

George QJ #10 -- Drainage Area

1. Original Oil in Place (stock-tank barrels) is given by the equation

$$\text{OOIP} = 7758 * A * h * \phi * S_o / B_o i$$

where $h * \phi * S_o$ is the hydrocarbon pore volume.

2. The log calculations for hydrocarbon pore volume yield $h * \phi * S_o = 0.769$.

3. $B_o i = 1.28$ from the Standing Correlations where the parameters are as follows:

Solution GOR	=	600
Temperature	=	110 degrees F
Gas Gravity	=	0.7
Tank Oil Gravity	=	42 degrees API

4. Ultimate Primary Recovery (N_p) = Recovery Factor * OOIP

where Recovery Factor (R_f) = 0.30

Estimated for gas-cap reservoir

5. Then, $N_p = R_f * 7758 * A * h * \phi * S_o / B_o i$

and, by rearranging, $A = N_p * B_o i / (R_f * 7758 * h * \phi * S_o)$ in acres

$$A = 419000 * 1.28 / (0.30 * 7758 * 0.769) \text{ in acres}$$

$A = 300 \text{ acres}$ is the Drainage Area

George QJ #9 -- Drainage Area

1. Original Oil in Place (stock-tank barrels) is given by the equation

$$OOIP = 7758 * A * h * \phi * S_o / B_o i$$

where $h * \phi * S_o$ is the hydrocarbon pore volume.

2. The log calculations for hydrocarbon pore volume yield **$h * \phi * S_o = 1.047$** .

3. **$B_o i = 1.28$** from the Standing Correlations where the parameters are as follows:

Solution GOR	=	600
Temperature	=	110 degrees F
Gas Gravity	=	0.7
Tank Oil Gravity	=	42 degrees API

4. Ultimate Primary Recovery (N_p) = Recovery Factor * OOIP

where Recovery Factor (**R_f**) = **0.30**

Estimated for gas-cap reservoir.

5. Then, $N_p = R_f * 7758 * A * h * \phi * S_o / B_o i$

and, by rearranging, $A = N_p * B_o i / (R_f * 7758 * h * \phi * S_o)$ in acres

$$A = 240000 * 1.28 / (0.30 * 7758 * 1.047) \text{ in acres}$$

A = 126 acres is the Drainage Area

George QJ #2Y -- Drainage Area

1. Original Gas in Place (Scf) is given by the equation

$$\text{OGIP} = 43560 * A * h * \phi * S_g * B_g$$

where $h * \phi * S_g$ is the hydrocarbon pore volume.

2. The log calculations for hydrocarbon pore volume yield $h * \phi * S_g = 0.773$.

3. $B_g = 35.35 * p / (zT)$ in Scf per cubic foot where the parameters are as follows:

Pressure	=	2312 psi	
Temperature	=	110 degrees F	= 570 degrees R
Gas Gravity	=	0.65	
Tc	=	390 degrees R	
Pc	=	667 psi	

$$\begin{array}{lcl} \text{Then } Tr & = & (460+110)/390 = 1.46 \\ Pr & = & 2312/667 = 3.47 \end{array}$$

$$\text{And } z = 0.74$$

$$\text{So } B_g = 35.35 * 2312 / (0.74 * 570) = 194 \text{ Scf/cubic foot}$$

4. Ultimate Recovery (Gp) = Recovery Factor * OGIP

$$\text{where Recovery Factor (Rf)} = 0.80$$

5. Then, $G_p = R_f * 43560 * A * h * \phi * S_g * B_g$

and, by rearranging, $A = G_p / (R_f * 43560 * h * \phi * S_g * B_g)$ in acres

$$A = 0.722 * 10^9 / (0.8 * 43560 * 0.773 * 194) \text{ in acres}$$

$$A = 138 \text{ acres is the Drainage Area}$$

Powers OL #6 -- Drainage Area

1. Original Gas in Place (Scf) is given by the equation

$$\text{OGIP} = 43560 * A * h * \phi * S_g * B_g$$

where $h * \phi * S_g$ is the hydrocarbon pore volume.

2. The log calculations for hydrocarbon pore volume yield **$h * \phi * S_g = 0.344$** .

3. **$B_g = 35.35 * p / (zT)$** in Scf per cubic foot where the parameters are as follows:

Pressure	=	2312 psi		
Temperature	=	110 degrees F	=	570 degrees R
Gas Gravity	=	0.65		
Tc	=	390 degrees R		
Pc	=	667 psi		

Then	Tr	=	(460+110)/390	=	1.46
	Pr	=	2312/667	=	3.47

And	z	=	0.74
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So $B_g = 35.35 * 2312 / (0.74 * 570) = \mathbf{194 \text{ Scf/cubic foot}}$

4. Ultimate Recovery (Gp) = Recovery Factor * OGIP

where Recovery Factor (**Rf**) = **0.80**

5. Then, $G_p = R_f * 43560 * A * h * \phi * S_g * B_g$

and, by rearranging, $A = G_p / (R_f * 43560 * h * \phi * S_g * B_g)$ in acres

$$A = 0.195 * 10^9 / (0.8 * 43560 * 0.344 * 194) \text{ in acres}$$

$$\mathbf{A = 84 \text{ acres}}$$
 is the Drainage Area