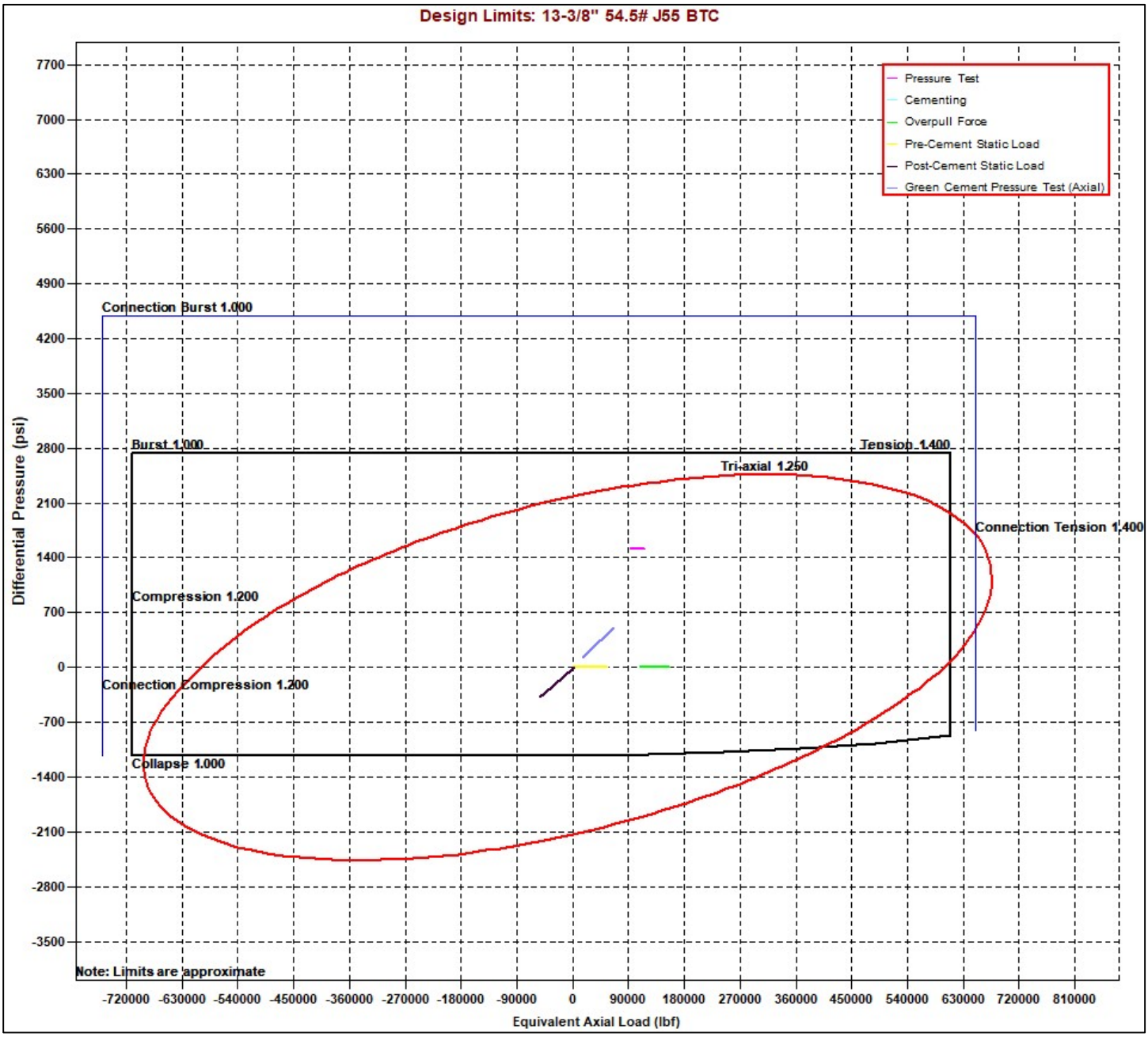

*TOC @ 500’ Above Prev. CSG*

# Oxy Blanket Design - Casing Design "A"

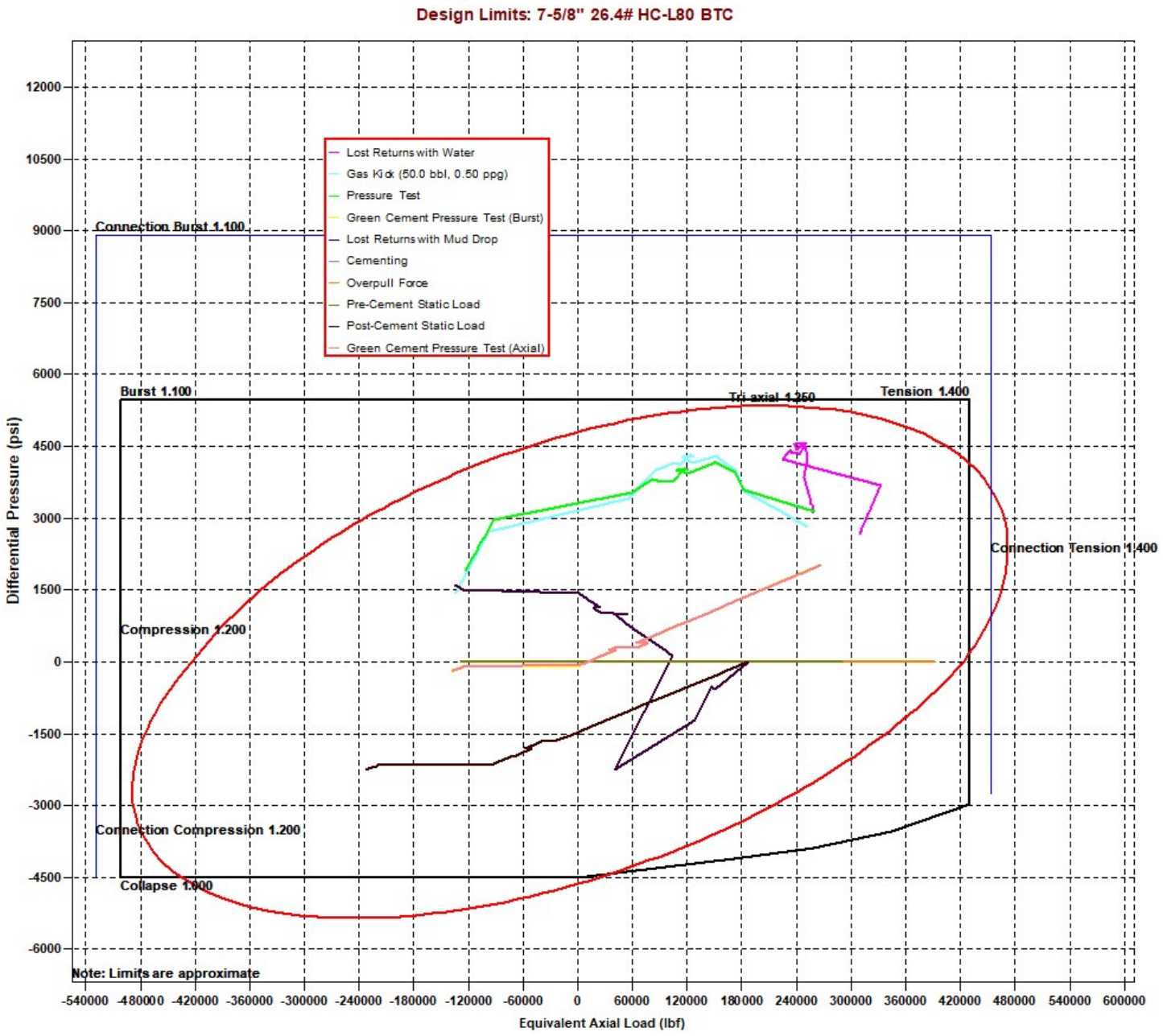
## 7. Landmark StressCheck Screenshots – Triaxial Output



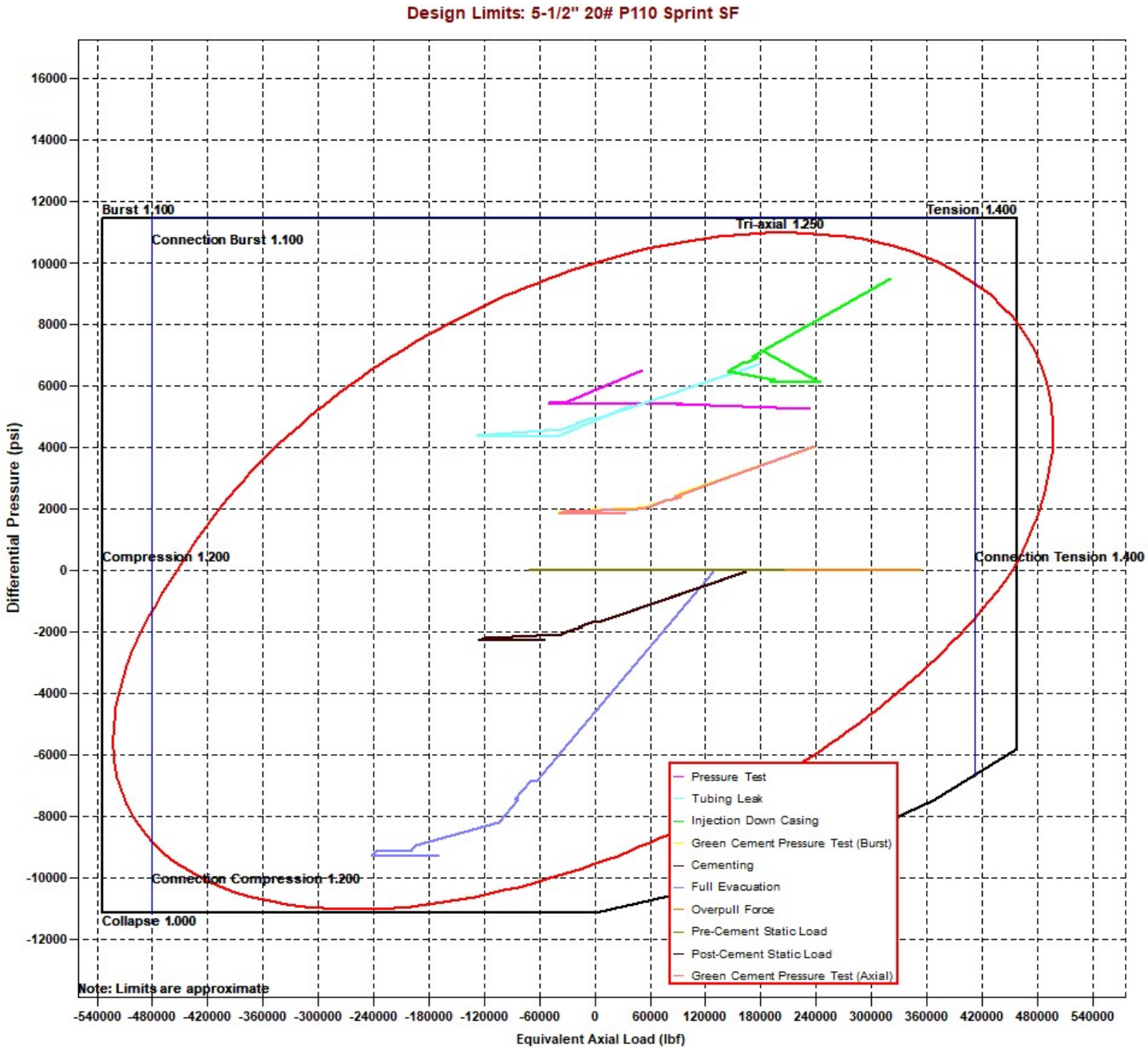
# Oxy Blanket Design - Casing Design "A"



# Oxy Blanket Design - Casing Design "A"



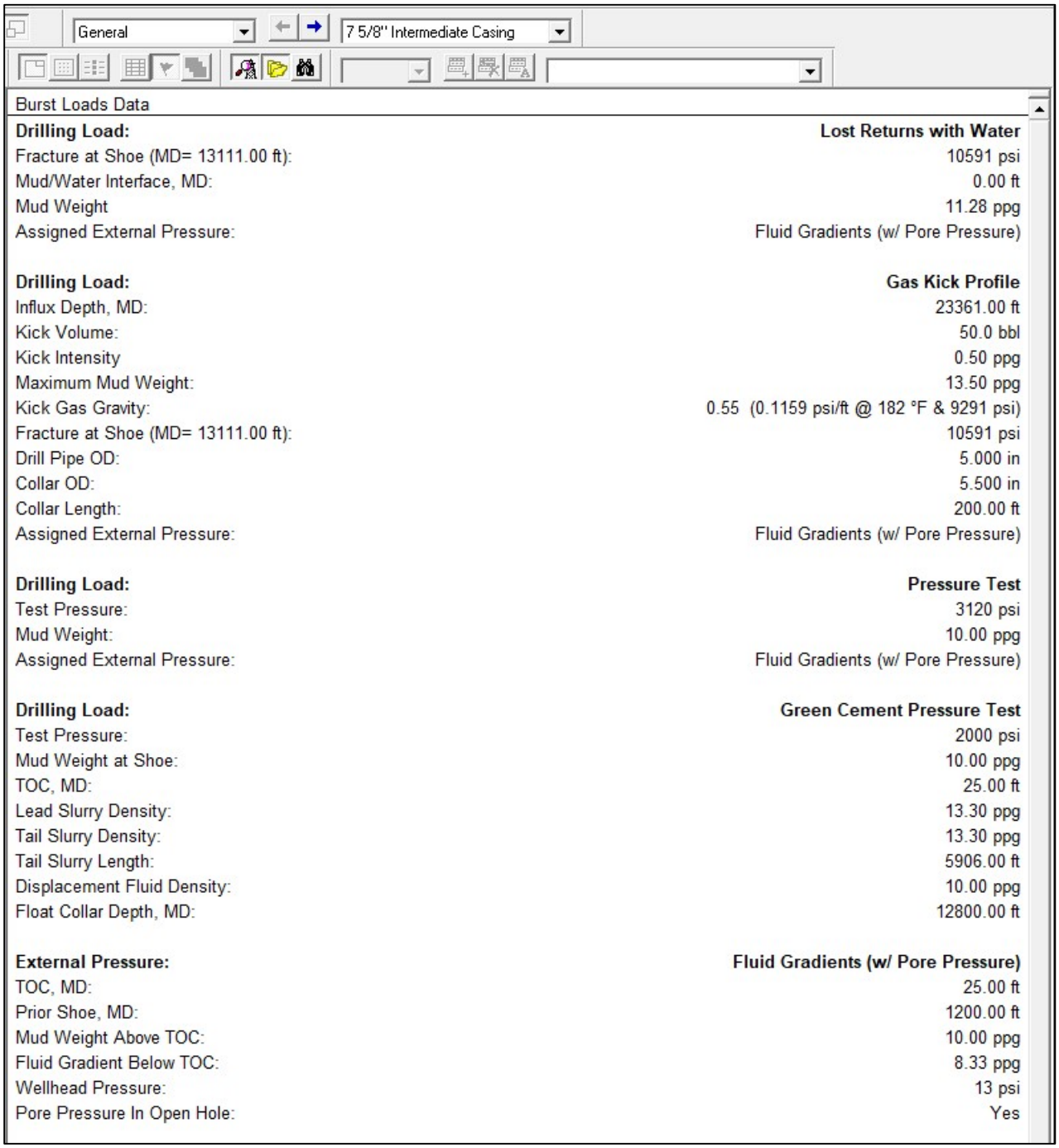
# Oxy Blanket Design - Casing Design "A"



# Oxy Blanket Design - Casing Design "A"

## 8. Landmark StressCheck Screenshots – Inputs for Intermediate CSG Load Cases

**Burst Load Cases**




Burst Loads Data

| | |
|---|---|
| **Drilling Load:** | **Lost Returns with Water** |
| Fracture at Shoe (MD= 13111.00 ft): | 10591 psi |
| Mud/Water Interface, MD: | 0.00 ft |
| Mud Weight | 11.28 ppg |
| Assigned External Pressure: | Fluid Gradients (w/ Pore Pressure) |
| | |
| **Drilling Load:** | **Gas Kick Profile** |
| Influx Depth, MD: | 23361.00 ft |
| Kick Volume: | 50.0 bbl |
| Kick Intensity | 0.50 ppg |
| Maximum Mud Weight: | 13.50 ppg |
| Kick Gas Gravity: | 0.55 (0.1159 psi/ft @ 182 °F & 9291 psi) |
| Fracture at Shoe (MD= 13111.00 ft): | 10591 psi |
| Drill Pipe OD: | 5.000 in |
| Collar OD: | 5.500 in |
| Collar Length: | 200.00 ft |
| Assigned External Pressure: | Fluid Gradients (w/ Pore Pressure) |
| | |
| **Drilling Load:** | **Pressure Test** |
| Test Pressure: | 3120 psi |
| Mud Weight: | 10.00 ppg |
| Assigned External Pressure: | Fluid Gradients (w/ Pore Pressure) |
| | |
| **Drilling Load:** | **Green Cement Pressure Test** |
| Test Pressure: | 2000 psi |
| Mud Weight at Shoe: | 10.00 ppg |
| TOC, MD: | 25.00 ft |
| Lead Slurry Density: | 13.30 ppg |
| Tail Slurry Density: | 13.30 ppg |
| Tail Slurry Length: | 5906.00 ft |
| Displacement Fluid Density: | 10.00 ppg |
| Float Collar Depth, MD: | 12800.00 ft |
| | |
| **External Pressure:** | **Fluid Gradients (w/ Pore Pressure)** |
| TOC, MD: | 25.00 ft |
| Prior Shoe, MD: | 1200.00 ft |
| Mud Weight Above TOC: | 10.00 ppg |
| Fluid Gradient Below TOC: | 8.33 ppg |
| Wellhead Pressure: | 13 psi |
| Pore Pressure In Open Hole: | Yes |

# Oxy Blanket Design - Casing Design "A"

## Collapse Load Cases

General | 7 5/8" Intermediate Casing

Collapse Loads Data

| | |
|---|---|
| **Drilling Load:** | **Cementing** |
| Mud Weight at Shoe: | 10.00 ppg |
| TOC, MD: | 25.00 ft |
| Lead Slurry Density: | 13.30 ppg |
| Tail Slurry Density: | 13.30 ppg |
| Tail Slurry Length: | 5906.00 ft |
| Displacement Fluid Density: | 10.00 ppg |
| Float Collar Depth, MD: | 12800.00 ft |
| Assigned External Pressure: | Fluid Gradients (w/ Pore Pressure) |
| | |
| **Drilling Load:** | **Lost Returns with Mud Drop** |
| Lost Returns Depth, MD: | 13110.89 ft |
| Pore Pressure at Lost Returns Depth: | 8183 psi |
| Pore Pressure Gradient at Lost Returns Depth: | 12.33 ppg |
| Mud Weight: | 13.50 ppg |
| Mud Drop Level, MD: | 1106.39 ft |
| Assigned External Pressure: | Fluid Gradients (w/ Pore Pressure) |
| | |
| **External Pressure:** | **Fluid Gradients (w/ Pore Pressure)** |
| TOC, MD: | 25.00 ft |
| Prior Shoe, MD: | 1200.00 ft |
| Fluid Gradient Above TOC: | 10.00 ppg |
| Fluid Gradient Below TOC: | 10.00 ppg |
| Wellhead Pressure: | 13 psi |
| Pore Pressure In Open Hole Below TOC: | No |

## Axial Load Cases

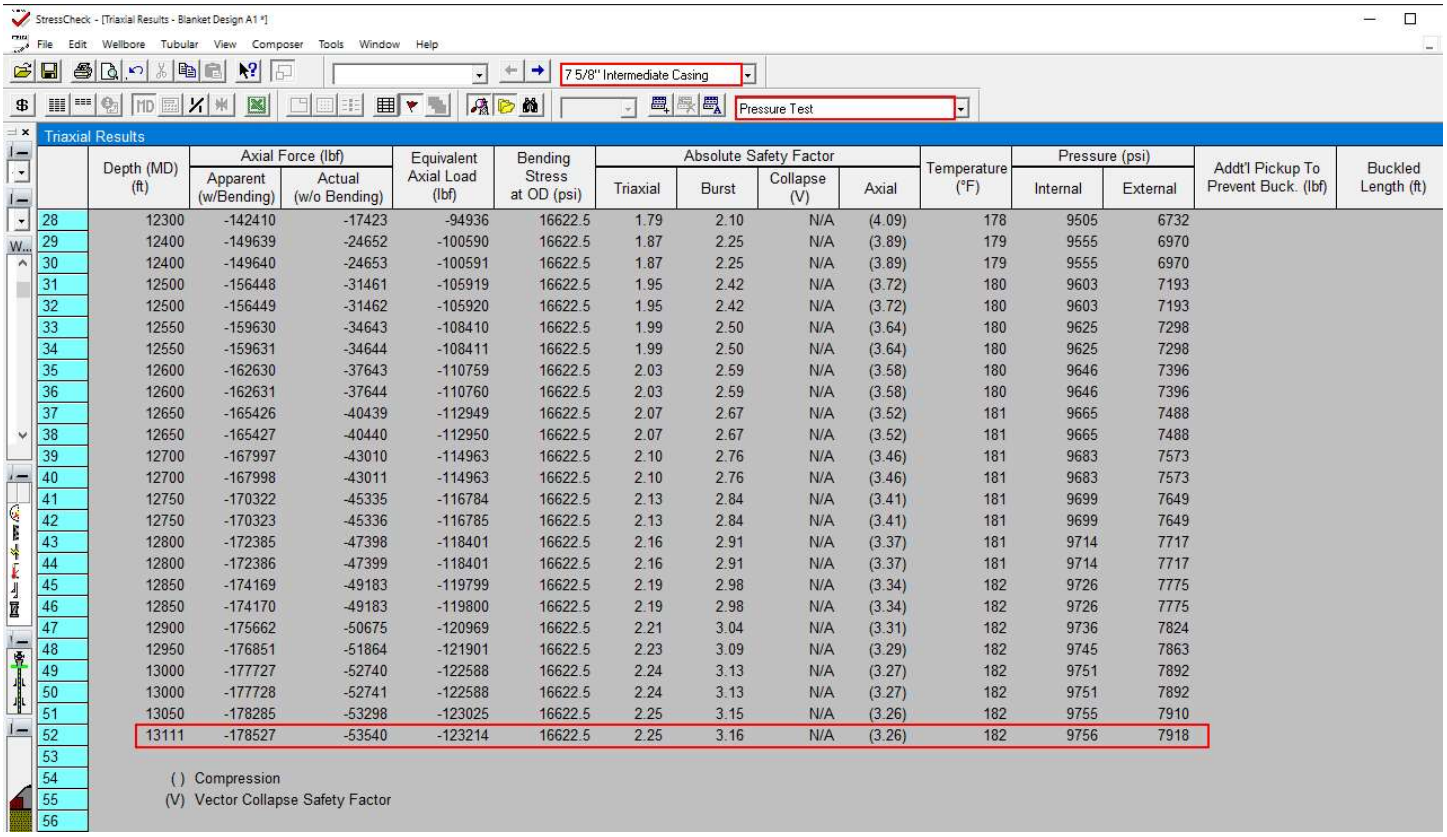
General | 7 5/8" Intermediate Casing

Axial Loads Data

| | |
|---|---|
| Overpull Force: | 100000 lbf |
| Pre-Cement Static Load: | Yes |
| Pickup Force: | 0 lbf |
| Post-Cement Static Load: | Yes |
| Green Cement Pressure Test: | 2000 psi |
| Service Loads: | Yes |

# Oxy Blanket Design - Casing Design "A"

## 9. Landmark StressCheck Screenshot – Int. Casing Triaxial Results Table (Pressure Test)




Triaxial Results

| | Depth (MD) (ft) | Axial Force (lbf) Apparent (w/Bending) | Axial Force (lbf) Actual (w/o Bending) | Equivalent Axial Load (lbf) | Bending Stress at OD (psi) | Absolute Safety Factor Triaxial | Burst | Collapse (V) | Axial | Temperature (°F) | Pressure (psi) Internal | Pressure (psi) External | Addt'l Pickup To Prevent Buck. (lbf) | Buckled Length (ft) |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 28 | 12300 | -142410 | -17423 | -94936 | 16622.5 | 1.79 | 2.10 | N/A | (4.09) | 178 | 9505 | 6732 | | |
| 29 | 12400 | -149639 | -24652 | -100590 | 16622.5 | 1.87 | 2.25 | N/A | (3.89) | 179 | 9555 | 6970 | | |
| 30 | 12400 | -149640 | -24653 | -100591 | 16622.5 | 1.87 | 2.25 | N/A | (3.89) | 179 | 9555 | 6970 | | |
| 31 | 12500 | -156448 | -31461 | -105919 | 16622.5 | 1.95 | 2.42 | N/A | (3.72) | 180 | 9603 | 7193 | | |
| 32 | 12500 | -156449 | -31462 | -105920 | 16622.5 | 1.95 | 2.42 | N/A | (3.72) | 180 | 9603 | 7193 | | |
| 33 | 12550 | -159630 | -34643 | -108410 | 16622.5 | 1.99 | 2.50 | N/A | (3.64) | 180 | 9625 | 7298 | | |
| 34 | 12550 | -159631 | -34644 | -108411 | 16622.5 | 1.99 | 2.50 | N/A | (3.64) | 180 | 9625 | 7298 | | |
| 35 | 12600 | -162630 | -37643 | -110759 | 16622.5 | 2.03 | 2.59 | N/A | (3.58) | 180 | 9646 | 7396 | | |
| 36 | 12600 | -162631 | -37644 | -110760 | 16622.5 | 2.03 | 2.59 | N/A | (3.58) | 180 | 9646 | 7396 | | |
| 37 | 12650 | -165426 | -40439 | -112949 | 16622.5 | 2.07 | 2.67 | N/A | (3.52) | 181 | 9665 | 7488 | | |
| 38 | 12650 | -165427 | -40440 | -112950 | 16622.5 | 2.07 | 2.67 | N/A | (3.52) | 181 | 9665 | 7488 | | |
| 39 | 12700 | -167997 | -43010 | -114963 | 16622.5 | 2.10 | 2.76 | N/A | (3.46) | 181 | 9683 | 7573 | | |
| 40 | 12700 | -167998 | -43011 | -114963 | 16622.5 | 2.10 | 2.76 | N/A | (3.46) | 181 | 9683 | 7573 | | |
| 41 | 12750 | -170322 | -45335 | -116784 | 16622.5 | 2.13 | 2.84 | N/A | (3.41) | 181 | 9699 | 7649 | | |
| 42 | 12750 | -170323 | -45336 | -116785 | 16622.5 | 2.13 | 2.84 | N/A | (3.41) | 181 | 9699 | 7649 | | |
| 43 | 12800 | -172385 | -47398 | -118401 | 16622.5 | 2.16 | 2.91 | N/A | (3.37) | 181 | 9714 | 7717 | | |
| 44 | 12800 | -172386 | -47399 | -118401 | 16622.5 | 2.16 | 2.91 | N/A | (3.37) | 181 | 9714 | 7717 | | |
| 45 | 12850 | -174169 | -49183 | -119799 | 16622.5 | 2.19 | 2.98 | N/A | (3.34) | 182 | 9726 | 7775 | | |
| 46 | 12850 | -174170 | -49183 | -119800 | 16622.5 | 2.19 | 2.98 | N/A | (3.34) | 182 | 9726 | 7775 | | |
| 47 | 12900 | -175662 | -50675 | -120969 | 16622.5 | 2.21 | 3.04 | N/A | (3.31) | 182 | 9736 | 7824 | | |
| 48 | 12950 | -176851 | -51864 | -121901 | 16622.5 | 2.23 | 3.09 | N/A | (3.29) | 182 | 9745 | 7863 | | |
| 49 | 13000 | -177727 | -52740 | -122588 | 16622.5 | 2.24 | 3.13 | N/A | (3.27) | 182 | 9751 | 7892 | | |
| 50 | 13000 | -177728 | -52741 | -122588 | 16622.5 | 2.24 | 3.13 | N/A | (3.27) | 182 | 9751 | 7892 | | |
| 51 | 13050 | -178285 | -53298 | -123025 | 16622.5 | 2.25 | 3.15 | N/A | (3.26) | 182 | 9755 | 7910 | | |
| 52 | 13111 | -178527 | -53540 | -123214 | 16622.5 | 2.25 | 3.16 | N/A | (3.26) | 182 | 9756 | 7918 | | |
| 53 | | | | | | | | | | | | | | |
| 54 | | ( ) Compression | | | | | | | | | | | | |
| 55 | | (V) Vector Collapse Safety Factor | | | | | | | | | | | | |
| 56 | | | | | | | | | | | | | | |

Internal Pressure = Surface Pressure + Hydrostatic = 9756 psi
External Pressure = Fluid Gradient w/ Pore Pressure = 7918 psi
Burst SF = 3.16

NOTE: *Specific load case inputs for the pressure test can be seen in **Section 8** above. The test pressure does not exceed 70% of the minimum internal yield.*

# Oxy Blanket Design - Casing Design "A"

## 10. Intermediate Non-API Casing Spec Sheet

AXIS PIPE AND TUBE

# Technical Data Sheet

7 5/8" 26.40 lbs/ft. L80HC - Axis HT

| Mechanical Properties | | |
|---|---|---|
| Minimum Yield Strength | psi. | 80,000 |
| Maximum Yield Strength | psi. | 95,000 |
| Minimum Tensile Strength | psi. | 95,000 |

| Dimensions | | Pipe | AXIS HT |
|---|---|---|---|
| Outside Diameter | in. | 7.625 | 8.500 |
| Wall Thickness | in. | 0.328 | - |
| Inside Diameter | in. | 6.969 | - |
| Standard Drift | in. | 6.844 | 6.844 |
| Alternate Drift | in. | - | - |
| Plain End Weight | lbs/ft. | - | - |
| Nominal Linear Weight | lbs/ft. | 26.40 | - |

| Performance | | Pipe | AXIS HT |
|---|---|---|---|
| Minimum Collapse Pressure | psi. | 4,320 | - |
| Minimum Internal Yield Pressure | psi. | 6,020 | 6,020 |
| Minimum Pipe Body Yield Strength | lbs. | 602 x 1,000 | - |
| Joint Strength | lbs. | - | 635 x 1,000 |

| Make-Up Torques | | Pipe | AXIS HT |
|---|---|---|---|
| Optimum Make-Up Torque | ft/lbs. | - | 8,000 |
| Maximum Operational Torque | ft/lbs. | - | 25,000 |

# Oxy Blanket Design - Casing Design “A”

## 11. Production Non-API Casing Spec Sheets

Printed on: 11/09/2021

Tenaris

### TenarisHydril Wedge 461 ® MS

| Coupling | Pipe Body |
|---|---|
| Grade: P110-ICY | Grade: P110-ICY |
| Body: White | 1st Band: White |
| 1st Band: Pale Green | 2nd Band: Pale Green |
| 2nd Band: - | 3rd Band: Pale Green |
| 3rd Band: - | 4th Band: - |
| | 5th Band: - |
| | 6th Band: - |

| | | | | | |
|---|---|---|---|---|---|
| Outside Diameter | 5.500 in. | Wall Thickness | 0.361 in. | Grade | P110-ICY |
| Min. Wall Thickness | 87.50 % | Pipe Body Drift | API Standard | Type | Casing |
| Connection OD Option | MS | | | | |

#### Pipe Body Data

| Geometry | | | | Performance | |
|---|---|---|---|---|---|
| Nominal OD | 5.500 in. | Wall Thickness | 0.361 in. | Body Yield Strength | 729 x1000 lb |
| Nominal Weight | 20 lb/ft | Plain End Weight | 19.83 lb/ft | Min. Internal Yield Pressure | 14,360 psi |
| Drift | 4.653 in. | OD Tolerance | API | SMYS | 125,000 psi |
| Nominal ID | 4.778 in. | | | Collapse Pressure | 12,300 psi |

#### Connection Data

| Geometry | | Performance | | Make-Up Torques | |
|---|---|---|---|---|---|
| Connection OD | 6.050 in. | Tension Efficiency | 100 % | Minimum | 17,000 ft-lb |
| Coupling Length | 7.714 in. | Joint Yield Strength | 729 x1000 lb | Optimum | 18,000 ft-lb |
| Connection ID | 4.778 in. | Internal Pressure Capacity | 14,360 psi | Maximum | 21,600 ft-lb |
| Make-up Loss | 3.775 in. | Compression Efficiency | 100 % | | |
| Threads per inch | 3.40 | Compression Strength | 729 x1000 lb | Operation Limit Torques | |
| Connection OD Option | Ms | Max. Allowable Bending | 104 °/100 ft | Operating Torque | 43,000 ft-lb |
| | | External Pressure Capacity | 12,300 psi | Yield Torque | 51,000 ft-lb |
| | | Coupling Face Load | 273,000 lb | | |
| | | | | Buck-On | |
| | | | | Minimum | 21,600 ft-lb |
| | | | | Maximum | 23,100 ft-lb |

#### Notes

This connection is fully interchangeable with:
Wedge 441® - 5.5 in. - 0.304 / 0.361 in.
Wedge 461® - 5.5 in. - 0.304 / 0.415 / 0.476 in.
Connections with Dopeless® Technology are fully compatible with the same connection in its Standard version
In October 2019, TenarisHydril Wedge XP® 2.0 was renamed TenarisHydril Wedge 461™. Product dimensions and properties remain identical and both connections are fully interchangeable

For the lastest performance data, always visit our website: www.tenaris.com

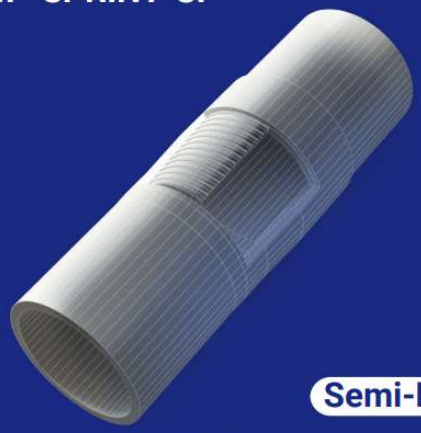
# Oxy Blanket Design - Casing Design “A”

Generated on May 21, 2024

## CONNECTION DATA SHEET

OD: **5.500 in.** Grade: **P110**
Weight: **20.00 lb/ft** Drift: **4.653 in. (API)**
Wall Th.: **0.361 in.**

### VAM® SPRINT-SF



Semi-Flush

**Field Torque Values**

**Make-up Torque (ft-lb)**
20,000 **MIN**
22,500 **OPTI**
25,000 **MAX**

**Torque with Sealability (ft-lb)**
36,000 **MTS**

**Locked Flank Torque (ft-lb)**
4,500 **MIN**
15,750 **MAX**

*(2) MTS: Maximum Torque with Sealability.*

### PIPE BODY PROPERTIES

| | | |
|---|---|---|
| **Nominal OD** | 5.500 | *in.* |
| **Nominal ID** | 4.778 | *in.* |
| **Nominal Wall Thickness** | 0.361 | *in.* |
| **Minimum Wall Thickness** | 87.5 | *%* |
| **Nominal Weight (API)** | 20.00 | *lb/ft* |
| **Plain End Weight** | 19.83 | *lb/ft* |
| **Drift** | 4.653 | *in.* |
| **Grade Type** | API 5CT | |
| **Minimum Yield Strength** | 110 | *ksi* |
| **Maximum Yield Strength** | 140 | *ksi* |
| **Minimum Ultimate Tensile Strength** | 125 | *ksi* |
| **Pipe Body Yield Strength** | 641 | *klb* |
| **Internal Yield Pressure** | 12,640 | *psi* |
| **Collapse Pressure** | 11,100 | *psi* |

### CONNECTION PROPERTIES

| | | |
|---|---|---|
| **Connection Type** | Semi-Premium Integral Semi-Flu | |
| **Nominal Connection OD** | 5.783 | *in.* |
| **Nominal Connection ID** | 4.718 | *in.* |
| **Make-up Loss** | 5.965 | *in.* |
| **Tension Efficiency** | 90 | *% Pipe Body* |
| **Compression Efficiency** | 90 | *% Pipe Body* |
| **Internal Pressure Efficiency** | 100 | *% Pipe Body* |
| **External Pressure Efficiency** | 100 | *% Pipe Body* |

### JOINT PERFORMANCES

| | | |
|---|---|---|
| **Tension Strength** | 577 | *klb* |
| **Compression Strength** | 577 | *klb* |
| **Internal Pressure Resistance** | 12,640 | *psi* |
| **External Pressure Resistance** | 11,100 | *psi* |
| **Maximum Bending, Structural** | 78 | *°/100 ft* |
| **Maximum Bending, with Sealability(1)** | 30 | *°/100 ft* |

*(1) Sealability rating demonstrated as per API RP 5C5 / ISO 13679*

# Oxy Blanket Design - Casing Design "A"

DWC/C-HT-IS

## Connection Data Sheet

| OD (in.) | WEIGHT (lbs./ft.) | WALL (in.) | GRADE | API DRIFT (in.) | RBW% | CONNECTION |
|---|---|---|---|---|---|---|
| 5.500 | Nominal: 20.00<br>Plain End: 19.83 | 0.361 | ‡VST P110MY | 4.653 | 87.5 | DWC/C-HT-IS |

| PIPE PROPERTIES | | |
|---|---|---|
| Nominal OD | 5.500 | in. |
| Nominal ID | 4.778 | in. |
| Nominal Area | 5.828 | sq.in. |
| Grade Type | | API 5CT |
| Min. Yield Strength | 125 | ksi |
| Max. Yield Strength | 140 | ksi |
| Min. Tensile Strength | 135 | ksi |
| Yield Strength | 729 | klb |
| Ultimate Strength | 787 | klb |
| Min. Internal Yield Pressure | 14,360 | psi |
| Collapse Pressure | 12,090 | psi |

| CONNECTION PROPERTIES | | |
|---|---|---|
| Connection Type | Semi-Premium T&C | |
| Connection OD (nom) | 6.050 | in. |
| Connection ID (nom) | 4.778 | in. |
| Make-Up Loss | 4.125 | in. |
| Coupling Length | 9.250 | in. |
| Critical Cross Section | 5.828 | sq.in. |
| Tension Efficiency | 89.1% | of pipe |
| Compression Efficiency | 88.0% | of pipe |
| Internal Pressure Efficiency | 86.1% | of pipe |
| External Pressure Efficiency | 100.0% | of pipe |

| CONNECTION PERFORMANCES | | |
|---|---|---|
| Yield Strength | 649 | klb |
| Parting Load | 729 | klb |
| Compression Rating | 641 | klb |
| Min. Internal Yield Pressure | 12,360 | psi |
| External Pressure Resistance | 12,090 | psi |
| Maximum Uniaxial Bend Rating | 91.7 | °/100 ft |
| Reference String Length w 1.4 Design Factor | 22,890 | ft. |

| FIELD TORQUE VALUES | | |
|---|---|---|
| Min. Make-up torque | 16,600 | ft.lb |
| Opti. Make-up torque | 17,950 | ft.lb |
| Max. Make-up torque | 19,300 | ft.lb |
| Min. Shoulder Torque | 1,660 | ft.lb |
| Max. Shoulder Torque | 13,280 | ft.lb |
| Max. Delta Turn | 0.200 | Turns |
| †Maximum Operational Torque | 23,800 | ft.lb |
| †Maximum Torsional Value (MTV) | 26,180 | ft.lb |

**† Maximum Operational Torque and Maximum Torsional Value only valid with Vallourec P110MY Material.**
**‡ P110MY - Coupling Min Yield Strength is 110ksi and Coupling Max Yield is 125ksi.**

"VST = Vallourec Star as the mill source for the pipe, "P110EC" is the grade name"

**Need Help? Contact: tech.support@vam-usa.com**

**For detailed information on performance properties, refer to DWC Connection Data Notes on following page(s).**

Connection specifications within the control of VAM USA were correct as of the date printed. Specifications are subject to change without notice. Certain connection specifications are dependent on the mechanical properties of the pipe. Mechanical properties of mill proprietary pipe grades were obtained from mill publications and are subject to change. Properties of mill proprietary grades should be confirmed with the mill. Users are advised to obtain current connection specifications and verify pipe mechanical properties for each application.

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VAM USA

# Oxy Blanket Design - Casing Design “A”

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**DWC Connection Data Sheet Notes:**

1. DWC connections are available with a seal ring (SR) option.
2. All standard DWC/C connections are interchangeable for a given pipe OD. DWC connections are interchangeable with DWC/C-SR connections of the same OD and wall.
3. Connection performance properties are based on nominal pipe body and connection dimensions.
4. DWC connection internal and external pressure resistance is calculated using the API rating for buttress connections. API Internal pressure resistance is calculated from formulas 31, 32, and 35 in the API Bulletin 5C3.
5. DWC joint strength is the minimum pipe body yield strength multiplied by the connection critical area.
6. API joint strength is for reference only. It is calculated from formulas 42 and 43 in the API Bulletin 5C3.
7. Bending efficiency is equal to the compression efficiency.
8. The torque values listed are recommended. The actual torque required may be affected by field conditions such as temperature, thread compound, speed of make-up, weather conditions, etc.
9. Connection yield torque is not to be exceeded.
10. Reference string length is calculated by dividing the joint strength by both the nominal weight in air and a design factor (DF) of 1.4. These values are offered for reference only and do not include load factors such as bending, buoyancy, temperature, load dynamics, etc.
11. DWC connections will accommodate API standard drift diameters.
12. DWC/C family of connections are compatible with API Buttress BTC connections. Please contact tech.support@vam-usa.com for details on connection ratings and make-up.



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# Oxy Blanket Design - Casing Design "B"

## 1. Casing Program

**The designs and associated details listed in this document are the "worst case scenario" boundaries for design safety factors.**

**Location and lithology have NOT been accounted for in these designs; however, the designs are NOT valid for wells within KPLA Boundaries or Capitan Reef areas. The specific well details will be based on the APD/Sundry package and the information listed in the COA.**

**The mud program listed below will remain the same between each design variation.**

**Hole will be full during casing run for well control and tensile SF.**

**Casing will be kept at least half full during run for these designs to meet BLM collapse SF requirement.**

| | | MD | | TVD | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| Section | Hole Size (in) | From (ft) | To (ft) | From (ft) | To (ft) | Csg. OD (in) | Csg Wt. (ppf) | Grade | Conn. |
| Surface | 17.5 | 0 | 1200 | 0 | 1200 | 13.375 | 54.5 | J-55 | BTC |
| Intermediate 1 | 12.25† | 0 | 4832 | 0 | 4832 | 10.75 | 45.5 | L-80 HC | BTC-SC |
| Intermediate 2 | 9.875 | 0 | 13111* | 0 | 12775* | 7.625 | 26.4 | L-80 HC | BTC Axis-HT |
| Production | 6.75 | 0 | 23361 | 0 | 12775 | 5.5 | 20 | P-110 | Wedge 461 Sprint SF DWC/C-HT-IS |

*Curve could be in intermediate or production section

†Oxy requests the option to set intermediate 1 casing shallower, yet still below the salts, if required due to losses or hole conditions. Cement volumes may be adjusted if casing is set shallower and a DV tool may be run incase hole conditions merit pumping a second stage cement job to comply with the permitted top of cement. If cement is circulated to surface during first stage, Oxy will drop a cancelation cone and not pump the second stage. Well specific depths for the pad will be included with the casing setting depths information submitted for review.

All casing strings will be tested in accordance with 43 CFR part 3170 Subpart 3172.

| *All Casing SF Values will meet or exceed those below* | | | |
|---|---|---|---|
| SF Collapse | SF Burst | Body SF Tension | Joint SF Tension |
| 1.00 | 1.100 | 1.4 | 1.4 |

### §Annular Clearance Variance Request

As per the agreement reached in the Oxy/BLM face-to-face meeting on Feb 22, 2018, Oxy requests permission to allow deviation from the 0.422" annular clearance requirement. Please see Annular Clearance Variance attachment for further details.

§Annular Clearance Variance Request may not apply to all connections used or presented.

# Oxy Blanket Design - Casing Design "B"

## 2. Trajectory / Boundary Conditions

| Section | MD | | TVD | | Max. Angle | Max. Planned DLS |
|---|---|---|---|---|---|---|
| | Deepest KOP (ft) | End Build (ft) | Deepest KOP (ft) | End Build (ft) | | |
| Surface | 0 | 1200 | 0 | 1200 | 5° | 1°/100 ft |
| Salt | 0 | 4832 | 0 | 4832 | 5° | 1°/100 ft |
| Intermediate | 5000 (inside Cherry Canyon) | 6500 | 4980 | 6390 | 20° | 2°/100 ft |
| | 12211 | 13111 | 12202 | 12775 | 92° ‡ | 12°/100 ft ‡ |
| Production | 12211 (~100' MD past ICP) | 13111 | 12202 | 12775 | 92° ‡ | 12°/100 ft ‡ |

‡ Applies only when intermediate casing depth is deepened to landing point to match TVD of production in some areas where required to accommodate higher MWs in depleted areas.

Oxy has reviewed casing burst, collapse, and axial loadcases in Landmark StressCheck with the boundary conditions in the table above which satisfies Oxy and BLM minimum design criteria. Triaxial plots for each casing string is shown in Section 7 and intermediate load case inputs are shown in Section 8.

## 3. Cementing Program

NOTE: Blanket design is for technical review only. The cement volumes will be adjusted to ensure cement tops meet BLM requirements.

| Section | Stage | Slurry: | Sacks | Yield (ft^3/ft) | Density (lb/gal) | Excess: | TOC | Placement | Description |
|---|---|---|---|---|---|---|---|---|---|
| Surface | 1 | Surface - Tail | 1253 | 1.33 | 14.8 | 100% | - | Circulate | Class C+Accel. |
| Int.1 | 1 | Intermediate - Tail | 85 | 1.33 | 14.8 | 20% | 4,332 | Circulate | Class C+Accel. |
| Int.1 | 1 | Intermediate - Lead | 676 | 1.73 | 12.9 | 50% | - | Circulate | Class Pozz+Ret. |
| Int. 2 | 1 | Intermediate 1S - Tail | 793 | 1.68 | 13.2 | 5% | 7,206 | Circulate | Class C+Ret., Disper. |
| Int. 2 | 2 | Intermediate 2S - Tail BH | 1002 | 1.71 | 13.3 | 25% | - | Bradenhead | Class C+Accel. |
| Prod. | 1 | Production - Tail | 609 | 1.84 | 13.3 | 25% | 12,611 | Circulate | Class C+Ret. |
| Prod. | 2* | Production - Tail | TBD | 1.84 | 13.3 | 50% | 500' inside prev csg | Circulate | Class C+Ret. |

**Only applies in scenario where planned single stage job TOC is not 500' above previous shoe as designed/programmed requiring bradenhead 2nd stage to meet requirements*

As Reviewed and Approved by BLM on Feb 8, 2024: Oxy uses a Class C / Pozzolan mix on its production cement slurry, which has the same fluid properties as Class H, and has been pilot and field blend tested to have as good or better compressive strength development at our target densities.

**Offline Cementing Request**

Oxy requests a variance to cement the 9.625" and/or 7.625" intermediate casing strings offline in accordance to the approved variance, EC Tran 461365. Please see Offline Cementing Variance attachment for further details.

# Oxy Blanket Design - Casing Design "B"

**Bradenhead CBL Request**

Oxy requests permission to adjust the CBL requirement after bradenhead cement jobs, on 7-5/8" intermediate casings, as per the agreement reached in the OXY/BLM meeting on September 5, 2019. Please see Bradenhead CBL Variance attachment for further details.

## 4. Pressure Control Equipment

| BOP installed and tested before drilling which hole? | Size? | Min. Required WP | Type | ✓ | Tested to: | TVD Depth (ft) per Section: |
|---|---|---|---|---|---|---|
| 12.25" Hole | 13-5/8" | 5M | Annular | ✓ | 70% of working pressure | 4832 |
| | | 5M | Blind Ram | ✓ | 250 psi / 5000 psi | |
| | | | Pipe Ram | | | |
| | | | Double Ram | ✓ | | |
| | | | Other* | | | |
| 9.875" Hole | 13-5/8" | 5M | Annular | ✓ | 70% of working pressure | 12102 |
| | | 5M | Blind Ram | ✓ | 250 psi / 5000 psi | |
| | | | Pipe Ram | | | |
| | | | Double Ram | ✓ | | |
| | | | Other* | | | |
| 6.75" Hole | 13-5/8" | 5M | Annular | ✓ | 100% of working pressure | 12775 |
| | | 10M | Blind Ram | ✓ | 250 psi / 10000 psi | |
| | | | Pipe Ram | | | |
| | | | Double Ram | ✓ | | |
| | | | Other* | | | |

*Specify if additional ram is utilized
**Curve could be in intermediate or production section

BOP/BOPE will be tested by an independent service company to 250 psi low and the high pressure indicated above per 43 CFR part 3170 Subpart 3172 requirements. The System may be upgraded to a higher pressure but still tested to the working pressure listed in the table above. If the system is upgraded all the components installed will be functional and tested.

Pipe rams will be operationally checked each 24 hour period. Blind rams will be operationally checked on each trip out of the hole. These checks will be noted on the daily tour sheets. Other accessories to the BOP equipment will include a Kelly cock and floor safety valve (inside BOP) and choke lines and choke manifold. See attached schematics.

**5M Annular BOP Request**

Per BLM's Memorandum No. NM-2017-008: *Decision and Rationale for a Variance Allowing the Use of a 5M Annular Preventer with a 10M BOP Stack*, Oxy requests to employ a 5M annular with a 10M BOPE stack in the pilot and lateral sections of the well and will ensure that two barriers to flow are

# Oxy Blanket Design - Casing Design "B"

| |
|---|
| Formation integrity test will be performed per 43 CFR part 3170 Subpart 3172. |
| On Exploratory wells or on that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Will be tested in accordance with 43 CFR part 3170 Subpart 3172. |

| | |
|---|---|
| A variance is requested for the use of a flexible choke line from the BOP to Choke Manifold. Coflex hoses are in compliance with API 16C and meets inspection and testing requirements. See attached for specs and hydrostatic test chart. | |
| Y | Are anchors required by manufacturer? |

A multibowl or a unionized multibowl wellhead system will be employed. The wellhead and connection to the BOPE will meet all API 6A requirements. The BOP will be tested per 43 CFR part 3170 Subpart 3172 after installation on the surface casing which will cover testing requirements for a maximum of 30 days. If any seal subject to test pressure is broken the system must be tested. We will test the flange connection of the wellhead with a test port that is directly in the flange. We are proposing that we will run the wellhead through the rotary prior to cementing surface casing as discussed with the BLM on October 8, 2015.

See attached Schematics.

**BOP Break Testing Request**

Oxy requests permission to adjust the BOP break testing requirements as per the agreement reached in the OXY/BLM meeting on September 5, 2019. Please see BOP Break Testing Variance attachment for further details.

**Hammer Union Variance**

Oxy requests permission for hammer unions behind the choke to be routed to the gas buster. The hammer unions will not be subject to wellbore pressure in compliance with API STD 53.

**Oxy will use Cameron ADAPT wellhead system that uses an OEC top flange connection. This connection has been fully vetted and verified by API to Spec 6A and carries an API monogram.**

# Oxy Blanket Design - Casing Design "B"

## 5. Mud Program & Drilling Conditions

| Section | Depth - MD | | Depth - TVD | | Type | Weight (ppg) | Viscosity | Water Loss |
|---|---|---|---|---|---|---|---|---|
| | From (ft) | To (ft) | From (ft) | To (ft) | | | | |
| Surface | 0 | 1200 | 0 | 1200 | Water-Based Mud | 8.6 - 8.8 | 40-60 | N/C |
| Intermediate 1 | 1200 | 4832 | 1200 | 4832 | Saturated Brine-Based or Oil-Based Mud | 8.0 – 10.0 | 35-45 | N/C |
| Intermediate 2 | 1200 | 13111* | 1200 | 12775* | Saturated Brine-Based or Oil-Based Mud | 8.0 - 10.0 | 35-45 | N/C |
| Production | 13111 | 23361 | 12775 | 12775 | Water-Based or Oil-Based Mud | 9.5 - 13.5 | 38-50 | N/C |

*Curve could be in intermediate or production section*

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times. The following is a general list of products: Barite, Bentonite, Gypsum, Lime, Soda Ash, Caustic Soda, Nut Plug, Cedar Fiber, Cotton Seed Hulls, Drilling Paper, Salt Water Clay, CACL2. Oxy will use a closed mud system.

### Drilling Blind Request

In the event total losses are encountered in the intermediate section, Oxy requests permission to drill blind due to depleted formations where risk of hydrocarbon kicks are unlikely.

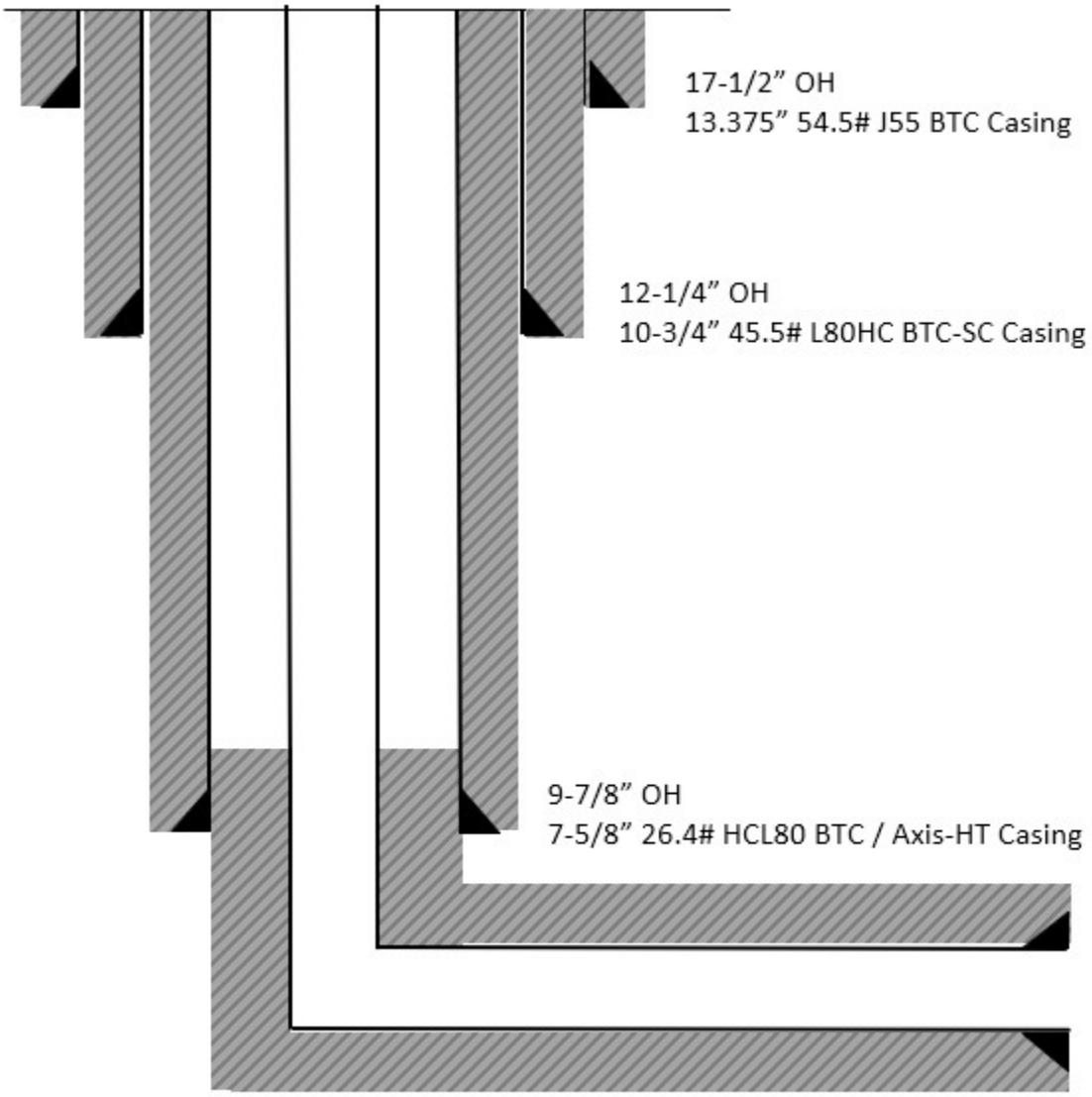
- Oxy will first attempt to cure losses before proceeding with drilling blind
- Drilling blind will only be allowed in the Castille and formations below
- While drilling blind, will monitor backside by filling-up on connections and utilizing gas monitors
- Depths at which losses occurred and attempt to cure losses with relevant details (LCM sweep info, etc.) will be documented in the drillers log and Subsequent Reports to the BLM.
- If a well control event (hydrocarbon kick) occurs while drilling blind, the BLM will be notified after the well is secured and returned to static.

| | |
|---|---|
| What will be used to monitor the loss or gain of fluid? | PVT/MD Totco/Visual Monitoring |

Pump high viscosity sweeps as needed for hole cleaning. The mud system will be monitored visually/manually as well as with an electronic PVT. The necessary mud products for additional weight and fluid loss control will be on location at all times. Appropriately weighted mud will be used to isolate potential gas, oil, and water zones until such time as casing can be cemented into place for zonal isolation.

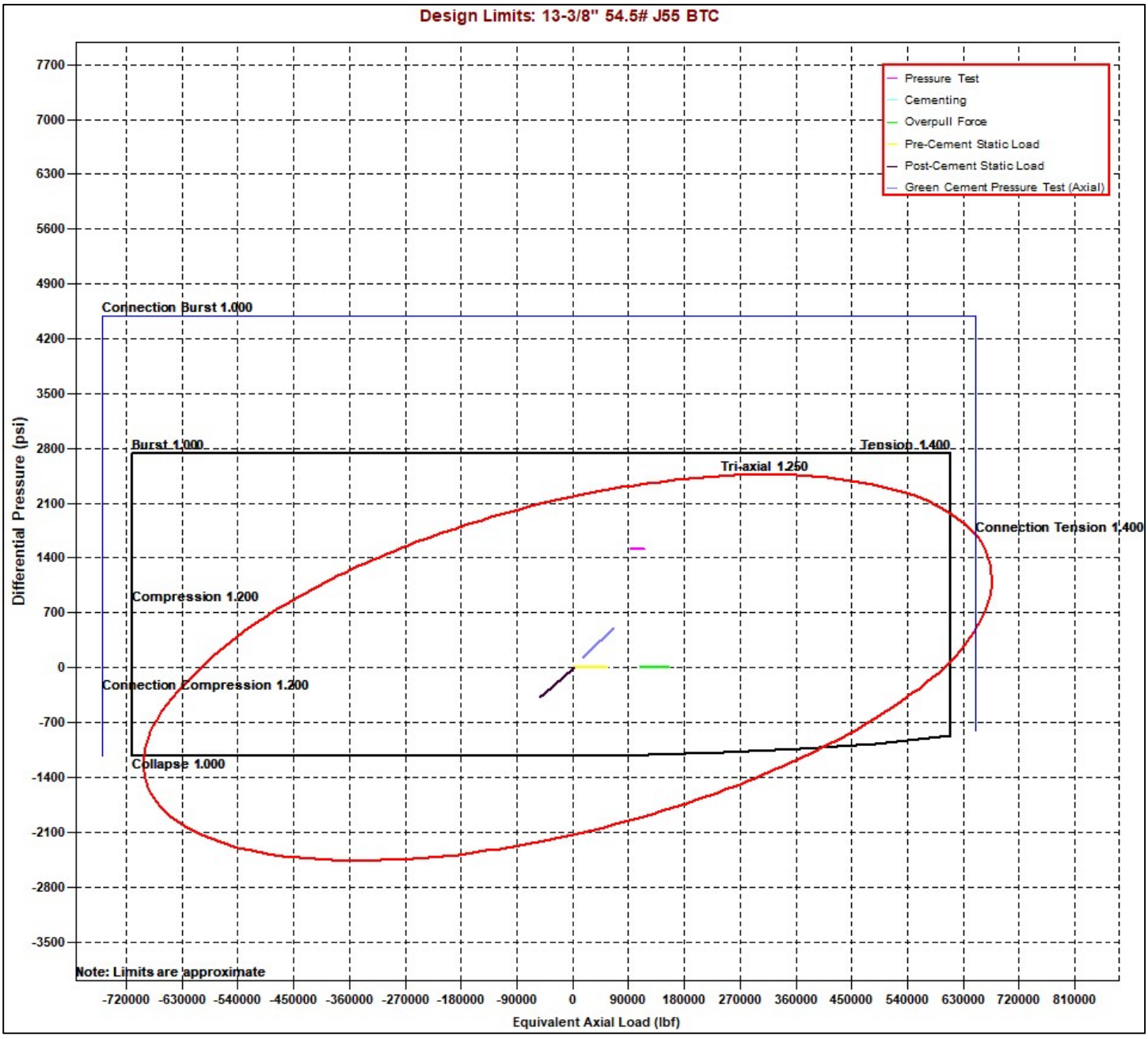
# Oxy Blanket Design - Casing Design “B”

## 6. Wellbore Diagram

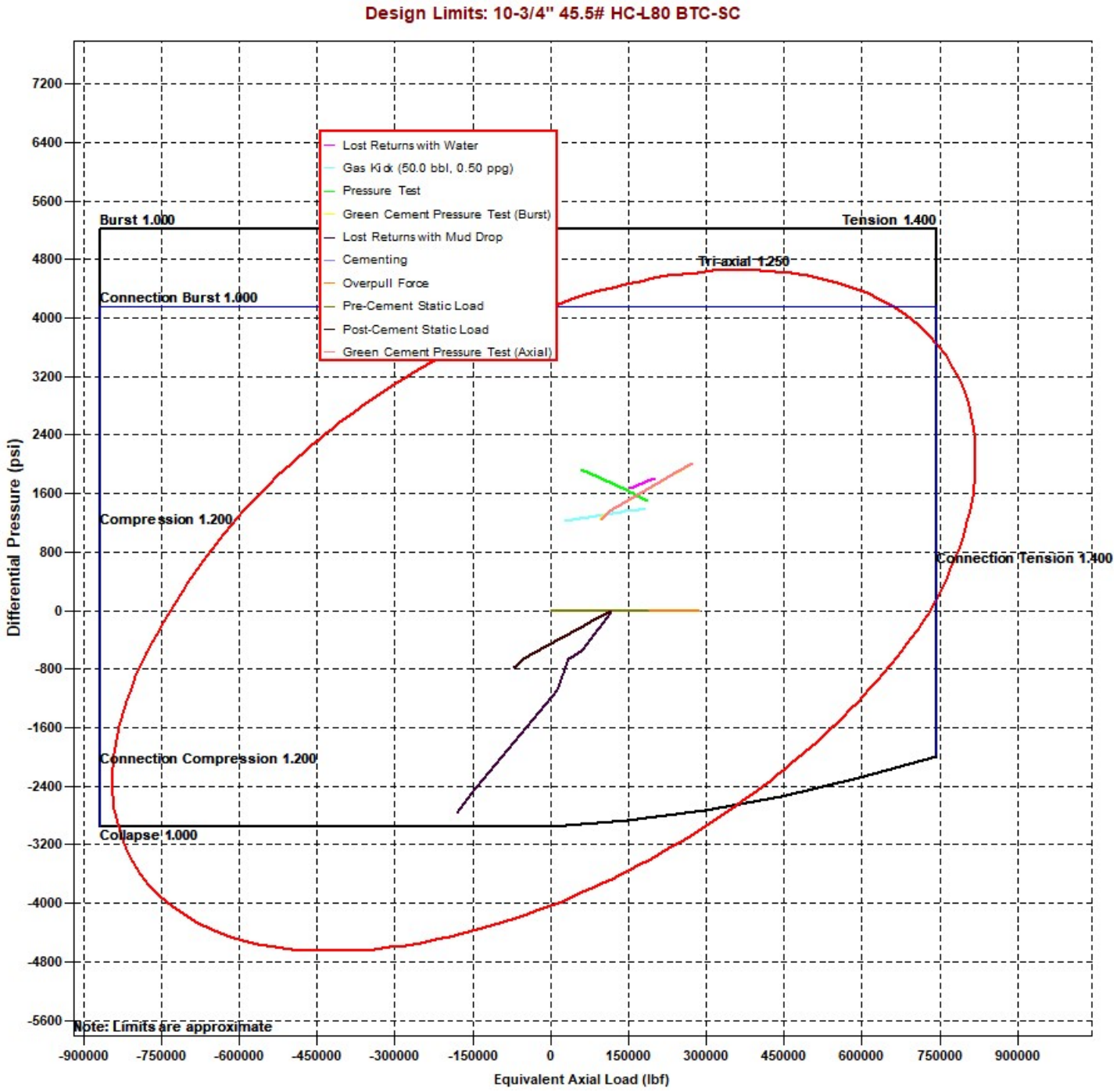


# Oxy Blanket Design - Casing Design “B”

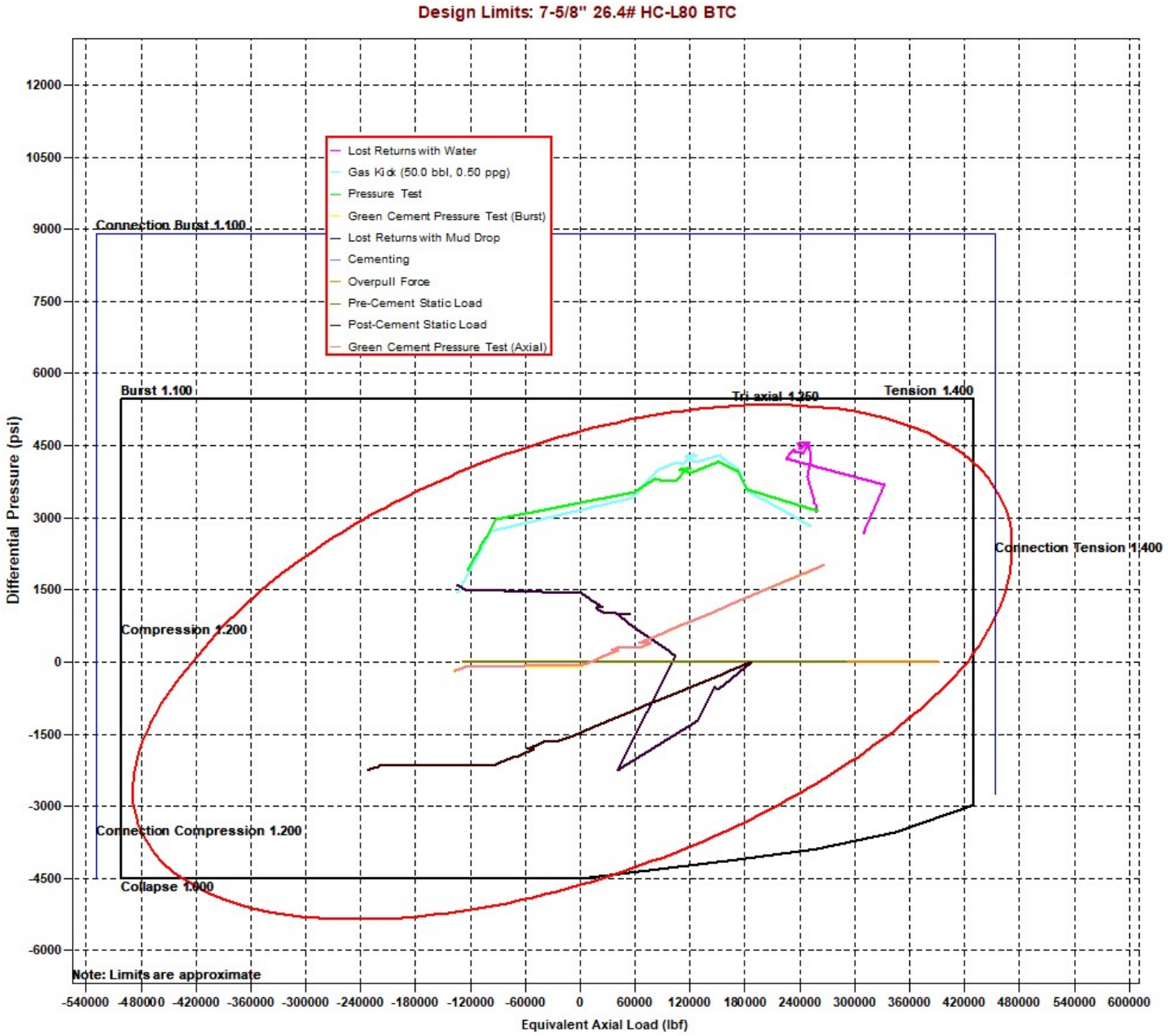
## 7. Landmark StressCheck Screenshots – Triaxial Output



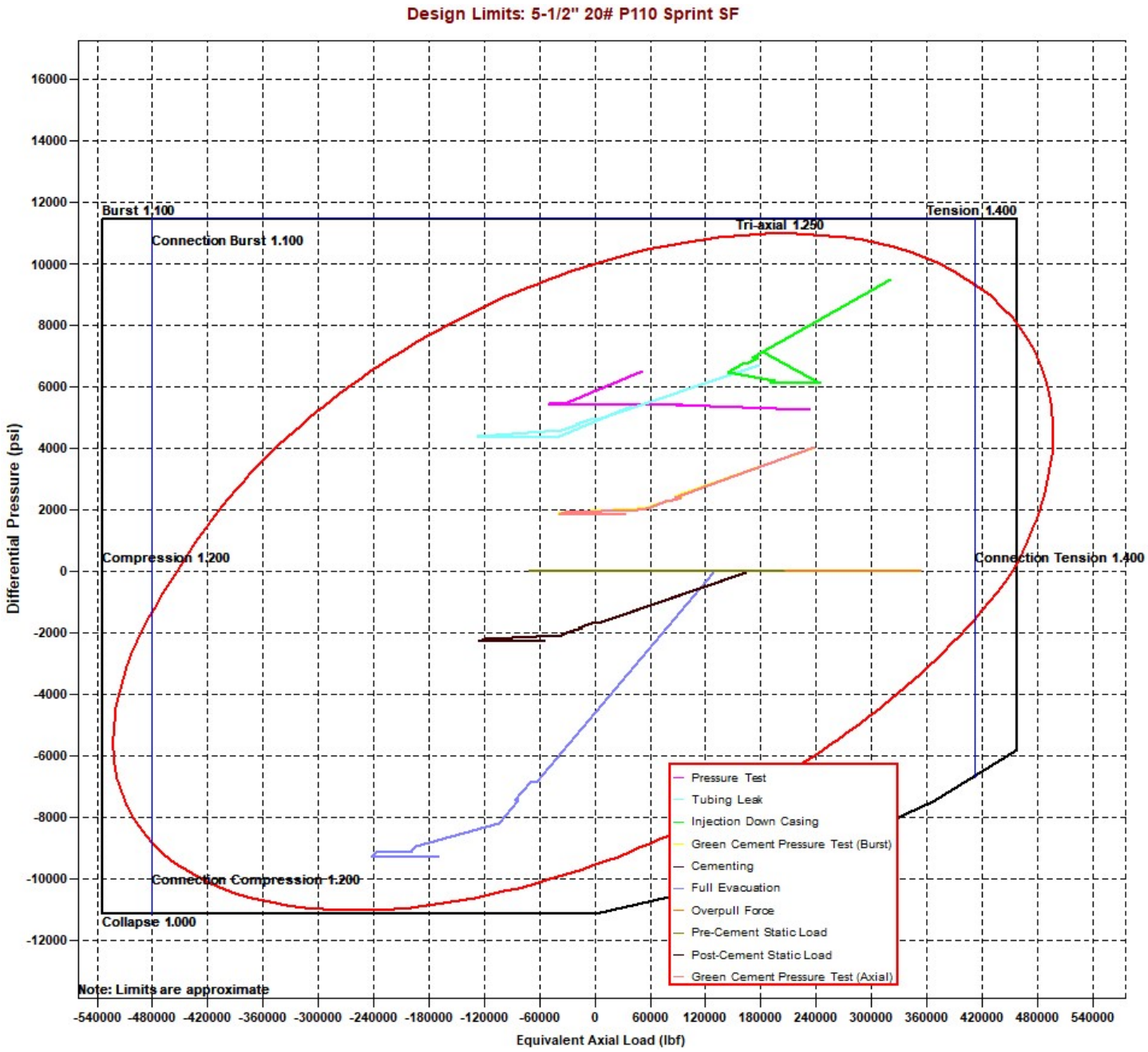
# Oxy Blanket Design - Casing Design "B"



# Oxy Blanket Design - Casing Design “B”



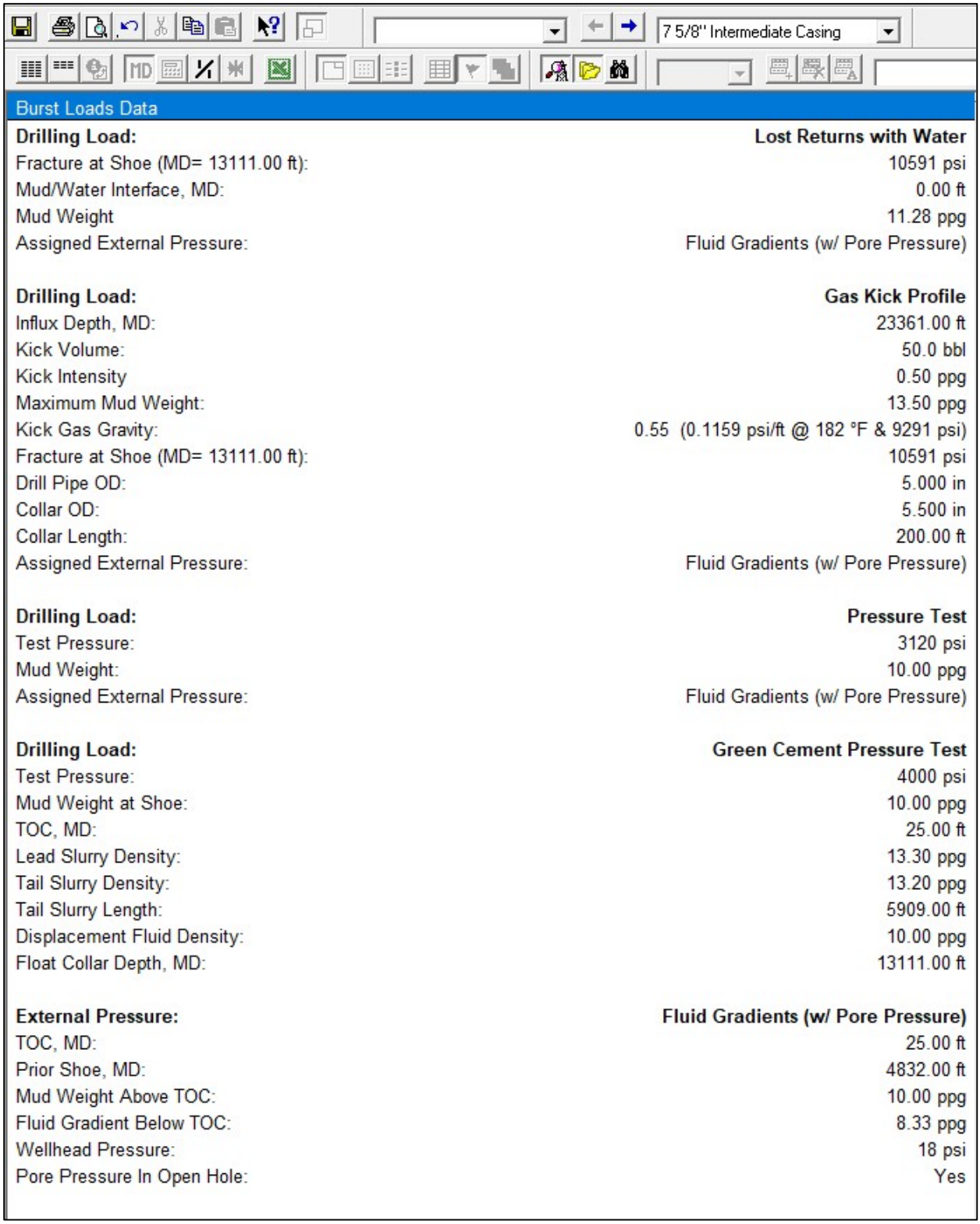
# Oxy Blanket Design - Casing Design "B"



# Oxy Blanket Design - Casing Design "B"

## 8. Landmark StressCheck Screenshots – Inputs for Intermediate 2 CSG Load Cases

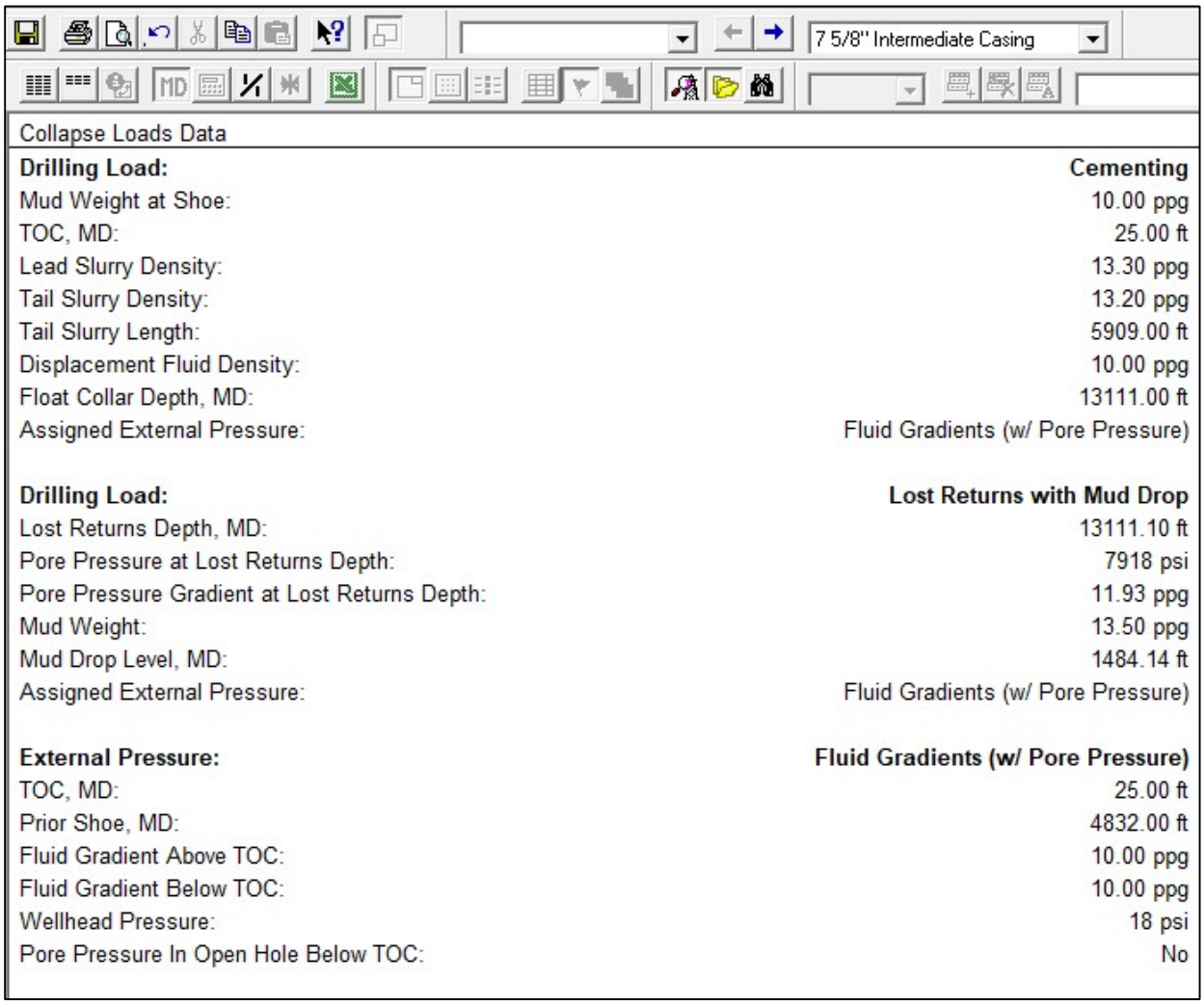
**Burst Load Cases**




| | |
|---|---|
| **Drilling Load:** | **Lost Returns with Water** |
| Fracture at Shoe (MD= 13111.00 ft): | 10591 psi |
| Mud/Water Interface, MD: | 0.00 ft |
| Mud Weight | 11.28 ppg |
| Assigned External Pressure: | Fluid Gradients (w/ Pore Pressure) |
| | |
| **Drilling Load:** | **Gas Kick Profile** |
| Influx Depth, MD: | 23361.00 ft |
| Kick Volume: | 50.0 bbl |
| Kick Intensity | 0.50 ppg |
| Maximum Mud Weight: | 13.50 ppg |
| Kick Gas Gravity: | 0.55 (0.1159 psi/ft @ 182 °F & 9291 psi) |
| Fracture at Shoe (MD= 13111.00 ft): | 10591 psi |
| Drill Pipe OD: | 5.000 in |
| Collar OD: | 5.500 in |
| Collar Length: | 200.00 ft |
| Assigned External Pressure: | Fluid Gradients (w/ Pore Pressure) |
| | |
| **Drilling Load:** | **Pressure Test** |
| Test Pressure: | 3120 psi |
| Mud Weight: | 10.00 ppg |
| Assigned External Pressure: | Fluid Gradients (w/ Pore Pressure) |
| | |
| **Drilling Load:** | **Green Cement Pressure Test** |
| Test Pressure: | 4000 psi |
| Mud Weight at Shoe: | 10.00 ppg |
| TOC, MD: | 25.00 ft |
| Lead Slurry Density: | 13.30 ppg |
| Tail Slurry Density: | 13.20 ppg |
| Tail Slurry Length: | 5909.00 ft |
| Displacement Fluid Density: | 10.00 ppg |
| Float Collar Depth, MD: | 13111.00 ft |
| | |
| **External Pressure:** | **Fluid Gradients (w/ Pore Pressure)** |
| TOC, MD: | 25.00 ft |
| Prior Shoe, MD: | 4832.00 ft |
| Mud Weight Above TOC: | 10.00 ppg |
| Fluid Gradient Below TOC: | 8.33 ppg |
| Wellhead Pressure: | 18 psi |
| Pore Pressure In Open Hole: | Yes |

# Oxy Blanket Design - Casing Design "B"

## Collapse Load Cases




Collapse Loads Data

| | |
|---|---|
| **Drilling Load:** | **Cementing** |
| Mud Weight at Shoe: | 10.00 ppg |
| TOC, MD: | 25.00 ft |
| Lead Slurry Density: | 13.30 ppg |
| Tail Slurry Density: | 13.20 ppg |
| Tail Slurry Length: | 5909.00 ft |
| Displacement Fluid Density: | 10.00 ppg |
| Float Collar Depth, MD: | 13111.00 ft |
| Assigned External Pressure: | Fluid Gradients (w/ Pore Pressure) |
| | |
| **Drilling Load:** | **Lost Returns with Mud Drop** |
| Lost Returns Depth, MD: | 13111.10 ft |
| Pore Pressure at Lost Returns Depth: | 7918 psi |
| Pore Pressure Gradient at Lost Returns Depth: | 11.93 ppg |
| Mud Weight: | 13.50 ppg |
| Mud Drop Level, MD: | 1484.14 ft |
| Assigned External Pressure: | Fluid Gradients (w/ Pore Pressure) |
| | |
| **External Pressure:** | **Fluid Gradients (w/ Pore Pressure)** |
| TOC, MD: | 25.00 ft |
| Prior Shoe, MD: | 4832.00 ft |
| Fluid Gradient Above TOC: | 10.00 ppg |
| Fluid Gradient Below TOC: | 10.00 ppg |
| Wellhead Pressure: | 18 psi |
| Pore Pressure In Open Hole Below TOC: | No |

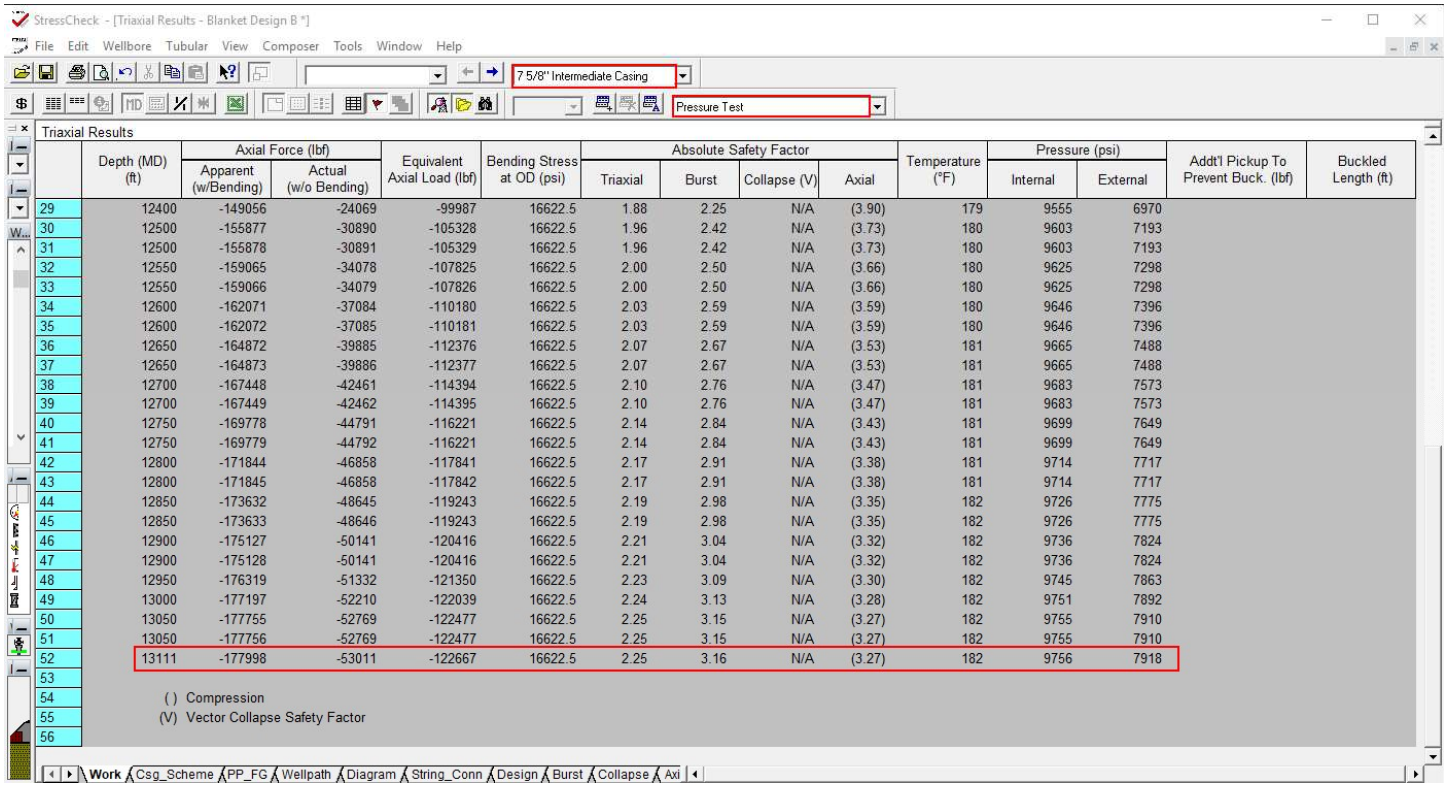
## Axial Load Cases


Axial Loads Data

| | |
|---|---|
| Overpull Force: | 100000 lbf |
| Pre-Cement Static Load: | Yes |
| Pickup Force: | 0 lbf |
| Post-Cement Static Load: | Yes |
| Green Cement Pressure Test: | 2000 psi |
| Service Loads: | Yes |

# Oxy Blanket Design - Casing Design "B"

## 9. Landmark StressCheck Screenshot – Int. Casing Triaxial Results Table (Pressure Test)



StressCheck - [Triaxial Results - Blanket Design B *]

File Edit Wellbore Tubular View Composer Tools Window Help

7 5/8" Intermediate Casing | Pressure Test

Triaxial Results

| | Depth (MD) (ft) | Axial Force (lbf) Apparent (w/Bending) | Axial Force (lbf) Actual (w/o Bending) | Equivalent Axial Load (lbf) | Bending Stress at OD (psi) | Absolute Safety Factor Triaxial | Burst | Collapse (V) | Axial | Temperature (°F) | Pressure (psi) Internal | External | Addt'l Pickup To Prevent Buck. (lbf) | Buckled Length (ft) |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 29 | 12400 | -149056 | -24069 | -99987 | 16622.5 | 1.88 | 2.25 | N/A | (3.90) | 179 | 9555 | 6970 | | |
| 30 | 12500 | -155877 | -30890 | -105328 | 16622.5 | 1.96 | 2.42 | N/A | (3.73) | 180 | 9603 | 7193 | | |
| 31 | 12500 | -155878 | -30891 | -105329 | 16622.5 | 1.96 | 2.42 | N/A | (3.73) | 180 | 9603 | 7193 | | |
| 32 | 12550 | -159065 | -34078 | -107825 | 16622.5 | 2.00 | 2.50 | N/A | (3.66) | 180 | 9625 | 7298 | | |
| 33 | 12550 | -159066 | -34079 | -107826 | 16622.5 | 2.00 | 2.50 | N/A | (3.66) | 180 | 9625 | 7298 | | |
| 34 | 12600 | -162071 | -37084 | -110180 | 16622.5 | 2.03 | 2.59 | N/A | (3.59) | 180 | 9646 | 7396 | | |
| 35 | 12600 | -162072 | -37085 | -110181 | 16622.5 | 2.03 | 2.59 | N/A | (3.59) | 180 | 9646 | 7396 | | |
| 36 | 12650 | -164872 | -39885 | -112376 | 16622.5 | 2.07 | 2.67 | N/A | (3.53) | 181 | 9665 | 7488 | | |
| 37 | 12650 | -164873 | -39886 | -112377 | 16622.5 | 2.07 | 2.67 | N/A | (3.53) | 181 | 9665 | 7488 | | |
| 38 | 12700 | -167448 | -42461 | -114394 | 16622.5 | 2.10 | 2.76 | N/A | (3.47) | 181 | 9683 | 7573 | | |
| 39 | 12700 | -167449 | -42462 | -114395 | 16622.5 | 2.10 | 2.76 | N/A | (3.47) | 181 | 9683 | 7573 | | |
| 40 | 12750 | -169778 | -44791 | -116221 | 16622.5 | 2.14 | 2.84 | N/A | (3.43) | 181 | 9699 | 7649 | | |
| 41 | 12750 | -169779 | -44792 | -116221 | 16622.5 | 2.14 | 2.84 | N/A | (3.43) | 181 | 9699 | 7649 | | |
| 42 | 12800 | -171844 | -46858 | -117841 | 16622.5 | 2.17 | 2.91 | N/A | (3.38) | 181 | 9714 | 7717 | | |
| 43 | 12800 | -171845 | -46858 | -117842 | 16622.5 | 2.17 | 2.91 | N/A | (3.38) | 181 | 9714 | 7717 | | |
| 44 | 12850 | -173632 | -48645 | -119243 | 16622.5 | 2.19 | 2.98 | N/A | (3.35) | 182 | 9726 | 7775 | | |
| 45 | 12850 | -173633 | -48646 | -119243 | 16622.5 | 2.19 | 2.98 | N/A | (3.35) | 182 | 9726 | 7775 | | |
| 46 | 12900 | -175127 | -50141 | -120416 | 16622.5 | 2.21 | 3.04 | N/A | (3.32) | 182 | 9736 | 7824 | | |
| 47 | 12900 | -175128 | -50141 | -120416 | 16622.5 | 2.21 | 3.04 | N/A | (3.32) | 182 | 9736 | 7824 | | |
| 48 | 12950 | -176319 | -51332 | -121350 | 16622.5 | 2.23 | 3.09 | N/A | (3.30) | 182 | 9745 | 7863 | | |
| 49 | 13000 | -177197 | -52210 | -122039 | 16622.5 | 2.24 | 3.13 | N/A | (3.28) | 182 | 9751 | 7892 | | |
| 50 | 13050 | -177755 | -52769 | -122477 | 16622.5 | 2.25 | 3.15 | N/A | (3.27) | 182 | 9755 | 7910 | | |
| 51 | 13050 | -177756 | -52769 | -122477 | 16622.5 | 2.25 | 3.15 | N/A | (3.27) | 182 | 9755 | 7910 | | |
| 52 | 13111 | -177998 | -53011 | -122667 | 16622.5 | 2.25 | 3.16 | N/A | (3.27) | 182 | 9756 | 7918 | | |
| 53 | | | | | | | | | | | | | | |
| 54 | ( ) Compression | | | | | | | | | | | | | |
| 55 | (V) Vector Collapse Safety Factor | | | | | | | | | | | | | |
| 56 | | | | | | | | | | | | | | |

Work | Csg_Scheme | PP_FG | Wellpath | Diagram | String_Conn | Design | Burst | Collapse | Axi

Internal Pressure = Surface Pressure + Hydrostatic = 9756 psi

External Pressure = Fluid Gradient w/ Pore Pressure = 7918 psi

Burst SF = 3.16

NOTE: *Specific load case inputs for the pressure test can be seen in **Section 8** above. The test pressure does not exceed 70% of the minimum internal yield.*

# Oxy Blanket Design - Casing Design “B”

## 10. Intermediate Non-API Casing Spec Sheet

Printed on: 06/19/2023

Tenaris

### API BTC -Special Clearance

| Coupling | Pipe Body |
|---|---|
| Grade: J55 (Casing) | Grade: J55 (Casing) |
| Body: Bright Green | 1st Band: Bright Green |
| 1st Band: White | 2nd Band: - |
| 2nd Band: - | 3rd Band: - |
| 3rd Band: - | 4th Band: - |

| | | | | | |
|---|---|---|---|---|---|
| Outside Diameter | 10.750 in. | Wall Thickness | 0.400 in. | Grade | J55 (Casing) |
| Min. Wall Thickness | 87.50 % | Pipe Body Drift | Alternative Drift | Type | Casing |
| Connection OD Option | Special Clearance | | | | |

**Pipe Body Data**

| Geometry | | | | Performance | |
|---|---|---|---|---|---|
| Nominal OD | 10.750 in. | Drift | 9.875 in. | SMYS | 55,000 psi |
| Wall Thickness | 0.400 in. | Plain End Weight | 44.26 lb/ft | Min UTS | 75,000 psi |
| Nominal Weight | 45.500 lb/ft | OD Tolerance | API | Body Yield Strength | 715 x1000 lb |
| Nominal ID | 9.950 in. | | | Min. Internal Yield Pressure | 3580 psi |
| | | | | Collapse Pressure | 2090 psi |
| | | | | Max. Allowed Bending | 23 °/100 ft |

**Connection Data**

| Geometry | | Performance | |
|---|---|---|---|
| Thread per In | 5 | Joint Strength | 796 x1000 lb |
| Connection OD | 11.250 in. | Coupling Face Load | 329 x1000 lb |
| Hand Tight Stand Off | 1 in. | Internal Pressure Capacity | 3290 psi |

Notes

For products according to API Standards 5CT & 5B; Performance calculated considering API Technical Report 5C3 (Sections 9 & 10) equations.
For geometrical and steel grades combinations not considered in the API Standards 5CT and/or 5B; Performance calculations indirectly derived from API Technical Report 5C3 (Sections 9 & 10) equations.
Couplings OD are shown according to current API 5CT 10th Edition.

# Oxy Blanket Design - Casing Design "B"

AXIS PIPE AND TUBE

## Technical Data Sheet

7 5/8" 26.40 lbs/ft. L80HC - Axis HT

| Mechanical Properties | | |
|---|---|---|
| Minimum Yield Strength | psi. | 80,000 |
| Maximum Yield Strength | psi. | 95,000 |
| Minimum Tensile Strength | psi. | 95,000 |

| Dimensions | | Pipe | AXIS HT |
|---|---|---|---|
| Outside Diameter | in. | 7.625 | 8.500 |
| Wall Thickness | in. | 0.328 | - |
| Inside Diameter | in. | 6.969 | - |
| Standard Drift | in. | 6.844 | 6.844 |
| Alternate Drift | in. | - | - |
| Plain End Weight | lbs/ft. | - | - |
| Nominal Linear Weight | lbs/ft. | 26.40 | - |

| Performance | | Pipe | AXIS HT |
|---|---|---|---|
| Minimum Collapse Pressure | psi. | 4,320 | - |
| Minimum Internal Yield Pressure | psi. | 6,020 | 6,020 |
| Minimum Pipe Body Yield Strength | lbs. | 602 x 1,000 | - |
| Joint Strength | lbs. | - | 635 x 1,000 |

| Make-Up Torques | | Pipe | AXIS HT |
|---|---|---|---|
| Optimum Make-Up Torque | ft/lbs. | - | 8,000 |
| Maximum Operational Torque | ft/lbs. | - | 25,000 |



## 11. Production Non-API Casing Spec Sheets

# Oxy Blanket Design - Casing Design “B”

Printed on: 11/09/2021

Tenaris

## TenarisHydril Wedge 461 ® MS

| Coupling | Pipe Body |
|---|---|
| Grade: P110-ICY | Grade: P110-ICY |
| Body: White | 1st Band: White |
| 1st Band: Pale Green | 2nd Band: Pale Green |
| 2nd Band: - | 3rd Band: Pale Green |
| 3rd Band: - | 4th Band: - |
| | 5th Band: - |
| | 6th Band: - |

| | | | | | |
|---|---|---|---|---|---|
| Outside Diameter | 5.500 in. | Wall Thickness | 0.361 in. | Grade | P110-ICY |
| Min. Wall Thickness | 87.50 % | Pipe Body Drift | API Standard | Type | Casing |
| Connection OD Option | MS | | | | |

### Pipe Body Data

| Geometry | | | | Performance | |
|---|---|---|---|---|---|
| Nominal OD | 5.500 in. | Wall Thickness | 0.361 in. | Body Yield Strength | 729 x1000 lb |
| Nominal Weight | 20 lb/ft | Plain End Weight | 19.83 lb/ft | Min. Internal Yield Pressure | 14,360 psi |
| Drift | 4.653 in. | OD Tolerance | API | SMYS | 125,000 psi |
| Nominal ID | 4.778 in. | | | Collapse Pressure | 12,300 psi |

### Connection Data

| Geometry | | Performance | | Make-Up Torques | |
|---|---|---|---|---|---|
| Connection OD | 6.050 in. | Tension Efficiency | 100 % | Minimum | 17,000 ft-lb |
| Coupling Length | 7.714 in. | Joint Yield Strength | 729 x1000 lb | Optimum | 18,000 ft-lb |
| Connection ID | 4.778 in. | Internal Pressure Capacity | 14,360 psi | Maximum | 21,600 ft-lb |
| Make-up Loss | 3.775 in. | Compression Efficiency | 100 % | | |
| Threads per inch | 3.40 | Compression Strength | 729 x1000 lb | Operation Limit Torques | |
| Connection OD Option | Ms | Max. Allowable Bending | 104 °/100 ft | Operating Torque | 43,000 ft-lb |
| | | External Pressure Capacity | 12,300 psi | Yield Torque | 51,000 ft-lb |
| | | Coupling Face Load | 273,000 lb | | |
| | | | | Buck-On | |
| | | | | Minimum | 21,600 ft-lb |
| | | | | Maximum | 23,100 ft-lb |

### Notes

This connection is fully interchangeable with:
Wedge 441® - 5.5 in. - 0.304 / 0.361 in.
Wedge 461® - 5.5 in. - 0.304 / 0.415 / 0.476 in.
Connections with Dopeless® Technology are fully compatible with the same connection in its Standard version
In October 2019, TenarisHydril Wedge XP® 2.0 was renamed TenarisHydril Wedge 461™. Product dimensions and properties remain identical and both connections are fully interchangeable

For the lastest performance data, always visit our website: www.tenaris.com

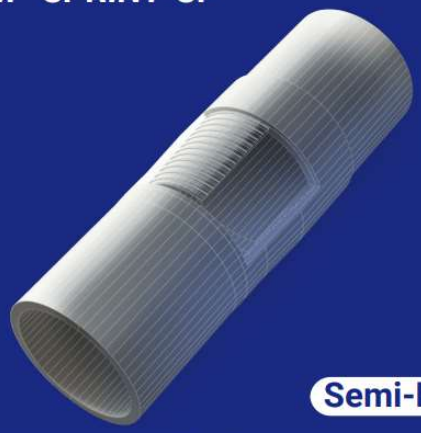
# Oxy Blanket Design - Casing Design “B”

Generated on May 21, 2024

## CONNECTION DATA SHEET

OD: **5.500 in.** Grade: **P110**
Weight: **20.00 lb/ft** Drift: **4.653 in. (API)**
Wall Th.: **0.361 in.**

### VAM® SPRINT-SF



Semi-Flush

**Field Torque Values**

**Make-up Torque (ft-lb)**
20,000 **MIN**
22,500 **OPTI**
25,000 **MAX**

**Torque with Sealability (ft-lb)**
36,000 **MTS**

**Locked Flank Torque (ft-lb)**
4,500 **MIN**
15,750 **MAX**

*(2) MTS: Maximum Torque with Sealability.*

### PIPE BODY PROPERTIES

| | | |
|---|---|---|
| **Nominal OD** | 5.500 | *in.* |
| **Nominal ID** | 4.778 | *in.* |
| **Nominal Wall Thickness** | 0.361 | *in.* |
| **Minimum Wall Thickness** | 87.5 | *%* |
| **Nominal Weight (API)** | 20.00 | *lb/ft* |
| **Plain End Weight** | 19.83 | *lb/ft* |
| **Drift** | 4.653 | *in.* |
| **Grade Type** | API 5CT | |
| **Minimum Yield Strength** | 110 | *ksi* |
| **Maximum Yield Strength** | 140 | *ksi* |
| **Minimum Ultimate Tensile Strength** | 125 | *ksi* |
| **Pipe Body Yield Strength** | 641 | *klb* |
| **Internal Yield Pressure** | 12,640 | *psi* |
| **Collapse Pressure** | 11,100 | *psi* |

### CONNECTION PROPERTIES

| | | |
|---|---|---|
| **Connection Type** | Semi-Premium Integral Semi-Flu | |
| **Nominal Connection OD** | 5.783 | *in.* |
| **Nominal Connection ID** | 4.718 | *in.* |
| **Make-up Loss** | 5.965 | *in.* |
| **Tension Efficiency** | 90 | *% Pipe Body* |
| **Compression Efficiency** | 90 | *% Pipe Body* |
| **Internal Pressure Efficiency** | 100 | *% Pipe Body* |
| **External Pressure Efficiency** | 100 | *% Pipe Body* |

### JOINT PERFORMANCES

| | | |
|---|---|---|
| **Tension Strength** | 577 | *klb* |
| **Compression Strength** | 577 | *klb* |
| **Internal Pressure Resistance** | 12,640 | *psi* |
| **External Pressure Resistance** | 11,100 | *psi* |
| **Maximum Bending, Structural** | 78 | *°/100 ft* |
| **Maximum Bending, with Sealability(1)** | 30 | *°/100 ft* |

*(1) Sealability rating demonstrated as per API RP 5C5 / ISO 13679*

# Oxy Blanket Design - Casing Design "B"

DWC/C-HT-IS

## Connection Data Sheet

| OD (in.) | WEIGHT (lbs./ft.) | WALL (in.) | GRADE | API DRIFT (in.) | RBW% | CONNECTION |
|---|---|---|---|---|---|---|
| 5.500 | Nominal: 20.00<br>Plain End: 19.83 | 0.361 | ‡VST P110MY | 4.653 | 87.5 | DWC/C-HT-IS |

| PIPE PROPERTIES | | |
|---|---|---|
| Nominal OD | 5.500 | in. |
| Nominal ID | 4.778 | in. |
| Nominal Area | 5.828 | sq.in. |
| Grade Type | | API 5CT |
| Min. Yield Strength | 125 | ksi |
| Max. Yield Strength | 140 | ksi |
| Min. Tensile Strength | 135 | ksi |
| Yield Strength | 729 | klb |
| Ultimate Strength | 787 | klb |
| Min. Internal Yield Pressure | 14,360 | psi |
| Collapse Pressure | 12,090 | psi |

| CONNECTION PROPERTIES | | |
|---|---|---|
| Connection Type | Semi-Premium T&C | |
| Connection OD (nom) | 6.050 | in. |
| Connection ID (nom) | 4.778 | in. |
| Make-Up Loss | 4.125 | in. |
| Coupling Length | 9.250 | in. |
| Critical Cross Section | 5.828 | sq.in. |
| Tension Efficiency | 89.1% | of pipe |
| Compression Efficiency | 88.0% | of pipe |
| Internal Pressure Efficiency | 86.1% | of pipe |
| External Pressure Efficiency | 100.0% | of pipe |

| CONNECTION PERFORMANCES | | |
|---|---|---|
| Yield Strength | 649 | klb |
| Parting Load | 729 | klb |
| Compression Rating | 641 | klb |
| Min. Internal Yield Pressure | 12,360 | psi |
| External Pressure Resistance | 12,090 | psi |
| Maximum Uniaxial Bend Rating | 91.7 | °/100 ft |
| Reference String Length w 1.4 Design Factor | 22,890 | ft. |

| FIELD TORQUE VALUES | | |
|---|---|---|
| Min. Make-up torque | 16,600 | ft.lb |
| Opti. Make-up torque | 17,950 | ft.lb |
| Max. Make-up torque | 19,300 | ft.lb |
| Min. Shoulder Torque | 1,660 | ft.lb |
| Max. Shoulder Torque | 13,280 | ft.lb |
| Max. Delta Turn | 0.200 | Turns |
| †Maximum Operational Torque | 23,800 | ft.lb |
| †Maximum Torsional Value (MTV) | 26,180 | ft.lb |

**† Maximum Operational Torque and Maximum Torsional Value only valid with Vallourec P110MY Material.**
**‡ P110MY - Coupling Min Yield Strength is 110ksi and Coupling Max Yield is 125ksi.**

"VST = Vallourec Star as the mill source for the pipe, "P110EC" is the grade name"

**Need Help? Contact: tech.support@vam-usa.com**

**For detailed information on performance properties, refer to DWC Connection Data Notes on following page(s).**

Connection specifications within the control of VAM USA were correct as of the date printed. Specifications are subject to change without notice. Certain connection specifications are dependent on the mechanical properties of the pipe. Mechanical properties of mill proprietary pipe grades were obtained from mill publications and are subject to change. Properties of mill proprietary grades should be confirmed with the mill. Users are advised to obtain current connection specifications and verify pipe mechanical properties for each application.

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03/04/2024 08:36:50 PM

VAM USA

# Oxy Blanket Design - Casing Design “B”

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VAM® USA Sales E-mail: VAMUSAsales@vam-usa.com
Tech Support Email: tech.support@vam-usa.com

**DWC Connection Data Sheet Notes:**

1. DWC connections are available with a seal ring (SR) option.
2. All standard DWC/C connections are interchangeable for a given pipe OD. DWC connections are interchangeable with DWC/C-SR connections of the same OD and wall.
3. Connection performance properties are based on nominal pipe body and connection dimensions.
4. DWC connection internal and external pressure resistance is calculated using the API rating for buttress connections. API Internal pressure resistance is calculated from formulas 31, 32, and 35 in the API Bulletin 5C3.
5. DWC joint strength is the minimum pipe body yield strength multiplied by the connection critical area.
6. API joint strength is for reference only. It is calculated from formulas 42 and 43 in the API Bulletin 5C3.
7. Bending efficiency is equal to the compression efficiency.
8. The torque values listed are recommended. The actual torque required may be affected by field conditions such as temperature, thread compound, speed of make-up, weather conditions, etc.
9. Connection yield torque is not to be exceeded.
10. Reference string length is calculated by dividing the joint strength by both the nominal weight in air and a design factor (DF) of 1.4. These values are offered for reference only and do not include load factors such as bending, buoyancy, temperature, load dynamics, etc.
11. DWC connections will accommodate API standard drift diameters.
12. DWC/C family of connections are compatible with API Buttress BTC connections. Please contact tech.support@vam-usa.com for details on connection ratings and make-up.



03/04/2024 08:36:50 PM

# Oxy USA Inc. - TUNA NUT 24_13 FED COM 23H
## Drill Plan

### 1. Geologic Formations

| | | | |
|---|---|---|---|
| TVD of Target (ft): | 10874 | Pilot Hole Depth (ft): | |
| Total Measured Depth (ft): | 21155 | Deepest Expected Fresh Water (ft): | 1027 |

**Delaware Basin**

| Formation | MD-RKB (ft) | TVD-RKB (ft) | Expected Fluids |
|---|---|---|---|
| Rustler | 1027 | 1027 | |
| Salado | 1686 | 1686 | Salt |
| Castile | 3478 | 3478 | Salt |
| Delaware | 4898 | 4898 | Oil/Gas/Brine |
| Bell Canyon | 4989 | 4989 | Oil/Gas/Brine |
| Cherry Canyon | 5786 | 5786 | Oil/Gas/Brine |
| Brushy Canyon | 7093 | 7093 | Losses |
| Bone Spring | 8741 | 8733 | Oil/Gas |
| Bone Spring 1st | 9863 | 9838 | Oil/Gas |
| Bone Spring 2nd | 10562 | 10524 | Oil/Gas |
| Bone Spring 3rd | | | Oil/Gas |
| Wolfcamp | | | Oil/Gas |
| Penn | | | Oil/Gas |
| Strawn | | | Oil/Gas |

*H2S, water flows, loss of circulation, abnormal pressures, etc.

### 2. Casing Program

| | | MD | | TVD | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| Section | Hole Size (in) | From (ft) | To (ft) | From (ft) | To (ft) | Csg. OD (in) | Csg Wt. (ppf) | Grade | Conn. |
| Surface | 17.5 | 0 | 1087 | 0 | 1087 | 13.375 | 54.5 | J-55 | BTC |
| Intermediate | 9.875 | 0 | 10148 | 0 | 10117 | 7.625 | 26.4 | L-80 HC | BTC |
| Production | 6.75 | 0 | 21155 | 0 | 10874 | 5.5 | 20 | P-110 | Sprint-SF |

All casing strings will be tested in accordance with 43 CFR part 3170 Subpart 3172

*Oxy requests the option to run the 10.75" Intermediate I as a contingency string to be run only if severe hole conditions dictate an additional casing string necessary. This would make the planned 7.625" / 7.827" Casing the Intermediate II.
**If 4S Contingency is not required, Oxy requests permission to transition from 12.25" to 9.875" Intermediate I at 1st trip point below Brushy top (estimated top in formation table above). Cement volumes will be updated on C103 submission.

| *All Casing SF Values will meet or exceed those below* | | | |
|---|---|---|---|
| **SF Collapse** | **SF Burst** | **Body SF Tension** | **Joint SF Tension** |
| 1.00 | 1.100 | 1.4 | 1.4 |

| | Y or N |
|---|---|
| Is casing new? If used, attach certification as required in 43 CFR 3160 | Y |
| Does casing meet API specifications? If no, attach casing specification sheet. | Y |
| Is premium or uncommon casing planned? If yes attach casing specification sheet. | Y |
| Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria). | Y |
| Will the intermediate pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing? | Y |
| | |
| Is well located within Capitan Reef? | N |
| If yes, does production casing cement tie back a minimum of 50' above the Reef? | |
| Is well within the designated 4 string boundary. | |
| | |
| Is well located in SOPA but not in R-111-Q? | N |
| If yes, are the first 2 strings cemented to surface and 3rd string cement tied back 500' into previous casing? | |
| | |
| Is well located in R-111-Q and SOPA? | N |
| If yes, are the first three strings cemented to surface? | |
| Is 2nd string set 100' to 600' below the base of salt? | |
| | |
| Is well located in high Cave/Karst? | N |
| If yes, are there two strings cemented to surface? | |
| (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs? | |
| | |
| Is well located in critical Cave/Karst? | N |
| If yes, are there three strings cemented to surface? | |

## 3. Cementing Program

| Section | Stage | Slurry: | Sacks | Yield (ft^3/ft) | Density (lb/gal) | Excess: | TOC | Placement | Description |
|---|---|---|---|---|---|---|---|---|---|
| Surface | 1 | Surface - Tail | 1135 | 1.33 | 14.8 | 100% | - | Circulate | Class C+Accel. |
| Int. | 1 | Intermediate 1S - Tail | 377 | 1.68 | 13.2 | 5% | 7,343 | Circulate | Class C+Ret., Disper. |
| Int. | 2 | Intermediate 2S - Tail BH | 1332 | 1.71 | 13.3 | 25% | - | Bradenhead | Class C+Accel. |
| Prod. | 1 | Production - Tail | 652 | 1.84 | 13.3 | 25% | 9,648 | Circulate | Class C+Ret. |

**Offline Cementing Request**

Oxy requests a variance to cement the 9.625” and/or 7.625” intermediate casing strings offline in accordance to the approved variance, EC Tran 461365. Please see Offline Cementing Variance attachment for further details.

**Bradenhead CBL Request**

Oxy requests permission to adjust the CBL requirement after bradenhead cement jobs, on 7-5/8” intermediate casings, as per the agreement reached in the OXY/BLM meeting on September 5, 2019. Please see Bradenhead CBL Variance attachment for further details.

## 4. Pressure Control Equipment

| BOP installed and tested before drilling which hole? | Size? | Min. Required WP | Type | ✓ | Tested to: | Deepest TVD Depth (ft) per Section: |
|---|---|---|---|---|---|---|
| 9.875" Hole | 13-5/8" | 5M | Annular | ✓ | 70% of working pressure | 10117 |
| | | 5M | Blind Ram | ✓ | 250 psi / 5000 psi | |
| | | | Pipe Ram | | | |
| | | | Double Ram | ✓ | | |
| | | | Other* | | | |
| 6.75" Hole | 13-5/8" | 5M | Annular | ✓ | 70% of working pressure | 10874 |
| | | 5M | Blind Ram | ✓ | 250 psi / 5000 psi | |
| | | | Pipe Ram | | | |
| | | | Double Ram | ✓ | | |
| | | | Other* | | | |

*Specify if additional ram is utilized

BOP/BOPE will be tested by an independent service company to 250 psi low and the high pressure indicated above per 43 CFR part 3170 Subpart 3172 requirements. The System may be upgraded to a higher pressure but still tested to the working pressure listed in the table above. If the system is upgraded all the components installed will be functional and tested.

Pipe rams will be operationally checked each 24 hour period. Blind rams will be operationally checked on each trip out of the hole. These checks will be noted on the daily tour sheets. Other accessories to the BOP equipment will include a Kelly cock and floor safety valve (inside BOP) and choke lines and choke manifold.

| | |
|---|---|
| | Formation integrity test will be performed per 43 CFR part 3170 Subpart 3172. |
| | On Exploratory wells or on that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Will be tested in accordance with 43 CFR part 3170 Subpart 3172. |
| | |
| | A variance is requested for the use of a flexible choke line from the BOP to Choke Manifold. See attached for specs and hydrostatic test chart. |
| | Y Are anchors required by manufacturer? |
| | A multibowl or a unionized multibowl wellhead system will be employed. The wellhead and connection to the BOPE will meet all API 6A requirements. The BOP will be tested per 43 CFR part 3170 Subpart 3172 after installation on the surface casing which will cover testing requirements for a maximum of 30 days. If any seal subject to test pressure is broken the system must be tested. We will test the flange connection of the wellhead with a test port that is directly in the flange. We are proposing that we will run the wellhead through the rotary prior to cementing surface casing as discussed with the BLM on October 8, 2015.<br><br>See attached schematics. |

**BOP Break Testing Request**

Oxy requests permission to adjust the BOP break testing requirements as per the agreement reached in the OXY/BLM meeting on September 5, 2019. Please see BOP Break Testing Variance attachment for further details.

**Oxy will use Cameron ADAPT wellhead system that uses an OEC top flange connection. This connection has been fully vetted and verified by API to Spec 6A and carries an API monogram.**

## 5. Mud Program

| Section | Depth - MD | | Depth - TVD | | Type | Weight (ppg) | Viscosity | Water Loss |
|---|---|---|---|---|---|---|---|---|
| | From (ft) | To (ft) | From (ft) | To (ft) | | | | |
| Surface | 0 | 1087 | 0 | 1087 | Water-Based Mud | 8.6 - 8.8 | 40-60 | N/C |
| Intermediate | 1087 | 10148 | 1087 | 10117 | Saturated Brine-Based or Oil-Based Mud | 8.0 - 10.0 | 35-45 | N/C |
| Production | 10148 | 21155 | 10117 | 10874 | Water-Based or Oil-Based Mud | 8.0 - 9.6 | 38-50 | N/C |

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times. The following is a general list of products: Barite, Bentonite, Gypsum, Lime, Soda Ash, Caustic Soda, Nut Plug, Cedar Fiber, Cotton Seed Hulls, Drilling Paper, Salt Water Clay, CACL2. Oxy will use a closed mud system.

| | |
|---|---|
| What will be used to monitor the loss or gain of fluid? | PVT/MD Totco/Visual Monitoring |

## 6. Logging and Testing Procedures

| Logging, Coring and Testing. | |
|---|---|
| Yes | Will run GR from TD to surface (horizontal well – vertical portion of hole). |
| | Stated logs run will be in the Completion Report and submitted to the BLM. |
| No | Logs are planned based on well control or offset log information. |
| No | Drill stem test? If yes, explain |
| No | Coring? If yes, explain |

| Additional logs planned | | Interval |
|---|---|---|
| No | Resistivity | |
| No | Density | |
| Yes | CBL | Production string |
| Yes | Mud log | Bone Spring – TD |
| No | PEX | |

## 7. Drilling Conditions

| Condition | Specify what type and where? |
|---|---|
| BH Pressure at deepest TVD | 5429 psi |
| Abnormal Temperature | No |
| BH Temperature at deepest TVD | 167°F |

Pump high viscosity sweeps as needed for hole cleaning. The mud system will be monitored visually/manually as well as with an electronic PVT. The necessary mud products for additional weight and fluid loss control will be on location at all times. Appropriately weighted mud will be used to isolate potential gas, oil, and water zones until such time as casing can be cemented into place for zonal

| Hydrogen Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the operator will comply with the provisions of 43 CFR part 3170 Subpart 3172. If Hydrogen Sulfide is encountered, measured values and formations will be provided to the BLM. | |
|---|---|
| N | H2S is present |
| Y | H2S Plan attached |

## 8. Other facets of operation

| | Yes/No |
|---|---|
| Will the well be drilled with a walking/skidding operation? If yes, describe.<br>We plan to drill the 4 well pad in batch by section: all surface sections, intermediate sections and production sections. The wellhead will be secured with a night cap whenever the rig is not over the well. | Yes |
| Will more than one drilling rig be used for drilling operations? If yes, describe.<br>Oxy requests the option to contract a Surface Rig to drill, set surface casing, and cement for this well. If the timing between rigs is such that Oxy would not be able to preset surface, the Primary Rig will MIRU and drill the well in its entirety per the APD. Please see the attached document for information on the spudder rig. | Yes |

**Total Estimated Cuttings Volume:** 1669 bbls

# C-102

Submit Electronically
Via OCD Permitting

## State of New Mexico
## Energy, Minerals, & Natural Resources Department
## OIL CONSERVATION DIVISION

Revised July 9, 2024
PAGE 1 OF 2

Submittal Type: ☐ Initial Submittal ☑ Amended Report ☐ As Drilled

### WELL LOCATION INFORMATION

| API Number | Pool Code | Pool Name |
|---|---|---|
| 30-025-54090 | 51683 | RED TANK; BONE SPRING |

| Property Code | Property Name | Well Number |
|---|---|---|
| | TUNA NUT 24_13 FED COM | 23H |

| OGRID No. | Operator Name | Ground Level Elevation |
|---|---|---|
| 16696 | OXY USA INC. | 3761' |

Surface Owner: ☐ State ☐ Fee ☐ Tribal ☑ Federal
Mineral Owner: ☐ State ☐ Fee ☐ Tribal ☑ Federal

### Surface Location

| UL | Section | Township | Range | Lot | Ft. from N/S | Ft. from E/W | Latitude (NAD83) | Longitude (NAD83) | County |
|---|---|---|---|---|---|---|---|---|---|
| M | 24 | 22S | 32E | | 390' FSL | 1155' FWL | 32.37111843 | -103.63316613 | LEA |

### Bottom Hole Location

| UL | Section | Township | Range | Lot | Ft. from N/S | Ft. from E/W | Latitude (NAD83) | Longitude (NAD83) | County |
|---|---|---|---|---|---|---|---|---|---|
| C | 13 | 22S | 32E | | 20' FNL | 1400' FWL | 32.39902994 | -103.63239520 | LEA |

| Dedicated Acres | Infill or Defining Well | Defining Well API | Overlapping Spacing Unit (Y/N) | Consolidation Code |
|---|---|---|---|---|
| 1280.00 | INFILL | N/A | N | N/A |

Order Numbers: TBD
Well setbacks are under Common Ownership: ☐ Yes ☒ No

### Kick Off Point (KOP)

| UL | Section | Township | Range | Lot | Ft. from N/S | Ft. from E/W | Latitude (NAD83) | Longitude (NAD83) | County |
|---|---|---|---|---|---|---|---|---|---|
| N | 24 | 22S | 32E | | 50' FSL | 1400' FWL | 32.37018788 | -103.63237096 | LEA |

### First Take Point (FTP)

| UL | Section | Township | Range | Lot | Ft. from N/S | Ft. from E/W | Latitude (NAD83) | Longitude (NAD83) | County |
|---|---|---|---|---|---|---|---|---|---|
| N | 24 | 22S | 32E | | 100' FSL | 1400' FWL | 32.37032529 | -103.63237107 | LEA |

### Last Take Point (LTP)

| UL | Section | Township | Range | Lot | Ft. from N/S | Ft. from E/W | Latitude (NAD83) | Longitude (NAD83) | County |
|---|---|---|---|---|---|---|---|---|---|
| C | 13 | 22S | 32E | | 100' FNL | 1400' FWL | 32.39881004 | -103.63239499 | LEA |

| Unitized Area or Area of Uniform Interest | Spacing Unit Type | Ground Floor Elevation |
|---|---|---|
| N | ☒ Horizontal ☐ Vertical | 3761' |

### OPERATOR CERTIFICATIONS

*I hereby certify that the information contained herein is true and complete to the best of my knowledge and belief, and, if the well is a vertical or directional well, that this organization either owns a working interest or unleased mineral interest in the land including the proposed bottom hole location or has a right to drill this well at this location pursuant to a contract with an owner of a working interest or unleased mineral interest, or to a voluntary pooling agreement or a compulsory pooling order heretofore entered by the division.*

*If this well is a horizontal well, I further certify that this organization has received the consent of at least one lessee or owner of a working interest or unleased mineral interest in each tract (in the target pool or formation) in which any part of the well's completed interval will be located or obtained a compulsory pooling order from the division.*

Melissa Guidry 03/27/25
Signature Date

Melissa Guidry
Printed Name

melissa_guidry@oxy.com
Email Address

### SURVEYOR CERTIFICATIONS

*I hereby certify that the well location shown on this plat was plotted from field notes of actual surveys made by me or under my supervision, and that the same is true and correct to the best of my belief.*

LLOYD P. SHORT NEW MEXICO 21653 PROFESSIONAL SURVEYOR

Signature and Seal of Professional Surveyor

| Certificate Number | Date of Survey |
|---|---|
| 21653 | NOVEMBER 27, 2024 |


No allowable will be assigned to this completion until all interests have been consolidated or a non-standard unit has been approved by the division.

ACREAGE DEDICATION PLATS

# TUNA NUT 24_13 FED COM 23H

PAGE 2 OF 2

**BHL** (NAD83)
X:757675.99' / Y:509607.53'
LAT:32.39902994 / LON:-103.63239520

**BHL** (NAD27)
X:716493.59' / Y:509546.92'
LAT:32.39890686 / LON:-103.63190878

**LTP** (NAD83)
X:757676.58' / Y:509527.53'
LAT:32.39881004 / LON:-103.63239499

**LTP** (NAD27)
X:716494.18' / Y:509466.92'
LAT:32.39868695 / LON:-103.63190857

**PPP-2** (NAD83)
X:757714.23' / Y:504344.96'
LAT:32.38456441 / LON:-103.63238306

**PPP-2** (NAD27)
X:716531.69' / Y:504284.50'
LAT:32.38444127 / LON:-103.63189715

**PPP-1** (NAD83)
X:757733.41' / Y:501705.15'
LAT:32.37730820 / LON:-103.63237696

**PPP-1** (NAD27)
X:716550.80' / Y:501644.76'
LAT:32.37718504 / LON:-103.63189130

**FTP** (NAD83)
X:757751.87' / Y:499164.77'
LAT:32.37032529 / LON:-103.63237107

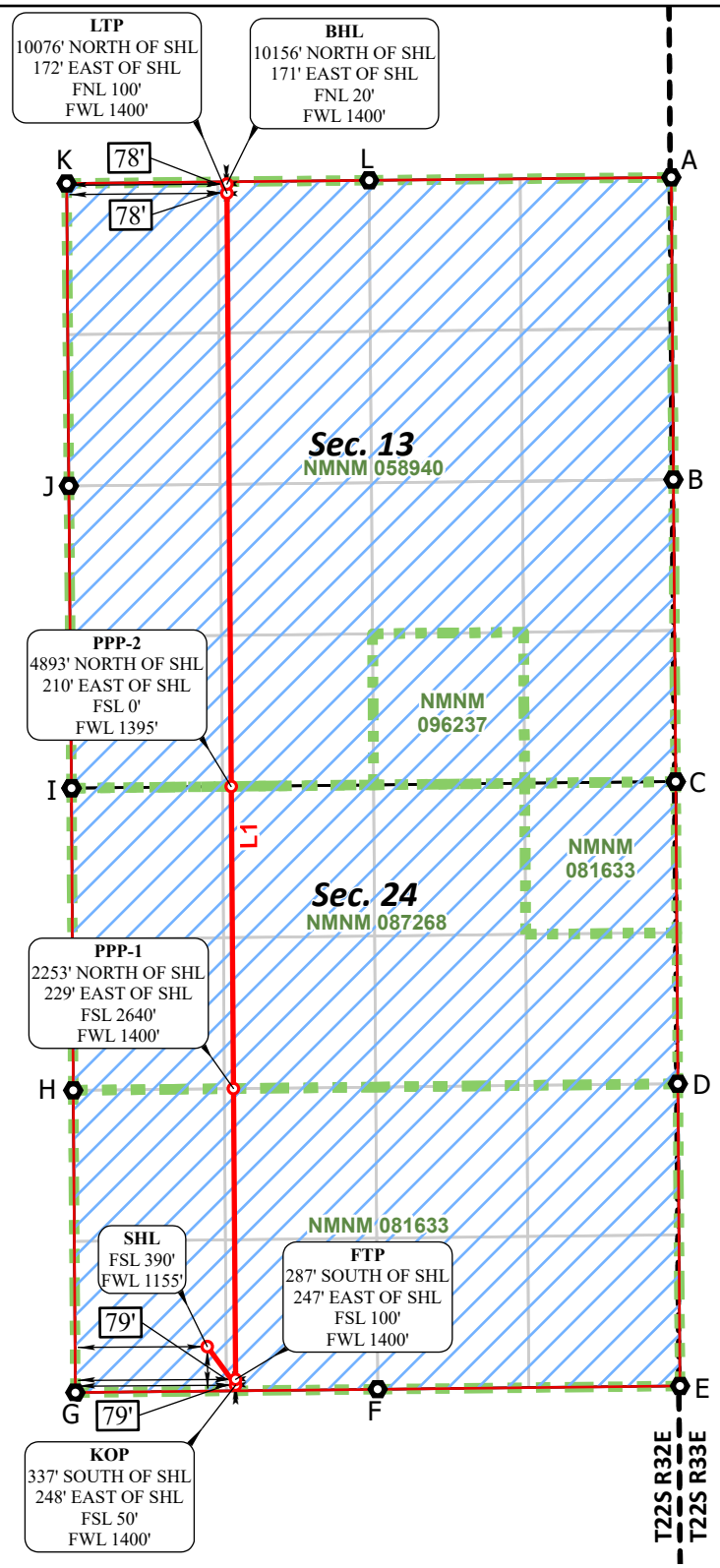
**FTP** (NAD27)
X:716569.20' / Y:499104.45'
LAT:32.37020210 / LON:-103.63188565

**KOP** (NAD83)
X:757752.23' / Y:499114.78'
LAT:32.37018788 / LON:-103.63237096

**KOP** (NAD27)
X:716569.56' / Y:499054.47'
LAT:32.37006469 / LON:-103.63188556

**SHL** (NAD83)
X:757504.51' / Y:499451.71'
LAT:32.37111843 / LON:-103.63316613

**SHL** (NAD27)
X:716321.85' / Y:499391.39'
LAT:32.37099525 / LON:-103.63268067




| CORNER COORDINATES NAD 83, SPCS NM EAST | CORNER COORDINATES NAD 27, SPCS NM EAST |
|---|---|
| A - X: 761558.98' / Y:509666.12' | A - X: 720376.55' / Y:509605.50' |
| B - X: 761577.70' / Y:507026.11' | B - X: 720395.20' / Y:506965.57' |
| C - X: 761597.23' / Y:504386.86' | C - X: 720414.67' / Y:504326.39' |
| D - X: 761616.41' / Y:501747.24' | D - X: 720433.78' / Y:501686.85' |
| E - X: 761635.45' / Y:499107.07' | E - X: 720452.76' / Y:499046.75' |
| F - X: 758993.62' / Y:499078.62' | F - X: 717810.94' / Y:499018.31' |
| G - X: 756352.66' / Y:499049.16' | G - X: 715169.99' / Y:498988.85' |
| H - X: 756333.80' / Y:501689.98' | H - X: 715151.20' / Y:501629.59' |
| I - X: 756319.04' / Y:504329.83' | I - X: 715136.51' / Y:504269.37' |
| J - X: 756295.56' / Y:506970.96' | J - X: 715113.10' / Y:506910.43' |
| K - X: 756275.91' / Y:509612.69' | K - X: 715093.52' / Y:509552.08' |
| L - X: 758919.12' / Y:509640.71' | L - X: 717736.71' / Y:509580.10' |

*FTP TO LTP LINE BEARINGS

| LINE | BEARING |
|---|---|
| L1 | N 00°24'59" W ~ 10363.03' |

*FTP TO LTP LEASE DISTANCES

| TRACT | DISTANCE |
|---|---|
| NMNM 081633 | 2540.44' |
| NMNM 087268 | 2639.88' |
| NMNM 058940 | 5182.71' |
| TOTAL | 10363.03' |

Drill Line Events | Section Corners | Drill Line | Dimension Lines | Federal Leases | HSU | HSU Corners

JOB No. R4195_016_14071
REV 0 NDS 11/26/2024

All bearings and coordinates refer to New Mexico State Plane Coordinate System, East Zone, U.S. Survey Feet.

Distances/areas relative to NAD 83 grid measurements. Combined Scale Factor: 0.99975697 and a Convergence Angle: 0.07066669°

## OXY APD CHANGE SUNDRY LIST FORM

| | |
|---|---|
| DATE SUNDRY WORKSHEET CREATED | 3/27/2025 |
| WELL NAME_NUMBER | TUNA NUT 24_13 FED COM 23H |
| API NUMBER | 30-025-54090 |
| ESTIMATED SPUD DATE | 7/1/2025 |

| | ITEM | APD BASE LINE (For Regulatory to Complete) | SUNDRY PLAN (Groups to complete the latest plan) |
|---|---|---|---|
| | | Date APD/BASE LINE APPROVED: 11/26/24 | DATE Sundry Worksheet : 03/27/25 |
| Surface Planning | NAME | TUNA NUT 24_13 FED COM 23H | TUNA NUT 24_13 FED COM 23H |
| | NSL | NO | NO |
| | SHL | 275' FSL 1425' FWL | 390' FSL 1155' FWL |
| | PAD | REDTNK_T22SR32E_2401 | REDTNK_T22SR32E_2401 |
| | BHL | 20' FNL 2250' FWL | 20' FNL 1400' FWL |
| | HSU SIZE, ACRES | 640 | 1280 |
| | POOL | RED TANK | RED TANK |
| | TVD | 10933 | 10874' |
| | TARGET FORMATION | BONE SPRING | BONE SPRING |

**CASING PROGRAM**

| APD BASE LINE | | | | | | | |
|---|---|---|---|---|---|---|---|
| Section | Hole Size (in.) | MD | TVD | Csg OD | Csg WT | Grade | Conn. |
| Surface | 17.5 | 940 | 940 | 13.375 | 54.5 | J-55 | BTC |
| Int | 9.875 | 10186 | 10102 | 7.625 | 26.4 | L-80 HC | BTC |
| Int2 | | | | | | | |
| Prod | 6.75 | 21496 | 10933 | 5.5 | 20 | P-110 | Sprint-SF |
| Liner | | | | | | | |

| SUNDRY PLAN | | | | | | | |
|---|---|---|---|---|---|---|---|
| Section | Hole Size (in.) | MD | TVD | Csg OD (in) | Csg WT (ppf) | Grade | Conn. |
| Surface | 17.5 | 1087 | 1087 | 13.375 | 54.5 | J-55 | BTC |
| Int | 9.875 | 10148 | 10117 | 7.625 | 26.4 | L-80 HC | BTC |
| Int2 | | | | | | | |
| Prod | 6.75 | 21155 | 10874 | 5.5 | 20 | P-110 | Sprint-SF |
| Liner | | | | | | | |

**CEMENT PROGRAM**

| APD BASE LINE | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| Section/Stage | Slurry | Sacks | Yield (ft^3/ | Density (lb | Excess | TOC | Placement | Description |
| Surf | Surface - Tail | 982 | 1.33 | 14.8 | 100% | | Circulate | Class C+Accel |
| Int/2 | Intermediate 1S - Tail | 155 | 1.68 | 13.2 | 5% | 9030 | Circulate | Class C+Ret, Disper |
| Int | Intermediate 2S - Tail | 395 | 1.68 | 13.2 | 5% | 7246 | Circulate | Class C+Ret, Disper |
| Int | Intermediate 2S - Tail BH | 1293 | 1.71 | 13.3 | 25% | | Bradenhead | Class C+Accel |
| Prod | Production - Tail | 669 | 1.84 | 13.3 | 25% | 9686 | Circulate | Class C+Ret |
| | | | | | | | | |

| SUNDRY PLAN | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| Section/Stage | Slurry | Sacks | Yield (ft^3/ft) | Density (lb/gal) | Excess | TOC | Placement | Description |
| Surf | Surface - Tail | 1135 | 1.33 | 14.8 | 100% | | Circulate | Class C+Accel |
| Int/1 | Intermediate 1S - Tail | 377 | 1.68 | 13.2 | 5% | 7343 | Circulate | Class C+Ret, Disper |
| Int2 | Intermediate 2S - Tail BH | 1332 | 1.71 | 13.3 | 25% | | Bradenhead | Class C+Accel |
| Prod | Production - Tail | 652 | 1.84 | 13.3 | 25% | 9648 | Circulate | Class C+Ret |
| | | | | | | | | |
| | | | | | | | | |

**VARIANCES**

| APD BASE LINE | |
|---|---|
| BOP Break Tesing Variance | X |
| 5M Annular BOP Variance | |
| Bradenhead CBL Variance | X |
| Offline Cementing Variance | X |
| Production Annular Clearance Variance | |
| Flexible Choke Line Variance | |
| (Pilot Hole, Logs etc.) | |

| SUNDRY PLAN | |
|---|---|
| BOP Break Tesing Variance | X |
| 5M Annular BOP Variance | |
| Bradenhead CBL Variance | X |
| Offline Cementing Variance | X |
| Production Annular Clearance Variance | |
| Flexible Choke Line Variance | |
| (Pilot Hole, Logs etc.) | |

Sante Fe Main Office
Phone: (505) 476-3441

General Information
Phone: (505) 629-6116

Online Phone Directory
https://www.emnrd.nm.gov/ocd/contact-us

# State of New Mexico
# Energy, Minerals and Natural Resources
# Oil Conservation Division
# 1220 S. St Francis Dr.
# Santa Fe, NM 87505



## CONDITIONS

| Operator: | OGRID: |
|---|---|
| OXY USA INC<br>P.O. Box 4294<br>Houston, TX 772104294 | 16696 |
| | Action Number:<br>457111 |
| | Action Type:<br>[C-103] NOI Change of Plans (C-103A) |

**CONDITIONS**

| Created By | Condition | Condition Date |
|---|---|---|
| matthew.gomez | A [C-103] Sub. Drilling (C-103N) is required within (10) days of spud. | 5/9/2025 |
| matthew.gomez | Notify the OCD 24 hours prior to casing & cement. | 5/9/2025 |
| matthew.gomez | Any previous COA's not addressed within the updated COA's still apply. | 5/9/2025 |