Initial

Application Part I

Received 10/23/21

This application is placed in file for record. It MAY or MAY NOT have been reviewed to be determined Administratively Complete

| ENER | E OF NEW MEXICO GY, MINERALS AND NATURAL URCES DEPARTMENT | Oil Conservation Division 1220 South St. Francis Dr. Santa Fe, New Mexico 87505 | FORM C-108 Revised June 10, 2003 |
|---------------|---|--|---|
| | APPLIC | CATION FOR AUTHORIZATION 1 | TO INJECT |
| [. | PURPOSE:Secondary Storage Application qualifies for administrative | Recovery Pressure Ma | |
| II. Techne | OPERATOR: _ N e w Mexico Institute ology | of Mining & | |
| | ADDRESS: 801 Leroy PL Socorro, | NM 87801 | |
| | CONTACT PARTY: Cleve McDanie | l, PhD | _PHONE:1-575-835-5018 |
| 111. | WELL DATA: Complete the data require Additional sheets may be | | each well proposed for injection. |
| | Is this an expansion of an existing project If yes, give the Division order number a | ct? Yes X uthorizing the project: | No |
| V. | Attach a map that identifies all wells and drawn around each proposed injection w | | ed injection well with a one-half mile radius circle ea ofreview. |
| VI. | | each well's type, construction, date drill | w which penetrate the proposed injection zone. ed, location, depth, record of completion, and a |
| VII. | Whether the system is open or closs Proposed average and maximum in Sources and an appropriate analysis produced water; and, If injection is for disposal purposes | aily rate and volume of fluids to be injected; ajjection pressure; s of injection fluid and compatibility wi | st or within one mile of the proposed well, attach a or inferred from existing literature, studies, nearby |
| *VIII. | depth. Give the geologic name, and dep | oth to bottom of all underground sources 10,000 mg/I or less) overlying the prop | thologic detail, geologic name, thickness, and s of drinking water (aquifers containing waters with osed injection zone as well as any such sources |
| IX. | Describe the proposed stimulation progr | ram, if any. | |
| *X. resubr | Attach appropriate logging and test data nitted). | a on the well. (If well logs have been fi | iled with the Division, they need not be |
| *XI. | Attach a chemical analysis of fresh wate injection or disposal well showing location | | f available and producing) within one mile of any en. |
| XII. | | | we examined available geologic and engineering etween the disposal zone and any underground |
| XIII. | Applicants must complete the "Proof of | fNotice" section on the reverse side of t | his form. |
| XIV. | Certification: I hereby certify that the i and belief. | nformation submitted with this applicat | ion is true and correct to the best of my knowledge -5 |
| | E: = PhD TURE: •; A2 1,5F6A BA BA D2 7.4 4 J tL | TITLE: Vice President for Adminis | stration and F i n a n c e 10/13/2021 |

* If the information required under Sections VI, VIII, X, and XI above has been previously submitted, it need not be resubmitted. Please show the date and circumstances of the earlier submittal:

DISTRIBUTION: Original and one copy to Santa Fe with one copy to the appropriate District Office

Side 2

III. WELL DATA

- The following well data must be submitted for each injection well covered by this application. The data must be both in tabular A. and schematic form and shall include:
 - (1) Lease name; Well No.; Location by Section, Township and Range; and footage location within the section.
 - (2) Each casing string used with its size, setting depth, sacks of cement used, hole size, top of cement, and how such top was determined.
 - (3) A description of the tubing to be used including its size, lining material, and setting depth.
 - (4) The name, model, and setting depth of the packer used or a description of any other seal system or assembly used.

Division District Offices have supplies of Well Data Sheets which may be used or which may be used as models for this purpose. Applicants for several identical wells may submit a "typical data sheet" rather than submitting the data for each well.

- Β. The following must be submitted for each injection well covered by this application. All items must be addressed for the initial well. Responses for additional wells need be shown only when different. Information shown on schematics need not be repeated.
 - (1) The name of the injection formation and, if applicable, the field or pool name.
 - (2) The injection interval and whether it is perforated or open-hole.
 - (3) State if the well was drilled for injection or, if not, the original purpose of the well.
 - (4) Give the depths of any other perforated intervals and detail on the sacks of cement or bridge plugs used to seal off such perforations.
 - (5) Give the depth to and the name of the next higher and next lower oil or gas zone in the area of the well, if any.
- XIV. PROOF OF NOTICE

All applicants must furnish proof that a copy of the application has been furnished, by certified or registered mail, to the owner of the surface of the land on which the well is to be located and to each leasehold operator within one-half mile of the well location.

Where an application is subject to administrative approval, a proof of publication must be submitted. Such proof shall consist of a copy of the legal advertisement which was published in the county in which the well is located. The contents of such advertisement must include:

- (1) The name, address, phone number, and contact party for the applicant;
- (2) The intended purpose of the injection well; with the exact location of single wells or the Section, Township, and Range location of multiple wells;
- (3) The formation name and depth with expected maximum injection rates and pressures; and,

(4) A notation that interested parties must file objections or requests for hearing with the Oil Conservation Division, 1220 South St. Francis Dr., Santa Fe, New Mexico 87505, within 15 days.

NO ACTION WILL BE TAKEN ON THE APPLICATION UNTIL PROPER PROOF OF NOTICE HAS BEEN SUBMITTED.

NOTICE: Surface owners or offset operators must file any objections or requests for hearing of administrative applications within 15 days from the date this application was mailed to them. Side 1

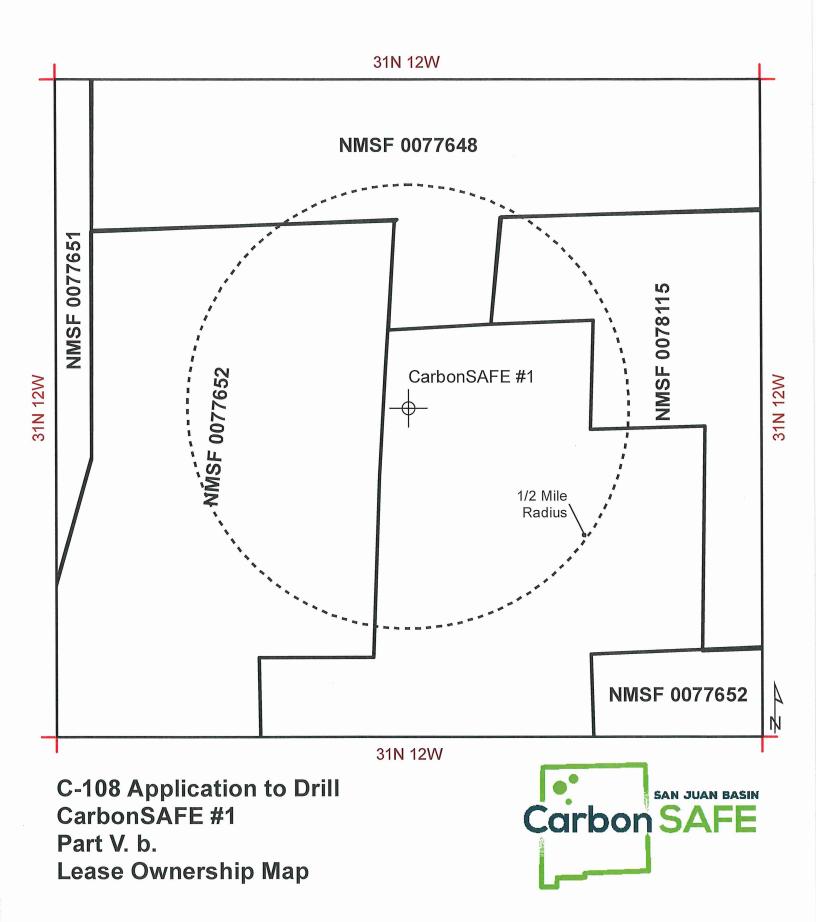
INJECTION WELL

| cuSign Envelope ID: 23594B2A-B20B-4C83-AF2E-C8E9E923B391 | | |
|---|-----------------|--------------------|
| OPERATOR: New Mexico Institute of Mining & Technology | | _ |
| WELL NAME & NUMBER:SJB_CarbonSafe #001 | | |
| WELL LOCATION:2236 FNL 1021 FELH14 FOOTAGE LOCATION SECTION TOWNSHIP RANGE | 31NU | 12W JNIT LETTER |
| <u>WELLBORE SCHEMATIC</u> <u>WELLBORE SCHEMATIC</u> <u>CONSTRUCTION DATA</u> | | <u>WELL</u> |
| Surface Casing | | |
| Hole Size:17 1/2" | Casing Size: | _13 3/8" |
| Cemented with:1216 Type III _ SX. | or | ft ³ |
| Top of Cement:1500' | Method Determin | ned: |
| Intermediate Casing | | |
| Hole Size:12 1/4" | Casing Size: 9 | 5/8" |
| Cemented with:544_Type III sx. | 01* | ft ³ |
| Top of Cement:5500' | Method Determin | ned: |
| Production Casing | | |
| Hole Size:8 ³ / ₄ " | Casing Size:5 | /2" |
| Cemented with:864sx. | 01' | ft ³ |
| Top of Cement:Surface | Method Determin | ned: |
| Total Depth:8800' | | |
| Injection Interval | | |
| feet | to | |
| (Perforated or Open Hole; indicate which) | | |

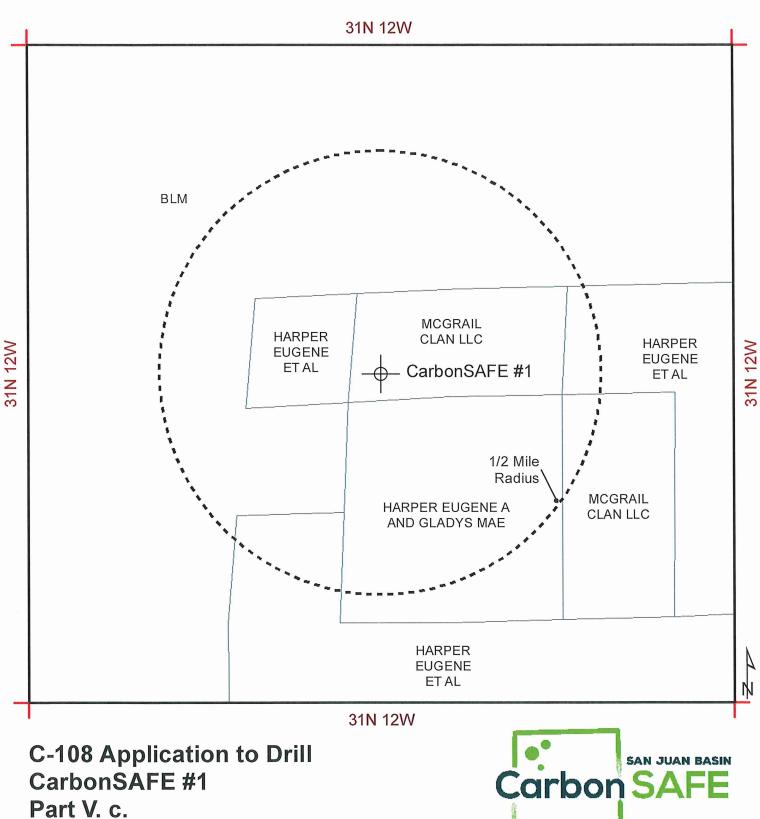
INJECTION WELL DATA SHEET

| Tubing Size:2 | 7/8"Lining Material: |
|---------------|--|
| 3,600psi | Type of Packer: Retrievable Packer Elastomer seal or metal seal max load 45,000lbf max pressure |
| | Packer Setting Depth: _8,150' |
| | Other Type of Tubing/Casing Seal (if applicable): |
| | Additional Data |
| No | 1. Is this a new well drilled for injection? XYes |
| | If no, for what purpose was the well originally drilled? |
| | · · · · · · · · · · · · · · · · · · · |
| | 2. Name of the Injection Formation: |
| | 3. Name of Field or Pool (if applicable): |
| | Has the well ever been perforated in any other zone(s)? List all such perforated intervals and give plugging detail, i.e. sacks of cement or plug(s) used. |
| | 5. Give the name and depths of any oil or gas zones underlying or overlying the |
| proposed | 5. Give the name and depths of any oil or gas zones underlying or overlying the injection zone in this area: |
| | · |
| | |
| | |
| | |

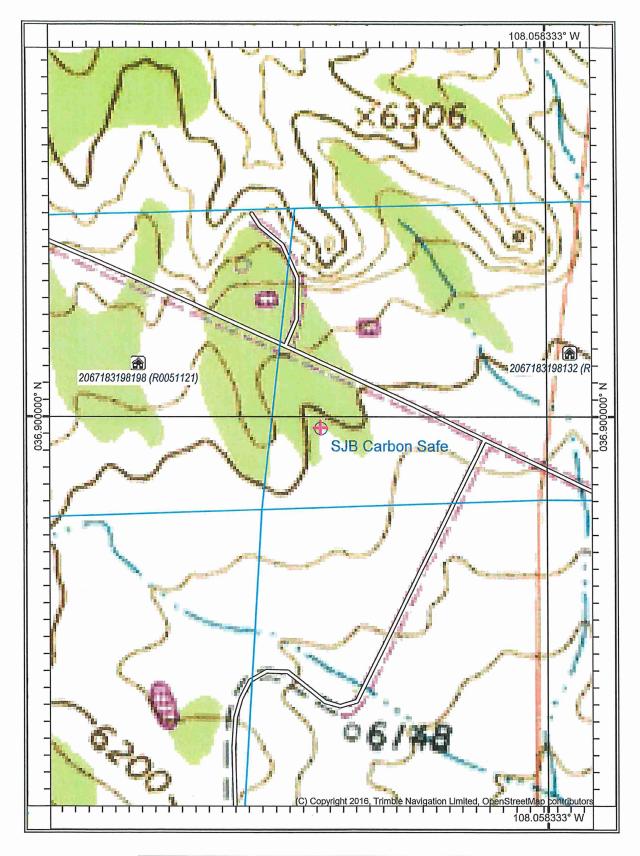
Township 31 North, Range 12 West San Juan County, NM

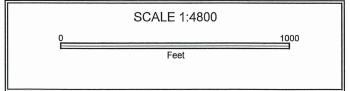


Township 31 North, Range 12 West San Juan County, NM



Surface Ownership Map





Affirmative Statement of Examination of Geologic Data

Based on the available geologic data we find no evidence of open faults and/or any other hydrologic connection between the target injection zone for the SJB CarbonSafe #001 and any underground sources of drinking water.

Name: Dana Ulmer - Scholle Title: Asst. Research Scuntost

Signature: Aun S. Meme-Glade Date: 10/12/2021

Affirmative Statement of Examination of Geologic Data

Based on the available geologic data we find no evidence of open faults and/or any other hydrologic connection between the target injection zone for the SJB CarbonSafe #001 and any underground sources of drinking water.

Name: William Ampomah Signature:

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Title: Ashistant Rofesson, NHUT

Date: 10/12/2021

SJB CarbonSafe #001 Well Description

The SJB CarbonSAFE #001 will be drilled as a stratigraphic test well in the area of interest to an approximate depth of 8,800'. The principal zones of interest for characterization are the Morrison and Entrada formation. Data to be gathered from the wellbore will include open-hole and cased hole logs, continuous core samples from the target reservoir intervals and seals, fluid samples from sandstone formations and known USDW's. The long-term injection test will be performed in the Entrada formation. All the data and analysis collected from this stratigraphic test well will assist on Class VI well permit application through the EPA UIC program.

Geological Review

The Nacimiento Formation forms a broad outcrop belt in the region surrounding the proposed drill site (NMBGMR Geologic Map, 2003). These Paleocene strata are nonresistant, forming low relief, rounded hills typical of badland topography. The Nacimiento, San Jose and Ojo Alamo formations make up the surficial deposits within the San Juan Basin (Fassett, 1985). The Nacimiento Formation conformably overlies the Paleocene Ojo Alamo Sandstone and is conformably overlain by the Eocene San Jose Formation (Fassett, 1974, 1985). The Nacimiento Formation grades into Animas Formation in the northeastern-most part of the San Juan Basin in New Mexico and Colorado (Fassett, 1995; Fassett and Hinds, 1971).

The Nacimiento Formation was deposited during the initial stages of down warping of the San Juan Basin (Fassett, 1985). The terrestrial, low-energy Nacimiento Formation includes braided stream, lacustrine, flood plain deposited sediments (Brimhall, 1973; Fassett, 1985). The Nacimiento Formation is dominated by mudstones and siltstones with unconsolidated sandstone channels (Brimhall, 1973; Stone et al., 1983). The Nacimiento Formation is usually very difficult to identify on well logs, because of the variety of facies present in the unit (Brimhall, 1973). The thickness of unit ranges from 500 to 1300 feet with the thickest sections in the center of the basin (Steven et al., 1974).

Groundwater is associated with the braided-stream-deposited sandstones and is therefore controlled by the distribution of these facies within the subsurface. These deposits appear to behave hydrologically like San Jose aquifers. There are no known aquifer tests for the Nacimiento Formation (Stone, 1983), but specific capacities have been reported for six wells that range from 0.24 to 2.30 gallons per minute per foot of drawdown (Levings et al., 1990). The Nacimiento does provide water for domestic and stock use and is recharged by precipitation.

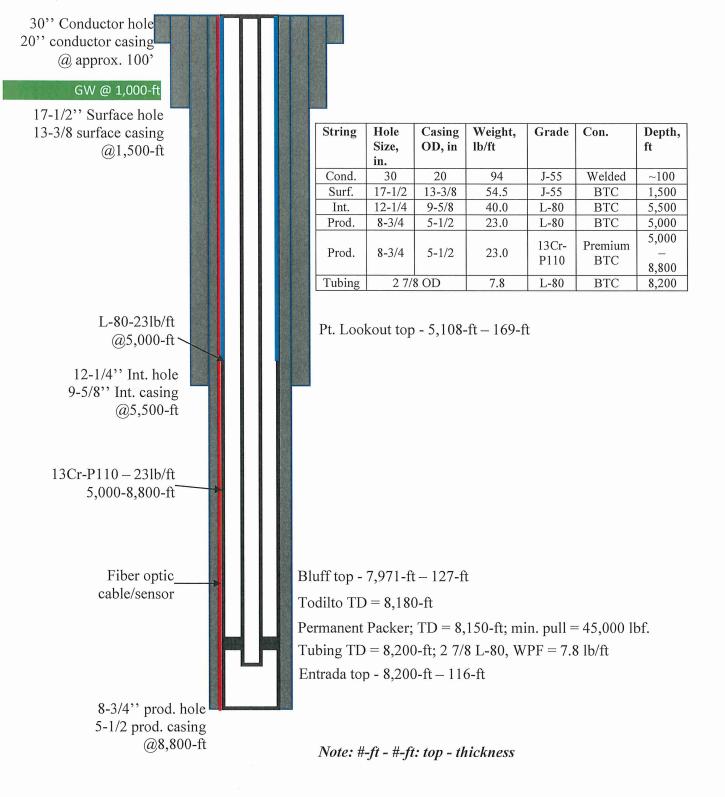
References

- Brimhall, R.M., 1973, Ground-water hydrology of Tertiary rocks of the San Juan Basin, New Mexico, in Fassett, J.E., ed., Cretaceous and Tertiary rocks of the Southern Colorado Plateau: Four Corners Geological Society Memoir, p. 197-207.
- Fassett, J. E., 1985, Early Tertiary paleogeography and paleotectonics of the San Juan Basin Area, New Mexico and Colorado, *in* R. M. Flores, and S. S. Kaplan, eds., Cenozoic Paleogeography of West-Central United States: Denver, Rocky Mountain Section, SEPM, p. 317-334.
- Fassett, J.E., 1974, Cretaceous and Tertiary rocks of the eastern San Juan Basin, New Mexico and Colorado, in Guidebook of Ghost Ranch, central-northern New Mexico: New Mexico Geological Society, 25th Field Conference, p. 225-230.
- Fassett, J.E., and Hinds, J.S., 1971, Geology and fuel resources of the Fruitland Formation and Kirtland Shale of the San Juan Basin, New Mexico and Colorado: USGS Professional Paper 676, 76 p.
- Levings, G.W., Craigg, S.D., Dam, W.L., Kernodle, J.M., and Thorn, C.R., 1990, Hydrogeology of the San Jose, Nacimiento, and Animas Formations in the San Juan structural basin, New Mexico, Colorado, Arizona, and Utah: USGS Hydrologic Investigations Atlas HA-720-A, 2 sheets.
- Stone, W.J., Lyford, F.P., Frenzel, P.F., Mizell, N.H., and Padgett, E.T., 1983, Hydrogeology and water resources of San Juan Basin, New Mexico: New Mexico Bureau of Mines and Mineral Resources, Hydrologic Report 6.

DISTRICT I State of New Mexico Energy, Minerals & Natural Resources Department Form C-102 1625 N. French Dr., Hobbs, N.M. 88240 Revised August 1, 2011 Phone: (575) 393-6161 Fax: (575) 393-0720 Submit one copy to appropriate DISTRICT II 811 S. First St., Artesia, N.M. 88210 Phone: (575) 748-1283 Fax: (575) 748-9720 OIL CONSERVATION DIVISION District Office 1220 South St. Francis Dr. DISTRICT III Santa Fe, NM 87505 1000 Rio Brazos Rd., Aztec, N.M. 87410 Phone: (505) 334-6178 Fax: (505) 334-6170 DISTRICT IV □ AMENDED REPORT 1220 S. St. Francis Dr., Santa Fe, NM 87505 Phone: (505) 476-3460 Fax: (505) 476-3462 WELL LOCATION AND ACREAGE DEDICATION PLAT ¹API Number ⁸ Pool Code ⁸Pool Name ⁶ Well Number ⁴Property Code ⁵Property Name SJB CARBON SAFE 1 "OGRID No. ⁸Operator Name ⁹ Elevation NEW MEXICO INSTITUTE OF MINING & TECHNOLOGY 6207' 15847 ¹⁰ Surface Location UL or lot no. Feet from the North/South line Section Township Range Lot Idn Feet from the East/West line County Н 14 31-N 12-W 2236 NORTH 1021 EAST SAN JUAN ¹¹ Bottom Hole Location If Different From Surface UL or lot no. Section Township Lot Idn Feet from the North/South line Feet from the East/West line Range County ¹⁸ Dedicated Acres ¹⁸ Joint or Infill ¹⁴ Consolidation Code 15 Order No. NO ALLOWABLE WILL BE ASSIGNED TO THIS COMPLETION UNTIL ALL INTERESTS HAVE BEEN CONSOLIDATED OR A NON-STANDARD UNIT HAS BEEN APPROVED BY THE DIVISION 16 2461.02' S88'54'11"W 17 OPERATOR CERTIFICATION FND BLM "1951" BC I hereby certify that the information contained herein FND BLM "1951" BC is true and complete to the best of my knowledge and is true and complete to the cest of my knowledge and bellef, and that this organization either owns a working interest or unleased mineral interest in the land including the proposed bottom hole location or has a right to drill this well at this location pursuant 2584.68' 1 3 2 4 to a contract with an owner of such a mineral or a working interest, or to a voluntary pooling agreement or a compulsory pooling order heretofore entered by the division. SJB CARBON SAFE #1 45,07" 2236' FNL 1021' FEL LAT. 36.899871° N Signature Date S06" 5 LONG. 108.061716° W 6 NAD83 Printed Name 1021' E-mail Address FND BLM SURVEYOR CERTIFICATION 18 I hereby certify that the well location shown on this plat was plotted from field notes of actual surveys made by 7 8 9 me or under my supervision, and that the same is true and correct to the best of my belief. W. RUSS JULY 12, 2021 - Hung Signature and Sealest Professional Surveyor Date of Survey m /OR ICEN 15703 ENSED 10 11 PROFESSIONA GLEN W. RUSSEL Certificate Number 15703

Well Name: SJB CarbonSAFE #1 Objective formation: Entrada County, State: San Juan County, NM Surface Legal Location: 12-31N-12W Surface Lease Line Footage: TBD API #: TBD

Rig: TBD Ground Elevation: 6,207-ft RBK Elevation: 6,237-ft TD: 8,800-ft MD: 8,800-ft Useable-quality GW: ~1,000-ft



New Mexico Institute of Mining and Technology CarbonSAFE Project

Strat Well Injection Design Report

1. Lithology - Pore and Fracture Pressure

The pore and fracture pressure of the interested area are provided by Tom Bratton and shown in Fig. 1.

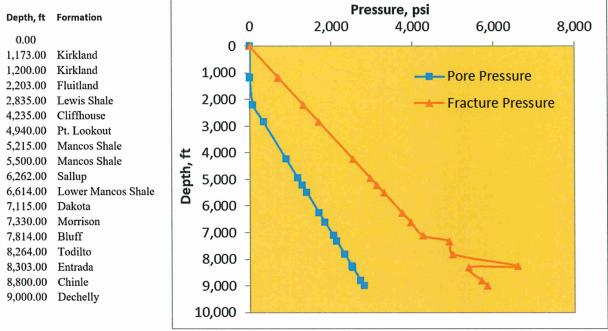


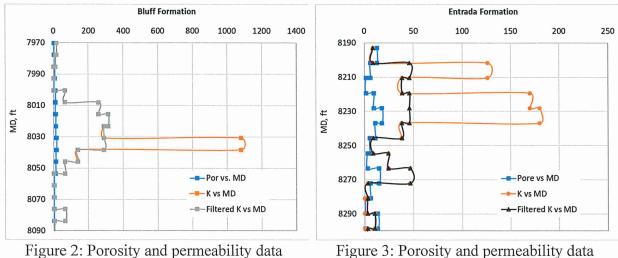
Figure 1: Pore and fracture pressure

2. Porosity and Permeability Data

The porosity and permeability data were given by Luke Martin for different formations. Due to the fact that the Bluff and Entrada formations are the two promising injection zones, this analysis will focus only on these two formations.

The porosity and permeability data for the Bluff and Entrada formation are plotted and shown in Fig. 2 and Fig. 3, respectively. Note that Fig. 2 and Fig. 3 show the original permeability and filtered permeability. We believed that the permeability values of the Bluff formation with the magnitude of more than 1000 mD are the outliers and hence we treated these values as the same values as the permeability of the formation right above it. Similarly, the permeability values of the Entrada formation with the magnitude of more than 100 mD are considered as outliers. We treated these values as the same values as the same values as the permeability of the formation swere then calculated. In addition, we considered the

maximum and minimum permeability values of these two formations for all of the simulations. The results are shown in Table 1.



of the Bluff formation

Figure 3: Porosity and permeability data of the Entrada formation

| Table 1: Maximum, minimum, and average permeability values of the Bluff and Entrada | Table 1: Maximum, | minimum, | and average | permeability values | of the | Bluff and Entrada |
|---|-------------------|----------|-------------|---------------------|--------|-------------------|
|---|-------------------|----------|-------------|---------------------|--------|-------------------|

| Formation type | Bottom MD, ft | Permeability, mD | | | | | |
|----------------|---------------|------------------|---------|---------|--|--|--|
| ronnation type | Bottom MD, It | Maximum | Average | Minimum | | | |
| Bluff | 8,094 | 288 | 95 | 0.39 | | | |
| Entrada | 8,380 | 46 | 25 | 3 | | | |

3. Injection Pressure Design

The surface injection pressure is calculated as follows

$$P_{inf} = BHP - P_h + \Delta P_f$$

Where P_{inj} is the surface injection pressure in psi; BHP is the bottomhole pressure in psi, and the ΔP_f is the frictional pressure losses in the production tubing in psi,

The BHP is calculated using the flowing equation in the reservoir with the following assumptions: 1-D radial flow, pseudo-steady state flow, and incompressible fluids.

The inputs for the simulations are presented in Table 2.

Table 2: Simulation input

| 1 | | |
|--|------------------------------------|------------------------|
| Production Casing ID (5 ¹ / ₂ OD) | 4.670 | in |
| Production tubing ID (2 7/8 OD) | 2.440 | in |
| Reservoir area | 125 | acre |
| Reservoir radius | 1316 | ft |
| Bo | 1.200 | bbl/STB |
| Bluff formation Thickness of Bluff | 1453.680 | in |
| Bluff formation Permeability | 0.393 | mD |
| Skin factor | 0.0 | |
| Fluid viscosity | 1.0 | cp |
| Fluid density | 8.5 | ppg |
| Liquid injection rate | 6000 | BPD |
| Safety factor | 500 | psi |
| Bluff formation Permeability Skin factor Fluid viscosity Fluid density Liquid injection rate | 0.393 0.0 1.0 8.5 6000 | mD cp ppg BPD |

Using the maximum, average, and minimum permeability values for the Bluff and Entrada formations as shown in Table 1, the estimated BHP and the surface injection pressure for the Bluff and Entrada are shown in Table 3.

Table 3: BHP and injection pressure prediction

| | | | | | Maximu ermeabi | | 8 | | Minimur Permeabil | The second s | | |
|---------|-------|-------|-------|-----|-------------------|--------|----|-------|----------------------|--|---------|---------|
| | MD, | Pore, | Frac, | К, | BHP, | P_inj, | К, | BHP, | P_inj, | К, | BHP, | P_inj, |
| | ft | psi | psi | mD | psi | psi | mD | psi | psi | mD | psi | psi |
| Bluff | 8,094 | 2,325 | 5,000 | 289 | 2,560 | 51 | 95 | 3,035 | 526 | 0.39 | 174,472 | 171,963 |
| Entrada | 8,380 | 2,521 | 5,396 | 46 | 4,079 | 1,463 | 24 | 5,415 | 2,800 | 3.00 | 26,408 | 23,793 |

If the average permeability values (Bluff K = 95 mD and the Entrada K = 24 mD) are used, the estimated BHP are predicted as 3,035 psi and 5,415 psi for the Bluff and for the Entrada, respectively. Note that the BHP at the Entrada is 5,415 psi which is a little bit higher than the formation fracture pressure. Therefore, one can conclude that the liquid injection rate of 6,000 BPD is the upper limit. Above this rate, the formation will be fracture.

If the minimum permeability values are used, the BHP and the injection pressure are unrealistic. With the liquid rate of 6,000 BPD, the permeability of the Bluff and Entrada must be 26 mD and 30 mD or higher, respectively, to ensure the BHP less than the fracture pressure and to avoid the formation fracturing.

To be more practical, the minimum permeability simulations will not be discussed further in this report. The estimated BHP and injection pressure for the Bluff and Entrada for the two cases: maximum permeability and average permeability are shown in Fig. 4. One can easily recognize that the Bluff formation is much better quality for injection in comparison to the Entrada formation. At the injection rate of 6,000 BPD, the BHP and the injection pressure when Bluff (average K = 95 mD) is the injection formation are 3,035 psi and 525 psi, respectively. At the same rate, the

BHP and the injection pressure when Entrada (average K = 24 mD) is the injection formation are 5,415 psi and 2,800 psi, respectively.

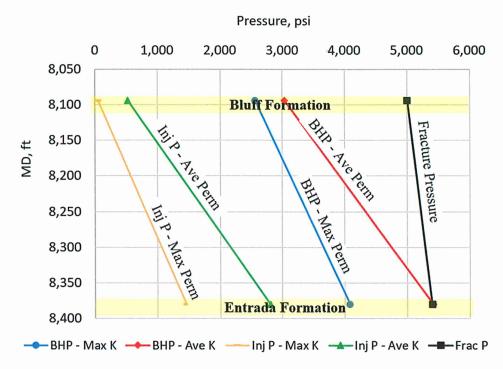


Figure 4: BHP and injection pressure for the maximum and average permeability cases

4. Summary

- Bluff is the much better candidate to be used as an injection formation compared to the Entrada.
- If the average permeability of the Bluff (K = 95 mD) is used, the maximum liquid rate can be injected is 17,500 BPD. This rate will create a BHP of 4,396 psi which is less than the formation fracture pressure and the surface injection pressure of about 5,000 psi which is the pressure rating for most of the surface equipment.
- If the average permeability of the Entrada (K = 24 mD) is used, the maximum liquid rate can be injected is about 6,000 BPD. This rate will create a BHP of about 5,300 psi which is very close to the formation fracture pressure.
- If the liquid injection rate is 6,000 psi, the minimum permeability values of the Bluff and the Entrada are 26 mD and 30 mD to avoid formation fracture.

Drilling Plan

Well Name: SJB CarbonSAFE #1

Well Location: Section 12, T 31 N, R 12 W, San Juan County, New Mexico.

-108.061174 and 36.899774.

San Juan County, New Mexico

1. Estimated Tops of Geological Markers (MD)

The estimated tops of important geological markers are as follows:

| Formations/Groups | Measured Depth, ft |
|---------------------|--------------------|
| Ojo Alamo Ss. | 1,330 |
| Kirtland Sh. | 1,920 |
| Fruitland Fm. | 2,059 |
| Pictured Cliffs Ss. | 2,769 |
| Lewis Sh. | 2,904 |
| Mesaverde Grp. | 4,334 |
| Mancos Sh. | 5,305 |
| Greenhorn Ls. | 7,073 |
| Graneros Sh. | 7,135 |
| Dakota Ss. | 7,185 |
| Brushy Basin Mbr. | 7,340 |
| Salt Wash Mbr. | 7,650 |
| Bluff Fm. | 7,920 |
| Summerville Fm. | 8,090 |
| Todilto Fm. | 8,173 |
| Entrada Fm. | 8,192 |
| Carmel Fm. | 8,306 |
| Chinle Grp. | 8,528 |

The referenced surface elevation is 6,207', KB 6,237'.

2. Estimated Depth of Potential Water, Oil, Gas, & Other Mineral Bearing Formations

| Formation | Substance | Depth Unit, ft |
|---|----------------------------|----------------|
| Fruitland Sands/Coal | Gas/Water/Coal-bed Methane | 2092 |
| Pictured Cliffs | Gas | 2737 |
| Mesaverde Group (all 3 formations, Cliff House, Menefee and Pt. Lookout) | Gas/Water | 4334 |
| Mancos | Gas/Minor Oil | 5277 |

| Gallup Ss | Gas/Minor Oil/Water | 6424 |
|-------------|---------------------|------|
| Dakota Ss | Gas/Minor Oil/Water | 7233 |
| Morrison Ss | Water | 7420 |
| Entrada Ss | Oil/Water | 8200 |

All shows of fresh water and minerals will be reported and protected.

3. Pressure Control

a) Pressure control equipment and configuration will be designed to meet 5M standards.

b) Working pressure on rams and BOPE will be 5000 psi

c) Function test and visual inspection of BOP will be conducted daily and noted in the IADC Daily Drilling Report.

d) The Annular BOP will be pressure tested to a minimum of 50 percent of its rated working pressure.

e) Blind and Pipe Rams/BOP will be tested against a test plug to 100 percentage of rated working pressure.

f) Pressure tests are required before drilling out from under all casing strings set and cemented in place.

g) BOP controls must be installed prior to drilling the surface casing plug and will remain in use until the well is completed or abandoned.

h) BOP testing procedures and testing frequency will conform to Onshore Order No. 2.

i) BOP remote controls shall be located on the rig floor at a location readily accessible to the driller. Master controls shall be on the ground at the accumulator and shall have the capability to function all preventers.

j) The kill line shall be 2-inch minimum and contain two kill line valves, one of which shall be a check valve.

k) The choke line shall be a 2-inch minimum and contain two choke line valves (2-inch minimum).

I) The choke line shall be 2-inch minimum and contain two adjustable chokes

m) Hand wheels shall be installed on all ram preventers.

n) Safety valves and wrenches (with subs for drill string connections) shall be available on the rig floor at all times.

o) Inside BOP or float sub shall also be available on the rig floor at all times.

4. CASING & CEMENTING PROGRAM

The proposed casing and cementing program has been designed to protect and/or isolate all usable water zones, potentially productive zones, lost circulation zones, abnormally pressured zones, and any prospectively valuable deposits of minerals. Any isolating medium other than cement shall receive approval prior to use. The casing setting depth shall be calculated to position the casing seat opposite a competent formation which will contain the maximum pressure to which it will be exposed during normal drilling operations. All indications of useable water shall be reported.

| Casing /Tubing String | Casing /tubing Depth, TVD ¹ , ft | Casing /Tubing Depth, MD ² , ft | Borehole Diameter, in. | Casing /Tubing Outside Diameter, in | Coupling Outside Diameter, in. | Casing/Tubing Material (Weight /Grade /Connection) | String Weight in Air, Ib |
|-----------------------------|--|---|------------------------------|---|---|---|--------------------------------|
| Conductor | 0-100 | 0-100 | 30 | 20 | 20 | 94 lb/ft, J-55, Welded | 9,400 |
| Surface | 0-1,500 | 0-1,500 | 17 1/2 | 13 3/8 | 14.375 | 54.5 lb/ft, J-55, BTC | 81,750 |
| Intermed. | 0-5,500 | 0-5,500 | 12 1/4 | 9 5/8 | 10.625 | 40 lb/ft, L-80, BTC | 220,000 |
| Laura | 0-5,000 | 0-5,000 | 8 3/4 | 5 1/2 | 6.05 | 23 lb/ft, L80, BTC | 115,000 |
| Long String | 5,000- 8,800 | 5,000- 8,800 | 8 3/4 | 5 1/2 | 6.05 | 23 lb/ft, Cr13- P110, Premium BTC | 87,400 |

a) The proposed casing design is as follows:

| Casing /Tubing String | Casing /Tubing Material (Weight /Grade /Connection) | Casing /Tubing Diameters (Outside /Inside / Drift Diameter), in. | Yield, ksi | Tensile, ksi | Internal (Burst) Yield, psi | Collapse, psi | Body Yield, 1000 Ibs | Joint Strength 1000 lbs |
|-----------------------------|--|---|---------------|-----------------|--------------------------------------|------------------|-------------------------------|-------------------------------|
| Conductor | 94 lb/ft, J-55, Welded | 20/19/- | 55 | 75 | 1530 | 520 | 1480 | 1402 |
| Surface | 54.5 lb/ft, J- 55, BTC | 13.375 /12.615 /12.459 | 55 | 75 | 2730 | 1130 | 853 | 909 |
| Intermed. | 40 lb/ft, L-80, BTC | 9.625 /8.835 /8.679 | 80 | 95 | 5750 | 3090 | 916 | 947 |
| Long | 23 lb/ft, L80, BTC | 5.5 /4.67 /4.545 | 80 | 95 | 8990 | 11160 | 530 | 550 |
| Long String | 23 lb/ft, Cr13- P110, Premium BTC | 5.5 /4.67/ 4.545 | 110 | 125 | 12360 | 14540 | 729 | 724 |

Casing design is subject to revision based on geologic conditions encountered.

All casing strings below the conductor shall be pressure tested to 0.22 psi per foot of casing string length or 1,500 psi, whichever is greater, but not to exceed 70 percent of the minimum internal yield. If pressure declines more than 10 percent in 30 minutes, corrective action shall be taken.

| Casing | Depth | Cement Volume, sacks | Cement Type & Yield | Designed TOC | Centralizers |
|--------------|-------|---|--|-----------------|--|
| Conductor | 100 | 127 | Type I Neat 14.8 ppg | Surface | None |
| Surface | 1500 | 1216 | Type III Cement+ 1% CaCI + 0.25Iblsk Cello Flake + 0.2% FL, 14.6ppg, 1.38cuft/sk | Surface | 1 per joint on bottom 3 joints |
| Intermediate | 5500 | 50% open hole excess Stage 1 Lead: 544 sks Tail: 226 sks Stage 2 Lead: 422 sks Tail: 237 sks | Lead (Stages 1 and 2): Type III + 3% CaCI + 0.25lb/sk CelloFlake + 5lb/sk LCM, 12.1 ppg 2.13cuft/sk Tail (Stage 1): Type III Cmt + 1% CaCI + 0.25lb/sk Cello Flake 14.5ppg 1.38cuft/sk | Surface | 1 per joint for bottom 3 joints, 1 on every 3 joints for remaining joints |
| Production | 8800 | 75% open hole excess Lead: 864 sks Tail: 1258 sks | Lead: Class G cmt + 0.04 gal/sk antifoam +0.30 % Dispersant + 0.50 % Retarder, Evercrete cement, 16.1ppg, 1.07 cuft/sk | Surface | 3 per joint |

b) The proposed cementing program is as follows:

Top plugs shall be used to reduce contamination of cement by displacement fluid. A bottom plug or other acceptable technique, such as a pre-flush fluid, inner string cement method, etc. shall be utilized to help isolate the cement from contamination by the mud fluid being displaced ahead of the cement slurry.

Actual volumes will be calculated and determined by conditions onsite. All cement slurries will meet or exceed minimum BLM and New Mexico Oil Conservation Division requirements. Slurries used will be the slurries listed above or equivalent slurries depending on service provider selected. Cement yields may change depending on slurries selected.

All waiting on cement times shall be a minimum of 8 hours or adequate to achieve a minimum of 500 psi compressive strength at the casing shoe prior to drilling out.

| Hole Size, in | Drilling Fluid System | Measured Depth, ft | Fluid Density, ppg | Plastic Viscosity, cp | Yield Point, Ib /100ft ² | API Fluid loss, cm ³ | РН | Circulation Rate, GPM |
|---------------------|-----------------------------|--------------------------|--------------------------|-----------------------------|--|--|----------|--------------------------|
| 17 1/2 | Water- based Mud | 0–1,500 | 8.3-9.2 | 9-14 | 1-10 | 1-10 | 9- 10 | 500 |
| 12 1/4 | Water- based Mud | 1,500- 5,500 | 8.4-8.6 | 9-14 | 1-10 | 1-10 | 9- 10 | 500 |
| 8 3/4 | Water- based Mud | 5,000- 8,800 | 8.5 | 9-14 | 1-10 | 1-10 | 9- 10 | 500 |

5. DRILLING FLUIDS PROGRAM

*Mud program may change based on mud engineer's field recommendation.

There will be sufficient mud on location to control a blowout should one occur. Mud flow and volume will be monitored both visually and with electronic pit volume totalizers. Mud tests shall be performed every 24 hours after mudding up to determine, as applicable: density, viscosity, gel strength, filtration, and pH.

A closed-loop system will be used to recover drilling fluid and dry cuttings in both phases of the well and on all hole intervals, including fresh water and oil-based operations. Above-ground tanks will be utilized to hold cuttings and fluids for rig operations. A frac tank will be on location to store fresh water. Waste will be disposed of properly at an EPA-approved hazardous waste facility. Fresh water cuttings will be disposed by the service from company. The location will be lined in accordance with the Surface Use Plan of Operations.

- 6. TESTING, CORING and LOGGING
- a) Drill Stem Testing -None anticipated
- b) Coring program

The coring will cover the contiguous intervals from 7,410' to 8,346' in order to cover the following coring intervals for research purposes.

| Coring interval #1 | Look if there is enough of a seal between the lower reservoir units (Salt Wash, Bluff, and Entrada) and the Dakota Ss. (a gas producer in the area). | 7,410'-7,530' |
|-----------------------|--|---------------|
| Coring interval #2 | Look at both the transition between these two members of the Morrison and the lower Brushy Basin's sealing characteristics. | 7,621'-7,691' |
| Coring interval #3 | Collect cores in Salt Wash and Bluff formation, cap rock, and underlying formation. Also Collect cores in Entrada formation, cap rock, and underlying formation. | 7,866'-8,346' |

c) Mud Logging -Mud loggers will be on location from kick off point to TD.

d) Logging -See Below

| Well Logging | Logging Program | Depth Intervals |
|-----------------------------|--|--------------------|
| | Surface Casing | |
| Measurements While Drilling | Near Bit Gamma Ray (GR) and Annular Pressure while drilling (APWD) | 1,500'-0' |
| Open Hole | Triple combo (Resistivity, Density, Neutron, Gamma Ray [GR], Caliper[CALI], and Spontaneous Potential [SP]) | 1,500'-0' |
| Cased Hole | Cement bond log [CBL/VDL/CCL], Radial (Azimuthal) cement evaluation, Flexural wave imaging, temperature | 1,500'-0' |
| | Intermediate Casing | |
| Measurements While Drilling | Near Bit Gamma Ray (Gr) and Annular Pressure while drilling (APWD) | 5,500'- 1,500' |
| Open Hole | Triple combo (Resistivity, Density, Neutron, Gamma Ray, Caliper, SP), Dipole sonic, Formation Imager - FMI | 5,500'- 1,500' |
| Cased Hole | Cement bond log [CBL/VDL/CCL], Radial (Azimuthal) cement evaluation, Flexural wave imaging, temperature | 5,500'- 1,500' |
| | Production Casing | |
| Measurements While Drilling | Near Bit Gamma Ray (GR) and Annular Pressure while drilling (APWD) | 8,800'- 5,500' |
| | Triple combo (Resistivity, Density, Neutron, Gamma Ray [GR], caliper, and spontaneous potential [SP]) Dipole Sonic, including long recording times to see reflections from fractures and faults, Formation Imager - | 8,800'- 5,500' |
| Open Hole | FMI, Litho Scanner with Spectral Gamma Ray, Magnetic Resonance Scanner, Dielectric Scanner, Formation Fluid Samples of porous zones, Sidewall Coring | 8,800'- 5,500' |
| Cased Hole | Cement bond log [CBL/VDL/CCL], Radial (Azimuthal) cement evaluation, Flexural wave imaging, temperature, Cased Hole Nuclear Spectroscopy, Casing Inspection Log, Zero Offset Vertical Seismic Profile | 8,800'- 5,000' |

7. ABNORMAL PRESSURES & HYDROGEN SULFIDE

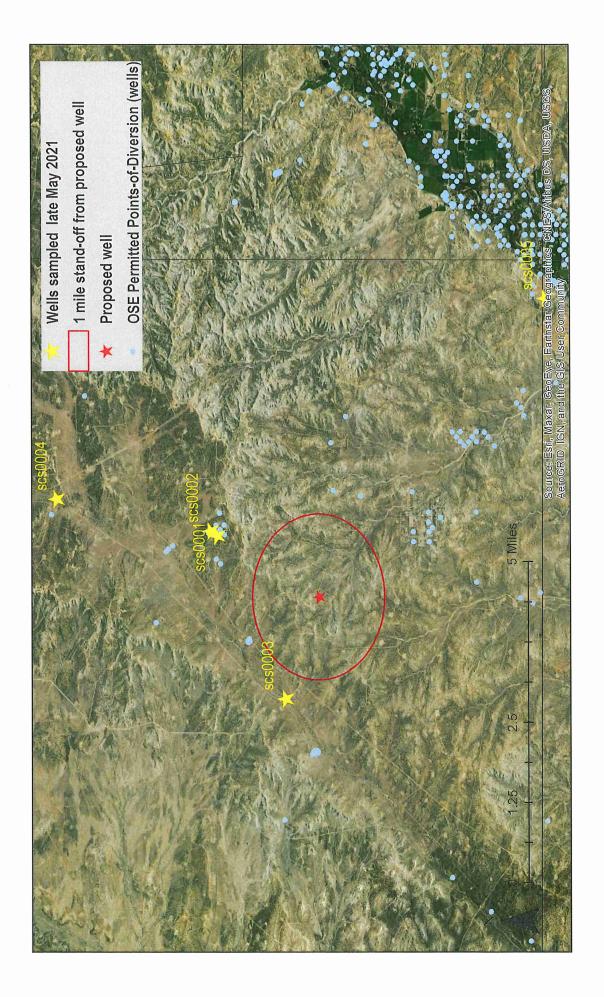
The anticipated bottom hole pressure is +/-3,300 psi. No abnormal pressure or temperatures are anticipated.

No hydrogen sulfide gas is anticipated, however, if H_2S is encountered, the guidelines in Onshore Order No. 6 will be followed.

8. ANTICIPATED START DATE AND DURATION OF OPERATIONS

Drilling is estimated to commence on November 30, 2021. It is anticipated that completion operations will begin within 60 days after the well has been drilled depending on coring and logging schedules with various service companies.

It is anticipated that the drilling of this well will take approximately 31 days.



Water Sampling and Analysis Report

The sampling and analyses provided were all done in-house at New Mexico Tech. The waters were sampled from shallow (<500 ft) water wells within five miles of the proposed stratigraphic test well site (Figs. 1 and 2). A total seven wells were sampled.

At each well, two 1-L acid washed Nalgene bottles were triple-rinsed with well water and filled. One 1-L bottle was reserved for general chemistry analysis. The other was subsequently resampled with a peristaltic pump with acid-washed silicone tubing into one 45 mL amber glass bottle for stable isotopes, and through a 0.45 μ m filter into two 125 mL acid washed Nalgene bottles where were acidified with two drops of UHP nitric acid. One filtered sample was reserved for trace metals analysis and the other was reserved for ⁸⁷Sr/⁸⁶Sr analysis at NETL. Samples were kept on ice in a cooler or refrigerator until they were analyzed.

The pH of all of the samples are basic, mostly around a pH of 8. SCS006 has a pH of 10.56. Specific conductivities range from 604 to 18,576 uS/cm. Temperatures ranged from 12 C to nearly 20 C.

| Sample Da | ta Table | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|-----------|-------------|---------|-------------|------|-------------|--------------------------|-------------|--------|------|----------|------|---------|---------|--------|--------------------------------------|--------|----------|---------|---------------------------------|-----------|----------------|---------------------------|-------------|---------------|--------------------------|--------|------------------|---------|
| | | | we | ell | | | date | | do_m | | | orp_m | | | Alkalinity as | | | Bromide | (NO ₃ ⁻) | Phosphate | $(SO_4^{2^-})$ | Lithium(Li) (mg/L) | Sodium | Potassium (K) | Magnesium (Mg) (mg/L) | (Ca) | 1DS Calculati | |
| pointid | oseid | easting | northing de | epth | use | status | sampled | temp_c | g∟ | spcond | рн | V | (uS/cm) | (mg/L) | HCO ₃ ⁻ (mg/L) | (mg/L) |) (mg/L) | (mg/L) | (mg/L) | (mg/L) | (mg/L) | (mg/L) | (Na) (mg/L) | | | | on (mg/L) | (ing/L) |
| scs0001 | pre-records | 763013 | 4090387 10 | 00 | irrigation | active | 18-May-21 | 14.73 | 8.11 | 1697.00 | 7.62 | -12.50 | 1430.0 | 0.0 | 185.44 | 30.26 | 0.00 | 0.00 | 4.17 | <0.50 | 635.34 | 1.42 | 145.01 | 5.86 | 14.29 | 210.51 | 1136.7 | 224.80 |
| scs0002 | sj03738 | 763104 | 4090558 11 | 15 | undeveloped | open | 19-May-21 | 12.21 | 5.63 | 604.00 | 8.79 | -94.20 | 510.0 | 0.0 | 273.28 | 8.2 | 2.0 | 0.00 | 1.0 | <0.50 | 56.8 | 0.07 | 122.7 | 0.7 | 0.8 | 5.5 | 332.2 | 6.30 |
| scs0003 | pre-records | 759787 | 4088574 10 | 00 | not used | inactive but equipped | 20-May-21 | 15.12 | 1.00 | 7141.00 | 8.79 | -184.10 | 6420.0 | 0.0 | 68.32 | 455.93 | 0.00 | 0.00 | 0.00 | <0.50 | 3181.23 | 6.57 | 1329.21 | 27.08 | 38.99 | 414.07 | 5480.1 | 453.05 |
| scs0004 | sj03996 | 763621 | 4094459 12 | 20 | livestock | active | 50 May 2021 | 13.87 | 0.79 | 2176.00 | 8.07 | -89.20 | 1808.0 | 0.0 | 295.24 | 11.19 | 1.63 | 0.00 | 1.63 | <0.50 | 930.05 | 0.00 | 127.19 | 4.48 | 17.20 | 328.26 | 1566.9 | 345.46 |
| scs0005 | sj03309 | 768040 | 4082256 24 | 40 | not used | inactive but eq | uipped | | | 20497.00 | 7.70 | | | | | | | | | | | | | | | | | |

Culpepper Martin #106 Analytical Results

New Mexico Tech was only able to obtain page 5 of pages (1-9) of the referenced water analytical results for the Culpepper Martin #106 from Green Analytical. The complete chain of custody was unable to be obtained from HilCorp Energy.



dzufelt@greenanalytical.com p: 970.247.4220 f: 970.247.4227 75 Suttle Street Durango, CO 81303

www.GreenAnalytical.com

| Conoco Phillips-Farmington | Project: PO4 & API+ & Fe/Mn | |
|----------------------------|---------------------------------|----------------|
| 3401 30th Street | Project Name / Number: Area 1 | Reported: |
| Farmington NM, 87401 | Project Manager: Darrell Savage | 07/20/15 12:00 |
| | | |

Culpepper Martin #106

| | | 150 | 7057-03 (W | /ater) | | | | | |
|-------------------------------------|---------|-------|------------|----------|----------|----------|---------------|-------|---------|
| Analyte | Result | RL | MDL | Units | Dilution | Analyzed | Method | Notes | Analyst |
| General Chemistry | | | | | | | | | |
| Alkalinity, Bicarbonate* | 3980 | 10.0 | | mg/L | 20 | 07/13/15 | 2320 B | | ABP |
| Alkalinity, Carbonate* | 40.0 | 10.0 | | mg/L | 20 | 07/13/15 | 2320 B | | ABP |
| Alkalinity, Hydroxide* | <10.0 | 10.0 | | mg/L | 20 | 07/13/15 | 2320 B | | ABP |
| Alkalinity, Total* | 4020 | 10.0 | | mg/L | 20 | 07/13/15 | 2320 B | | ABP |
| Chloride* | 710 | 50.0 | 25.0 | mg/L | 5 | 07/18/15 | 4500-Cl- C | | LLG |
| Conductivity* | 9430 | 10.0 | | uS/cm | 1 | 07/08/15 | 2510 B | | MAJ |
| pH* | 7.91 | | | pH Units | 1 | 07/08/15 | EPA150.1 | | MAJ |
| Phosphate (PO4) | 1.12 | 0.768 | 0.276 | mg/L | 5 | 07/14/15 | EPA365.3/Calc | | LLG |
| Phosphorus, Total | 0.365 | 0.250 | 0.0900 | mg/L | 5 | 07/14/15 | EPA365.3 | Q3 | LLG |
| Resistivity | 106 | | | ohm/cm | 1 | 07/20/15 | 2510 B | | DJZ |
| TDS* | 5670 | 10.0 | | mg/L | 1 | 07/13/15 | EPA160.1 | | ABP |
| Specific Gravity | 1.004 | | | N/A | 1 | 07/09/15 | Hydrometer | | ABP |
| Sulfate | 2.60 | 10.0 | 1.68 | mg/L | 1 | 07/14/15 | 4500-SO42- E | | ABP |
| Potentially Dissolved Metals by ICP | | | | | | | | | |
| Hardness | 45.9 | 4.62 | 1.40 | mg/L | 10 | 07/10/15 | 2340 B | | JLM |
| Silica Potentially Dissolved | 24.5 | 10.7 | 5.34 | mg/L | 10 | 07/10/15 | 2340 B | | JLM |
| Barium* | 7.90 | 0.100 | 0.026 | mg/L | 10 | 07/10/15 | EPA200.7 | | JLM |
| Calcium* | 10.3 | 0.200 | 0.028 | mg/L | 10 | 07/10/15 | EPA200.7 | | JLM |
| Iron* | 8.76 | 0.500 | 0.035 | mg/L | 10 | 07/10/15 | EPA200.7 | | JLM |
| Lead* | <1.00 | 1.00 | 0.246 | mg/L | 10 | 07/10/15 | EPA200.7 | | JLM |
| Magnesium* | 4.94 | 1.00 | 0.324 | mg/L | 10 | 07/10/15 | EPA200.7 | | JLM |
| Manganese* | 0.155 | 0.050 | 0.007 | mg/L | 10 | 07/10/15 | EPA200.7 | | JLM |
| Potassium* | 37.0 | 10.0 | 3.35 | mg/L | 10 | 07/10/15 | EPA200.7 | | JLM |
| Silicon | 11.5 | 5.00 | 2.50 | mg/L | 10 | 07/10/15 | EPA200.7 | | JLM |
| Sodium* | 2230 | 10.0 | 3.05 | mg/L | 10 | 07/10/15 | EPA200.7 | | JLM |
| Strontium* | 3.60 | 1.00 | 0.004 | mg/L | 10 | 07/10/15 | EPA200.7 | | JLM |
| Zinc* | < 0.500 | 0.500 | 0.022 | mg/L | 10 | 07/10/15 | EPA200.7 | | JLM |
| Cation / A nion Polones | (75 | | | | | | | | |

Cation/Anion Balance

6.75

Green Analytical Laboratories

ellie Zufett

Debbie Zufelt, Reports Manager

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Page 5 of 9

| Table 1. | Water | sampling | well | inventory. |
|----------|-------|----------|------|------------|
|----------|-------|----------|------|------------|

| ġ | | | | | | | | | | | |
|---|---------|---------|----------|-------|-------|----------|--------|-------|--------|-------|----------|
| | | | | | | Active | Field | Gen. | Trace | Sr- | Stable |
| | Well ID | Easting | Northing | Depth | Fm. | pump | param. | chem. | metals | ratio | isotopes |
| | SCS001 | 763013 | 4090387 | 100 | Nac | Х | Х | Х | Х | Х | Х |
| | SCS002 | 761304 | 4090558 | 115 | alluv | open | Х | Х | Х | Х | Х |
| | SCS003 | 759787 | 4088574 | 100 | Nac | inactive | Х | Х | Х | Х | Х |
| | SCS004 | 763621 | 4094459 | 120 | Nac | Х | Х | Х | Х | Х | Х |
| | SCS005 | 762040 | 4082256 | 240 | Nac | inactive | ? | | | | Х |
| | SCS006 | 762939 | 4086923 | UNK | Nac | open | Х | Х | Х | Х | Х |
| | SCS007 | 764960 | 4087558 | UNK | Nac | inactive | Х | Х | Х | Х | Х |
| | | | | | | | | | | | |

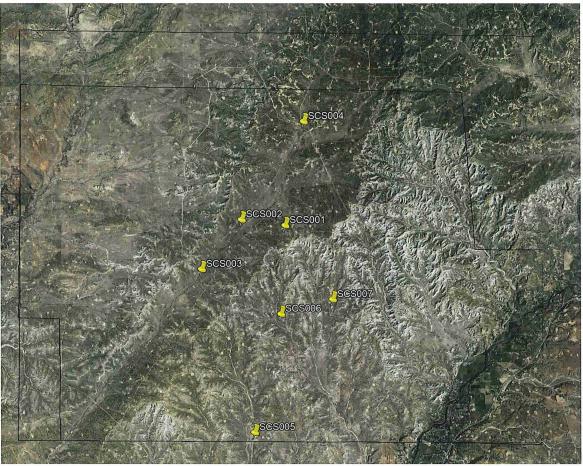


Figure 2. Locations of sampled wells.

| Well ID | SCS0001 | SCS0002 | SCS0003 | SCS0004 | Blank | SCS0006 | SCS0007 |
|---|----------|---------|---------|---------|--------------------|---------|----------|
| pH (field) | 7.62 | 8.79 | 8.79 | 8.07 | - | 10.56 | 7.87 |
| Spec. Cond. | 1007 | 004 | 7744 | 0.170 | | 0.404 | 40.570 |
| (uS/cm) | 1697 | 604 | 7741 | 2176 | - | 9,181 | 18,576 |
| DO (mg/L) | 8.11 | 5.63 | 1.00 | 0.79 | - | 0.04 | 1.08 |
| Temp (C) Alkalinity as | 14.73 | 12.21 | 15.12 | 13.87 | - 1953) - 1953) | 15.72 | 19.87 |
| CO_3^{-2} (mg/L) | | | | | | 384.0 | 0.0 |
| Alkalinity as | | | | | | 364.0 | 0.0 |
| (mg/L) | 185.44 | 273.28 | 68.32 | 295.24 | 2.44 | 1,171.0 | 146.4 |
| Chloride | | | | | | 0 / T / | |
| (mg/L) | 30.26 | 8.2 | 455.93 | 11.19 | 0.0 | 317.1 | 2,385.2 |
| Fluoride (F ⁻) | | | | | | | |
| (mg/L) Bromide | 0.00 | 2.0 | 0.00 | 1.63 | 0.0 | 0.0 | 0.0 |
| (mg/L) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.0 | 0.0 |
| Nitrate (NO ₃ -) | a Carlos | | | | | | |
| (mg/L) | 4.17 | 1.0 | 0.00 | 1.63 | 0.0 | 0.0 | 0.0 |
| Phosphate | | | | | | | |
| (mg/L) | <0.50 | <0.50 | <0.50 | <0.50 | <0.50 | <0.50 | <0.50 |
| Sulfate (SO ₄ ²⁻) (mg/L) | 005.04 | 50.0 | 0404.00 | 000.05 | | 0.000.0 | 0.055.0 |
| Lithium(Li) | 635.34 | 56.8 | 3181.23 | 930.05 | 0.0 | 2,909.0 | 6,655.8 |
| (mg/L) | 1.42 | 0.07 | 6.57 | 0.00 | 0.00 | 0.0 | 0.0 |
| Sodium (Na) | | | | | | | |
| (mg/L) | 145.01 | 122.7 | 1329.21 | 127.19 | 0.6 | 2,408.4 | 4,683.3 |
| Potassium (K) (mg/L) | 5.86 | 0.7 | 27.08 | 4.48 | 0.5 | 18.4 | 10.8 |
| Magnesium | 0.00 | 0.1 | 21.00 | -110 | 0.0 | 10.4 | 10.0 |
| (Mg) (mg/L) | 14.29 | 0.8 | 38.99 | 17.20 | 0.5 | 0.6 | 22.4 |
| Calcium (Ca) | 210 51 | 5 5 | 414.07 | 220.00 | 0.0 | 2 4 | 120.0 |
| (mg/L) | 210.51 | 5.5 | 414.07 | 328.26 | 0.9 | 3.4 | 430.0 |
| TDS Calculation | | | | | | | |
| (mg/L) | 1136.7 | 332.2 | 5480.1 | 1566.9 | 3.7 | 6,233.1 | 14,259.7 |

Table 2. Field parameters and general chemistry.



New Mexico Office of the State Engineer Water Column/Average Depth to Water

(quarters are 1=NW 2=NE 3=SW 4=SE) (quarters are smallest to largest) (NA

(NAD83 UTM in meters)

No records found.

PLSS Search:

Section(s): 14

Township: 31N Range: 12W

The data is furnished by the NMOSE/ISC and is accepted by the recipient with the expressed understanding that the OSE/ISC make no warranties, expressed or implied, concerning the accuracy, completeness, reliability, usability, or suitability for any particular purpose of the data.

10/14/21 5:03 PM

WATER COLUMN/ AVERAGE DEPTH TO WATER



New Mexico Office of the State Engineer Water Column/Average Depth to Water

(quarters are 1=NW 2=NE 3=SW 4=SE) (quarters are smallest to largest) (NAD83 UTM in meters)

No records found.

PLSS Search:

Section(s): 13

Township: 31N Range: 12W

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10/14/21 5:03 PM

WATER COLUMN/ AVERAGE DEPTH TO WATER



New Mexico Office of the State Engineer Water Column/Average Depth to Water

(quarters are 1=NW 2=NE 3=SW 4=SE) (quarters are smallest to largest) (NAD

(NAD83 UTM in meters)

No records found.

PLSS Search:

Section(s): 14

Township: 32N

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Range: 12W

10/14/21 5:04 PM

WATER COLUMN/ AVERAGE DEPTH TO WATER

| API 30-045 Well type Gas Pro Construction 2012 Date Drilled (Spund) 1/29/ | | EAST #007 30-045-10814 Gas Producer | EAST #007E 30-045-24146 Gas Producer | EAST #007F 30-045-30438 Gas Producer | EAST #103 30-045-27850 Gas Producer | HARPER #001 30-045-10712 Gas Producer | HARPER #001A 30-045-22850 | HARPER #002 30-045-10676 | HARPER #002E 30-045-23647 | HARPER #003 30-045-24675 | HARPER COM #100 30-045-27515 | GRENIER #011F 30-045-30466 | GRENIER #005B 30-045-30000 | GRENIER #005A 30-045-21878 |
|--|----------|---|--|--|---|---|------------------------------|-----------------------------|------------------------------|-----------------------------|---------------------------------|-------------------------------|-------------------------------|-------------------------------|
| API 30-045 Well type Gas Pro Construction 2012 Date Drilled (Spund) 1/29/ | Producer | Gas Producer | | | | | | | 30-045-23647 | 30-045-24675 | 30-045-27515 | 30-045-30466 | 30-045-30000 | 30-045-21878 |
| Construction Date Drilled (Spund) 1/29/ | | | Gas Producer | Gas Producer | Gas Producer | Gas Producer | 0.0 | | | | | | | |
| Construction Date Drilled (Spund) 1/29/ | 29/1977 | | | | | | Gas Producer | Gas Producer | Gas Producer | Gas Producer | Gas Producer | Gas Producer | Gas Producer | Gas Producer |
| Bate Brines (opana) | 29/1977 | | | | | | | | | | | | | |
| | | 05/02/1962 | 5/24/1980 | 04/29/2001 | 6/9/1990 | 3/18/1952 | 03/08/1978 | 3/29/1962 | 10/22/1979 | 2/19/1981 | 03/03/1990 | 06/01/2001 | 1/23/2000 | 9/16/1975 |
| prod) 12/1/ | /1/1977 | 6/4/1962 | 10/1/1980 | 3/13/2001 | 1/1/1992 | N/A | 6/1/1978 | N/A | 3/1/1980 | 1/1/1982 | 1/1/1992 | 7/26/2001 | 4/10/2000 | 12/1/1975 |
| Location M-14-31N | 1N-12W | D-14-31N-12W | L-14-31N-12W | F-14-31N-12W | K-14-31N-12W | I-14-31N-12W | G-14-31N-12W | P-14-31N-12W | H-14-31N-12W | P-14-31N-12W | G-14-31N-12W | D-13-31N-12W | E-13-31N-12W | L-13-31N-12W |
| | 8940926 | 36.9037132 | 36.8962288 | 36.9018059 | 36.895546 | 36.8962173 | 36.9014854 | 36.8938637 | 36.9011497 | 36.8943748 | 36.900753 | 36.9034233 | 36.9020424 | 36.8966255 |
| Long -108.07 | .0737228 | -108.0718765 | -108.0726929 | -108.0677719 | -108.0710449 | -108.0610046 | -108.0624161 | -108.0610275 | -108.0609055 | -108.0620117 | -108.0633087 | -108.0558319 | -108.055397 | -108.0540314 |
| | 5463 | 7560 | 7480 | 7550 | 2772 | 5253 | 5471 | 7348 | 7590 | 2920 | 2727 | 7430 | 5427 | 5150 |
| | /1/1977 | N/A | 10/1/1980 | 3/13/2001 | 1/1/1992 | N/A | 6/1/1978 | N/A | 3/1/1980 | 1/1/1982 | 1/1/1992 | 7/26/2001 | 4/10/2000 | 12/1/1975 |
| | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A |

Offset Well Information

| Well Name | API |
|--------------------------|------------|
| PATTERSON B COM 001 | 3004504169 |
| PATTERSON B COM 001 | 3004504170 |
| GOULDING 001 | 3004504171 |
| OLIVER SRC #001 | 3004510395 |
| EAST #005 | 3004510475 |
| ELLIOTT A LS #001 | 3004510495 |
| RICHARDSON SRC #006 | 3004510497 |
| EAST #011 | 3004510599 |
| EAST #004 | 3004510605 |
| SARAH M HEDGES #002 | 3004510607 |
| EAST #002 | 3004510610 |
| RICHARDSON #003 | 3004510612 |
| EAST #006 | 3004510612 |
| GRENIER #012 | 3004510673 |
| ~ | |
| HARPER #002 | 3004510676 |
| CASE B #004 | 3004510685 |
| GRENIER #008 | 3004510692 |
| HARPER #001 | 3004510712 |
| RICHARDSON SRC #007 | 3004510723 |
| STATE GAS COM BA #001 | 3004510759 |
| GRENIER #011 | 3004510763 |
| STATE GAS COM N #001 | 3004510765 |
| GRENIER #010 | 3004510768 |
| GRENIER #009 | 3004510780 |
| PRE-ONGARD WELL #008 | 3004510784 |
| GRENIER #005 | 3004510787 |
| GRENIER #002 | 3004510788 |
| EAST #001 | 3004510789 |
| RICHARDSON SRC #002 | 3004510790 |
| RICHARDSON #009 | 3004510813 |
| EAST #007 | 3004510814 |
| CHOKE CHERRY CANYON #001 | 3004510842 |
| DAVIS #002 | 3004510853 |
| RICHARDSON SRC #001 | 3004510854 |
| DAVIS #006 | 3004510855 |
| DAVIS #008 | 3004510857 |
| RICHARDSON #008 | 3004510868 |
| DAVIS #009 | 3004510878 |
| DAVIS #001 | 3004510931 |
| RICHARDSON SRC #004 | 3004510933 |
| DAVIS #010 | 3004510946 |
| DAVIS #004 | 3004510947 |
| GRENIER #004 | 3004510949 |
| RICHARDSON #010 | 3004510950 |
| GRENIER #014 | 3004510952 |
| DAVIS #007 | 3004510957 |
| DAVIS #011 | 3004510998 |
| PATTERSON A COM #001 | 3004511012 |
| DAVIS #005 | 3004511013 |
| | 0001011010 |

| DUSENBERRY #002 | 3004511032 |
|-----------------------|------------|
| GRENIER #015 | 3004511668 |
| RICHARDSON #011 | 3004512178 |
| CASE B #010 | 3004520311 |
| GRENIER #010 | 3004520427 |
| EAST #013 | 3004520427 |
| OLIVER #002 | 3004520481 |
| OLIVER SRC #003 | 3004520481 |
| EAST #014 | 3004520482 |
| EAST #014 | 3004520511 |
| | |
| GRENIER #021 | 3004520533 |
| PRE-ONGARD WELL #019 | 3004520535 |
| EAST #020 | 3004520555 |
| DAVIS #014 | 3004520648 |
| DAVIS #015 | 3004520653 |
| PATTERSON #003 | 3004520654 |
| PATTERSON C COM #001 | 3004520716 |
| DAVIS #016 | 3004520742 |
| CASE B #014 | 3004520888 |
| ELLIOT A LS #002 | 3004521029 |
| RICHARDSON #012 | 3004521273 |
| GRENIER #004A | 3004521795 |
| EAST #002A | 3004521798 |
| EAST #022 | 3004521799 |
| RICHARDSON #001A | 3004521877 |
| GRENIER #005A | 3004521878 |
| RICHARDSON #002A | 3004521879 |
| RICHARDSON #012A | 3004521880 |
| DAVIS #001A | 3004522112 |
| GRENIER #002A | 3004522262 |
| DAVIS #003A | 3004522264 |
| DAVIS #002A | 3004522266 |
| DAVIS #004A | 3004522267 |
| GRENIER #003A | 3004522268 |
| EAST #001A | 3004522269 |
| DAVIS #006A | 3004522314 |
| STATE GAS COM M #001A | 3004522765 |
| PATTERSON B COM #001A | 3004522839 |
| HARPER #001A | 3004522850 |
| EAST #009A | 3004522853 |
| RICHARDSON #004A | 3004522862 |
| RICHARDSON #003A | 3004522864 |
| EAST #005A | 3004522865 |
| EAST #004A | 3004522866 |
| RICHARDSON #006A | 3004522881 |
| DAVIS #017 | 3004523022 |
| CASE B #004A | 3004523191 |
| HEDGES #003 | 3004523367 |
| DAVIS #018 | 3004523372 |
| ELLIOTT A LS #001A | 3004523383 |
| CASE A #001 | 3004523458 |
| GRENIER #011E | 3004523646 |

| HARPER #002E | 3004523647 |
|-----------------------|------------|
| DAVIS #008E | 3004523759 |
| RICHARDSON #007E | 3004523794 |
| RICHARDSON #007E | 3004523872 |
| DAVIS #007E | 3004523873 |
| | |
| PATTERSON B COM #001E | 3004523959 |
| DAVIS #009E | 3004523982 |
| DAVIS #013E | 3004524018 |
| RICHARDSON #008E | 3004524019 |
| CASE A #004 | 3004524041 |
| DAVIS #010E | 3004524145 |
| EAST #007E | 3004524146 |
| RICHARDSON #009E | 3004524147 |
| CASE A #004E | 3004524618 |
| HARPER #003 | 3004524675 |
| GRENIER #015E | 3004525331 |
| CASE A #001E | 3004525624 |
| GRENIER #101 | 3004527247 |
| PRE-ONGARD WELL #104 | 3004527249 |
| GRENIER #102 | 3004527271 |
| PRE-ONGARD WELL #500 | 3004527294 |
| RICHARDSON #101 | 3004527295 |
| DAVIS #501 | 3004527296 |
| DAVIS #502 | 3004527363 |
| RICHARDSON #100 | 3004527387 |
| DAVIS #504 | 3004527395 |
| PRE-ONGARD WELL #102 | 3004527450 |
| PRE-ONGARD WELL #102 | 3004527466 |
| PRE-ONGARD WELL #103 | 3004527468 |
| PRE-ONGARD WELL #100 | 3004527473 |
| HARPER COM #100 | 3004527515 |
| DAVIS #505 | 3004527526 |
| PRE-ONGARD WELL #105 | 3004527530 |
| PRE-ONGARD WELL #105 | 3004527559 |
| CASE B #021 | 3004527777 |
| EAST #103 | 3004527850 |
| EAST COM #105 | 3004527851 |
| RICHARDSON #102 | 3004527865 |
| PRE-ONGARD WELL #001 | 3004527904 |
| EAST #005M | 3004529646 |
| GRENIER #005B | 3004530000 |
| GRENIER #002B | 3004530007 |
| GRENIER #012M | 3004530117 |
| DAVIS #008R | 3004530417 |
| DAVIS #007F | 3004530437 |
| EAST #007F | 3004530438 |
| DAVIS #005B | 3004530445 |
| EAST #005B | 3004530464 |
| GRENIER #011F | 3004530466 |
| HARPER #002F | 3004530466 |
| DAVIS #505S | 3004530715 |
| EAST #008M | 3004530879 |
| LUNDI #UUOM | 3004330079 |

| EAST #006M | 3004530945 |
|-----------------------|------------|
| EAST #011M | 3004530947 |
| EAST #009M | 3004530948 |
| SARAH M HEDGES #002M | 3004532266 |
| STATE GAS COM M #002 | 3004532661 |
| SARAH M HEDGES #001A | 3004533039 |
| DAVIS #010M | 3004533127 |
| STATE GAS COM BB #003 | 3004533143 |
| DAVIS #013M | 3004533157 |
| DUSENBERRY #002B | 3004533210 |
| CASE A #004M | 3004533466 |
| EAST #020R | 3004533492 |
| DAVIS #501S | 3004533506 |
| GRENIER #102S | 3004533507 |
| ELLIOTT A LS #001M | 3004533612 |
| EAST #013R | 3004533620 |
| RICHARDSON SRC #100 | 3004533721 |
| DAVIS #009F | 3004534094 |
| PATTERSON B COM #001N | 3004534739 |
| RICHARDSON #008N | 3004534873 |
| ELLIOTT A #100 | 3004535199 |
| EAST #006N | 3004535255 |
| EAST #103S | 3004535312 |
| GRENIER #003 | 3004560038 |
| SARAH M HEDGES #001 | 3004560040 |

Half Mile Radius Review Offset Wells:

A two-mile radius review of was conducted of the offset wells of public record as demonstrated in the tabulated table and 2-mile Radius Map. After an extensive review it was determined that the referenced wells will not be affected by the injection into the Morrison and Entrada Formation.









Farmington Daily Times

Affidavit of Publication Ad # 0004843219 This is not an invoice

PATH THREE MARKETING 1508 CHALLEDON DR. SE

ALBUQUERQUE, NM 87123

I, being duly swom say: Farmington Daily Times, a daily newspaper of general circulation published in English at Farmington, said county and state, and that the hereto attached Legal Notice was published in a regular and entire issue of the said DAILY TIMES, a daily newsaper duly qualified for the purpose within the State of New Mexico for publication and appeared in the internet at The Daily Times web site on the following days(s):

07/28/2021

egal Clerk

Subscribed and sworn before me this July 28, 2021:

State of WI, County of Brown NOTARY PUBLIC

PS 1-

My commission expires

KATHLEEN ALLEN Notary Public State of Wisconsin

Ad # 0004843219 PO #: # of Affidavits1 This is not an invoice New Mexico Tech, located at 801 Leroy Place, Socorro, New Mexico 87801, is filing Form C-108 (Application for Authorization to drill a stratigraphic test well) with the New Mexico Oil Conservation Division for administrative approval for its logging, coring, well SJB CarbonSAFE #1. The pro-SĪB posed well will be located at 2236 FNL 1022 FEL Section 14 Township 31N Range 12W in San Juan County, New Mexico. The well will be drilled to 8,800 feet total depth from surface (6,207 surface elevation). feet Petrophysical logs, geophysical logs, cores and water samples will be collected in open and cased hole. Step rate testing (using water) will be performed in the Entrada formation (at depth) of 8,200 feet from surface). The purpose of the data collection is to characterize the subsurface geology of the San Juan Basin. Interested parties opposing the action must file objections or re-quests for hearing with the Oil Conservation Division, 1220 South St. Frances Drive, Santa Fe, New Mexico Santa Fe, New Mexico 87505, within 15 days. Addi-tional information can be obtained from the appli-cant, Dr. William Ampomah, at (575) 835-5018. #4843219, Daily Times, July 28, 2021