

<b>Well Name:</b> CO 34 27 FEDERAL COM	<b>Well Location:</b> T25S / R32E / SEC 3 / LOT 1 / 32.164947 / -103.655593	<b>County or Parish/State:</b> LEA / NM
<b>Well Number:</b> 709H	<b>Type of Well:</b> OIL WELL	<b>Allottee or Tribe Name:</b>
<b>Lease Number:</b> NMLC061936	<b>Unit or CA Name:</b>	<b>Unit or CA Number:</b>
<b>US Well Number:</b> 3002554287	<b>Operator:</b> CHEVRON USA INCORPORATED	

**Notice of Intent**

**Sundry ID:** 2854328

**Type of Submission:** Notice of Intent

**Type of Action:** APD Change

**Date Sundry Submitted:** 05/22/2025

**Time Sundry Submitted:** 10:42

**Date proposed operation will begin:** 05/22/2025

**Procedure Description:** CHEVRON USA INC IS REQUESTING CHANGES TO THE WELL BELOW: OLD NAME: CO 34 27 FEDERAL COM #709H (30-025-54287) NEW NAME: CO 34 27 FEDERAL COM #637H (30-025-54287) OLD POOL: WC-025 G-08 S223227D;UPPER WOLFCAMP NEW POOL: WC-025-G-08 S253216D;UPPER WOLFCAMP PLEASE SEE ATTACHED NEW C102, 9 POINT DRILL PLAN AND DIRECTIONAL DRILL PLAN REFLECTING CHANGES.

**NOI Attachments**

**Procedure Description**

5.5\_20\_pp\_w\_441\_casing\_pdf\_20250610070018.pdf

7\_5\_8\_w\_441\_casing\_spec\_sheet\_20250610070010.pdf

CO\_34\_27\_FEDERAL\_COM\_\_637H\_9\_PT\_Plan\_09June25\_20250610065954.pdf

DefPlan100ft\_CO3427FederalComNo.637H\_R1\_20250522104138.pdf

CO\_34\_27\_FEDERAL\_COM\_637H\_C102\_Cert051425\_20250522104059.pdf

Well Name: CO 34 27 FEDERAL COM

Well Location: T25S / R32E / SEC 3 / LOT 1 / 32.164947 / -103.655593

County or Parish/State: LEA / NM

Well Number: 709H

Type of Well: OIL WELL

Allottee or Tribe Name:

Lease Number: NMLC061936

Unit or CA Name:

Unit or CA Number:

US Well Number: 3002554287

Operator: CHEVRON USA INCORPORATED

### Conditions of Approval

#### Additional

Cotton\_Draw\_Casing\_Design\_OQE\_12June25\_BLM\_\_002\_\_20250618122855.pdf

\_CO\_3\_10\_FED\_AND\_CO\_34\_27\_FED\_COM\_Lea\_\_CHEVRON\_USA\_INCORPORATED\_45826\_JS\_20250618122855.pdf

CO\_34\_27\_FEDERAL\_COM\_637H\_COAs\_20250618122855.pdf

### Operator

I certify that the foregoing is true and correct. Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction. Electronic submission of Sundry Notices through this system satisfies regulations requiring a

Operator Electronic Signature: CINDY HERRERA-MURILLO

Signed on: JUN 10, 2025 07:00 AM

Name: CHEVRON USA INCORPORATED

Title: Permitting Specialist

Street Address: 1616 W BENDER BLVD

City: HOBBS

State: NM

Phone: (575) 263-0431

Email address: CHERRERAMURILLO@CHEVRON.COM

### Field

Representative Name:

Street Address:

City:

State:

Zip:

Phone:

Email address:

### BLM Point of Contact

BLM POC Name: CHRISTOPHER WALLS

BLM POC Title: Petroleum Engineer

BLM POC Phone: 5752342234

BLM POC Email Address: CWALLS@BLM.GOV

Disposition: Approved

Disposition Date: 06/18/2025

Signature: Chris Walls

Form 3160-5  
(October 2024)

UNITED STATES  
DEPARTMENT OF THE INTERIOR  
BUREAU OF LAND MANAGEMENT

FORM APPROVED  
OMB No. 1004-0220  
Expires: October 31, 2027

**SUNDRY NOTICES AND REPORTS ON WELLS**  
**Do not use this form for proposals to drill or to re-enter an abandoned well. Use Form 3160-3 (APD) for such proposals.**

5. Lease Serial No.	NMLC061936
6. If Indian, Allottee or Tribe Name	

<b>SUBMIT IN TRIPLICATE - Other instructions on page 2</b>		7. If Unit of CA/Agreement, Name and/or No.
1. Type of Well <input checked="" type="checkbox"/> Oil Well <input type="checkbox"/> Gas Well <input type="checkbox"/> Other		8. Well Name and No. CO 34 27 FEDERAL COM/709H
2. Name of Operator CHEVRON USA INCORPORATED		9. API Well No. 3002554287
3a. Address PO BOX 1392, BAKERSFIELD, CA 93302	3b. Phone No. (include area code) (661) 633-4000	10. Field and Pool or Exploratory Area WC-025 G-09 S253309P/UPPER WOLFCAMP
4. Location of Well (Footage, Sec., T.,R.,M., or Survey Description) SEC 3/T25S/R32E/NMP		11. Country or Parish, State LEA/NM

12. CHECK THE APPROPRIATE BOX(ES) TO INDICATE NATURE OF NOTICE, REPORT OR OTHER DATA

TYPE OF SUBMISSION	TYPE OF ACTION			
<input checked="" type="checkbox"/> Notice of Intent	<input type="checkbox"/> Acidize	<input type="checkbox"/> Deepen	<input type="checkbox"/> Production (Start/Resume)	<input type="checkbox"/> Water Shut-Off
<input type="checkbox"/> Subsequent Report	<input type="checkbox"/> Alter Casing	<input type="checkbox"/> Hydraulic Fracturing	<input type="checkbox"/> Reclamation	<input type="checkbox"/> Well Integrity
<input type="checkbox"/> Final Abandonment Notice	<input type="checkbox"/> Casing Repair	<input type="checkbox"/> New Construction	<input type="checkbox"/> Recomplete	<input type="checkbox"/> Other
	<input checked="" type="checkbox"/> Change Plans	<input type="checkbox"/> Plug and Abandon	<input type="checkbox"/> Temporarily Abandon	
	<input type="checkbox"/> Convert to Injection	<input type="checkbox"/> Plug Back	<input type="checkbox"/> Water Disposal	

13. Describe Proposed or Completed Operation: Clearly state all pertinent details, including estimated starting date of any proposed work and approximate duration thereof. If the proposal is to deepen directionally or recompleat horizontally, give subsurface locations and measured and true vertical depths of all pertinent markers and zones. Attach the Bond under which the work will be performed or provide the Bond No. on file with BLM/BIA. Required subsequent reports must be filed within 30 days following completion of the involved operations. If the operation results in a multiple completion or recompleat in a new interval, a Form 3160-4 must be filed once testing has been completed. Final Abandonment Notices must be filed only after all requirements, including reclamation, have been completed and the operator has detennined that the site is ready for final inspection.)

CHEVRON USA INC IS REQUESTING CHANGES TO THE WELL BELOW:

OLD NAME: CO 34 27 FEDERAL COM #709H (30-025-54287)

NEW NAME: CO 34 27 FEDERAL COM #637H (30-025-54287)

OLD POOL: WC-025 G-08 S223227D;UPPER WOLFCAMP

NEW POOL: WC-025-G-08 S253216D;UPPER WOLFCAMP

PLEASE SEE ATTACHED NEW C102, 9 POINT DRILL PLAN AND DIRECTIONAL DRILL PLAN REFLECTING CHANGES.

14. I hereby certify that the foregoing is true and correct. Name (Printed/Typed) CINDY HERRERA-MURILLO / Ph: (575) 263-0431	Title Permitting Specialist
Signature (Electronic Submission)	Date 06/10/2025

**THE SPACE FOR FEDERAL OR STATE OFFICE USE**

Approved by CHRISTOPHER WALLS / Ph: (575) 234-2234 / Approved	Title Petroleum Engineer	Date 06/18/2025
Conditions of approval, if any, are attached. Approval of this notice does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon.		Office CARLSBAD

Title 18 U.S.C Section 1001 and Title 43 U.S.C Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

(Instructions on page 2)

## GENERAL INSTRUCTIONS

This form is designed for submitting proposals to perform certain well operations and reports of such operations when completed as indicated on Federal and Indian lands pursuant to applicable Federal law and regulations. Any necessary special instructions concerning the use of this form and the number of copies to be submitted, particularly with regard to local area or regional procedures and practices, are either shown below, will be issued by or may be obtained from the local Federal office.

## SPECIFIC INSTRUCTIONS

*Item 4* - Locations on Federal or Indian land should be described in accordance with Federal requirements. Consult the local Federal office for specific instructions.

*Item 13*: Proposals to abandon a well and subsequent reports of abandonment should include such special information as is required by the local Federal office. In addition, such proposals and reports should include reasons for the abandonment; data on any former or present productive zones or other zones with present significant fluid contents not sealed off by cement or otherwise; depths (top and bottom) and method of placement of cement plugs; mud or other material placed below, between and above plugs; amount, size, method of parting of any casing, liner or tubing pulled and the depth to the top of any tubing left in the hole; method of closing top of well and date well site conditioned for final inspection looking for approval of the abandonment. If the proposal will involve **hydraulic fracturing operations**, you must comply with 43 CFR 3162.3-3, including providing information about the protection of usable water. Operators should provide the best available information about all formations containing water and their depths. This information could include data and interpretation of resistivity logs run on nearby wells. Information may also be obtained from state or tribal regulatory agencies and from local BLM offices.

## NOTICES

The privacy Act of 1974 and the regulation in 43 CFR 2.48(d) provide that you be furnished the following information in connection with information required by this application.

**AUTHORITY**: 30 U.S.C. 181 et seq., 351 et seq., 25 U.S.C. 396; 43 CFR 3160.

**PRINCIPAL PURPOSE**: The information is used to: (1) Evaluate, when appropriate, approve applications, and report completion of subsequent well operations, on a Federal or Indian lease; and (2) document for administrative use, information for the management, disposal and use of National Resource lands and resources, such as: (a) evaluating the equipment and procedures to be used during a proposed subsequent well operation and reviewing the completed well operations for compliance with the approved plan; (b) requesting and granting approval to perform those actions covered by 43 CFR 3162.3-2, 3162.3-3, and 3162.3-4; (c) reporting the beginning or resumption of production, as required by 43 CFR 3162.4-1(c) and (d) analyzing future applications to drill or modify operations in light of data obtained and methods used.

**ROUTINE USES**: Information from the record and/or the record will be transferred to appropriate Federal, State, local or foreign agencies, when relevant to civil, criminal or regulatory investigations or prosecutions in connection with congressional inquiries or to consumer reporting agencies to facilitate collection of debts owed the Government.

**EFFECT OF NOT PROVIDING THE INFORMATION**: Filing of this notice and report and disclosure of the information is mandatory for those subsequent well operations specified in 43 CFR 3162.3-2, 3162.3-3, 3162.3-4.

The Paperwork Reduction Act of 1995 requires us to inform you that:

The BLM collects this information to evaluate proposed and/or completed subsequent well operations on Federal or Indian oil and gas leases.

Response to this request is mandatory.

The BLM would like you to know that you do not have to respond to this or any other Federal agency-sponsored information collection unless it displays a currently valid OMB control number.

**BURDEN HOURS STATEMENT**: Public reporting burden for this form is estimated to average 8 hours per response, including the time for reviewing instructions, gathering and maintaining data, and completing and reviewing the form. Direct comments regarding the burden estimate or any other aspect of this form to U.S. Department of the Interior, Bureau of Land Management (1004-0137), Bureau Information Collection Clearance Officer (WO-630), 1849 C St., N.W., Mail Stop 401 LS, Washington, D.C. 20240

## Additional Information

### Location of Well

0. SHL: LOT 1 / 674 FNL / 487 FEL / TWSP: 25S / RANGE: 32E / SECTION: 3 / LAT: 32.164947 / LONG: -103.655593 ( TVD: 0 feet, MD: 0 feet )

PPP: NESE / 2639 FNL / 750 FEL / TWSP: 24S / RANGE: 32E / SECTION: 27 / LAT: 32.188564 / LONG: -103.656406 ( TVD: 12940 feet, MD: 18321 feet )

PPP: SESE / 25 FSL / 750 FEL / TWSP: 24S / RANGE: 32E / SECTION: 34 / LAT: 32.166867 / LONG: -103.656411 ( TVD: 12940 feet, MD: 13321 feet )

BHL: NENE / 25 FNL / 750 FEL / TWSP: 24S / RANGE: 32E / SECTION: 27 / LAT: 32.19575 / LONG: -103.656404 ( TVD: 12940 feet, MD: 23829 feet )

Cover Page



# Casing OQE

Team Member	Action	Time-Date (UTC)
Eric Wendt		
Danny Korf		
<b>Report Status</b>		Pending Approval

**Scope and Type Well Design Criteria**

Scope and Type Well Design Criteria	
Area(s)	South Lea County, NM - Cotton Draw
Formation(s)	All Targets from Avalon to Wolfcamp A
Casing Design(s)	4-String Type Well - Version Slimhole 2.0
Sour Service	No
Type Well Design Criteria	Deepest WCA in Cotton Draw - applicable to all shallower wells in the Cotton Draw Development Mid-case (expected) pore and frac pressures based on Cotton Draw MEM in 2025 South Lea BOD 2-mile lateral
WellSafe OQE	Meets WellSafe 2.0 Well Design and Plan - Drilling Requirements 8, 9, 10, and 11 See Completions/Workover/Intervention Well Design and Plan for Tubing Design OQE



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# 1 Load Case Assumptions

## 1.1 Surface Casing

### Surface Casing - Drilling Load Case Assumptions

Drilling Load Case Assumptions		
Surface Casing - 13.375" Casing 54.5 lbm/ft J55 BTC (0% OD to)		
	Internal Pressure Profile	External Pressure Profile
<b>Burst</b>	1) Pressure test to 1500 psi w/ 8.4 ppg MW 2) MASP of 843 psi connected linearly to frac gradient <sup>1</sup> at shoe.	1) Pore Pressure <sup>1</sup>
<b>Collapse</b>	1) Fixed mud drop at 2000' w/ 8.3 ppg min MW for next hole section. 2) Initial Conditions – Cementing w/ 8.4 ppg displacement fluid density.	1) 10.60 lbm/gal Max MW at TD 2) 8.40 lbm/gal at TD, Spacer, Cement
<b>Axial</b>	1) Casing weight, 8.4 ppg displacement fluid + 100 kips Overpull <sup>3</sup>	1) 8.40 lbm/gal at TD, Spacer, Cement

## 1.2 Intermediate 1 Casing

### Intermediate 1 Casing - Drilling Load Case Assumptions

Drilling Load Case Assumptions		
Casing - 10.75", 40.5#, J55, BTC, MCBU		
	Internal Pressure Profile	External Pressure Profile
<b>Burst</b>	1) Pressure test to 2000 psi w/ 8.4 ppg MW 2) MASP of 2479 psi connected linearly to frac gradient <sup>1</sup> at shoe.	1) Pore Pressure <sup>1</sup>
<b>Collapse</b>	1) Fixed mud drop at 2000' w/ 9 ppg min MW for next hole section. 2) Initial Conditions – Cementing w/ 8.4 ppg displacement fluid density.	1) 11.00 lbm/gal Max MW at TD 2) 9.00 lbm/gal at TD, Spacer, Cement
<b>Axial</b>	1) Casing weight, 8.4 ppg displacement fluid + 100 kips Overpull <sup>3</sup>	1) 9.00 lbm/gal at TD, Spacer, Cement

## 1.3 Production (Intermediate 2) Casing

### Production (Intermediate 2) Casing - Drilling and Production Load Case Assumptions

Drilling and Production Load Case Assumptions		
Production Casing - 7-5/8-inch, 29.7 lb/ft, P110-ICY, W441, MCBU		
	Internal Pressure Profile	External Pressure Profile
<b>Burst</b>	1) Pressure test to 9800 psi w/ 8.4 ppg MW ( <b>Completion Operations pressure test</b> ) 2) Frac Screenout Pressure 9300 psi w/ 10 ppg (2.6 PPA prop con) proppant-laden fluid density <sup>2</sup> . ( <b>Operational limit during frac execution</b> ) 3) Pressure test to 4700 psi w/ 8.4 ppg fluid density (Liner Top packer test) 4) Tubing leak w/ packer at 11,200' TVD and 8.7 ppg packer fluid density. 5) MASP of 4184 psi connected linearly to frac gradient <sup>1</sup> at shoe.	1) Pore Pressure <sup>1</sup>
<b>Collapse</b>	1) Evacuated Collapse, 0 psi 2) Fixed mud drop at 2000' w/ 9 ppg min MW for next hole section. 3) Initial Conditions – Cementing w/ 8.4 ppg displacement fluid density.	1) 12.00 lbm/gal Max MW at TD 2) 12.00 lbm/gal Max MW at TD 3) 9.00 lbm/gal at TD, Spacer, Cement
<b>Axial</b>	1) Casing weight, 8.4 ppg displacement fluid + 100 kips Overpull <sup>3</sup>	1) 9.00 lbm/gal at TD, Spacer, Cement



## 1.4 Production Liner

### Production Liner - Production Load Case Assumptions

Production Load Case Assumptions		
Production Liner - 5-1/2" 20 lb/ft P110ICY W441, MGBU		
	Internal Pressure Profile	External Pressure Profile
<b>Burst</b>	1) Pressure test to 9800 psi w/ 8.4 ppg MW ( <b>Completion Operations pressure test</b> ) 2) Frac Screenout Pressure 9300 psi w/ 10 ppg (2.6 PPA prop Con) proppant-laden fluid density <sup>2</sup> ( <b>Operational limit during frac execution</b> ). 3) Tubing leak w/ packer at 11,200' TVD and 8.7 ppg packer fluid density.	1) Pore Pressure <sup>1</sup>
<b>Collapse</b>	1) Evacuated Collapse, 0 psi 2) Initial Conditions – Cementing w/ 8.4 ppg displacement fluid density.	1) 15.00 lbm/gal Max MW at TD 2) 13.00 lbm/gal at TD, Spacer, Cement
<b>Axial</b>	1) Casing weight, 8.4 ppg displacement fluid + 100 kips Overpull <sup>3</sup>	1) 13.00 lbm/gal at TD, Spacer, Cement

<sup>1</sup>The mid-case (expected) pore and frac pressures are used and follow recommended gradients based on TOC

<sup>2</sup>Consideration is given to area specific produced water densities and maximum sand concentrations (details in Casing Pressure Test Plan section)

<sup>3</sup>Standard overpull is typically 100K but will be dictated by rig capacity and safety factors

Note:

- Full list of evaluated load cases can be found in Section 3.01 - Material and Connection Specifications and Load Case Evaluation Results
- Alternative load cases may need to be evaluated to establish surface pressure limitations based on well-specific conditions, equipment, and/or operational practices, e.g., casing collapse during planned or remedial top jobs, max differential across liner hanger PBR, annular pressure buildup, etc.

## 2 Maximum Anticipated Surface Pressure

Casing String Description	70% Burst	MASP <sub>SHP</sub>	MASP <sub>Frac</sub> @ shoe	MASP <sub>Frac</sub> in OH	MASP + 500	MASP Bullheading	P <sub>test</sub> <sub>future liner</sub>	P <sub>test</sub> <sub>liner lap</sub>	P <sub>test</sub> <sub>FIT/LOT</sub>
1 Surface	1,800	953	843	N/A	1,343	833	N/A	N/A	465
2 Intermediate 1	2,078	4,351	2,479	N/A	2,979	1,705	N/A	N/A	1,596
3 Production	7,675	4,184	N/A	N/A	4,684	3,240	6,088	2,161	1,387
4 Production Liner	8,281					N/A	N/A	N/A	N/A
5									
6									
7									
8							N/A	N/A	N/A

*As per Frac loads*

### Cotton\_Draw Slimhole 2.0 MASP Calculations

MASP determination methodology can be found in the Casing Pressure Test Calculator linked below;

[CO MASP calculator](#)

Pressure Test Calculator Note: MW values are intentionally on the low end (and possibly below) the expected MW range for the deepest WCA well in Cotton Draw to generate conservative MASP values and resultant casing test pressures that meet or exceed actual / expected pressure test requirements for all benches in Cotton Draw.

HC gradient - BLM basis of 0.22 psi/ft for and Young-Nagy gas gradient for the production hole section

## 3 Casing Design

### 3.1 Material and Connection Specifications

Section	17.5 in	12.25 in	9.875 in	6.75 in
Description	13.375" Casing 54.5 lbm/ft J55 BTC (0% OD tol)	10.75", 40.5#, J55, BTC, MCBU	7-5/8-inch, 29.7 lb/ft, P110-ICY, W441, MCBU	5-1/2" 20 lb/ft P110ICY W441, MCBU
Casing Type	Surface Casing	Casing	Production Casing	Production Liner
From (ft)	28.00	28.00	28.00	11679.41
To (ft)	1020.71	4882.79	11879.41	20937.46
Weight (lbm/ft)	54.50	40.50	29.70	20.00
Grade	J55	J55	P110ICY	P110ICY
Connection	BTC	BTC	W441	W441
BTC Torque	Unknown	Unknown	Unknown	Unknown
Min. MUT (kft.lbf)			22.00	15.00
Opt. MUT (kft.lbf)			23.00	16.00
Max. MUT (kft.lbf)			26.00	19.20
Operating Torque (kft.lbf)			33.00	36000.00
Nominal OD (in)	13.375	10.750	7.625	5.500
Nominal ID (in)	12.615	10.050	6.875	4.778
Drift (in)	12.459	9.894	6.750	4.653
Coupling OD (in)	14.375	11.750	7.900	5.852
Body Burst Rating (psi)	2730.00	3130.00	11070.00	14360.00
Body Collapse Rating (psi)	1130.00	1580.00	7360.00	12300.00
Body Tension Rating (lbf)		629000.00	1068000.00	729000.00
Body Compression Rating (lbf)		629000.00	1068000.00	729000.00
Connection Burst Rating (psi)		3130.00	11070.00	14360.00
Connection Collapse Rating (psi)		1580.00	7360.00	12300.00
Connection Tension Rating (lbf)	909000.00	700000.00	801000.00	594000.00
Connection Compression Rating (lbf)	909000.00	628000.00	801000.00	594000.00

Note: Any casing grade or connection with higher performance ratings than components used for this analysis may be utilized. Ensure casing connection operating torque limit is sufficient for casing rotation and meets BLM clearance requirement (0.422 inches on all sides in the hole/casing annulus), if applicable.

#### **Production Liner Note:**



**5-1/2" 20lb/ft P110-ICY W441 only required for WCA wells in Cotton Draw to meet the required SF for the full evacuation collapse load case. Pad-specific load case evaluation required for utilization of lower performance casing. 5" 13 lb/ft P110 is acceptable for all benches shallower than WCA in Cotton Draw.**

### 3.2 Load Case Evaluation Results

#### Casing Design Factors

String Type	Burst	Collapse	Tension	Compression	Von Mises	Connection Envelope (VME)
Surface Casing						
String Body	1.100	1.000	1.300	1.300	1.100	N/A
Non-API Connection	1.100	1.000	1.300	1.300	N/A	1.000
API Connection	1.100	1.000	1.600	1.600	N/A	1.000
Casing/Liner/Tieback						
String Body	1.100	1.000	1.300	1.300	1.100	N/A
Non-API Connection	1.100	1.000	1.300	1.300	N/A	1.000
API Connection	1.100	1.000	1.600	1.600	N/A	1.000
Production Casing/Liner/Tieback						
String Body	1.100	1.000	1.300	1.300	1.100	N/A
Non-API Connection	1.100	1.000	1.300	1.300	N/A	1.000
API Connection	1.100	1.000	1.600	1.600	N/A	1.000

#### Casing Design Results Summary

Section (Type)	String	Burst	Collapse	Tension	Compression	Von Mises	Buckling (deg/100ft)	Connection Envelope (VME)
17.5" (Surface Casing)	13.375" Casing 54.5 lbm/ft J55 BTC (0% OD tol)	1.712	2.014	C 4.196	C 8.183	1.806	1.004	N/A
12.25" (Casing)	10.75", 40.5#, J55, BTC, MCBU	1.260	1.039	2.322	C 4.692	1.412	1.505	N/A
9.875" (Production Casing)	7-5/8-inch, 29.7 lb/ft, P110-ICY, W441, MCBU	1.102	1.021	C 1.816	C 3.126	1.159	2.005	N/A
6.75" (Production Liner)	5-1/2" 20 lb/ft P110ICY W441, MCBU	1.899	1.271	C 3.031	C 2.463	1.532	8.040	N/A

#### Casing Design Results Detailed

Section (Type)	String	Load Case	Burst	Collapse	Tension	Compression	Von Mises	Buckling (deg/100ft)	Connection Envelope (VME)
17.5" (Surface Casing)	13.375" Casing 54.5 lbm/ft J55 BTC (0% OD tol)	Fixed Mud Drop Collapse - 4882.79 ft		2.014	C 133.767	C 8.183	5.092	1.004	N/A
17.5" (Surface Casing)	13.375" Casing 54.5 lbm/ft J55 BTC (0% OD tol)	MASP - TOC High - 4882.79 ft	3.242		C 9.732		3.574	1.004	N/A

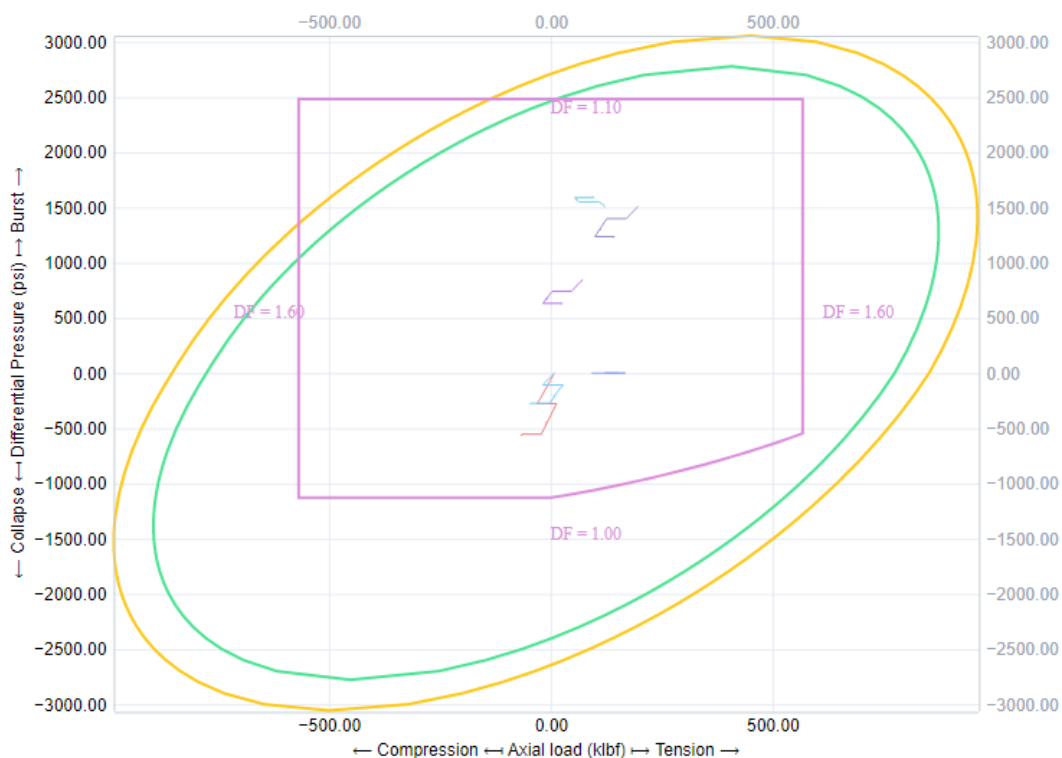


17.5" (Surface Casing)	13.375" Casing 54.5 lbm/ft J55 BTC (0% OD tol)	Pressure Test - TOC High - 1020.71 ft	1.712		C 5.900		1.806	1.004	N/A
17.5" (Surface Casing)	13.375" Casing 54.5 lbm/ft J55 BTC (0% OD tol)	MCBU DRAFT Green cement pressure test	1.813		C 4.196		2.042	1.004	N/A
17.5" (Surface Casing)	13.375" Casing 54.5 lbm/ft J55 BTC (0% OD tol)	Overpull			C 5.409		4.974	1.004	N/A
17.5" (Surface Casing)	13.375" Casing 54.5 lbm/ft J55 BTC (0% OD tol)	Initial Conditions		4.061	C 113.834	C 9.931	9.462	1.004	N/A
12.25" (Casing)	10.75", 40.5#, J55, BTC, MCBU	Fixed Mud Drop Collapse - 11879.41 ft		1.039	7.750	C 4.692	2.270	1.505	N/A
12.25" (Casing)	10.75", 40.5#, J55, BTC, MCBU	MASP - TOC High - 11879.41 ft	1.260		2.994		1.412	1.505	N/A
12.25" (Casing)	10.75", 40.5#, J55, BTC, MCBU	Pressure Test - TOC High - 4882.79 ft	1.484		3.271		1.601	1.505	N/A
12.25" (Casing)	10.75", 40.5#, J55, BTC, MCBU	MCBU DRAFT Green cement pressure test	1.560		2.519		1.729	1.505	N/A
12.25" (Casing)	10.75", 40.5#, J55, BTC, MCBU	Overpull			2.322		2.298	1.505	N/A
12.25" (Casing)	10.75", 40.5#, J55, BTC, MCBU	Initial Conditions		1.748	6.975	C 5.917	3.847	1.505	N/A
9.875" (Production Casing)	7-5/8-inch, 29.7 lb/ft, P110-ICY, W441, MCBU	MASP - TOC High - 20937.46 ft	2.633		C 2.654	C 10.489	2.697	2.005	N/A
9.875" (Production Casing)	7-5/8-inch, 29.7 lb/ft, P110-ICY, W441, MCBU	Pressure Test - TOC High - 11879.41 ft	2.289		C 2.555	C 13.537	2.424	2.005	N/A
9.875" (Production Casing)	7-5/8-inch, 29.7 lb/ft, P110-ICY, W441, MCBU	Pressure Test - TOC High - 20937.46 ft	1.102		C 1.873		1.159	2.005	N/A
9.875" (Production Casing)	7-5/8-inch, 29.7 lb/ft, P110-ICY, W441, MCBU	MCBU DRAFT Green cement pressure test	2.347		C 2.100		2.326	2.005	N/A
9.875" (Production Casing)	7-5/8-inch, 29.7 lb/ft, P110-ICY, W441, MCBU	Overpull			C 2.029		2.690	2.005	N/A
9.875" (Production Casing)	7-5/8-inch, 29.7 lb/ft, P110-ICY, W441, MCBU	Initial Conditions		3.649	C 3.887	C 5.819	5.035	2.005	N/A
9.875" (Production Casing)	7-5/8-inch, 29.7 lb/ft, P110-ICY, W441, MCBU	Evacuated Collapse - 20937.46 ft		1.021	C 3.907	C 3.126	1.591	2.005	N/A
9.875" (Production Casing)	7-5/8-inch, 29.7 lb/ft, P110-ICY, W441, MCBU	Frac job - TOC High - 20937.46 ft	1.111		C 1.816		1.191	2.005	N/A
9.875" (Production Casing)	7-5/8-inch, 29.7 lb/ft, P110-ICY, W441, MCBU	Hot Tubing Leak - TOC High - 20937.46 ft	1.514		C 2.777	C 9.161	1.573	2.005	N/A

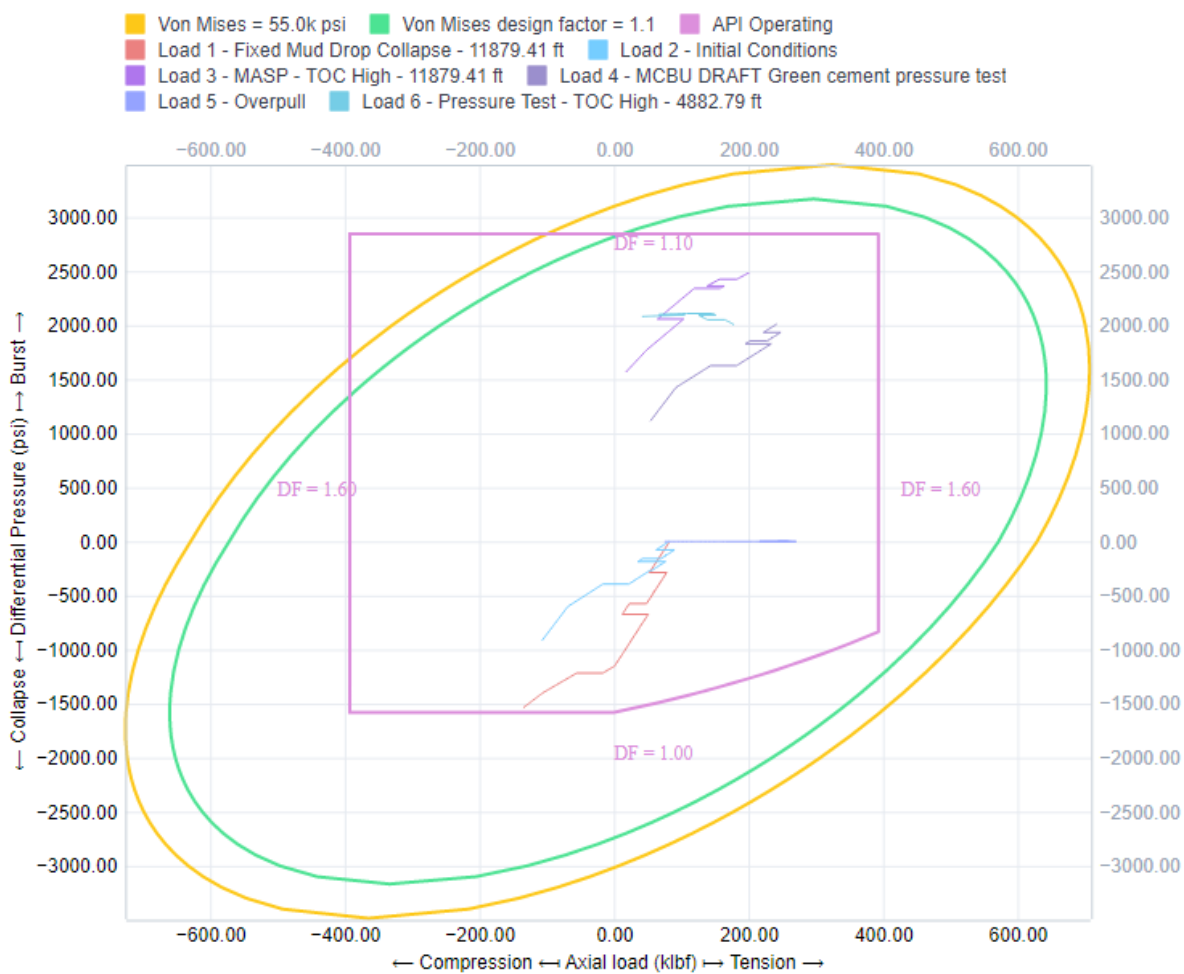


9.875" (Production Casing)	7-5/8-inch, 29.7 lb/ft, P110-ICY, W441, MCBU	Tubing Leak - TOC High - 20937.46 ft	1.525		C 2.196	C 9.830	1.605	2.005	N/A
6.75" (Production Liner)	5-1/2" 20 lb/ft P110ICY W441, MCBU	Pressure Test - TOC High - 20937.46 ft	1.955		C 8.171	C 9.064	2.064	8.040	N/A
6.75" (Production Liner)	5-1/2" 20 lb/ft P110ICY W441, MCBU	Overpull			C 4.750		4.249	8.040	N/A
6.75" (Production Liner)	5-1/2" 20 lb/ft P110ICY W441, MCBU	Initial Conditions		4.196		C 3.645	4.847	8.040	N/A
6.75" (Production Liner)	5-1/2" 20 lb/ft P110ICY W441, MCBU	Evacuated Collapse - 20937.46 ft		1.271		C 2.463	1.532	8.040	N/A
6.75" (Production Liner)	5-1/2" 20 lb/ft P110ICY W441, MCBU	Frac job - TOC High - 20937.46 ft	1.899		C 3.031	C 9.899	2.056	8.040	N/A
6.75" (Production Liner)	5-1/2" 20 lb/ft P110ICY W441, MCBU	Hot Tubing Leak - TOC High - 20937.46 ft	12.254			C 4.437	8.589	8.040	N/A
6.75" (Production Liner)	5-1/2" 20 lb/ft P110ICY W441, MCBU	Tubing Leak - TOC High - 20937.46 ft	12.272			C 4.437	8.977	8.040	N/A

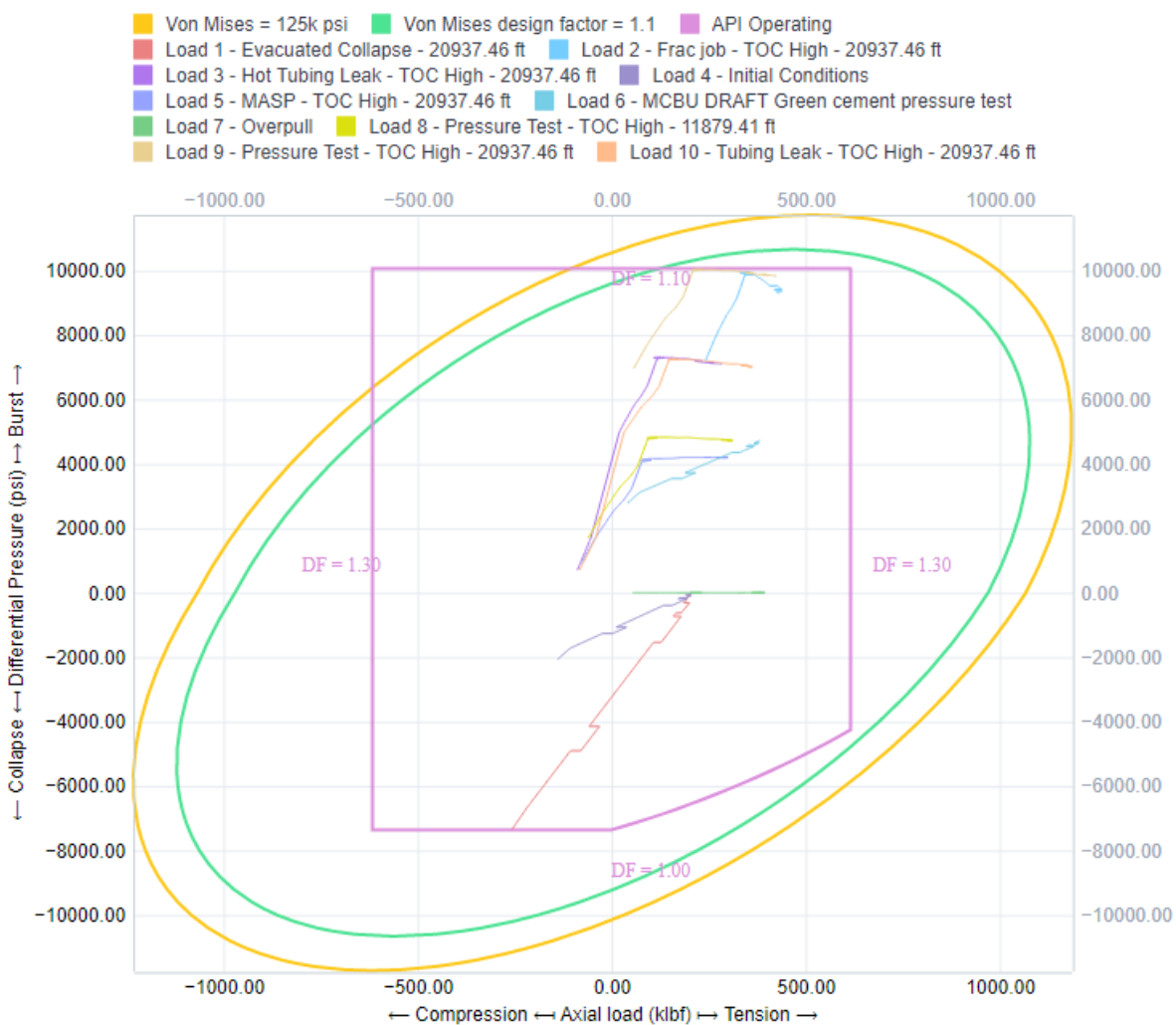
- Von Mises = 55.0k psi
- Von Mises design factor = 1.1
- API Operating
- Load 1 - Fixed Mud Drop Collapse - 4882.79 ft
- Load 2 - Initial Conditions
- Load 3 - MASP - TOC High - 4882.79 ft
- Load 4 - MCBU DRAFT Green cement pressure test
- Load 5 - Overpull
- Load 6 - Pressure Test - TOC High - 1020.71 ft



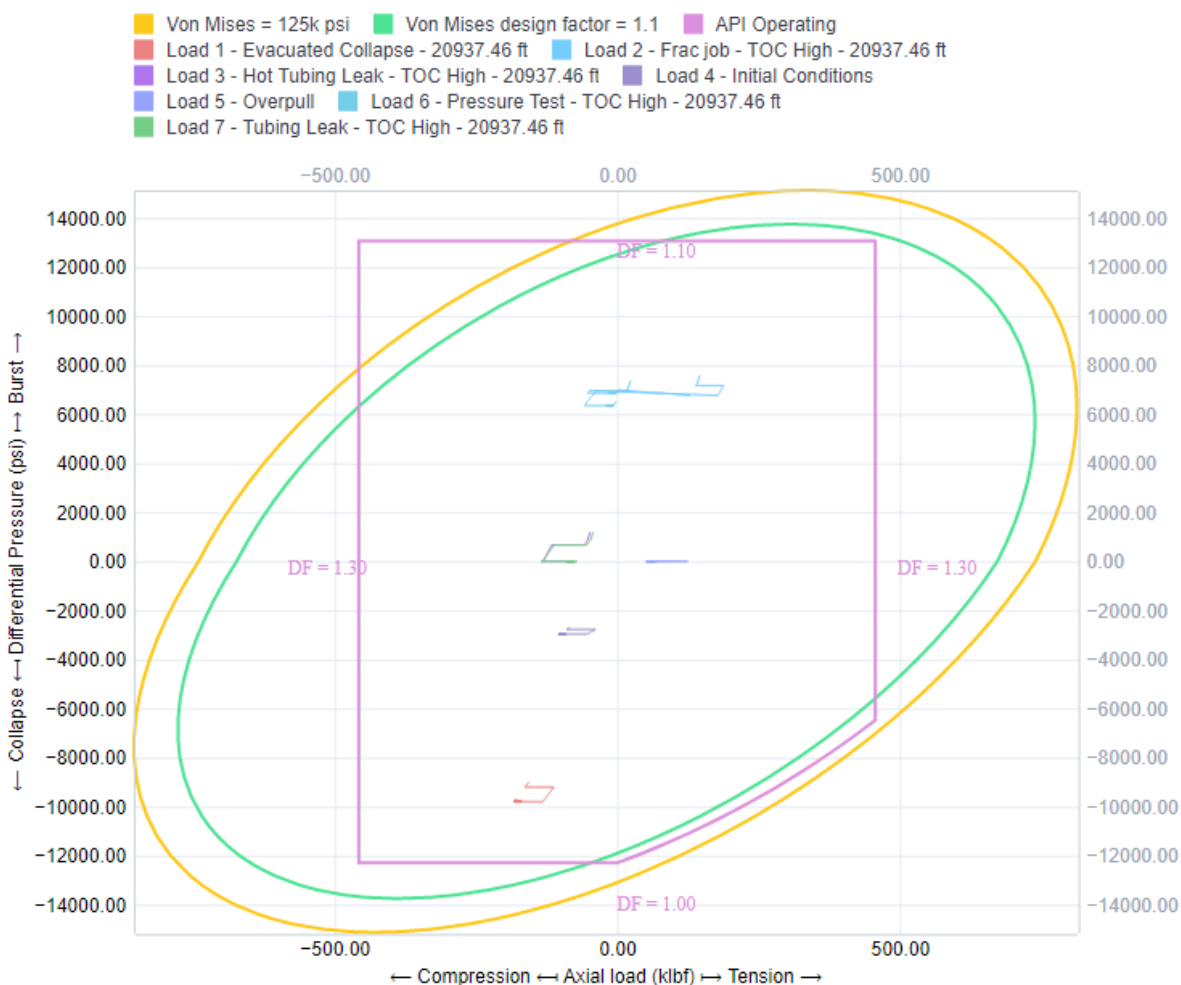
CASING TRIAXIAL: 13.375" Casing 54.5 lbm/ft J55 BTC (0% OD tol) (28 – 1022.76 ft)



CASING TRIAXIAL: 10.75", 40.5#, J55, BTC, MCBU (28 – 4753.66 ft)



CASING TRIAXIAL: 7-5/8-inch, 29.7 lb/ft, P110-ICY, BTC, MCBU (28 – 11578.58 ft)



CASING TRIAXIAL: 5-1/2" 20 lb/ft P110ICY W441, MCBU (11378.58 – 20493.75 ft)

### 3.3 Casing Accessories

If an accessory's ratings meet or exceed those of the adjacent tubular, no specific results need to be reported for the accessory.

[MCBU OCTG & Casing Accessories](#)

### 3.4 Liner Hanger - Differential Pressure Ratings

#### Liner Hanger Differential Pressure Rating Requirement

Assumptions for Maximum Anticipated Differential Pressure at Liner Top Packer		
Below Packer Element	Above Packer Element	Min. Packer Rating ( $\Delta P$ )
Mid-case pore pressure of 13.3 ppg between the element and cement at 11,235' TVD = 7,741 psi	Frac screenout pressure of 9,600 psi w/ 9.52 ppg proppant-laden fluid density = 15,162 psi at the top of liner	7,421 psi

[MCBU Liner hanger Systems](#)

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Basis for liner top packer pressure test:

A positive pressure test that is conducted on a barrier that isolates an exposed open hole section or liner lap should be a minimum of 500 psi in excess of the mid-case (expected) fracture gradient at the previous casing shoe

Test Pressure = ((MidFG@previous shoe from BoD - Current MW )\*0.052\*TVD of previous CSG shoe)+500

## 3.5 Material Strength - Temperature Deration, CRA, APB

### Temperature Derating

The local temperature (at each depth) is used to reduce all the ratings according to the reduction in yield stress per the Chevron Global Standard.

[Casing and Tubing SOP - Material Strength](#)

### Corrosion Resistant Alloys

The unconventional wells in the Permian Basin do not require CRA materials for any of the casing strings. Therefore, MCBU does not need to de-rate the casing to account for anisotropy due to variance in yield strength in the transverse and longitudinal directions.

### Annular Pressure Buildup

According to the [Casing and Tubing Design SOP](#) , MCBU is not required to analyze the APB effect on the external pressure profile since the operations are land based and have a wellhead valve at surface. Documented APB mitigation techniques are to bleed pressure as required. For circumstances in which a liner is implemented, the relatively low formation temperatures encountered and the success seen achieving a full column of cement behind the liner due not require the APB effect to be analyzed.

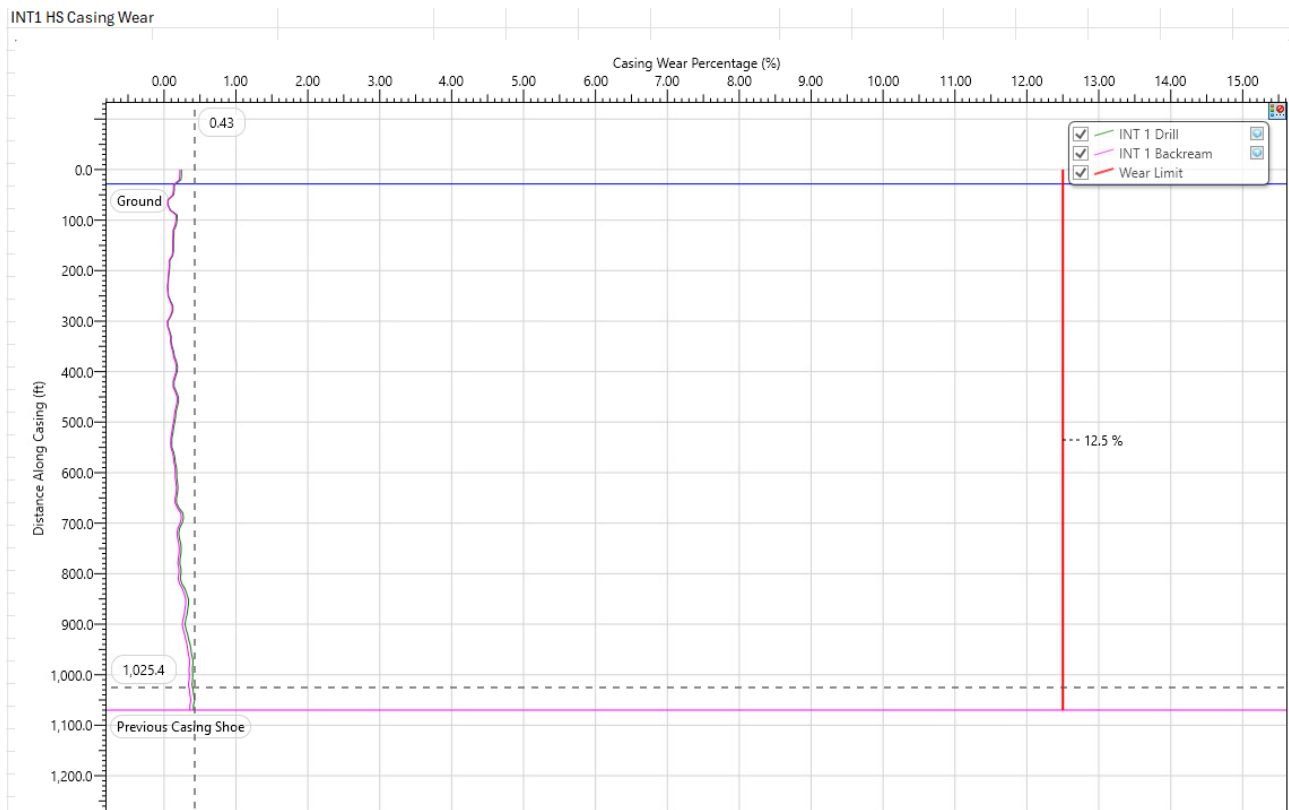
# 4 Casing Wear Analysis & Plan

Casing wear was Modeled in Well Plan - Casing Wear under the following hierarchy: "Chevron MCBU - Lower 48" (Company), "Lea County NM (NAD27 NME)" (Project), "Cotton Draw" (Site), "CO Pad 604 - Casing Wear BOD" (Well), "Pad 604 - CO 3-34 Federal No. 604H" (Wellbore), "Casing OQE - 604H" (Design)"

**Casing Wear Parameter Table**

Design Name	Drilled Hole Section	Impacted Casing	Depth Interval (ft MD)	ROP (ft/h)	RPM	WOB (kip)	Total Revolutions	Wear Factor	Max Wear %
4-String Slimhole 2.0	Intermediate 1	13-3/8"	1070 - 4800	120	70	60	129600	10	0.43
	Intermediate 2	10-3/4"	4800 - 11750	100	50	55	213600	10	4
	Production	7-5/8"	11750 - 23500	100	120	30	871200	10	10.6

Casing wear monitoring plan only required for high complexity and ERD wells



**Fig. 4.1 INT1 HS Casing Wear**

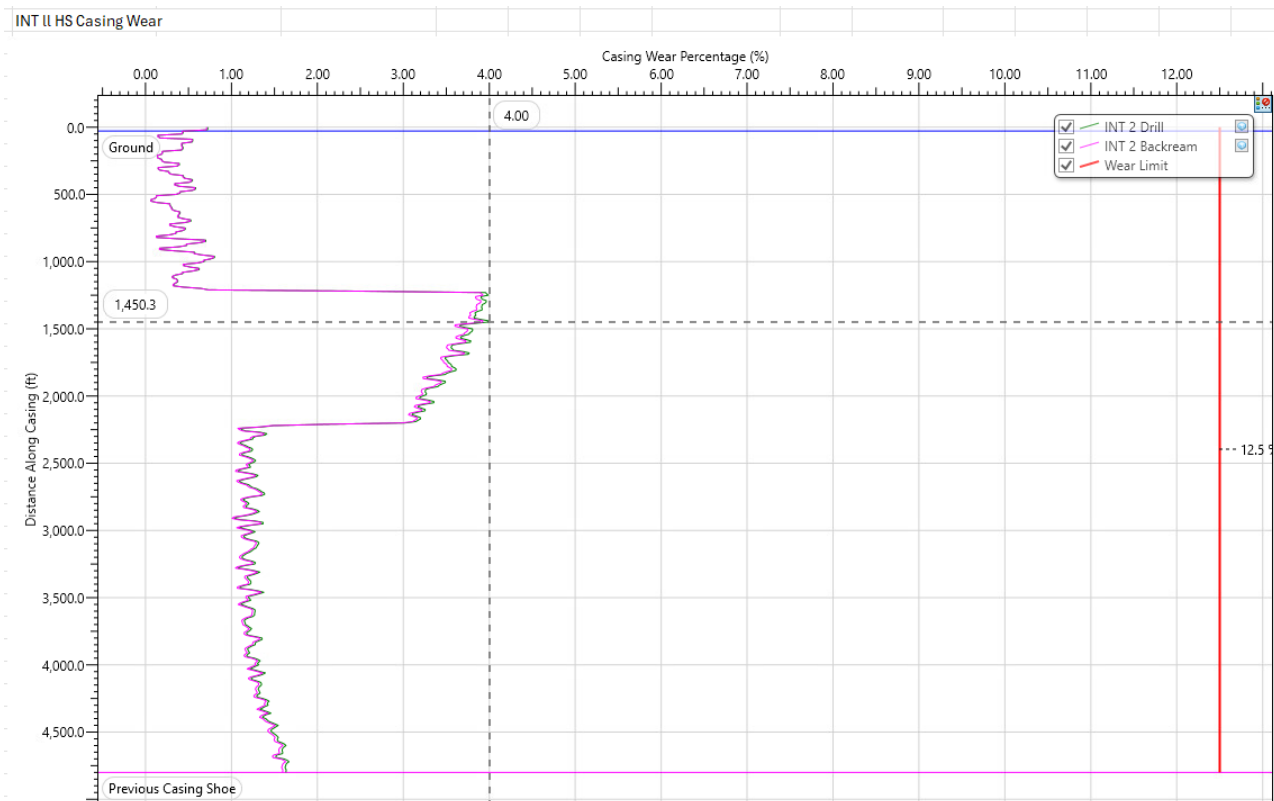


Fig. 4.2 INT2 HS Casing Wear

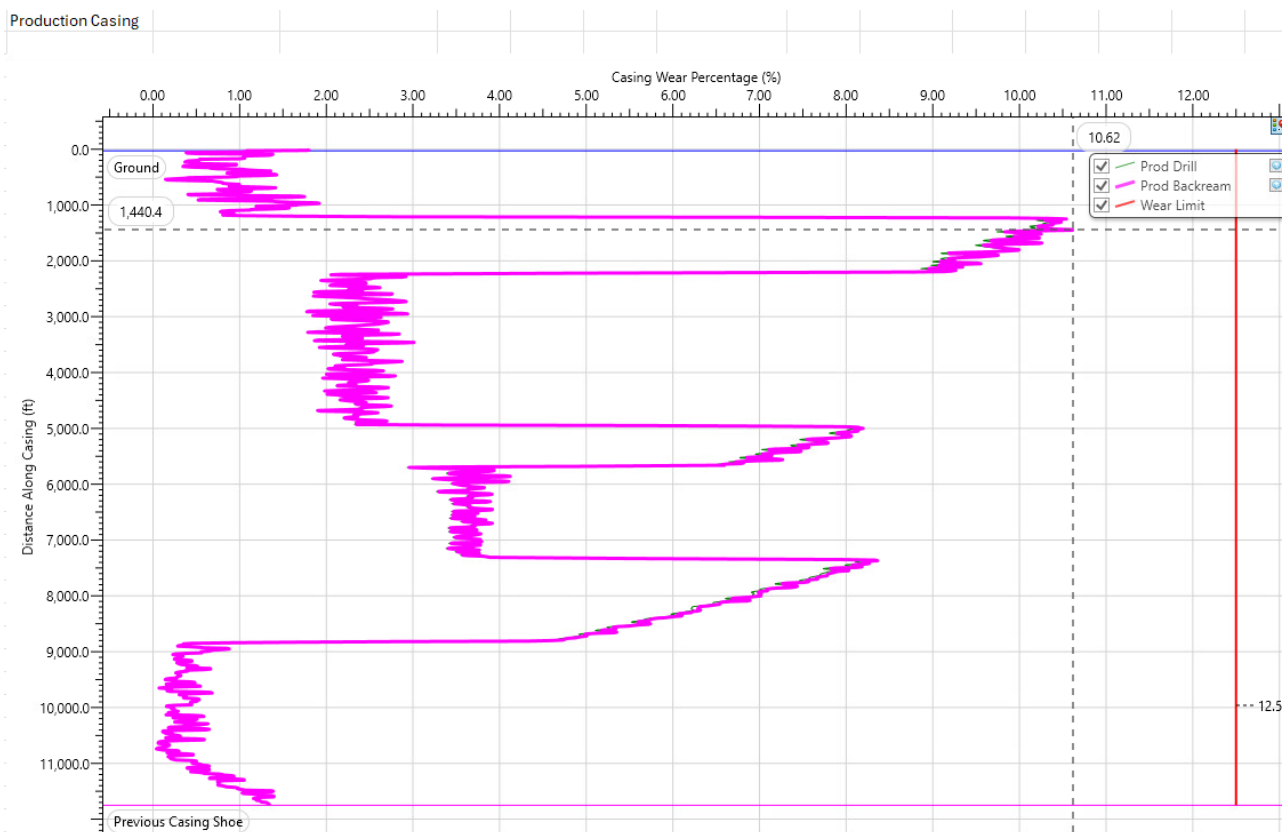


Fig. 4.3 PROD HS Casing Wear

## 5 Casing Pressure Test Plan

### Casing Pressure Test Plan

Design Name	Hole Section	Casing	Test Pressure (psi)	Test Fluid (ppg)	Max Pressure Test MW (ppg)	Basis for Test
4-String Slimhole 2.0	Surface	13-3/8"	1,500 <sup>1</sup>	8.3	10.6	Regulatory Requirement
	Intermediate 1	10-3/4"	2,000	8.3	10.6	70% Burst
	Production Casing	7-5/8"	4,700 <sup>2</sup>	8.3	15	MASP + 500 psi
	Production Liner	5-1/2"	9,800	8.4	8.4	Frac Pressure Test
			9,300 <sup>3</sup>	10 <sup>4</sup>	N/A	Operational pressure limit while pumping with a proppant laden fluid with an equivalent density of 10 ppg (2.6 PPA prop con, 8.5 ppg base fluid)

### Notes:

- OQE assumes the deepest casing set depths expected in Cotton Draw – DRP Engineer to verify casing set depths are less than or equal to depths in Casing Design OQE / Casing Pressure Test Calculator. Consult with C&D engineer to determine test pressure requirements if casing set depths are deeper.
- MASP calculations assume mid-case (expected) pore pressure.
- Casing pressures listed above should be used during execution and should **not** be adjusted if the actual MW is between test fluid weight and the maximum hole section MW.
- <sup>1</sup>For all areas in New Mexico, the BLM requires all casing strings to be tested to 0.22 psi per foot of casing string length or 1,500 psi, whichever is greater, but not to exceed 70% of the minimum internal yield. The team has standardized testing to 1,500 psi for this casing string.
- <sup>2</sup>This is the pressure test required to drill ahead based on MASP + 500 psi. The 7-5/8" casing will be tested up to 9,800 psi in conjunction with the 5-1/2" prior to commencing frac operations.
- <sup>3</sup>Maximum surface pressure w/ 10 ppg (2.6 PPA, 8.5 ppg base fluid) proppant laden fluid in well that results in a safety factor greater than 1.10. This will be the operational pressure limit during execution.
- <sup>4</sup>Fluid density calculated with 1.50 ppa sand concentration with 8.66 ppg produced water.



# 6 PPFG/Temp

## Pore pressure (MD)

MD (ft)	TVD (ft)	PRESSURE (psi)	EMW (lbm/gal)
28.00	28.00	0.00	0.00
812.80	812.64	291.28	6.90
1146.39	1145.20	404.54	6.80
3318.29	3198.76	1329.35	8.00
4970.16	4707.82	2005.41	8.20
5005.62	4740.21	2019.21	8.20
5964.39	5616.09	2421.48	8.30
7424.18	6962.93	3002.20	8.30
9083.00	8613.59	3803.40	8.50
9197.98	8728.57	4670.35	10.30
9597.74	9128.33	5168.77	10.90
10180.45	9711.04	5700.51	11.30
10432.77	9963.36	6003.89	11.60
10720.08	10250.67	6390.03	12.00
11268.36	10798.95	7068.40	12.60
12005.55	11535.89	8209.96	13.70
12540.70	11994.54	8723.30	14.00
13039.60	12161.41	8969.10	14.20
20937.46	12028.45	8773.26	14.04

## Fracture pressure (MD)

MD (ft)	TVD (ft)	PRESSURE (psi)	EMW (lbm/gal)
28.00	28.00	0.00	0.00
812.80	812.64	844.30	20.00
1146.39	1145.20	1070.84	18.00
3318.29	3198.76	2991.05	18.00
4970.16	4707.82	3546.15	14.50
5005.62	4740.21	2905.69	11.80
5964.39	5616.09	3209.19	11.00
7424.18	6962.93	4051.16	11.20
9083.00	8613.59	5682.73	12.70
9197.98	8728.57	6030.65	13.30
9597.74	9128.33	6449.11	13.60
10180.45	9711.04	6759.89	13.40
10432.77	9963.36	7349.60	14.20



10720.08	10250.67	7135.53	13.40
11268.36	10798.95	8358.67	14.90
12005.55	11535.89	9048.93	15.10
12540.70	11994.54	9657.94	15.50
13039.60	12161.41	10725.64	16.98
20937.46	12028.45	9874.93	15.80

Temperature

TVD (ft)	TEMPERATURE (degF)	GRADIENT (degF/(100 ft))
28.00	80.00	
49.00	80.00	
12164.78	175.00	0.78

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# 7 Change Log

**Table 7.1 Change Log**

Date	Updates	Name
Jun 12, 2025	OQE created to support the rollout of Slimhole 2.0 to Cotton Draw Pads (604, 601 & 607). This will serve as the baseline for other Cotton Draw pads going forward.	Chinedu Akwukwaegbu

Link to project: [Add web link to your project here](#)

\_CO 3 10 FED AND CO 34 27 FED COM\_Lea\_\_CHEVRON USA INCORPORATED\_45826\_JS

CO 3 10 FED AND CO 34 27 FED COM

13 3/8		surface csg in a		17 1/2		inch hole.		Design Factors				Surface		
Segment	#/ft	Grade	Coupling	Body	Collapse	Burst	Length	B@s	a-B	a-C	Weight			
"A"	54.50													
"B"														
w/8.4#/g mud, 30min Sfc Csg Test psig: 1,465												Totals:	1,021	55,645
Tail Cmt does not circ to sfc.														
Comparison of Proposed to Minimum Required Cement Volumes														
Hole Size	Annular Volume	1 Stage Cmt Sx	1 Stage CuFt Cmt	Min Cu Ft	1 Stage % Excess	Drilling Mud Wt	Calc MASP	Req'd BOPE				Min Dist Hole-Cplg		
17 1/2	0.6946	746	1091	709	54	10.60	1618	2M				1.56		
Site plat (pipe racks S or E) as per O.O. 1, III D.4-I: not found.														

10 3/4		casing inside the		13 3/8		Design Factors				Int 1				
Segment	#/ft	Grade	Coupling	Body	Collapse	Burst	Length	B@s	a-B	a-C	Weight			
"A"	40.50													
"B"														
w/8.4#/g mud, 30min Sfc Csg Test psig: 56												Totals:	4,893	198,167
The cement volume(s) are intended to achieve a top of 0 ft from surface or a 1021 overlap.														
Hole Size	Annular Volume	1 Stage Cmt Sx	1 Stage CuFt Cmt	Min Cu Ft	1 Stage % Excess	Drilling Mud Wt	Calc MASP	Req'd BOPE				Min Dist Hole-Cplg		
12 1/4	0.1882	853	1780	971	83	10.60	5110	10M				0.25		
D V Tool(s):												sum of sx	Σ CuFt	Σ%excess
t by stage % :												853	1780	83
Class 'C' tail cmt yld > 1.35												MASP is within 10% of 5000psig, need exrta equip?		
Burst Frac Gradient(s) for Segment(s): A, B, C, D = 0.64, b, c, d <0.70 a Problem!!												Keep Casing Full, Burst ok Chevron documentation attached		

7 5/8		casing inside the		10 3/4		Design Factors				Int 2				
Segment	#/ft	Grade	Coupling	Joint	Collapse	Burst	Length	B@s	a-B	a-C	Weight			
"A"	29.70													
"B"														
w/8.4#/g mud, 30min Sfc Csg Test psig: -48												Totals:	11,917	353,935
The cement volume(s) are intended to achieve a top of 4693 ft from surface or a 200 overlap.														
Hole Size	Annular Volume	1 Stage Cmt Sx	1 Stage CuFt Cmt	Min Cu Ft	1 Stage % Excess	Drilling Mud Wt	Calc MASP	Req'd BOPE				Min Dist Hole-Cplg		
9 5/8	0.1882	666	2096	1368	53	12.20	6906	10M				0.86		
Class 'C' tail cmt yld > 1.35												MASP is within 10% of 5000psig, need exrta equip?		
Burst Frac Gradient(s) for Segment(s): A, B, C, D = 0.62, b, c, d <0.70 a														

5 1/2		Liner w/top @		11717		Design Factors				Liner				
Segment	#/ft	Grade	Coupling	Body	Collapse	Burst	Length	B@s	a-B	a-C	Weight			
"A"	20.00													
"B"														
w/8.4#/g mud, 30min Sfc Csg Test psig: 2,717												Totals:	11,608	232,160
The cement volume(s) are intended to achieve a top of 11717 ft from surface or a 200 overlap.														
Hole Size	Annular Volume	1 Stage Cmt Sx	1 Stage CuFt Cmt	Min Cu Ft	1 Stage % Excess	Drilling Mud Wt	Calc MASP	Req'd BOPE				Min Dist Hole-Cplg		
6 3/4	0.0835	1241	1886	971	94	15.00						0.45		
Class 'H' tail cmt yld > 1.20												Capitan Reef est top XXXX. MASP is within 10% of 5000psig, need exrta equip?		

## PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

OPERATOR'S NAME:	CHEVRON USA INCORPORATED
WELL NAME & NO.:	CO 34 27 FEDERAL COM 637H
LOCATION:	Section 3, T.25 S., R.32 E., NMP
COUNTY:	Lea County, New Mexico

COA

H2S	<input checked="" type="radio"/> Yes	<input type="radio"/> No	
Potash	<input checked="" type="radio"/> None	<input type="radio"/> Secretary	<input type="radio"/> R-111-P
Cave/Karst Potential	<input checked="" type="radio"/> Low	<input type="radio"/> Medium	<input type="radio"/> High
Cave/Karst Potential	<input type="radio"/> Critical		
Variance	<input type="radio"/> None	<input checked="" type="radio"/> Flex Hose	<input type="radio"/> Other
Wellhead	<input type="radio"/> Conventional	<input checked="" type="radio"/> Multibowl	<input type="radio"/> Both
Wellhead Variance	<input type="radio"/> Diverter		
Other	<input type="checkbox"/> 4 String	<input type="checkbox"/> Capitan Reef	<input type="checkbox"/> WIPP
Other	<input checked="" type="checkbox"/> Fluid Filled	<input type="checkbox"/> Pilot Hole	<input type="checkbox"/> Open Annulus
Cementing	<input type="checkbox"/> Contingency Cement Squeeze	<input type="checkbox"/> EchoMeter	<input type="checkbox"/> Primary Cement Squeeze
Special Requirements	<input type="checkbox"/> Water Disposal	<input checked="" type="checkbox"/> COM	<input type="checkbox"/> Unit
Special Requirements	<input type="checkbox"/> Batch Sundry		
Special Requirements Variance	<input checked="" type="checkbox"/> Break Testing	<input checked="" type="checkbox"/> Offline Cementing	<input type="checkbox"/> Casing Clearance

### A. HYDROGEN SULFIDE

A Hydrogen Sulfide (H2S) Drilling Plan shall be activated AT SPUD. As a result, the Hydrogen Sulfide area must meet 43 CFR part 3170 requirements, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, please provide measured values and formations to the BLM.

### B. CASING

#### Primary Casing Design:

1. The **13-3/8** inch surface casing shall be set at approximately **1021 feet** (a minimum of **25 feet (Lea County)** into the Rustler Anhydrite, above the salt, and below usable fresh water) and cemented to the surface. The surface hole shall be **16 or 17.5** inch in diameter.
  - a. If cement does not circulate to the surface, the appropriate BLM office shall

be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.

- b. Wait on cement (WOC) time for a primary cement job will be a minimum of **8 hours** or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
- c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
- d. If cement falls back, remedial cementing will be done prior to drilling out that string.

**Operator is approved to use contingency cementing for the Intermediate and Production section. Operator shall notify the BLM before proceeding with contingency operation.**

2. The minimum required fill of cement behind the **10-3/4** inch intermediate casing is:

- Cement to surface. If cement does not circulate see B.1.a, c-d above.  
**Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.**

**Intermediate casing must be kept fluid filled to meet BLM minimum collapse requirement.**

3. The minimum required fill of cement behind the **7-5/8** inch intermediate casing is:

- Cement should tie-back at least **200 feet** into previous casing string. Operator shall provide method of verification.  
**Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.**

4. The minimum required fill of cement behind the **5-1/2** inch production liner is:

- Cement should tie-back **100 feet** into the previous casing. Operator shall provide method of verification.  
**Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.**

### C. PRESSURE CONTROL

1. Variance approved to use flex line from BOP to choke manifold. Manufacturer's specification to be readily available. No external damage to flex line. Flex line to be installed as straight as possible (no hard bends).'
2. Operator has proposed a multi-bowl wellhead assembly. This assembly will only be tested when installed on the **13-3/8** inch surface casing. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be **5000 (5M)** psi. **Variance is approved to use a 5000 (5M) Annular which shall be tested to 3500 (70% Working Pressure) psi.**
  - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
  - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
  - c. Manufacturer representative shall install the test plug for the initial BOP test.
  - d. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
  - e. Whenever any seal subject to test pressure is broken, all the tests in **43 CFR 3172.6(b)(9)** must be followed

### D. SPECIAL REQUIREMENT (S)

#### Communitization Agreement

- The operator will submit a Communitization Agreement to the Santa Fe Office, 301 Dinosaur Trail Santa Fe, New Mexico 87508, at least 90 days before the anticipated date of first production from a well subject to a spacing order issued by the New Mexico Oil Conservation Division. The Communitization Agreement will include the signatures of all working interest owners in all Federal and Indian leases subject to the Communitization Agreement (i.e., operating rights owners and lessees of record), or certification that the operator has obtained the written signatures of all such owners and will make those signatures available to the BLM immediately upon request.
- The operator will submit an as-drilled survey well plat of the well completion, but are not limited to, those specified in 43 CFR 3170.
- If the operator does not comply with this condition of approval, the BLM may take enforcement actions that include, but are not limited to, those specified in 43 CFR 3163.1.
- In addition, the well sign shall include the surface and bottom hole lease numbers. When the Communitization Agreement number is known, it shall also be on the sign.

#### (Note: For a minimum 5M BOPE or less (Utilizing a 10M BOPE system)

#### BOPE Break Testing Variance

- BOPE Break Testing is ONLY permitted for 5M BOPE or less. (Annular preventer

**must be tested to a minimum of 70% of BOPE working pressure and shall be higher than the MASP)**

- BOPE Break Testing is NOT permitted to drilling the production hole section.
- Variance only pertains to the intermediate hole-sections and no deeper than the Bone Springs formation.
- While in transfer between wells, the BOPE shall be secured by the hydraulic carrier or cradle.
- Any well control event while drilling require notification to the BLM Petroleum Engineer (575-706-2779) prior to the commencement of any BOPE Break Testing operations.
- A full BOPE test is required prior to drilling the first deep intermediate hole section. If any subsequent hole interval is deeper than the first, a full BOPE test will be required. (200' TVD tolerance between intermediate shoes is allowable).
- The BLM is to be contacted (575-689-5981 Lea County) 4 hours prior to BOPE tests.
- As a minimum, a full BOPE test shall be performed at 21-day intervals.
- In the event any repairs or replacement of the BOPE is required, the BOPE shall test as per 43 CFR 3170.

**Offline Cementing**

Contact the BLM prior to the commencement of any offline cementing procedure.

**GENERAL REQUIREMENTS**

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)

Eddy County

**EMAIL** or call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220,

[BLM\\_NM\\_CFO\\_DrillingNotifications@BLM.GOV](mailto:BLM_NM_CFO_DrillingNotifications@BLM.GOV)

(575) 361-2822

Lea County

Call the Hobbs Field Station, 414 West Taylor, Hobbs NM 88240,

(575) 689-5981

1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.
  - a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after installing and testing the wellhead, by installing a blind flange of like

pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).

- b. When the operator proposes to set surface casing with Spudder Rig
  - i. Notify the BLM when moving in and removing the Spudder Rig.
  - ii. Notify the BLM when moving in the 2<sup>nd</sup> Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.
  - iii. BOP/BOPE test to be conducted per **43 CFR 3172** as soon as 2<sup>nd</sup> Rig is rigged up on well.
2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the dog house or stairway area.
3. For intervals in which cement to surface is required, cement to surface should be verified with a visual check and density or pH check to differentiate cement from spacer and drilling mud. The results should be documented in the driller's log and daily reports.

#### A. CASING

1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.
2. Wait on cement (WOC) for Potash Areas: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends of both lead and tail cement, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
3. Wait on cement (WOC) for Water Basin: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement

reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.

4. Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.
5. No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.
6. On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.
7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.
8. Whenever a casing string is cemented in the R-111-Q potash area, the NMOCD requirements shall be followed.

## **B. PRESSURE CONTROL**

1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in **43 CFR 3172**.
2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor.

3. 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.
4. If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:
  - i. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
  - ii. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
  - iii. Manufacturer representative shall install the test plug for the initial BOP test.
  - iv. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR 3172.6(b)(9) must be followed.
  - v. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
5. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
  - i. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead cement), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).
  - ii. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the cement plug. The BOPE test can be initiated after bumping the cement plug with the casing valve open. (only applies to single stage cement jobs, prior to the cement setting up.)

- iii. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer and can be initiated immediately with the casing valve open. The operator also has the option of utilizing an independent tester to test without a plug (i.e. against the casing) pursuant to **43 CFR 3172** with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for 8 hours or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).
- iv. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.
- v. The results of the test shall be reported to the appropriate BLM office.
- vi. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
- vii. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.
- viii. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per **43 CFR 3172**.

### **C. DRILLING MUD**

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

### **D. WASTE MATERIAL AND FLUIDS**

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material

or fluid shall be disposed of on the well location or surrounding area. Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

JS 6/18/2025



# TenarisHydril Wedge 441®



Coupling	Pipe Body
Grade: P110-ICY	Grade: P110-ICY
Body: White	1st Band: White
1st Band: Pale Green	2nd Band: Pale Green
2nd Band: -	3rd Band: Pale Green
3rd Band: -	4th Band: -
	5th Band: -
	6th Band: -

Outside Diameter	5.500 in.	Wall Thickness	0.361 in.	Grade	P110-ICY
Min. Wall Thickness	87.50 %	Pipe Body Drift	API Standard	Type	Casing
Connection OD Option	REGULAR				

### Pipe Body Data

Geometry		Performance	
Nominal OD	5.500 in.	Wall Thickness	0.361 in.
Nominal Weight	20.00 lb/ft	Plain End Weight	19.83 lb/ft
Drift	4.653 in.	OD Tolerance	API
Nominal ID	4.778 in.		
		Body Yield Strength	729 x1000 lb
		Min. Internal Yield Pressure	14,360 psi
		SMYS	125,000 psi
		Collapse Pressure	12,300 psi

### Connection Data

Geometry		Performance		Make-Up Torques	
Connection OD	5.852 in.	Tension Efficiency	81.50 %	Minimum	15,000 ft-lb
Coupling Length	8.714 in.	Joint Yield Strength	594 x1000 lb	Optimum	16,000 ft-lb
Connection ID	4.778 in.	Internal Pressure Capacity	14,360 psi	Maximum	19,200 ft-lb
Make-up Loss	3.780 in.	Compression Efficiency	81.50 %		
Threads per inch	3.40	Compression Strength	594 x1000 lb		
Connection OD Option	Regular	Max. Allowable Bending	82.06 °/100 ft		
		External Pressure Capacity	12,300 psi		
				Operation Limit Torques	
				Operating Torque	36,000 ft-lb
				Yield Torque	42,000 ft-lb
				Buck-On	
				Minimum	19,200 ft-lb
				Maximum	20,700 ft-lb

### Notes

This connection is fully interchangeable with:  
 Wedge 441® - 5.5 in. - 0.304 (17.00) in. (lb/ft)  
 Wedge 461® - 5.5 in. - 0.304 (17.00) / 0.361 (20.00) / 0.415 (23.00) in. (lb/ft)  
 Connections with Dopeless® Technology are fully compatible with the same connection in its doped version

For the latest performance data, always visit our website: [www.tenaris.com](http://www.tenaris.com)  
 For further information on concepts indicated in this datasheet, download the Datasheet Manual from [www.tenaris.com](http://www.tenaris.com)

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# TenarisHydril Wedge 441<sup>®</sup>



Coupling	Pipe Body
Grade: P110-ICY	Grade: P110-ICY
Body: White	1st Band: White
1st Band: Pale Green	2nd Band: Pale Green
2nd Band: -	3rd Band: Pale Green
3rd Band: -	4th Band: -
	5th Band: -
	6th Band: -

Outside Diameter	7.625 in.	Wall Thickness	0.375 in.	Grade	P110-ICY
Min. Wall Thickness	90.00 %	Pipe Body Drift	API Standard	Type	Casing
Connection OD Option	REGULAR				

### Pipe Body Data

Geometry		Performance	
Nominal OD	7.625 in.	Wall Thickness	0.375 in.
Nominal Weight	29.70 lb/ft	Plain End Weight	29.06 lb/ft
Drift	6.750 in.	OD Tolerance	API
Nominal ID	6.875 in.		
		Body Yield Strength	1068 x1000 lb
		Min. Internal Yield Pressure	11,070 psi
		SMYS	125,000 psi
		Collapse Pressure	7360 psi

### Connection Data

Geometry		Performance		Make-Up Torques	
Connection OD	7.900 in.	Tension Efficiency	75 %	Minimum	22,000 ft-lb
Coupling Length	8.666 in.	Joint Yield Strength	801 x1000 lb	Optimum	23,000 ft-lb
Connection ID	6.875 in.	Internal Pressure Capacity	11,070 psi	Maximum	26,000 ft-lb
Make-up Loss	3.750 in.	Compression Efficiency	75 %		
Threads per inch	3.43	Compression Strength	801 x1000 lb	<b>Operation Limit Torques</b>	
Connection OD Option	Regular	Max. Allowable Bending	56 °/100 ft	Operating Torque	33,000 ft-lb
		External Pressure Capacity	7360 psi	Yield Torque	39,000 ft-lb
				<b>Buck-On</b>	
				Minimum	25,000 ft-lb
				Maximum	27,000 ft-lb

### Notes

Connection performance values are related to structural capabilities. For sealability-related performance information, request the Connection Service Envelope from your local Tenaris Representative.

For the latest performance data, always visit our website: [www.tenaris.com](http://www.tenaris.com)  
 For further information on concepts indicated in this datasheet, download the Datasheet Manual from [www.tenaris.com](http://www.tenaris.com)

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ONSHORE ORDER NO. 1  
Chevron  
CO 34 27 FEDERAL COM 637H  
Lea County

**Pad Summary: CO Pad 305**

The table below lists all the wells for the given pad and their respective name and TVD's (ft) for their production target intervals:

Well Name(s)	Target TVD	Formation Desc.
CO 34 27 FEDERAL COM 633H	12,350	Wolfcamp A
CO 3 10 FEDERAL 634H	12,350	Wolfcamp A
CO 34 27 FEDERAL COM 635H	12,350	Wolfcamp A
CO 3 10 FEDERAL 636H	12,350	Wolfcamp A
CO 34 27 FEDERAL COM 637H	12,350	Wolfcamp A
CO 3 10 FEDERAL 638H	12,350	Wolfcamp A

**1. GEOLOGICAL TOPS**

Elevation: As seen in C-102

The estimated tops of important geologic markers are as follows:

FORMATION	LITHOLOGIES	TVD	MD	Producing Formation?
Rustler (RSLR)	Sandstone	890	890	No
Saldo (SLDO)	Anhydrite/Salt	1,215	1,216	No
Castile (CSTL)	Anhydrite/Salt	3,278	3,286	No
Lamar (LMAR)	Limestone/Shale	4,818	4,826	No
Bell Canyon (BEL)	Sandstone/Limestone	4,861	4,869	No
Cherry Canyon (CHR)	Sandstone/Siltstone	5,723	5,731	No
Brushy Canyon (BCN)	Sandstone/Limestone	7,123	7,131	No
Bone Spring (BSL)	Shale/Siltstone	8,763	8,771	No
Upper Avalon (AVU)	Shale	8,878	8,886	No
Lower Avalon (AVL)	Shale	9,242	9,250	No
First Bone Spring Upper (FBU)	Sandstone/Shale	9,774	9,782	No
First Bone Spring Lower (FBL)	Sandstone/Shale	10,093	10,101	No
Second Bone Spring Upper (SBU)	Sandstone/Shale	10,431	10,439	No
Second Bone Spring Lower (SBL)	Sandstone/Shale	10,931	10,939	No
Third Bone Spring (TBS)	Sandstone/Shale	11,678	11,686	No
Wolfcamp A (WCA)	Sandstone/Shale	12,086	12,111	Yes: Oil & Natural Gas

WELLBORE LOCATIONS	MD	TVD
SHL	-	-
KOP	11,785	11,777
FTP	12,685	12,350
LTP	23,118	12,350
BHL	23,193	12,350

**2. BOP EQUIPMENT AND TESTING**

Rating Depth  TVD

**Equipment**

Chevron will have a minimum of a 5,000 psi rig stack for drill out below surface casing and a 10,000 psi rig stack for drilling the production hole section. See attached proposed schematics and 10,000 PSI Annular BOP Variance Request.

**Request Variance: Yes**

**Variance Request(s)**

Chevron respectfully request to vary from 43 CFR 3172 where it states: "(A full BOP Test) shall be performed: when initially installed and whenever any seal subject to test pressure is broken." We propose to break test if able to finish the next hole section within 21 days of the previous full BOP test. No BOP components nor any break will ever surpass 21 days between testing. A break test will consist of a 250 psi low / ≥ 5,000 psi high for 10 min each test against the connection that was broken when skidding the rig. Upon the first nipple up of the pad a full BOP test will be performed. A full BOP test will be completed prior to drilling the production lateral sections unless the BOP connection was not broken prior to drilling that hole section (example: drilling straight from production into production liner hole section). A break test will only be performed on operations where BLM documentation states a 5M or less BOP can be utilized.

Chevron respectfully requests a variance to use a FMC Technologies UH-S Multibowl wellhead, which will be run through the rig floor on surface casing. BOPE will be nipples up and tested after cementing surface casing. Subsequent tests will be performed as needed, not to exceed 30 days. The field report from FMC Technologies and BOP test information will be provided in a subsequent report at the end of the well. Please see the attached wellhead schematic. An installation manual has been placed on file with the BLM office and remains unchanged from previous submittal. All tests performed by third party.

**Testing Procedure**

The stack will be tested as specified in the attached testing requirements. Batch drilling of the surface, production, and production liner will take place. A full BOP test will be performed per hole section, unless approval from BLM is received otherwise (see variance request ). Flex choke hose will be used for all wells on the pad (see attached specs and variance). BOP test pressures and other documented tests may be recorded and documented via utilization of a Digital BOP Test Method in lieu of the standard test chart. In the event the digital test system is unavailable, the standard test chart will be used.

**3. CASING PROGRAM**

a. The proposed PRIMARY casing program will be as follows:

Purpose	Top (MD)	Top (TVD)	Bot (MD)	Bot (TVD)	Hole Size	Csg Size	Weight	Grade	Thread
Surface	0'	0'	1,021'	1,021'	17.5"	13.375"	54.5 #	J-55	BTC/STC
Intermediate 1	0'	0'	4,806'	4,798'	12.25"	10-3/4"	40.5 #	J-55	BTC/LTC
Intermediate 2	0'	0'	11,785'	11,777'	9-7/8"	7-5/8"	29.7 #	P-110	W441
Production Liner	11,585'	11,577'	23,193'	12,350'	6.75"	5-1/2"	20.0 #	P-110	W441

Surface casing set below magenta dolomite and above top of salt (25 ft below los medianos)

- b. All casing strings will be new pipe.
- c. Casing design depths subject to revision based on directional drilling and geologic conditions encountered.
- Chevron will keep casing fluid filled at all times and while RIH. Chevron will check casing at a minimum of every 20 jts (~840'), and never to surpass 1/3 of casing, while running intermediate and production casing in order to maintain collapse SF.

Casing String	Min SF Collapse	Min SF Burst	Min SF Axial (Joint)	Min SF Axial (Body)
Surface	2.01	1.72	16.34	15.33
Intermediate 1	0.60	0.64	3.23	3.24
Intermediate 2	0.99	1.60	3.05	3.05
Production Liner	1.28	2.08	2.40	2.95

4. **CEMENTING PROGRAM**

Slurry	Type	Top	Bottom	Quantity	Yield	Density	%Excess	Volume	Additives
				(sks)	(cuft/sk)	(ppg)		(cuft)	
<b>Surface Casing 13-3/8"</b>									
Lead	Class C	0'	521'	89	2.29	12.8	25	204	Extender, Antifoam, Retarder, Viscosifier
Tail	Class C	521'	1,021'	657	1.35	14.8	25	887	Extender, Antifoam, Retarder, Viscosifier
<b>Intermediate 1 Casing 10-3/4"</b>									
<i>Planned single stage cement job</i>									
Lead	Class C	0'	3,806'	575	2.29	11.5	25	1317	Extender, Antifoam, Retarder, Viscosifier
Tail	Class C	3,806'	4,806'	263	1.63	12.6	25	429	Extender, Antifoam, Retarder, Viscosifier
<i>Contingency: Top Job</i>									
1st Tail	Class C	0'	3,806'	1104	1.35	14.8	25	1490	Extender, Antifoam, Retarder, Viscosifier
<b>Intermediate 2 Casing 7-5/8"</b>									
<i>Planned single stage cement job</i>									
Lead	Class C	0'	10,785'	536	3.52	10.5	25	1885	Extender, Antifoam, Retarder, Viscosifier
Tail	Class C	10,785'	11,785'	124	1.52	12.6	25	188	Extender, Antifoam, Retarder, Viscosifier
<i>Contingency: Top Job</i>									
1st Tail	Class C	0'	8,785'	1223	1.35	14.8	25	1651	Extender, Antifoam, Retarder, Viscosifier
<b>Production Liner 5-1/2"</b>									
Lead	Class H	11,585'	23,193'	899	1.52	12.6	25	1366	Extender, Antifoam, Retarder, Viscosifier

Surface casing shall have at least one centralizer installed on each of the bottom three joints starting with the shoe joint.

5. **MUD PROGRAM**

Top	Bottom	Type	Min MW	Max MW at TD	Additional Characteristics
0'	1,021'	Spud Mud	8.3	10.6	
1,021'	4,806'	Brine	7.2	10.6	Saturated brine would be used through salt sections.
4,806'	11,785'	WBM/Brine	7.2	12.2	
11,785'	23,193'	OBM	9.0	15.0	Due to wellbore instability in the lateral, may exceed the MW window needed to maintain overburden stresses

A weighting agent and lost circulating material (LCM) will be onsite to mitigate pressure or lost circulation as hole conditions dictate.

If an open reserve pit is not approved by OCD, a closed system will be used consisting of above ground steel tanks and all wastes accumulated during drilling operations will be contained in a portable trash cage and removed from location and deposited in an approved sanitary landfill. If an open reserve pit is in place, pit construction, operation, and closure will follow all applicable rules and regulation. Sanitary wastes will be contained in a chemical porta-toilet and then hauled to an approved sanitary landfill.

All fluids and cuttings will be disposed of in accordance with New Mexico Oil Conservation Division rules and regulations. And transporting of E&P waste will follow EPA regulations and accompanying manifests.

A mud test shall be performed every 24 hours after mudding up to determine, as applicable: density, viscosity, gel strength, filtration, and pH.

Visual mud monitoring equipment shall be in place to detect volume changes indicating loss or gain of circulating fluid volume. When abnormal pressures are anticipated -- a pit volume totalizer (PVT), stroke counter, and flow sensor will be used to detect volume changes indicating loss or gain of circulating fluid volume.

6. **TESTING, LOGGING, AND CORING**

- a. **Production tests are not planned.**
- b. Logs run include: **Gamma Ray Log, Directional Survey**  
Neutron log exception granted by BLM Geologist C. Armistead on 6/11/2024
- c. **Coring Operations are not planned.**

7. **ABNORMAL PRESSURES AND HYDROGEN SULFIDE**

Anticipated BHP	9,633 psi
Anticipated BHT	215 °F
Anticipated abnormal pressures?	Yes
Describe abnormal pressures	Pressure ramp begins in the bottom of the Third Bone Spring formation
Contingency plan(s) description:	- Casing design accounts for pressure ramp - Mud weighting agents available on location to increase drilling fluid density - BOP, choke, and well control drills - BOP functioned and pressure tested

Hydrogen sulfide gas is not anticipated: However the H2S Contingency plan is attached with this APD in the event that H2S is encountered

8. **OTHER ITEMS**

- a. **Batch drilling** will be employed whereby the drilling rig may drill a specific hole section on all wells prior to moving to the next hole section.
- b. **Shallow rig** may be utilized to drill surface or intermediate sections. The production section will not be drilled by the shallow rig.
- c. **Wait on cement** duration for surface and intermediate string(s) will be based on time for tail slurry to develop 500 psi compressive strength and will follow rules as laid out in Onshore Order 2
- d. **Offline cementing** will be employed on the hole sections that run a long string casing to surface. Offline cementing schematic below.



CO 34 27 Federal Com No. 637H R1 mdv 12May25 Proposal Geodetic Report



Def Plan

Report Date: May 13, 2025 - 02:36 AM ( UTC 0 )
Client: Chevron
Field: NMI, Lea County (NAD 83)
Structure / Slot: Chevron CO Pad 305 / CO 34 27 Federal Com No. 637H
Well: CO 34 27 Federal Com No. 637H
Borehole: CO 34 27 Federal Com No. 637H
UBH / APH: Unknown / Unknown
Survey Name: CO 34 27 Federal Com No. 637H R1 mdv 12May25
Survey Date: May 12, 2025
Tort / AHD / DDI / ERD Ratio: 100.121 \* / 11275.049 ft / 6.326 / 0.913
Coordinate Reference System: NAD27 New Mexico State Plane, Eastern Zone, US Feet
Location Lat / Long: 32°53.36408'N, 103°39'18.18388'W
Location Grid NE YZ: N 424345.080 NUS, E 709899.040 NUS
CRS Grid Convergence Angle: 0.361°
Grid Scale Factor: 0.99995955(Applied)
Version / Patch: 2024.5.0.1
Survey / DLS Computation: Minimum Curvature / Lubinski
Vertical Section Azimuth: 359.650 °(Grid North)
Vertical Section Origin: 0.000 ft, 0.000 ft
TVD Reference Datum: RKB
TVD Reference Elevation: 3537.000 ft above MSL
Seabed / Ground Elevation: 3509.000 ft above MSL
Magnetic Declination: 6.265°
Total Gravity Field Strength: 988.427mgm (9.80665 Baseed)
Gravity Model: GARM
Total Magnetic Field Strength: 47412.563 nT
Magnetic Dip Angle: 59.712°
Declination Date: June 01, 2023
Magnetic Declination Model: IGM18.2025
North Reference: Grid North
Grid Convergence Used: 0.361°
Total Corr Mag North-Grid North: 5.907"
Local Coord Referenced To: Well Head

Table with columns: Comments, MD (ft), Incl (°), Azim (°), TVD (ft), TVDSS (ft), VSEC (ft), NS (ft), EW (ft), DLS (ft/100ft), Northing (ftUS), Easting (ftUS), Latitude (° ' " ), Longitude (° ' " ). Rows include Surface, Build 1.5'100ft, Rustler (RSLR), Hold, Saldo (SLDO), Drop 1.5'100ft, Hold Vertical, Castle (CSTL), Lamar (LMAR), Bell Canyon (BEL), Cherry Canyon (CHR), Brushy Canyon (BCN), Bone Spring (BSL), Upper Avalon (AVU), Lower Avalon (AVL), and First Bone Spring Upper (FBU).

Comments	MD (ft)	Incl (°)	Azim (°)	TVD (ft)	TVDSS (ft)	VSEC (ft)	NS (ft)	EW (ft)	DLS (ft/100ft)	Northing (ftUS)	Easting (ftUS)	Latitude (° '' )	Longitude (° '' )
First Bone Spring Lower (FBL)	10,101.06	0.00	48.90	10,093.00	6,556.00	126.90	127.80	146.52	0.00	424,472.87	710,035.55	32°9'54.619545" N	103°39'16.470087" W
	10,200.00	0.00	48.90	10,191.94	6,654.94	126.90	127.80	146.52	0.00	424,472.87	710,035.55	32°9'54.619545" N	103°39'16.470087" W
	10,300.00	0.00	48.90	10,291.94	6,754.94	126.90	127.80	146.52	0.00	424,472.87	710,035.55	32°9'54.619545" N	103°39'16.470087" W
	10,400.00	0.00	48.90	10,391.94	6,854.94	126.90	127.80	146.52	0.00	424,472.87	710,035.55	32°9'54.619545" N	103°39'16.470087" W
	10,439.06	0.00	48.90	10,431.00	6,894.00	126.90	127.80	146.52	0.00	424,472.87	710,035.55	32°9'54.619545" N	103°39'16.470087" W
Second Bone Spring Upper (SBU)	10,500.00	0.00	48.90	10,491.94	6,954.94	126.90	127.80	146.52	0.00	424,472.87	710,035.55	32°9'54.619545" N	103°39'16.470087" W
	10,600.00	0.00	48.90	10,591.94	7,054.94	126.90	127.80	146.52	0.00	424,472.87	710,035.55	32°9'54.619545" N	103°39'16.470087" W
	10,700.00	0.00	48.90	10,691.94	7,154.94	126.90	127.80	146.52	0.00	424,472.87	710,035.55	32°9'54.619545" N	103°39'16.470087" W
	10,800.00	0.00	48.90	10,791.94	7,254.94	126.90	127.80	146.52	0.00	424,472.87	710,035.55	32°9'54.619545" N	103°39'16.470087" W
	10,900.00	0.00	48.90	10,891.94	7,354.94	126.90	127.80	146.52	0.00	424,472.87	710,035.55	32°9'54.619545" N	103°39'16.470087" W
Second Bone Spring Lower (SBL)	10,939.06	0.00	48.90	10,931.00	7,394.00	126.90	127.80	146.52	0.00	424,472.87	710,035.55	32°9'54.619545" N	103°39'16.470087" W
	11,000.00	0.00	48.90	10,991.94	7,454.94	126.90	127.80	146.52	0.00	424,472.87	710,035.55	32°9'54.619545" N	103°39'16.470087" W
	11,100.00	0.00	48.90	11,091.94	7,554.94	126.90	127.80	146.52	0.00	424,472.87	710,035.55	32°9'54.619545" N	103°39'16.470087" W
	11,200.00	0.00	48.90	11,191.94	7,654.94	126.90	127.80	146.52	0.00	424,472.87	710,035.55	32°9'54.619545" N	103°39'16.470087" W
	11,300.00	0.00	48.90	11,291.94	7,754.94	126.90	127.80	146.52	0.00	424,472.87	710,035.55	32°9'54.619545" N	103°39'16.470087" W
Third Bone Spring (TBS)	11,400.00	0.00	48.90	11,391.94	7,854.94	126.90	127.80	146.52	0.00	424,472.87	710,035.55	32°9'54.619545" N	103°39'16.470087" W
	11,600.00	0.00	48.90	11,591.94	8,054.94	126.90	127.80	146.52	0.00	424,472.87	710,035.55	32°9'54.619545" N	103°39'16.470087" W
	11,686.06	0.00	48.90	11,678.00	8,141.00	126.90	127.80	146.52	0.00	424,472.87	710,035.55	32°9'54.619545" N	103°39'16.470087" W
	11,700.00	0.00	48.90	11,691.94	8,154.94	126.90	127.80	146.52	0.00	424,472.87	710,035.55	32°9'54.619545" N	103°39'16.470087" W
	11,785.10	0.00	48.90	11,777.04	8,240.04	126.90	127.80	146.52	0.00	424,472.87	710,035.55	32°9'54.619545" N	103°39'16.470087" W
Build 10"/100ft	11,800.00	1.49	359.62	11,791.94	8,254.94	127.10	127.99	146.52	10.00	424,473.07	710,035.55	32°9'54.621462" N	103°39'16.470087" W
	11,900.00	11.49	359.62	11,891.17	8,354.17	138.38	139.28	146.44	10.00	424,484.36	710,035.48	32°9'54.733168" N	103°39'16.470138" W
	12,000.00	21.49	359.62	11,986.94	8,449.94	167.73	167.63	146.25	10.00	424,512.70	710,035.29	32°9'55.013694" N	103°39'16.470266" W
	12,100.00	31.49	359.62	12,076.32	8,539.32	211.28	212.18	145.96	10.00	424,557.25	710,034.99	32°9'55.454516" N	103°39'16.470465" W
	12,200.00	41.49	359.62	12,166.00	8,629.00	258.84	259.74	145.67	10.00	424,602.81	710,034.69	32°9'55.514490" N	103°39'16.470622" W
	12,300.00	51.49	359.62	12,255.38	8,718.38	306.39	307.29	145.38	10.00	424,648.36	710,034.39	32°9'55.574464" N	103°39'16.470779" W
	12,400.00	61.49	359.62	12,344.76	8,807.76	353.94	354.84	145.09	10.00	424,693.91	710,034.09	32°9'55.634438" N	103°39'16.470936" W
	12,500.00	71.49	359.62	12,434.14	8,897.14	401.49	402.39	144.80	10.00	424,739.46	710,033.79	32°9'55.694412" N	103°39'16.471093" W
	12,600.00	81.49	359.62	12,523.52	8,986.52	449.04	450.04	144.51	10.00	424,785.01	710,033.49	32°9'55.754386" N	103°39'16.471250" W
	12,700.00	91.49	359.62	12,612.90	9,075.90	496.59	497.59	144.22	10.00	424,830.56	710,033.19	32°9'55.814360" N	103°39'16.471407" W
Wolfcamp A (WCA)	12,800.00	91.49	359.62	12,702.28	9,165.28	544.14	545.14	143.93	10.00	424,876.11	710,032.89	32°9'55.874334" N	103°39'16.471564" W
	12,900.00	91.49	359.62	12,791.66	9,254.66	591.69	592.69	143.64	10.00	424,921.66	710,032.59	32°9'55.934308" N	103°39'16.471721" W
	13,000.00	91.49	359.62	12,881.04	9,344.04	639.24	640.24	143.35	10.00	424,967.21	710,032.29	32°9'55.994282" N	103°39'16.471878" W
	13,100.00	91.49	359.62	12,970.42	9,433.42	686.79	687.79	143.06	10.00	425,012.76	710,031.99	32°9'56.054256" N	103°39'16.472035" W
	13,200.00	91.49	359.62	13,059.80	9,522.80	734.34	735.34	142.77	10.00	425,058.31	710,031.69	32°9'56.114230" N	103°39'16.472192" W
	13,300.00	91.49	359.62	13,149.18	9,612.18	781.89	782.89	142.48	10.00	425,103.86	710,031.39	32°9'56.174204" N	103°39'16.472349" W
	13,400.00	91.49	359.62	13,238.56	9,701.56	829.44	830.44	142.19	10.00	425,149.41	710,031.09	32°9'56.234178" N	103°39'16.472506" W
	13,500.00	91.49	359.62	13,327.94	9,790.94	876.99	877.99	141.90	10.00	425,194.96	710,030.79	32°9'56.294152" N	103°39'16.472663" W
	13,600.00	91.49	359.62	13,417.32	9,880.32	924.54	925.54	141.61	10.00	425,240.51	710,030.49	32°9'56.354126" N	103°39'16.472820" W
	13,700.00	91.49	359.62	13,506.70	9,969.70	972.09	973.09	141.32	10.00	425,286.06	710,030.19	32°9'56.414100" N	103°39'16.472977" W
Landing Point FTP Cross	13,800.00	91.49	359.62	13,596.08	10,059.08	1,019.64	1,020.64	141.03	10.00	425,331.61	710,029.89	32°9'56.474074" N	103°39'16.473134" W
	13,900.00	91.49	359.62	13,685.46	10,148.46	1,067.19	1,068.19	140.74	10.00	425,377.16	710,029.59	32°9'56.534048" N	103°39'16.473291" W
	14,000.00	91.49	359.62	13,774.84	10,237.84	1,114.74	1,115.74	140.45	10.00	425,422.71	710,029.29	32°9'56.594022" N	103°39'16.473448" W
	14,100.00	91.49	359.62	13,864.22	10,327.22	1,162.29	1,163.29	140.16	10.00	425,468.26	710,028.99	32°9'56.653996" N	103°39'16.473605" W
	14,200.00	91.49	359.62	13,953.60	10,416.60	1,209.84	1,210.84	139.87	10.00	425,513.81	710,028.69	32°9'56.713970" N	103°39'16.473762" W
	14,300.00	91.49	359.62	14,042.98	10,506.00	1,257.39	1,258.39	139.58	10.00	425,559.36	710,028.39	32°9'56.773944" N	103°39'16.473919" W
	14,400.00	91.49	359.62	14,132.36	10,595.40	1,304.94	1,305.94	139.29	10.00	425,604.91	710,028.09	32°9'56.833918" N	103°39'16.474076" W
	14,500.00	91.49	359.62	14,221.74	10,684.80	1,352.49	1,353.49	139.00	10.00	425,650.46	710,027.79	32°9'56.893892" N	103°39'16.474233" W
	14,600.00	91.49	359.62	14,311.12	10,774.20	1,400.04	1,401.04	138.71	10.00	425,696.01	710,027.49	32°9'56.953866" N	103°39'16.474390" W
	14,700.00	91.49	359.62	14,400.50	10,863.60	1,447.59	1,448.59	138.42	10.00	425,741.56	710,027.19	32°9'57.013840" N	103°39'16.474547" W
14,800.00	91.49	359.62	14,490.00	10,953.00	1,495.14	1,496.14	138.13	10.00	425,787.11	710,026.89	32°9'57.073814" N	103°39'16.474704" W	
MP, Turn 2"/100ft Hold	14,900.00	91.49	359.62	14,579.40	11,042.40	1,542.69	1,543.69	137.84	10.00	425,832.66	710,026.59	32°9'57.133788" N	103°39'16.474861" W
	15,000.00	91.49	359.62	14,668.80	11,131.80	1,590.24	1,591.24	137.55	10.00	425,878.21	710,026.29	32°9'57.193762" N	103°39'16.475018" W
	15,100.00	91.49	359.62	14,758.20	11,221.20	1,637.79	1,638.79	137.26	10.00	425,923.76	710,025.99	32°9'57.253736" N	103°39'16.475175" W
	15,200.00	91.49	359.62	14,847.60	11,310.60	1,685.34	1,686.34	136.97	10.00	425,969.31	710,025.69	32°9'57.313710" N	103°39'16.475332" W
	15,300.00	91.49	359.62	14,937.00	11,400.00	1,732.89	1,733.89	136.68	10.00	426,014.86	710,025.39	32°9'57.373684" N	103°39'16.475489" W
	15,400.00	91.49	359.62	15,026.40	11,489.40	1,780.44	1,781.44	136.39	10.00	426,060.41	710,025.09	32°9'57.433658" N	103°39'16.475646" W
	15,500.00	91.49	359.62	15,115.80	11,578.80	1,827.99	1,828.99	136.10	10.00	426,105.96	710,024.79	32°9'57.493632" N	103°39'16.475803" W
	15,600.00	91.49	359.62	15,205.20	11,668.20	1,875.54	1,876.54	135.81	10.00	426,151.51	710,024.49	32°9'57.553606" N	103°39'16.475960" W
	15,700.00	91.49	359.62	15,294.60	11,757.60	1,923.09	1,924.09	135.52	10.00	426,197.06	710,024.19	32°9'57.613580" N	103°39'16.4

Comments	MD (ft)	Incl (°)	Azim (°)	TVD (ft)	TVDSS (ft)	VSEC (ft)	NS (ft)	EW (ft)	DLS (°/100ft)	Northing (ftUS)	Easting (ftUS)	Latitude (°''')	Longitude (°''')
CO 34 27 Federal Com No. 637H BHL	23,192.77	90.00	359.67	12,350.00	8,813.00	11,207.52	11,208.22	78.98	0.00	435,552.82	709,968.02	32°11'44.268194"N	103°39'16.442431"W

Survey Type: Def Plan

Survey Error Model: WPTS Rev 0.

Description	Part	MD From (ft)	MD To (ft)	EOU Freq (ft)	Hole Size (in)	Casing Diameter (in)	Expected Max Inclination (deg)	Survey Tool Code	Vendor / Tool	Borehole / Survey
	1	0.000	23,199.421	1/100,000.25 - 8.75 - 6.125	3.625 - 7 - 6.125			B001Mb_MWD+HRGM		CO 34 27 Federal Com No. 637H / CO 34 27 Federal (

EOU Geometry:

End MD (ft)	Hole Size (in)	Casing Size (in)	Name
914.355	17.500	13.375	
4,391.061	12.250	9.625	
9,167.061	8.750	7.000	
23,192.767	6.125		



ACREAGE DEDICATION PLATS

This grid represents a standard section. You may superimpose a non-standard section, or larger area, over this grid. Operators must outline the dedicated acreage in a red box, clearly show the well surface location and bottom hole location, if it is directionally drilled, with the dimensions from the section lines in the cardinal directions. If this is a horizontal wellbore show on this plat the location of the First Take Point and Last Take Point, and the point within the Completed interval (other than the First Take Point or Last Take Point) that is closest to any outer boundary of the tract.

Surveyors shall use the latest United States government survey or dependent resurvey. Well locations will be in reference to the New Mexico Principal Meridian. If the land is not surveyed, contact the OCD Engineering Bureau. Independent subdivision surveys will not be acceptable.

(NAD 27 NM E)

<b>CO 34 27 FEDERAL COM NO. 637H WELL</b>	<b>PROPOSED KICK OFF POINT</b>	<b>PROPOSED FIRST TAKE POINT</b>
X=709,889.04	X=709,954.22	X=710,031.68
Y=424,345.08	Y=424,448.55	Y=425,046.34
LAT.32.164823°N	LAT.32.165107°N	LAT.32.166749°N
LONG.103.655051°W	LONG.103.654838°W	LONG.103.654576°W

<b>PROPOSED MID POINT</b>	<b>PPP</b>	<b>PROPOSED LAST TAKE POINT</b>
X=709,996.49	X=709,983.05	X=709,968.45
Y=430,310.00	Y=432,939.29	Y=435,477.82
LAT.32.181218°N	LAT.32.188446°N	LAT.32.195424°N
LONG.103.654582°W	LONG.103.654572°W	LONG.103.654567°W

**PROPOSED BOTTOM HOLE LOCATION**

X=709,968.02  
Y=435,552.82  
LAT.32.195630°N  
LONG.103.654567°W

(NAD 83/2011 NM E)

<b>CO 34 27 FEDERAL COM NO. 637H WELL</b>	<b>PROPOSED KICK OFF POINT</b>	<b>PROPOSED FIRST TAKE POINT</b>
X=751,074.14	X=751,139.32	X=751,216.75
Y=424,403.23	Y=424,506.70	Y=425,104.50
LAT.32.164947°N	LAT.32.165230°N	LAT.32.166872°N
LONG.103.655528°W	LONG.103.655315°W	LONG.103.655053°W

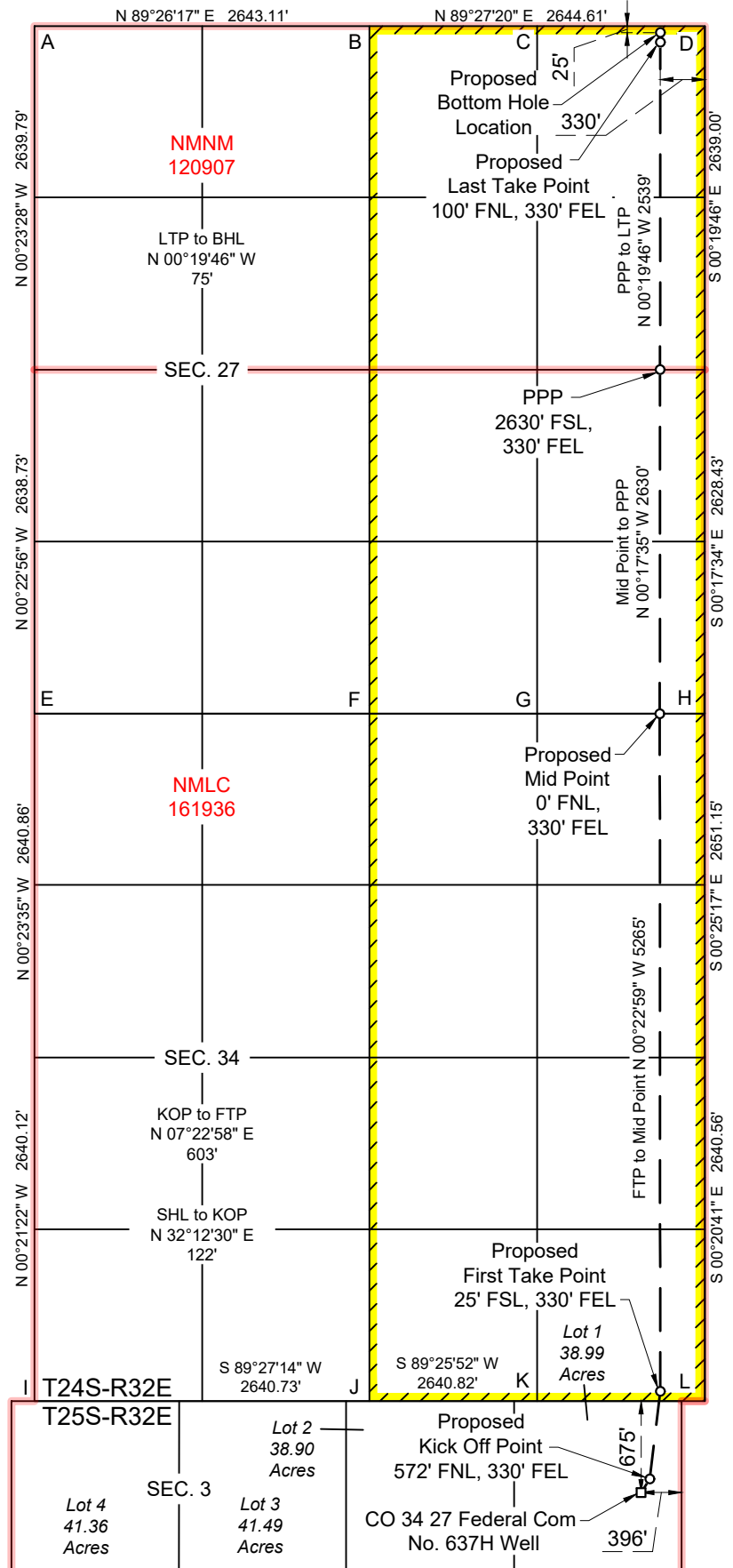
<b>PROPOSED MID POINT</b>	<b>PPP</b>	<b>PROPOSED LAST TAKE POINT</b>
X=751,181.34	X=751,167.78	X=751,153.06
Y=430,368.28	Y=432,997.62	Y=435,536.21
LAT.32.181342°N	LAT.32.188569°N	LAT.32.195547°N
LONG.103.655060°W	LONG.103.655050°W	LONG.103.655046°W

**PROPOSED BOTTOM HOLE LOCATION**

X=751,152.63  
Y=435,611.21  
LAT.32.195753°N  
LONG.103.655046°W

**CORNER COORDINATES**  
(NAD 27 NM E)

- A - X=705011.42, Y=435529.91 IP w/ CAP "1916"
- B - X=707653.89, Y=435555.83 IP w/ CAP "1916"
- C - X=708975.87, Y=435568.39
- D - X=710297.86, Y=435580.96 IP w/ CAP "1916"
- E - X=705047.04, Y=430252.55 IP w/ CAP "1913"
- F - X=707687.69, Y=430277.54 IP w/ CAP "1916"
- G - X=709007.07, Y=430296.09
- H - X=710326.46, Y=430314.64 IP w/ CAP "1916"
- I - X=705081.56, Y=424972.71 IP w/ CAP "1916"
- J - X=707721.70, Y=424998.40 IP w/ CAP "1916"
- K - X=709041.74, Y=425011.23
- L - X=710361.83, Y=425024.09 IP w/ CAP "1916"





ACREAGE DEDICATION PLATS

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Surveyors shall use the latest United States government survey or dependent resurvey. Well locations will be in reference to the New Mexico Principal Meridian. If the land is not surveyed, contact the OCD Engineering Bureau. Independent subdivision surveys will not be acceptable.

(NAD 27 NM E)

<b>CO 34 27 FEDERAL COM NO. 637H WELL</b>	<b>PROPOSED KICK OFF POINT</b>	<b>PROPOSED FIRST TAKE POINT</b>
X=709,869.04	X=709,954.22	X=710,031.68
Y=424,345.08	Y=424,448.55	Y=425,046.34
LAT.32.164824°N	LAT.32.165107°N	LAT.32.166749°N
LONG.103.655116°W	LONG.103.654838°W	LONG.103.654576°W

<b>PROPOSED MID POINT</b>	<b>PPP</b>	<b>PROPOSED LAST TAKE POINT</b>
X=709,996.49	X=709,983.05	X=709,968.45
Y=430,310.00	Y=432,939.29	Y=435,477.82
LAT.32.181218°N	LAT.32.188446°N	LAT.32.195424°N
LONG.103.654582°W	LONG.103.654572°W	LONG.103.654567°W

**PROPOSED BOTTOM HOLE LOCATION**

X=709,968.02  
Y=435,552.82  
LAT.32.195630°N  
LONG.103.654567°W

(NAD 83/2011 NM E)

<b>CO 34 27 FEDERAL COM NO. 637H WELL</b>	<b>PROPOSED KICK OFF POINT</b>	<b>PROPOSED FIRST TAKE POINT</b>
X=751,054.14	X=751,139.32	X=751,216.75
Y=424,403.23	Y=424,506.70	Y=425,104.50
LAT.32.164947°N	LAT.32.165230°N	LAT.32.166872°N
LONG.103.655593°W	LONG.103.655315°W	LONG.103.655053°W

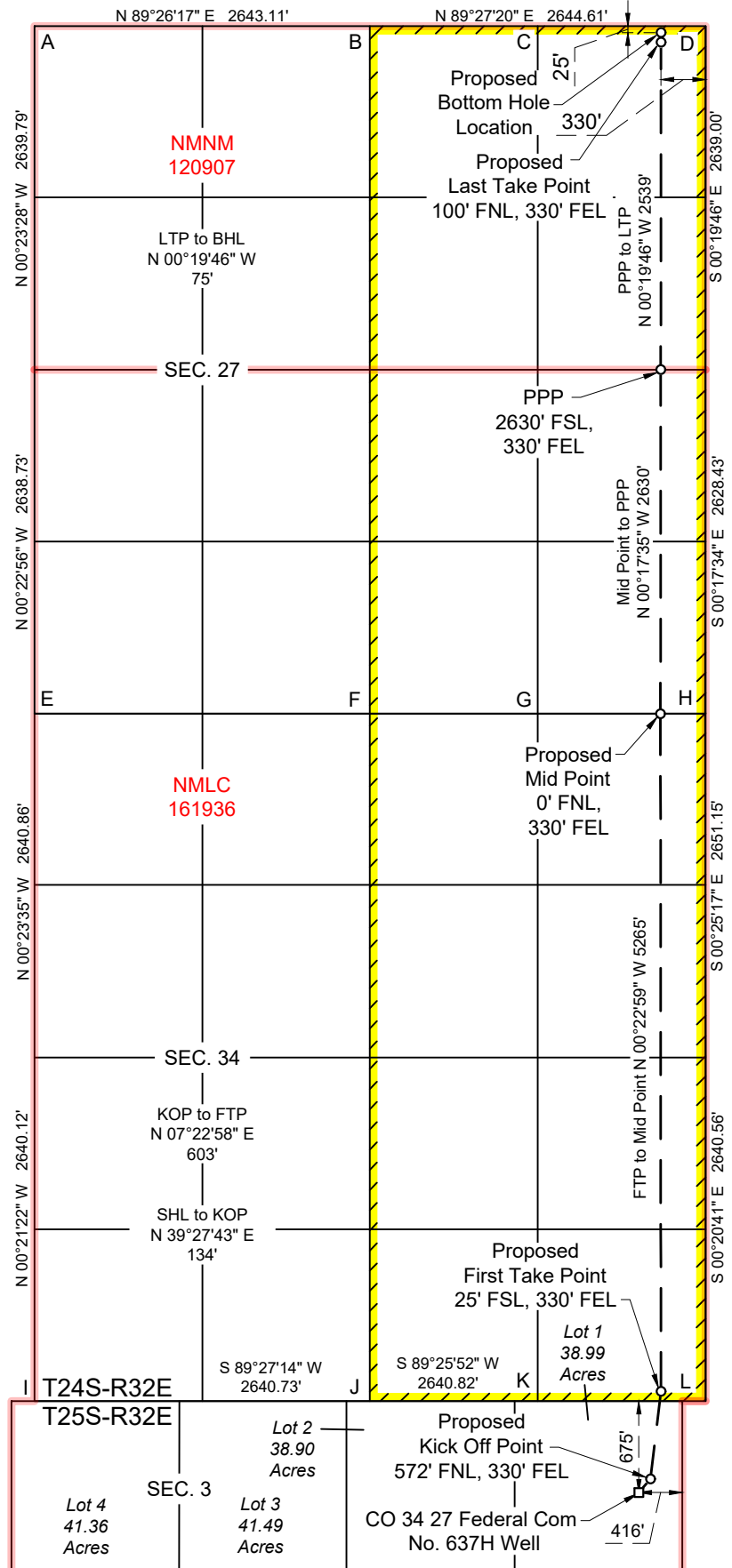
<b>PROPOSED MID POINT</b>	<b>PPP</b>	<b>PROPOSED LAST TAKE POINT</b>
X=751,181.34	X=751,167.78	X=751,153.06
Y=430,368.28	Y=432,997.62	Y=435,536.21
LAT.32.181342°N	LAT.32.188569°N	LAT.32.195547°N
LONG.103.655060°W	LONG.103.655050°W	LONG.103.655046°W

**PROPOSED BOTTOM HOLE LOCATION**

X=751,152.63  
Y=435,611.21  
LAT.32.195753°N  
LONG.103.655046°W

**CORNER COORDINATES**  
(NAD 27 NM E)

- A - X=705011.42, Y=435529.91 IP w/ CAP "1916"
- B - X=707653.89, Y=435555.83 IP w/ CAP "1916"
- C - X=708975.87, Y=435568.39
- D - X=710297.86, Y=435580.96 IP w/ CAP "1916"
- E - X=705047.04, Y=430252.55 IP w/ CAP "1913"
- F - X=707687.69, Y=430277.54 IP w/ CAP "1916"
- G - X=709007.07, Y=430296.09
- H - X=710326.46, Y=430314.64 IP w/ CAP "1916"
- I - X=705081.56, Y=424972.71 IP w/ CAP "1916"
- J - X=707721.66, Y=424997.87 IP w/ CAP "1916"
- K - X=709041.74, Y=425011.23
- L - X=710361.83, Y=425024.09 IP w/ CAP "1916"



Sante Fe Main Office  
Phone: (505) 476-3441

General Information  
Phone: (505) 629-6116

Online Phone Directory  
<https://www.emnrd.nm.gov/ocd/contact-us>

**State of New Mexico**  
**Energy, Minerals and Natural Resources**  
**Oil Conservation Division**  
**1220 S. St Francis Dr.**  
**Santa Fe, NM 87505**

CONDITIONS

Action 560193

**CONDITIONS**

Operator: CHEVRON U S A INC 6301 Deauville Blvd Midland, TX 79706	OGRID: 4323
	Action Number: 560193
	Action Type: [C-103] NOI Change of Plans (C-103A)

**CONDITIONS**

Created By	Condition	Condition Date
matthew.gomez	Notify the OCD 24 hours prior to casing & cement.	3/26/2026
matthew.gomez	If cement does not circulate to surface on any string, a Cement Bond Log (CBL) is required for that string of casing. If strata isolation is not achieved, remediation will be required before further operations may commence.	3/26/2026
matthew.gomez	All conducted logs must be submitted to the OCD.	3/26/2026
matthew.gomez	Cement must be in place for at least eight hours AND achieve a minimum compressive strength of 500 PSI before performing any further operations on the well.	3/26/2026
matthew.gomez	Administrative order required for non-standard location prior to production.	3/26/2026
matthew.gomez	No additives containing PFAS chemicals will be added to the drilling fluids or completion fluids used during drilling, completions, or recompletions operations.	3/26/2026
matthew.gomez	All previous COA's still apply.	3/26/2026