

CHEMICAL ENGINEERING GROUP WATER ANALYSIS REPORT

PN 3-60-63

To: T. O. Davis, File

Date Collected: 3-18, 19 Date Rec'd: 3-21-60 Date Rep'd: 3-23-60 Lab. No. 15,901
Source of Sample: Wellhead, Navajo B #1-W, HORSESHOE-GALLUP FLD., San Juan Co., New Mexico
CHEMICAL ANALYSIS

CONSTITUENTS	Mg. Liter	CONSTITUENTS	Mg. Liter	CONSTITUENTS	Mg. Liter
1. Total Solids	7,615	6. Calcium	192	11. Sulfates	4,570
2 pH	7.9	7. Magnesium	32	12. Carbonates	0
3 Sp. Grav. 60 F.	1.006	8. Iron 4 as Fe (6.7 FeS)		13. H ₂ S	0
4 Res. 68 F.		9. Chlorides	300	14. Hydroxide Ba	0
5 Sodium	2,215	10. Bicarbonates	305		
Pattern Code	A9A9AoAo: AoB5J5Ao				

INTERPRETATION

PROBLEM:

CONCLUSION:

REMARKS:

ATLANTIC COST \$14.74

COMMERCIAL COST \$ 28.00

AUTHORIZED BY T.O. Davis

CHARGE TO Navajo B #1-W

Approved by

HENRY LEWELLING

Reported by

MONTE KAPLAN

Na
100

Ca
10

Mg
10

Fe
10

Na

Ca

Mg

Fe

Cl
100

HCO₃
10

SO₄
10

CO₃
10

Cl

HCO₃

SO₄

CO₃

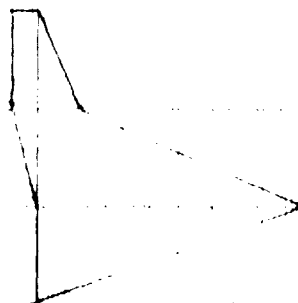


Exhibit D

Office of the State Engineer
P.O. Office Box 1079
Santa Fe, New Mexico

Re: Application;

In compliance with the New Mexico Oil Conservation Commissions' Memorandum No. 5-98, dated January 31, 1958. The Atlantic Refining Company is furnishing the following information:

1. Copy of our application to waterflood the Atlantic Navajo and Navajo 'B' Leases in the Horseshoe-Gallup Oil Pool, San Juan County, New Mexico.
2. The water source will be the Atlantic Navajo 'B' No. 1-2 well located in the Horseshoe-Gallup Field in the SW¹/₄ of Section 19 - T31N - R16W, San Juan County, New Mexico, and other wells in the project area if necessary.
3. The water will be produced from the Morrison formation which occurs between 2106 feet and 2802 feet in the Atlantic Navajo 'B' No. 1-2.
4. A copy of a water analysis is enclosed.

ILLEGIBLE

LARGE FORMAT
EXHIBIT HAS
BEEN REMOVED
AND IS LOCATED
IN THE NEXT FILE

EXHIBIT "C"

DESCRIPTION OF CASING PROGRAM OF INJECTION WELLSTHE ATLANTIC REFINING COMPANY APPLICATION FOR AN ORDERAUTHORIZING WATER INJECTION ON ITS NAVAJO AND NAVAJO "B" LEASES

<u>Lease and Well Number</u>	<u>Surface Casing</u>			<u>Producing Casing</u>			<u>Well Locations</u>	
	<u>Size</u>	<u>Setting Depth</u>	<u>Cement Sacks</u>	<u>Size</u>	<u>Setting Depth</u>	<u>Cement Sacks</u>	<u>Unit</u>	<u>Section</u>
Navajo 9	8 5/8	102.07	125	5 1/2	1446.72	135	B	30
16	8 5/8	100.90	115	5 1/2	1300.73	130	H	31
17	8 5/8	98.80	115	5 1/2	1286.00	130	B	31
22	8 5/8	98.97	115	5 1/2	1362.52	130	J	29
23	8 5/8	103.64	115	5 1/2	1379.01	130	F	29
24	8 5/8	95.70	115	4 1/2	1409.82	160	D	29
26	8 5/8	99.75	115	4 1/2	1347.09	190	B	29
28	8 5/8	94.26	115	4 1/2	1306.25	150	J	31
29	8 5/8	101.49	115	5 1/2	1366.00	130	F	31
Navajo "B" 1	8 5/8	102.06	115	5 1/2	1577.21	150	N	19
3	8 5/8	103.65	115	4 1/2	1446.21	180	P	19
4	8 5/8	97.47	115	4 1/2	1474.27	190	J	19
5	8 5/8	98.05	115	4 1/2	1487.72	195	F	19
7	8 5/8	98.03	115	4 1/2	1513.40	225	N	20
8	8 5/8	100.09	100	4 1/2	1588.24	150	L	20

OIL CONSERVATION COMMISSION
SANTA FE, NEW MEXICO

Date 6-2-60

CASE 1979

Hearing Date 6-1-60

My recommendations for an order in the above numbered cases are as follows:

1. Grant Atlantic request for a secondary recovery project in the Horseshoe Valley oil Pool.

2. Unit area to consist:

31 N-16 W

Sec. 18, S/2 SW/4

" 19, W/2, W/2 E/2, SE/4 NE/4, E/2 SE/4.

" 20, S/2, S/2 NW/4, SW/4 NE/4.

" 29, All

" 30, All

" 31, E/2, E/2 W/2, NW/4 SW/4, W/2 NW/4

" 32 All

Balance of Recommendation attached

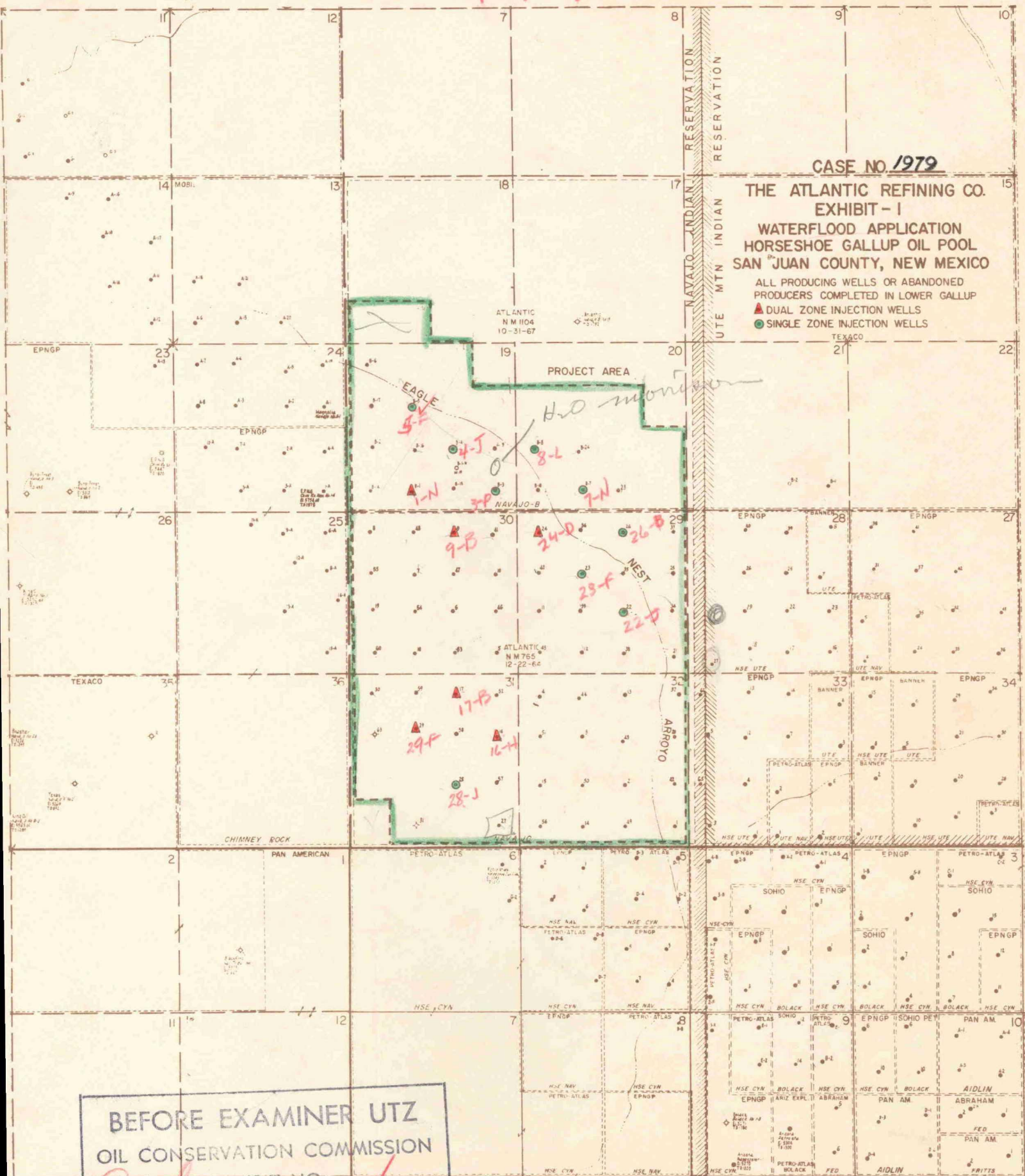
[Signature]

T31 N, R16 W

CASE NO. 1979

THE ATLANTIC REFINING CO.
EXHIBIT - I
WATERFLOOD APPLICATION
HORSESHOE GALLUP OIL POOL
SAN JUAN COUNTY, NEW MEXICO

ALL PRODUCING WELLS OR ABANDONED
PRODUCERS COMPLETED IN LOWER GALLUP
▲ DUAL ZONE INJECTION WELLS
● SINGLE ZONE INJECTION WELLS



BEFORE EXAMINER UTZ
OIL CONSERVATION COMMISSION

EXHIBIT NO. 1

CASE NO. 1979

PROPOSED GAS EQUIVALENT CREDIT FOR WATER INJECTION

HORSESHOE-GALLUP OIL POOL, SAN JUAN COUNTY, NEW MEXICO

RULE 7. Credit for daily average net water injected into the Horseshoe-Gallup Oil Pool through any injection well located within the project area may be converted to its gas equivalent and applied to any well producing with a gas-oil ratio in excess of two thousand cubic feet of gas per barrel of oil. Total credit for net water injected in the project area shall be the gas equivalent volume of the daily average net water injected during a one-month period. The daily average gas equivalent of net water injected shall be computed in accordance with the following formula:

$$E_g = (V_w \text{ inj} - V_w \text{ prod}) \times 5.61 \times \frac{P_a}{15.025} \times \frac{520^\circ}{T} \times \frac{1}{Z}$$

where:

E_g = Average daily gas equivalent of net water injected, cubic feet

$V_w \text{ inj}$ = Average daily volume of water injected, barrels

$V_w \text{ prod}$ = Average daily volume of water produced, barrels

5.61 = Cubic foot equivalent of one barrel of water

P_a = Average reservoir pressure at mid-point of the pay-zones of the Horseshoe-Gallup Oil Pool in project area, psig + 12.05 as determined from most recent survey.

15.025 = Pressure base, psi

520° = Temperature base of 60°F expressed as absolute temperature

T_s = Reservoir temperature of 87°F expressed as absolute temperature

Z = Compressibility factor from analysis of Horseshoe-Gallup gas at average reservoir pressure, P_a , interpolated from compressibility tabulation below:

Reservoir Pressure	Z	Reservoir Pressure	Z
50	.9725	450	.7220
100	.9465	500	.6900
150	.9215	550	.6560
200	.8885	600	.6135
250	.8600	650	.5655
300	.8325	700	.5220
350	.8030	750	.4630
400	.7710	800	.3935

400,000 stock tank barrels per month can be maintained for about nine years. At that time, the oil productivity declines because of the increasing amounts of water being produced.

Water Source

The Dakota formation should provide an ample supply of water for waterflood purposes. Atlantic drilled the Navajo #45 well through the Dakota formation to a total depth of 2078 feet. The Dakota sand was topped at 1816 feet and extended to 2063 feet with a few shale breaks. Two cores were cut (1846 to 1896 and 1989 to 2039) and two drill stem tests were taken. From 61 feet of analyzed core, 44 feet had an average air permeability of 167 mds. Results of the two DST's are tabulated below:

Test No.	Depth		Flow Period	Shut-In Period	Recovery	Flow Pressures	Final Shut-in Pressure
	From	To					
1	1849	1896	90 min.	30 min.	1585' water	119-701	745
2	1992	2039	90 min.	30 min.	1762' water	299-806	809

Analysis of the water recovered in DST #1 showed 4,996 ppm. total solids with a pH of 7.0. The solids constituents were as follows:

Sodium	1578 ppm
Calcium	24 ppm
Magnesium	1 ppm
Iron	0 ppm
Barium	0 ppm
Chloride	284 ppm
Bicarbonate	625 ppm
Sulfate	2484 ppm
Carbonate	0 ppm
Hydroxide	0 ppm

The Dakota sands are expected to be well developed in all areas of the field so water source wells could be located where they would be most convenient.

HORSESHOE-GALLUP FIELD STUDY

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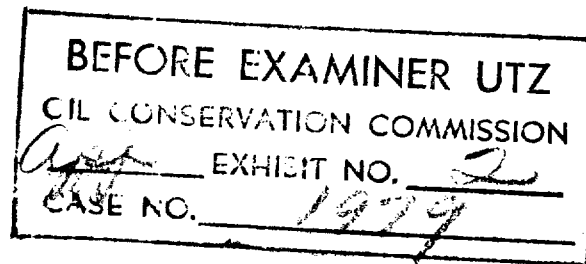
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HORSESHOE GALLUP FIELD
SAN JUAN COUNTY, NEW MEXICO

WATERFLOOD STUDY
UPPER AND LOWER TOCITO



THE ATLANTIC REFINING COMPANY

HORSESHOE GALLUP FIELD
SAN JUAN COUNTY, NEW MEXICO

WATERFLOOD STUDY
UPPER AND LOWER TOCITO

THE ATLANTIC REFINING COMPANY

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S U M M A R Y

INTRODUCTION

Since early in the life of the Horseshoe-Gallup Field it has been apparent that the normal producing mechanism will be solution-gas drive and that some form of fluid injection would be needed to maintain producing rates and increase recovery. A review of various fluid injection processes indicated that water injection would be the best. Low pressure gas injection is inefficient and the low reservoir pressure and shallow producing depths preclude use of miscible fluid injection, including high pressure gas injection. Accordingly, this report assembles reservoir data on the field, predicts the primary recovery performance, and shows the gain that will result from pressure maintenance by water injection. The calculated performance of an average 80-acre five-spot flood pattern is shown.

In this study, the extreme northwest extension of the field (north of Section 15, T-31-N, R-17-W) was not included.

CONCLUSIONS

The following conclusions are drawn from this study:

1. Primary oil recovery will be small--being approximately 12.3% of the oil in-place or 95 barrels per acre-foot.
2. Primary producing rates are beginning to decline. The rate of decline will increase sharply by the end of 1960.
3. Waterflooding will increase ultimate recovery to 51% of the total oil in-place or to 392 barrels per acre-foot.
4. An adequate source of water for flooding is probably available from the Dakota formation.

RECOMMENDATIONS

1. Waterflood operations should be started immediately in the field.
2. The operators should work out a cooperative plan for location of injection and producing wells.

DISCUSSION

FIELD BACKGROUND

Location

The Horseshoe-Gallup Field is located in San Juan County, New Mexico, approximately twenty miles west and about eight miles north of the town of Farmington, New Mexico.

Discovery

The field was discovered June 22, 1957 by the Arizona Explorations, Inc., Horseshoe Canyon "B" #1 well located in the NW/4 NW/4, Section 3, Township 30 North, Range 16 West, San Juan County, New Mexico. This well was drilled to a total depth of 1780' and had an initial potential of 120 BPD of 42° gravity oil.

Geology

The Horseshoe-Gallup Field is located in the southwestern part of the San Juan Basin. The oil reservoir trends northwest and southeast and is a stratigraphic trap approximately thirteen miles long and up to three miles wide. The Lower Gallup sandstone formation ranges in depth from about 800 feet at its northwestern end to about 5200 feet at the southeastern end. A structure map contoured on the Gallup sandstone (except for the extreme northwest end of the field) is shown on Page 1 of the Tables and Figures Section of this report. Its productive interval is composed of two sand sections known as the Upper and Lower Tocito. These sands are shown on longitudinal cross section A-A', page 2. The trace of this cross section is shown on the structure map. The average net thickness of the combined Upper and Lower Tocito is 17.8 feet and the average porosity is 16.1%. The two sands are continuous, however, the Upper Tocito changes into a shale in the northwestern part of the field and is not present as a pay zone. On the other hand, the Lower Tocito is not as wide, laterally, as the Upper Tocito.

RESERVOIR PROPERTIES

Summary

The following table lists average reservoir properties of the Tocito zones in the Horseshoe-Gallup Field determined from available geological, core, and PVT data:

Porosity (%)	16.1
Permeability, md. (md.) <i>Liquid</i>	82
Connate Water (%)	32.4
Initial Pressure (psig at +4175 datum)	215
Saturation Pressure (psig at +4175')	215
Reservoir Temperature (°F)	87
Area (developed acres)	10,200
Spacing (acres/well)	40
Number of wells (Aug. 1959)	234
Average Net Pay (Lower plus Upper Tocito) (ft.)	17.8
Original Oil in-place (bbls/ac.ft.)	770

Core Data

Analyses run on diamond cores taken in 45 wells were available. Thirty of these wells were on Atlantic's Navajo "A" and "B" leases. There were 398 core samples from the Upper Tocito whose permeability was 1 md. or greater. From the Lower Tocito, 345 samples had a permeability of 1 md. or greater. Four hundred and sixty-five Upper Tocito samples and 478 Lower Tocito samples had porosity values of 12% or greater.

The available core data were punched onto IBM cards for sorting, arranging in order of ascending permeability and porosity, and printing. Using permeabilities of 1 md., or above, graphs of air permeability versus per cent of total samples were constructed for the Upper and Lower Tocito, pages 9 and 10. These plots were

divided into five equal groups (based on number of samples) and average permeability determined for each group. With this average permeability and Atlantic's restored-state data, an average water saturation was determined for each of the five groups.

Porosity distribution curves (pages 13 and 14) were drawn in the same manner as the permeability distribution curves but using porosities of 12%, or above. The 12% porosity value corresponds approximately to 1 md. permeability. These plots were also divided into five equal groups based on number of samples and average porosity determined for each of the groups. With each group's respective average porosity and water saturation, an effective oil porosity was calculated for each group. This effective porosity versus per cent of total number of samples is shown on pages 15 and 16.

From the effective porosity distribution curves, the average effective oil porosity--porosity $\times$ (1 - connate water saturation)--of the Upper and Lower Tocito was determined to be 10.8% and 11.0%, respectively.

Fluid Properties

Atlantic obtained a bottom hole fluid sample from their Navajo #5 well on August 13, 1959. In order to obtain a sample representative of both the Upper and Lower Tocito zones, it was collected above the Upper zone at which point the pressure in the well bore was 150 pounds. The PVT study was run showing a 150# psi saturation pressure; however, to make this data compatible with actual reservoir conditions, the curves were extrapolated to 215 psi, the initial reservoir pressure. The formation volume factor, gas solubility, gas conversion factor, and oil viscosity versus pressure plots are shown as pages 5, 6, 7, and 8. The fluid properties are summarized on page 4.

Relative Permeability

Atlantic's Chemical Engineering Laboratory ran k_g/k_o curves on nine selected plugs from the Upper and Lower Tocito whose permeability corresponded to each of the five sample groups discussed in the Core Data Section. These curves were then

combined at equal flowing gas-oil ratios or at equal k_g/k_o 's. The curves for the Upper and Lower Tocito were so similar that only one curve was drawn. The average k_g/k_o versus effective oil saturation curve is shown on page 18. Pages 19 through 27 are the individual k_g/k_o curves plotted versus oil saturation. Page 17 is a relative permeability data summary.

PRIMARY PERFORMANCE

Since the field is limited around practically all its perimeter by lack of porous producing formation, solution gas drive will be the predominant producing mechanism. No water-oil contact has yet been found and, if one exists, it will not contribute to recovery in any significant degree. With the average relative permeability curve and the PVT data previously described, a solution gas drive performance calculation was run using the IBM 650 computer. The results of this calculation are shown on page 29. Under natural depletion, 12.3% of the initial oil in-place will be recovered to a 35 psig reservoir abandonment pressure, which corresponds to an economic limit of about 3 BOPD. This results in 95 barrels per acre-foot recovery by primary means out of 770 barrels per acre-foot originally in place.

Productivity index decline calculations were also run on the IBM 650 computer, the results of which are shown on page 31. Using these P.I. decline results, the field's future producing rates were predicted and are shown on page 30. This curve shows that the rate will decline slowly until late in 1960, after which the rate will drop rapidly.

Past performance of the Horseshoe-Gallup oil pool is shown on page 34. Development drilling is nearly complete with the limits of the pool almost completely defined.

WATERFLOOD PERFORMANCE

Approach

Examination of the core properties previously discussed shows a wide variation in permeabilities and porosities in the Upper and Lower Tocito sands which will cause the waterflood front to advance in a non-uniform manner. In order to calculate quantitatively the advance of the flood front, we have treated the reservoir as a system of parallel, separate, uniform layers each of which have different permeabilities, porosities, and residual oil values. The procedure involves the following steps:

- (1) The core properties (permeability and porosity) were arranged in ascending order as shown on pages 9, 10, 13, and 14.
- (2) The reservoir was arbitrarily divided into five layers of uniform thickness. Core properties were assigned to these layers according to the per cent incidence shown on the above mentioned figures.
- (3) Performances based on the core properties were calculated and averaged to obtain an average performance of each layer.
- (4) The total reservoir performance was determined by summing the average behavior of individual layer performances.

Several assumptions were made to facilitate this calculation. These are that (1) the reservoir is repressured and is operating under a constant pressure drop from injection wells to producing wells, (2) there is no cross-flow between layers, and (3) there is no flow of oil behind the waterflood front in any of the layers. The last assumption is consistent with laboratory observations of waterflood performance of water wet reservoirs. Based on the laboratory flooding tests of fresh cores taken from the Horseshoe-Gallup Field, it was concluded that the reservoir is water wet. Page 28 presents the results of the fresh core waterfloods.

Flood Pattern

The choice of the flooding pattern is dependent on several factors. These are (1) the mobility ratio (this is the mobility of the water divided by the mobility of the oil), (2) the permeability of the reservoir, (3) field oil rate (capacity or allowable control). From the fluid and rock properties, a mobility ratio equal to one was calculated. This means that both water and oil have the same ease of movement in the reservoir. As a result, one injection well can supply enough water to support one producing well. This situation describes a five-spot development.

The second factor which must be examined in choosing a pattern is the permeability of the formation. The higher the permeability, the higher will be the total number of barrels of water that can be injected per day and the higher will be the resulting oil rate. The five-spot pattern gives the maximum throughput rate for a one to one mobility ratio situation. This leads into the third consideration which is the oil rate.

If the Horseshoe-Gallup Field were to be produced at capacity, the optimum pattern to support that rate would be the five-spot. However, in view of the probable restriction of the field oil rate below capacity, a variation from the five-spot pattern can be used in flooding the field. In the center areas of the field where injection capacities are high, fewer injection wells are needed to support the oil rate. In this area a nine-spot pattern (three producing wells per one injection well) or a peripheral type pattern might be used. The edges of the field have lower permeabilities and thicknesses and, here, a five-spot pattern is required to support the oil rate.

Throughput Rate

Throughput rate can be defined as a steady state total rate (oil plus water) which can be produced from a particular well pattern by imposing a given pressure drop. In magnitude, it is equal to the pressure drop across the system divided

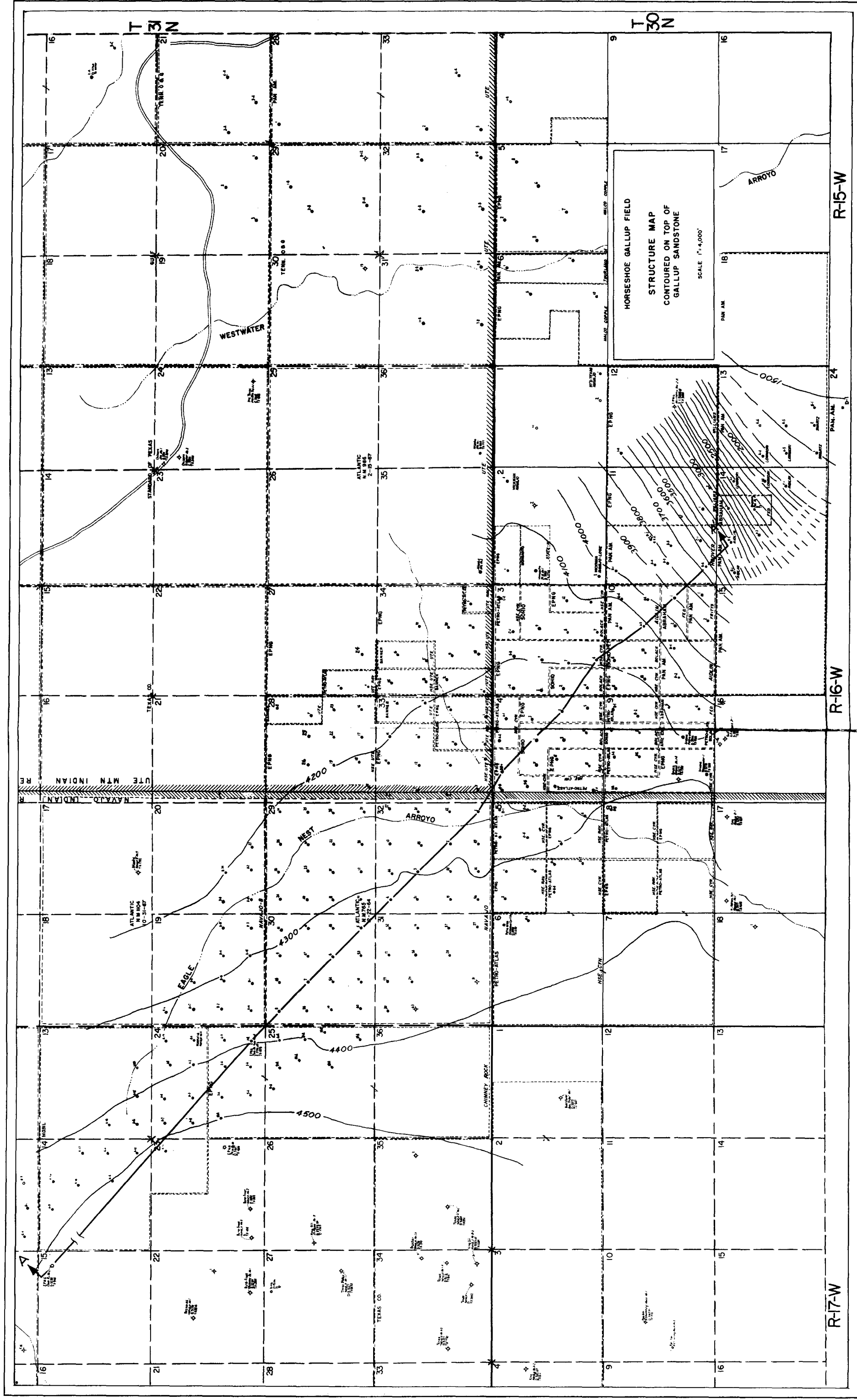
by the total resistance of the system. To determine the maximum capacity rate, a pressure drop of 1180 psi was used based on the assumptions of 1200 psi bottom hole injection pressure (less than formation breakdown) and 20 psi bottom hole producing pressure. Since the mobility of the water is equal to the mobility of the oil, the throughput rate is constant after fill-up. The steady state throughput rate after fill-up was calculated by the use of an equation for the five-spot developed by Morris Muskat.

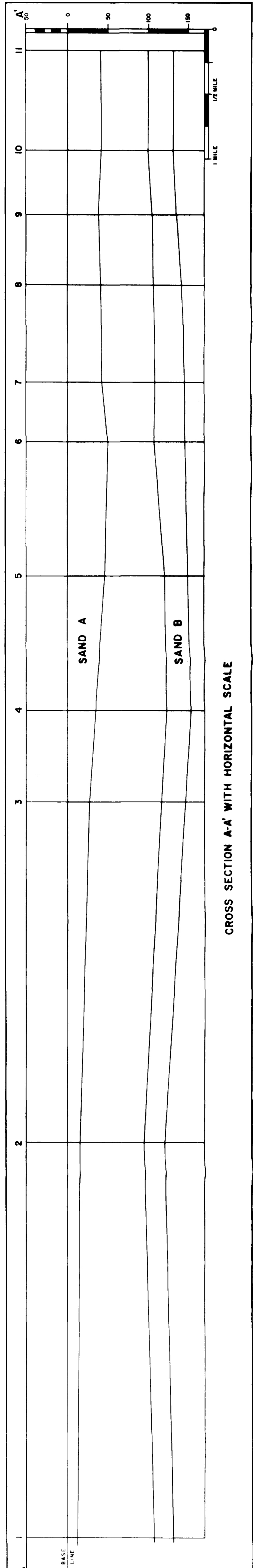
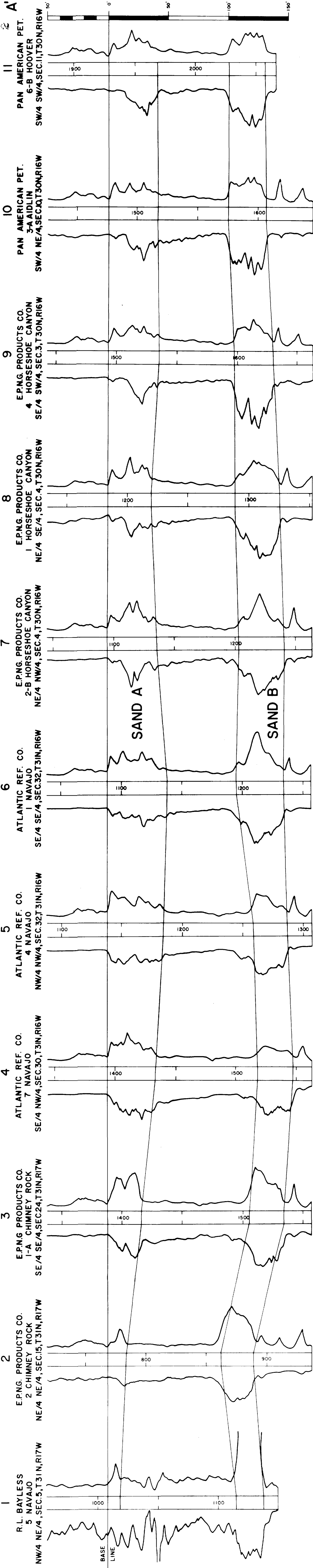
Typical Performance

To obtain the over-all performance, the volumes injected and produced were added at a given time to produce the over-all performance. Page 33 shows the performance of a typical five-spot area. The over-all properties of this five-spot are the same as those listed under the section entitled "Reservoir Properties - Summary." The graph on page 33 shows that the typical 80-acre five-spot will produce about 490,000 stock tank barrels of oil in 15 years. In order to produce this amount of oil, 2.3 million barrels of water must be injected, and 1.6 million barrels of water will be produced.

The waterflood results are summarized on page 32. On an acre-foot basis, primary recovery is estimated to be 95 bbl/acre-foot. The total recovery estimated from primary plus waterflood is 392 bbls/acre-foot which amounts to 51% of the initial oil in-place.

Page 30 shows the results of the five-spot flooding performance (which gives approximately the same results as using five-spots in combination with nine-spots) applied to the field as a whole compared to the primary field performance. As shown, the increase in oil rate to 400,000 barrels per month occurs rapidly. By starting the waterflood early in the field life, there is little gas space to fill up (the initial gas saturation is estimated to be 4.8 per cent of the pore volume when flooding operations begin). Our calculations show that the rate of about





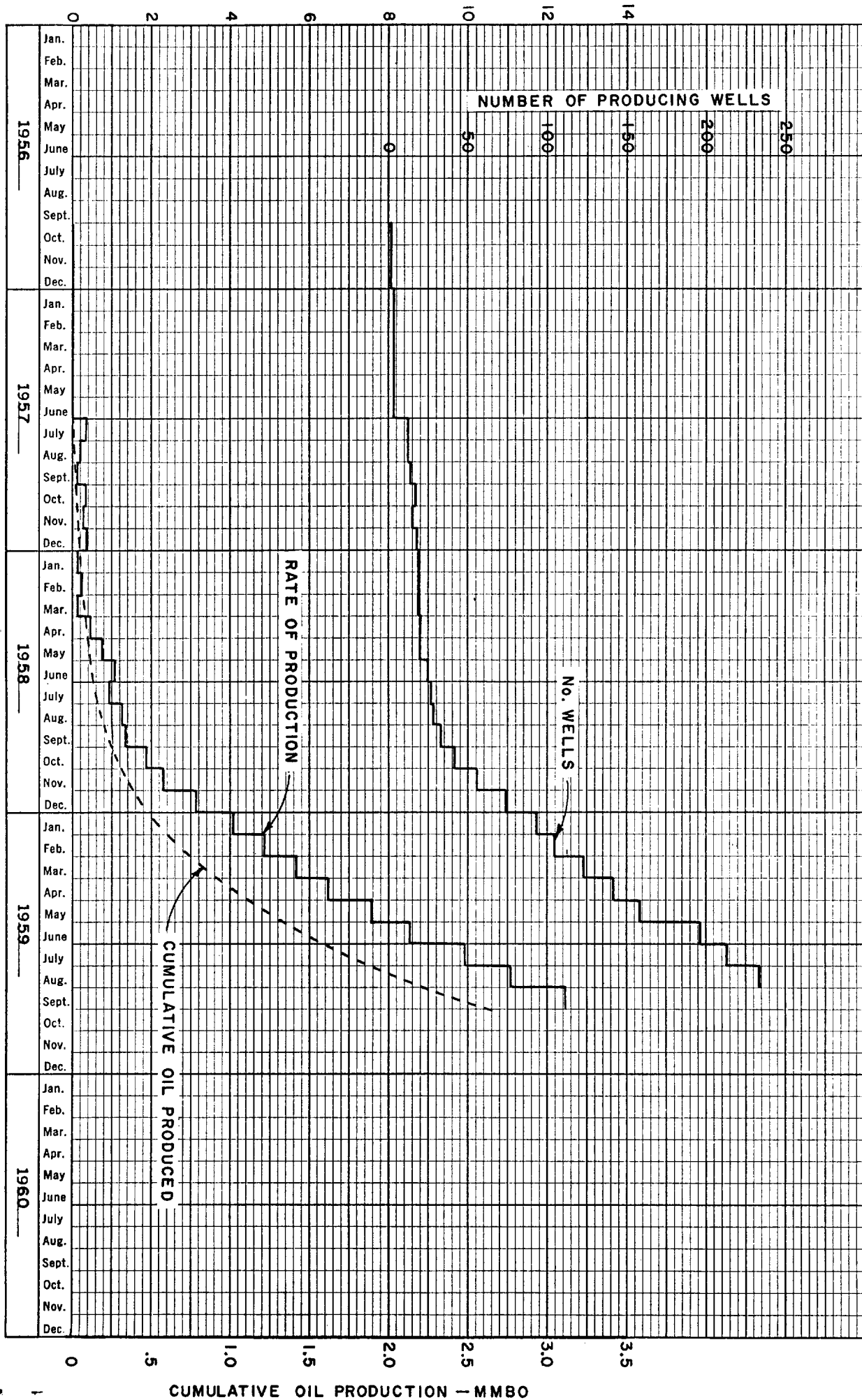
LONGITUDINAL CROSS-SECTION A-A'

(REPRODUCED FROM EL PASO EXHIBIT NO. 5, CASE NO. 1596,
PRESENTED TO N.M.O.C.C. FEB. 4, 1959)

HORSESHOE GALLUP FIELD

SAN JUAN COUNTY, NEW MEXICO

PERFORMANCE HISTORY HORSESHOE GALLUP OIL FIELD UPPER AND LOWER TOCITO



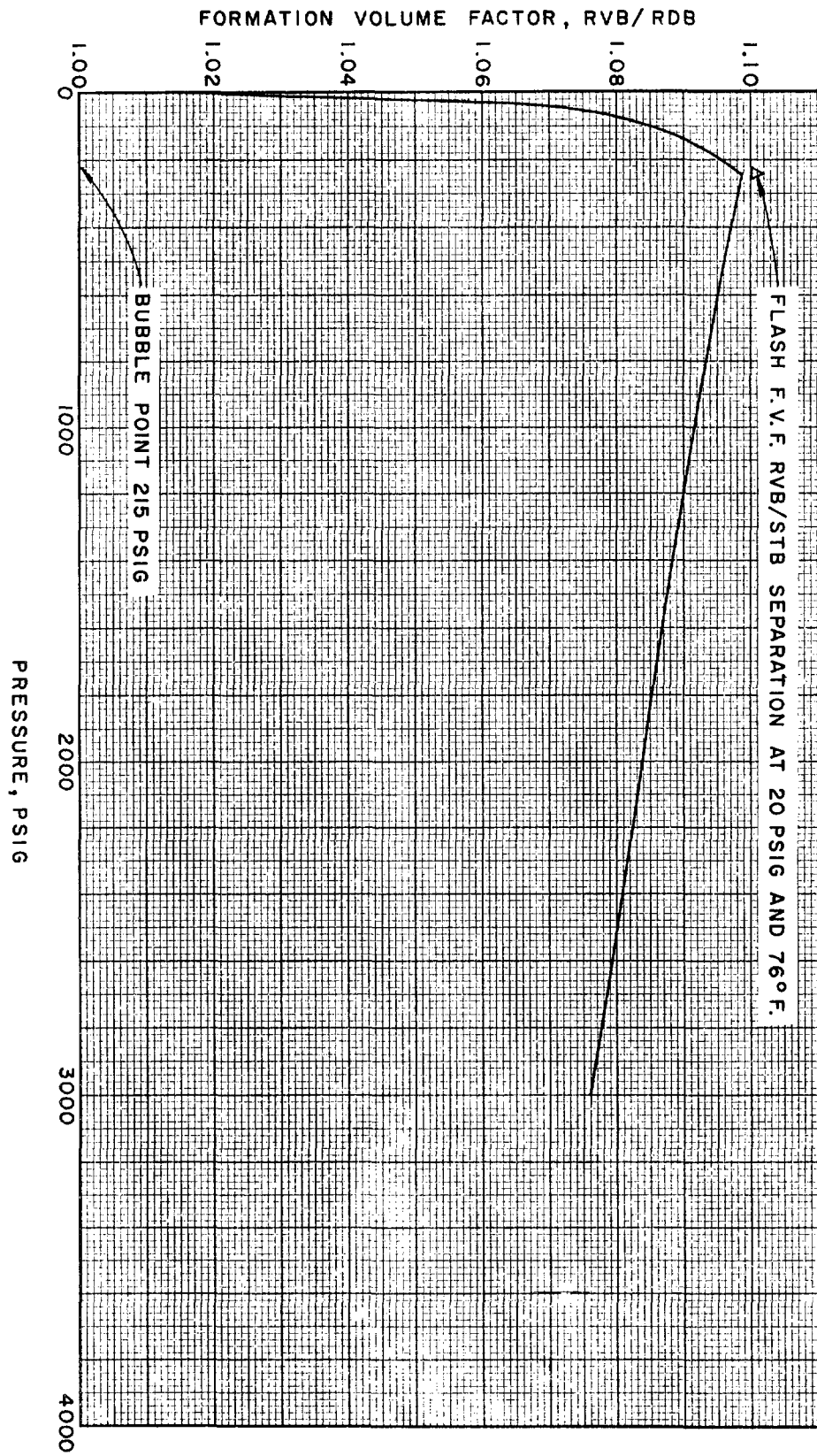
HORSESHOE-GALLUP FIELD

SUMMARY OF FLUID PROPERTIES

Original Reservoir Pressure	215 psig at +4175 datum
Saturation Pressure	215 psig at + 4175 datum
Reservoir Temperature	87 °F
Solution Gas-Oil Ratio	147 SCF/STB
Formation Volume Factor at 215 psig	1.10 rvb/STB
Crude Oil Gravity at 60 °F	42 °API
Oil Viscosity at 215 psig and 87 °F	1.63 cp.
Water Viscosity at 87 °F	0.88 cp.
Oil Compressibility at 87 °F	7×10^{-6} vol/vol/psi slightly above bubble point
	4.6×10^{-3} vol/vol/psi slightly below bubble point

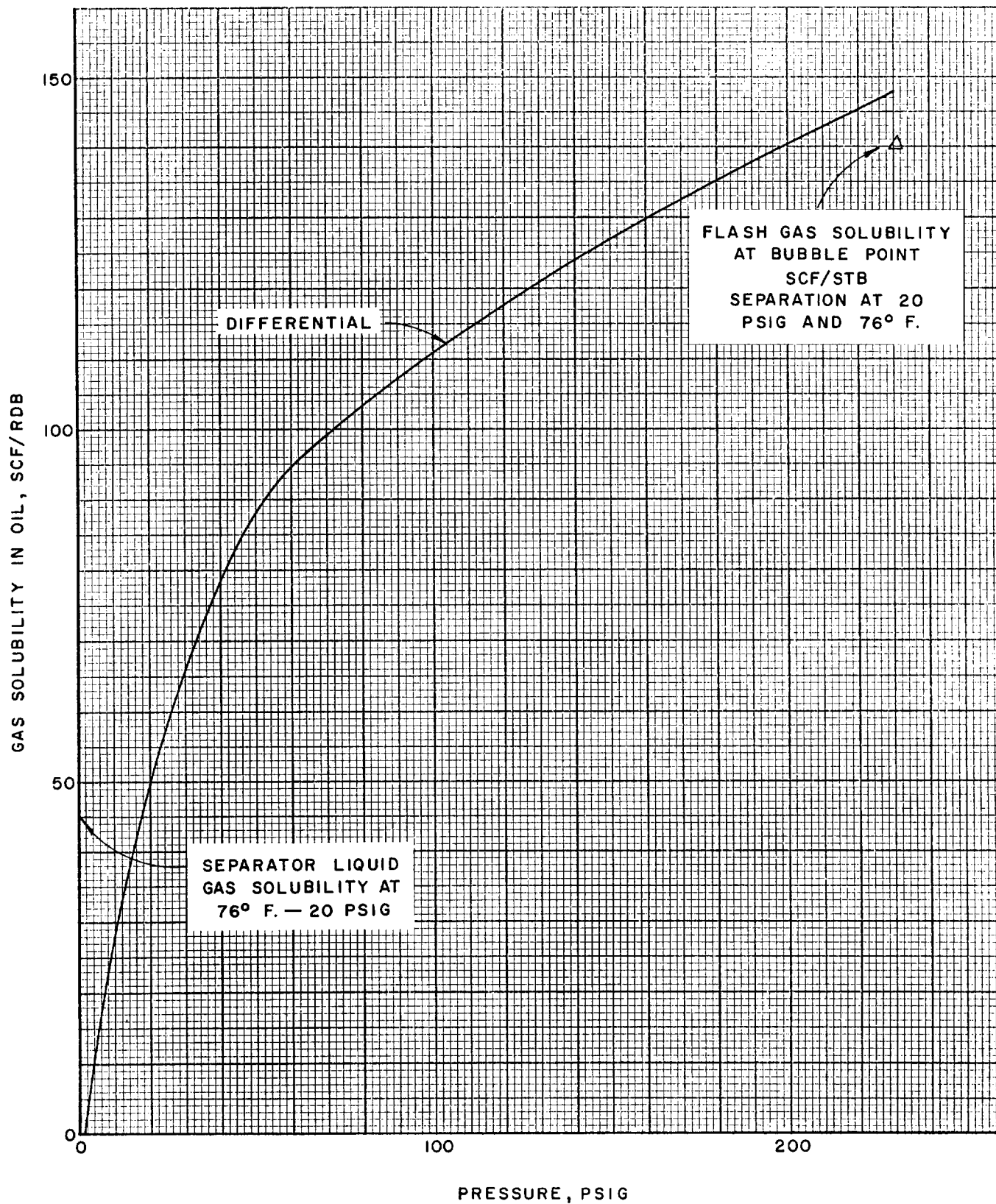
FORMATION VOLUME FACTORS

NAVAJO Nº 5 WELL
GALLUP SAND
HORSESHOE - GALLUP FIELD
SAN JUAN COUNTY, NEW MEXICO



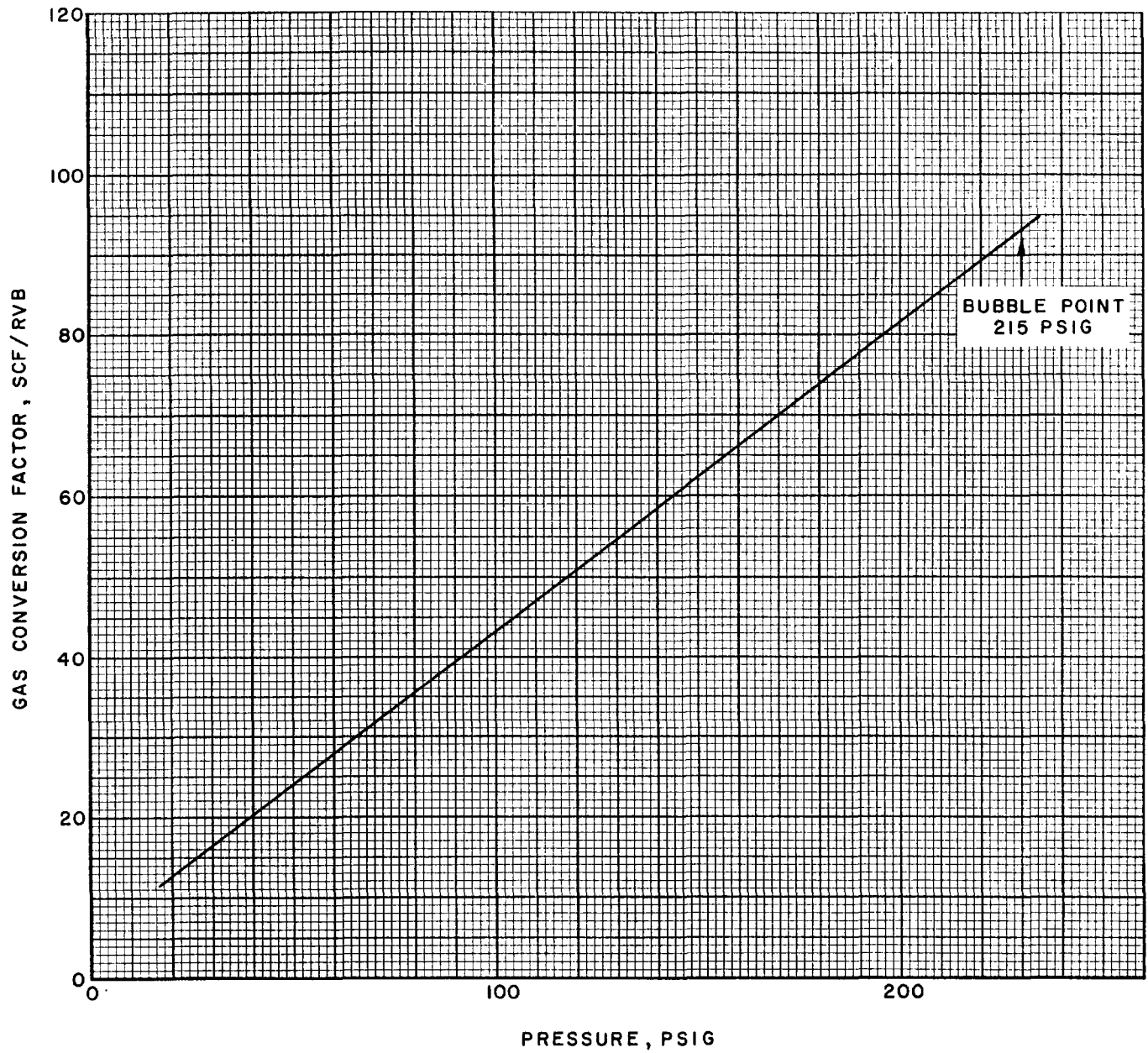
TOTAL SOLUTION GAS SOLUBILITIES AND GAS SOLUBILITY IN SEPARATOR LIQUID

NAVAJO NO 5 WELL
GALLUP SAND
HORSESHOE - GALLUP FIELD
SAN JUAN COUNTY, NEW MEXICO



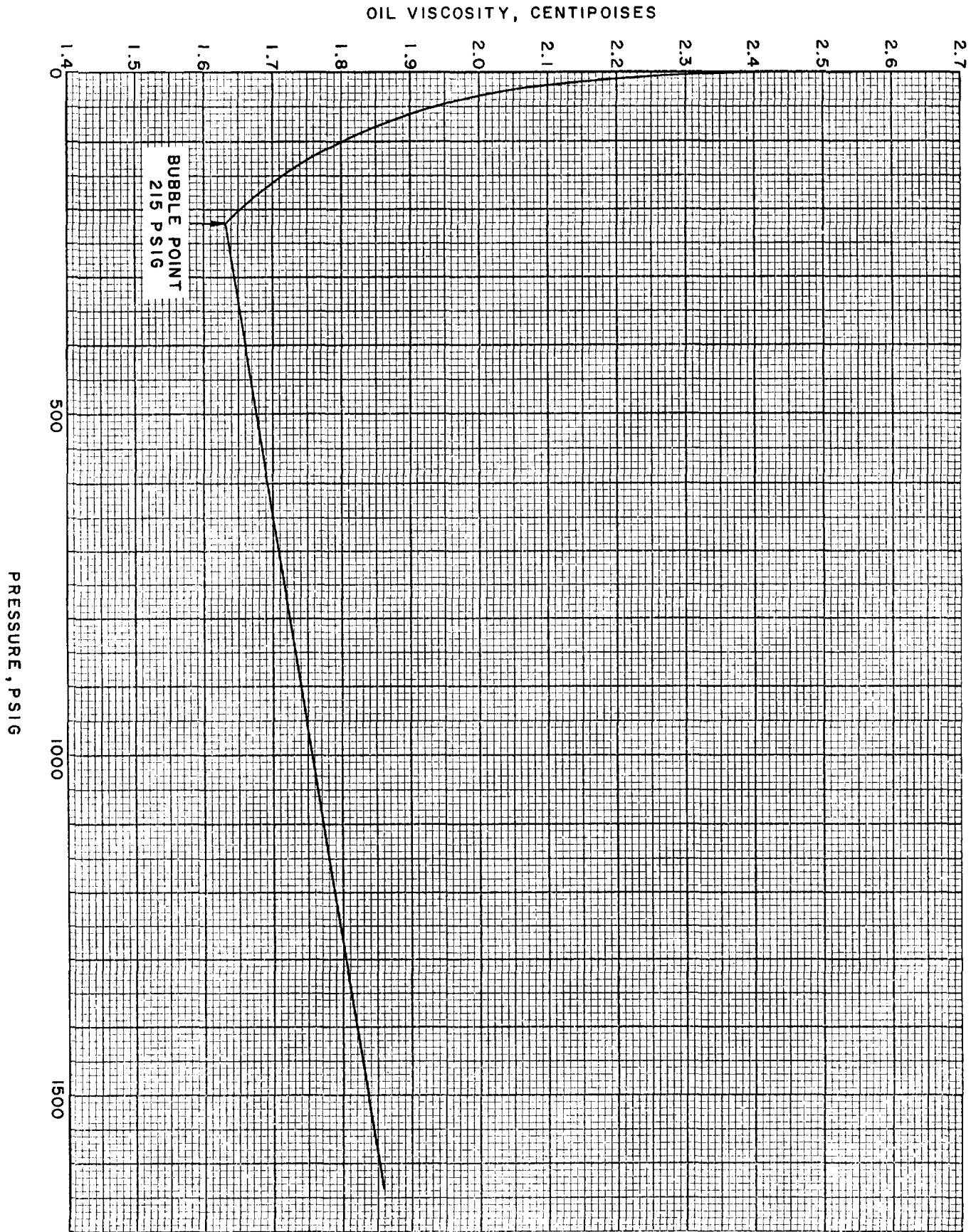
GAS CONVERSION FACTOR

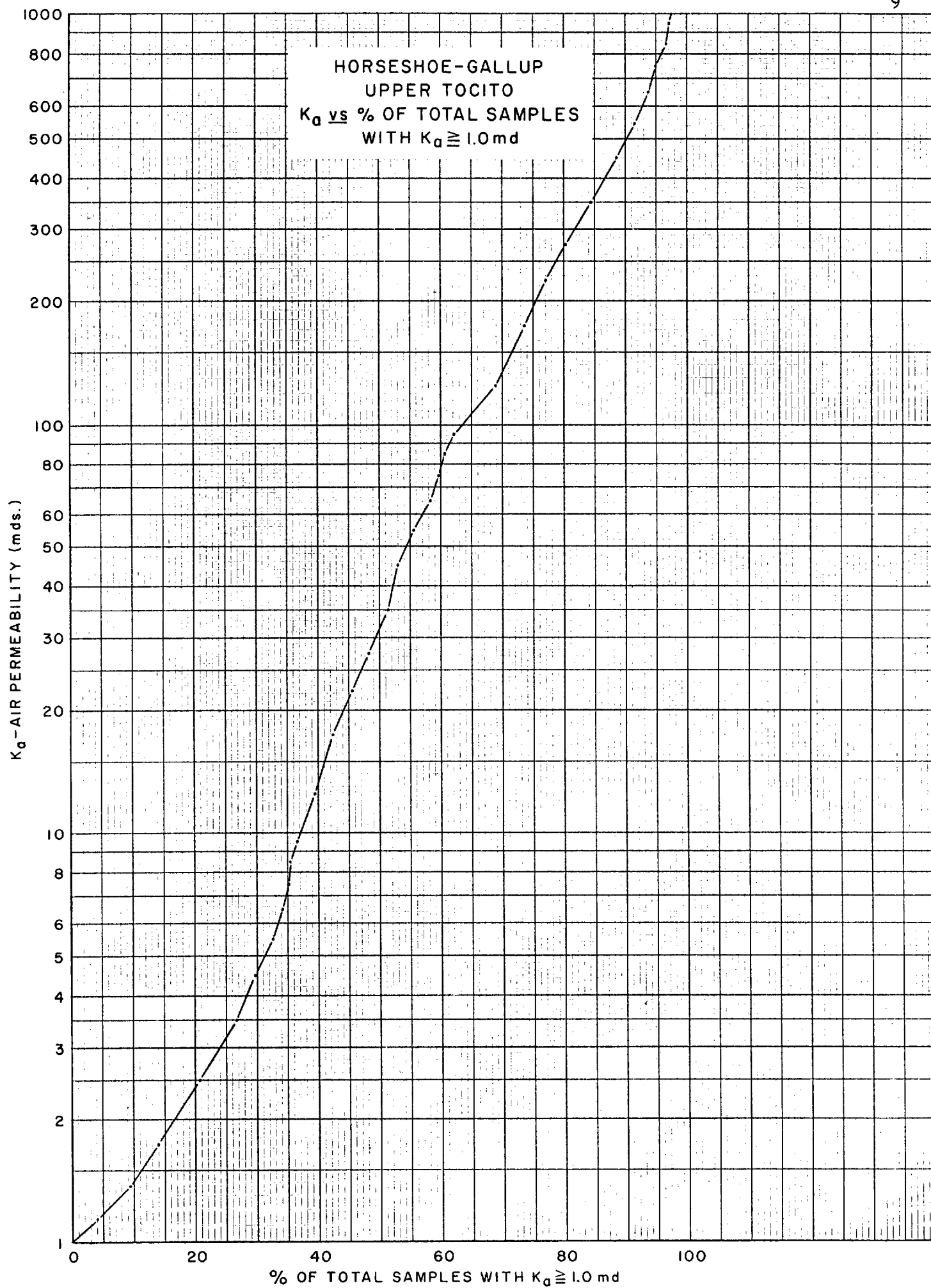
NAVAJO NO 5 WELL
GALLUP SAND
HORSESHOE - GALLUP FIELD
SAN JUAN COUNTY, NEW MEXICO

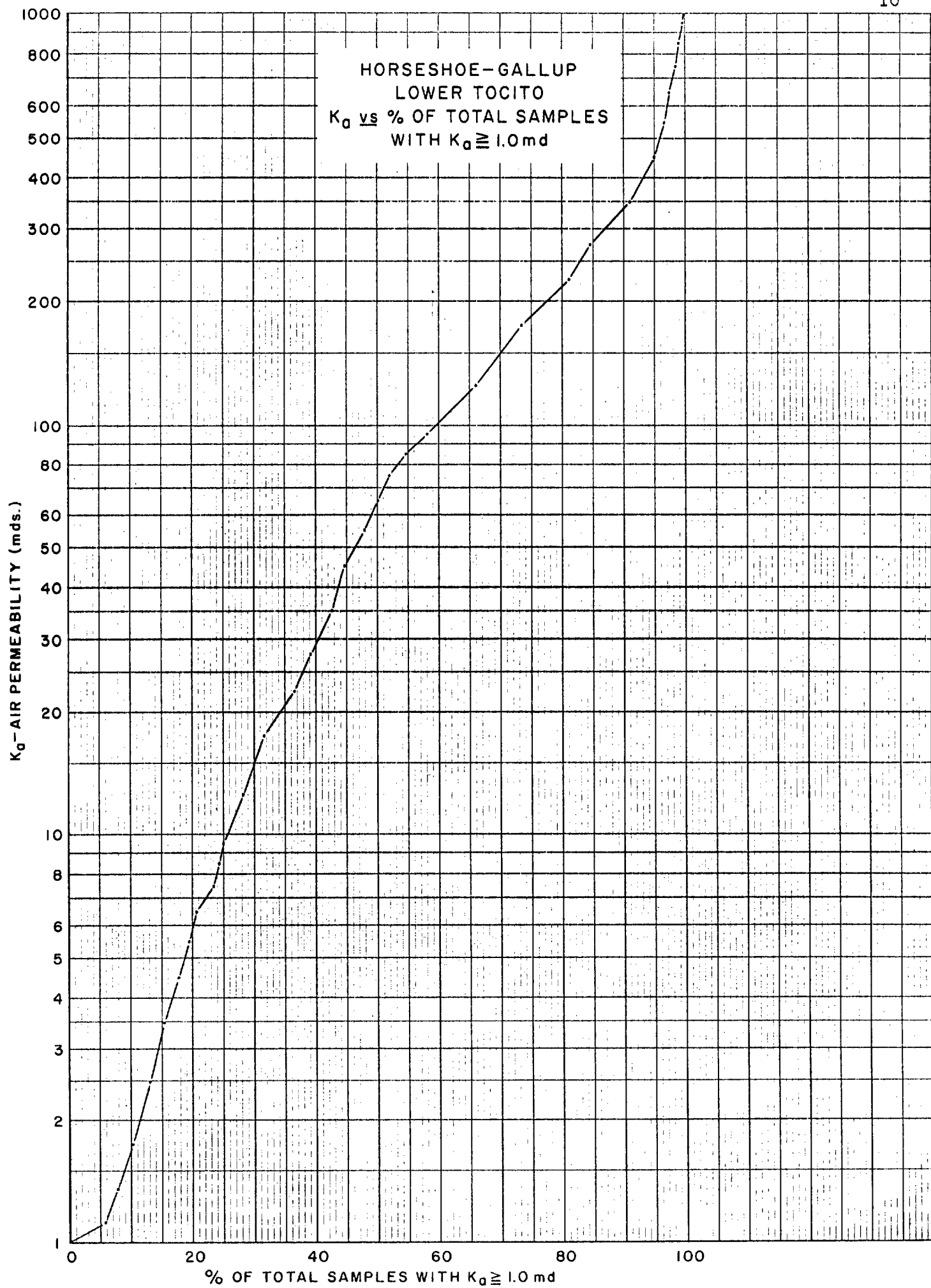


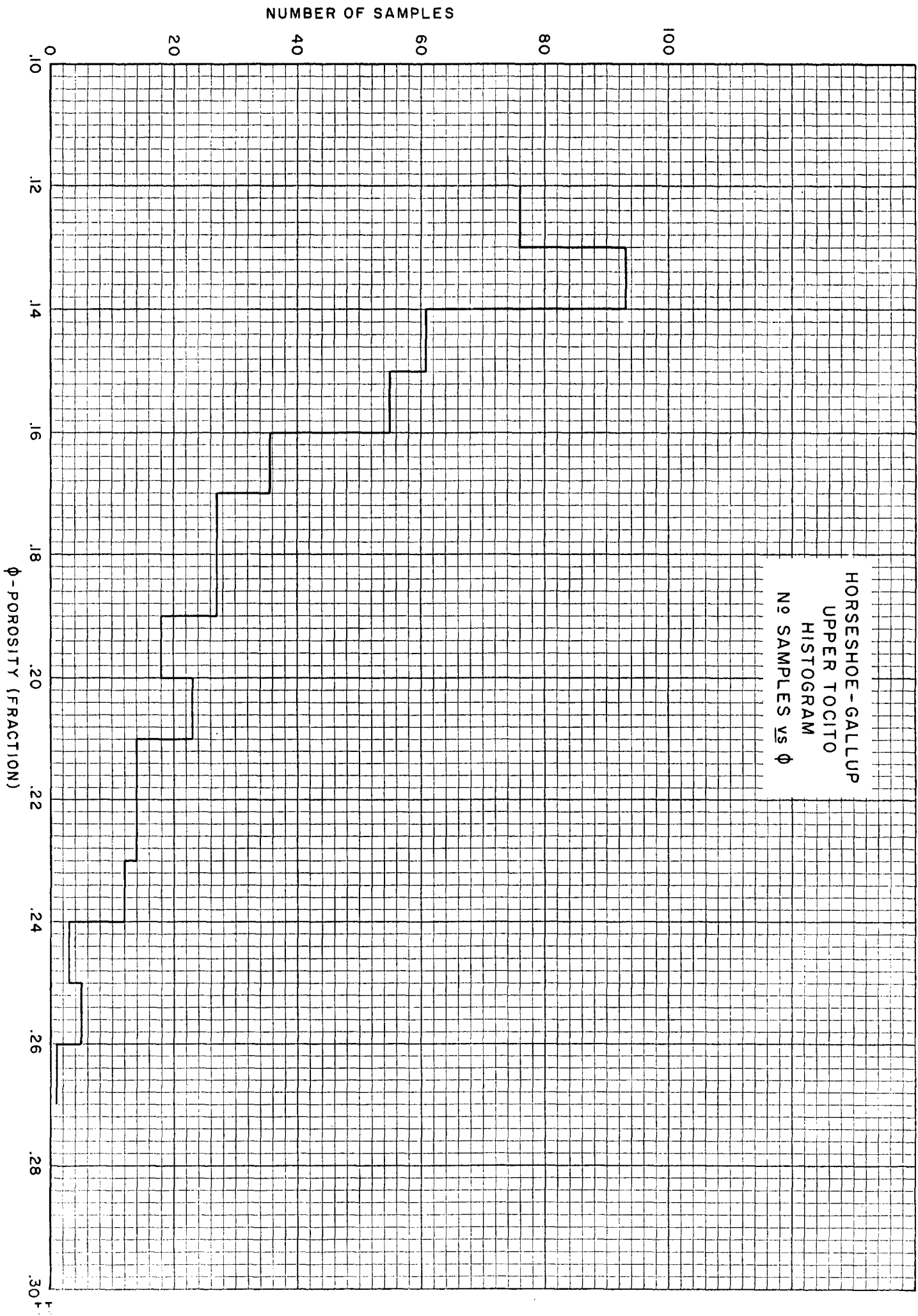
NAVAJO NO 5 WELL
 GALLUP SAND
 HORSESHOE - GALLUP FIELD
 SAN JUAN COUNTY, NEW MEXICO

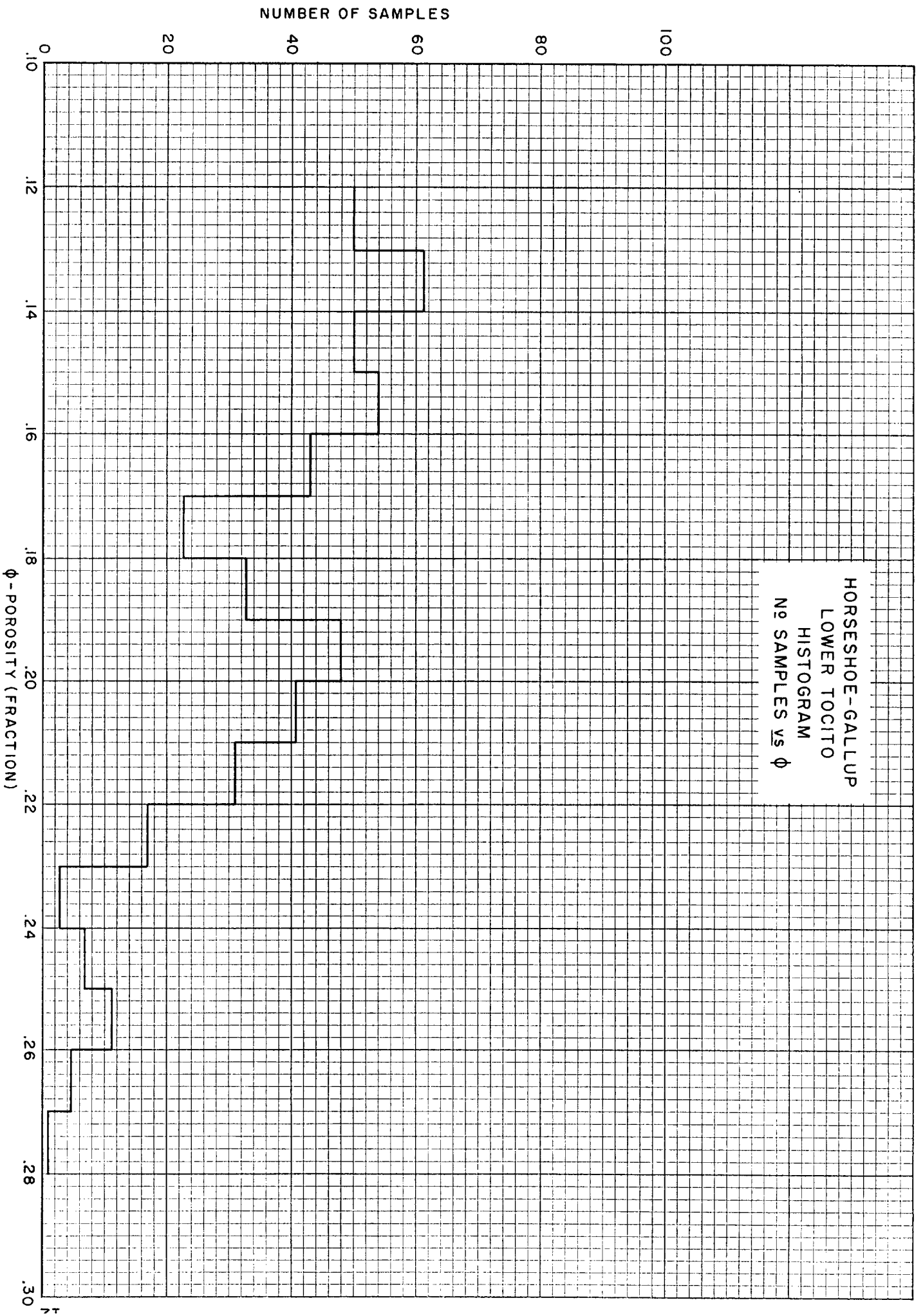
OIL VISCOSITY

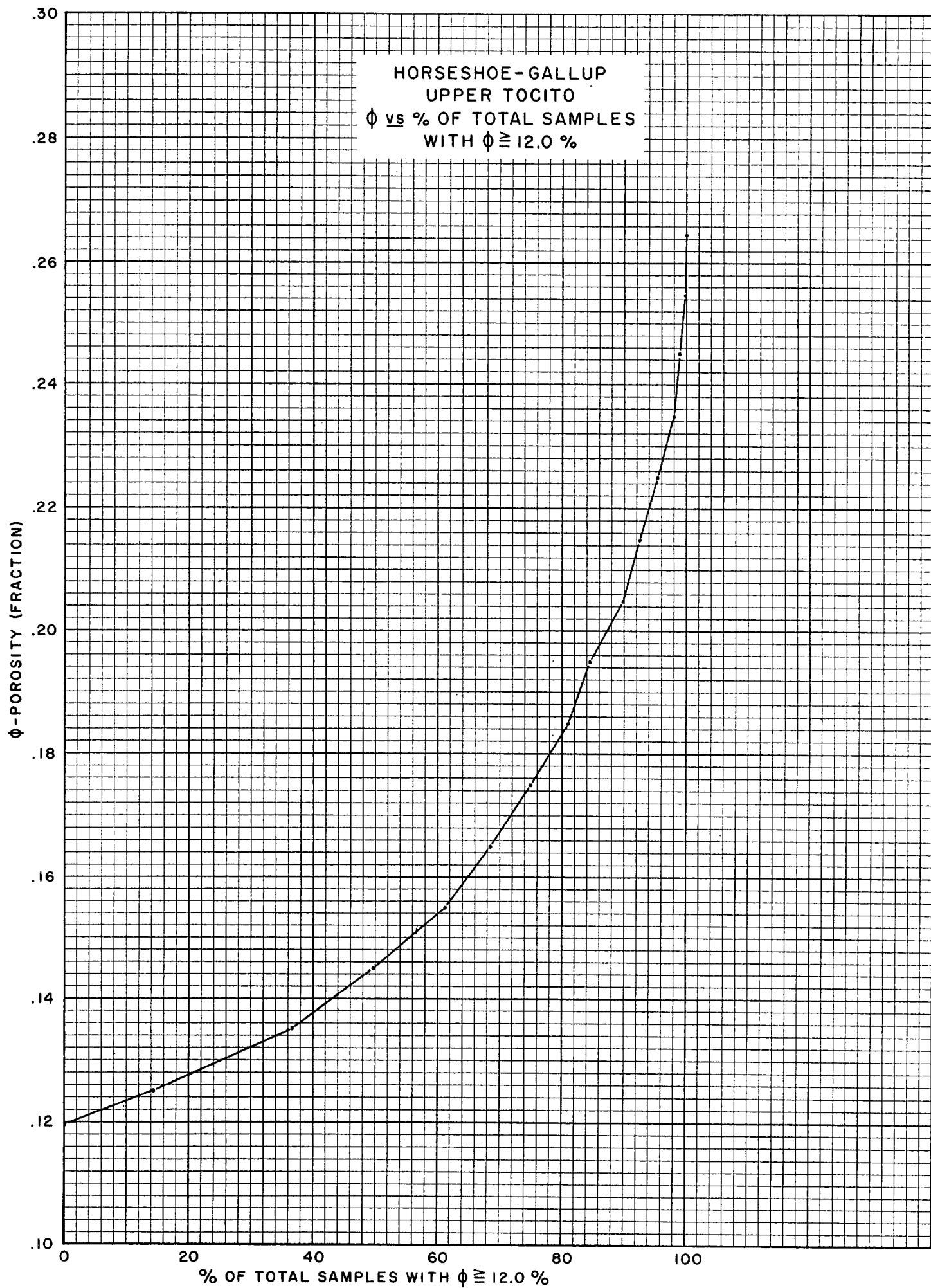


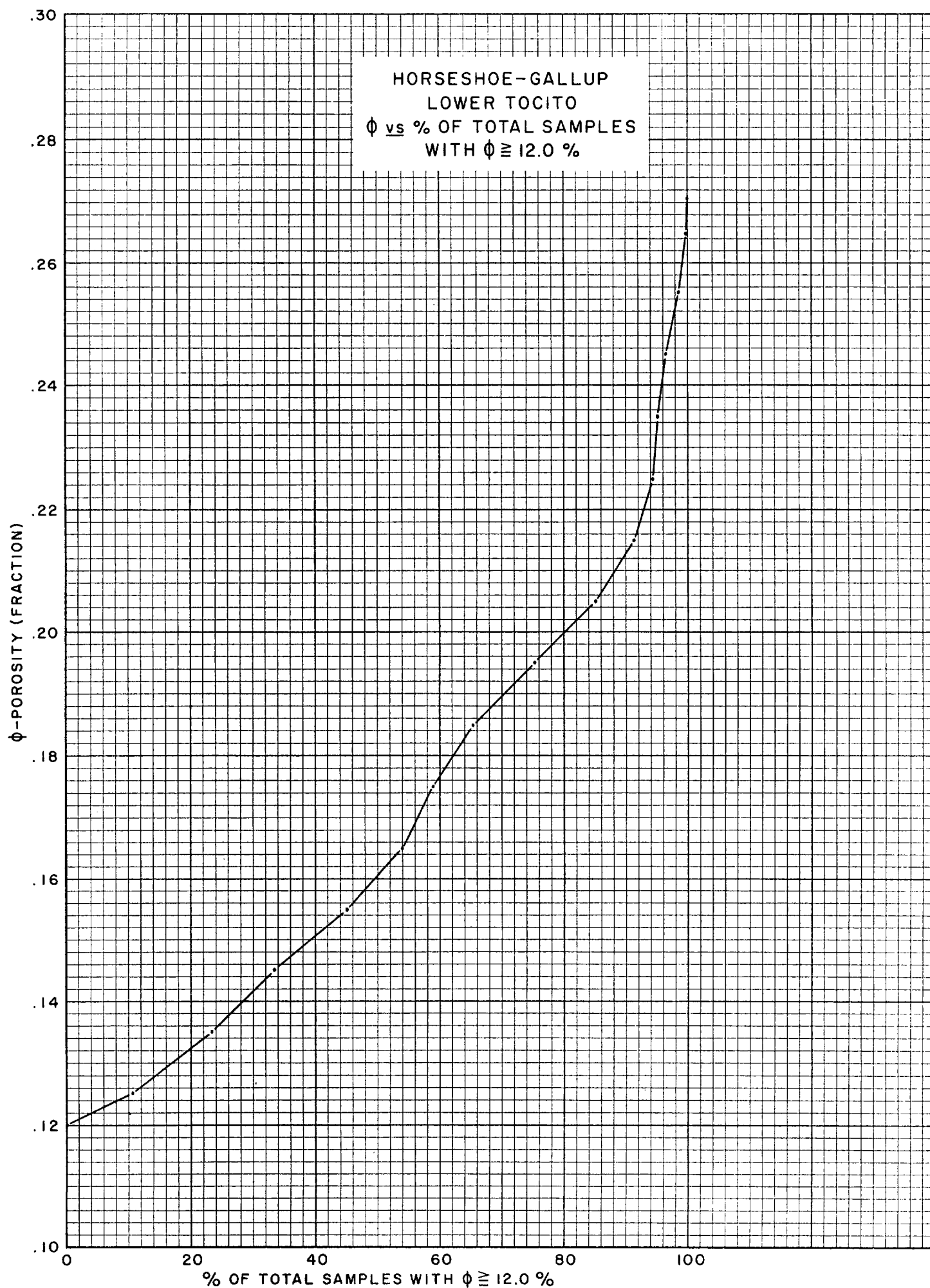


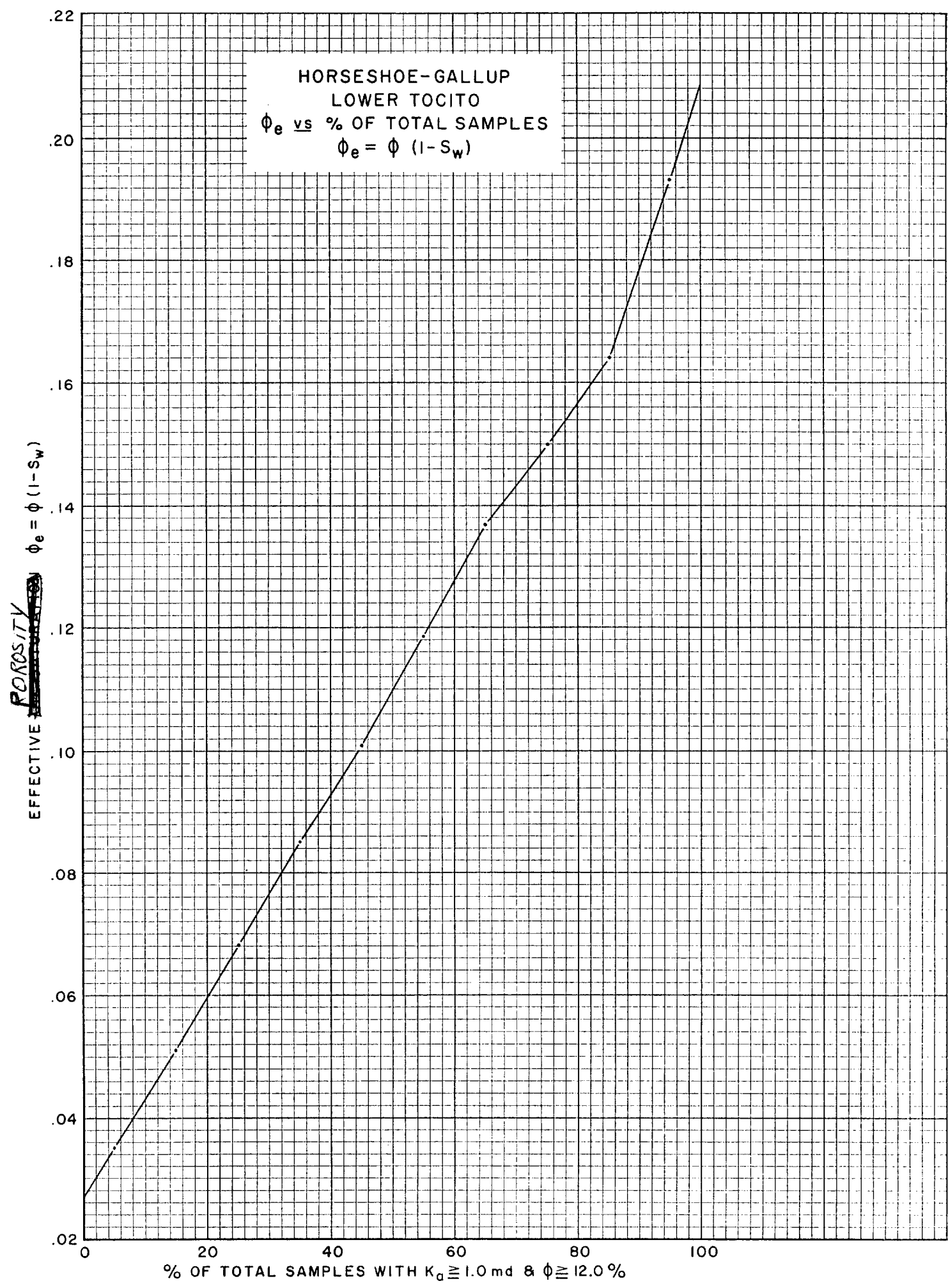






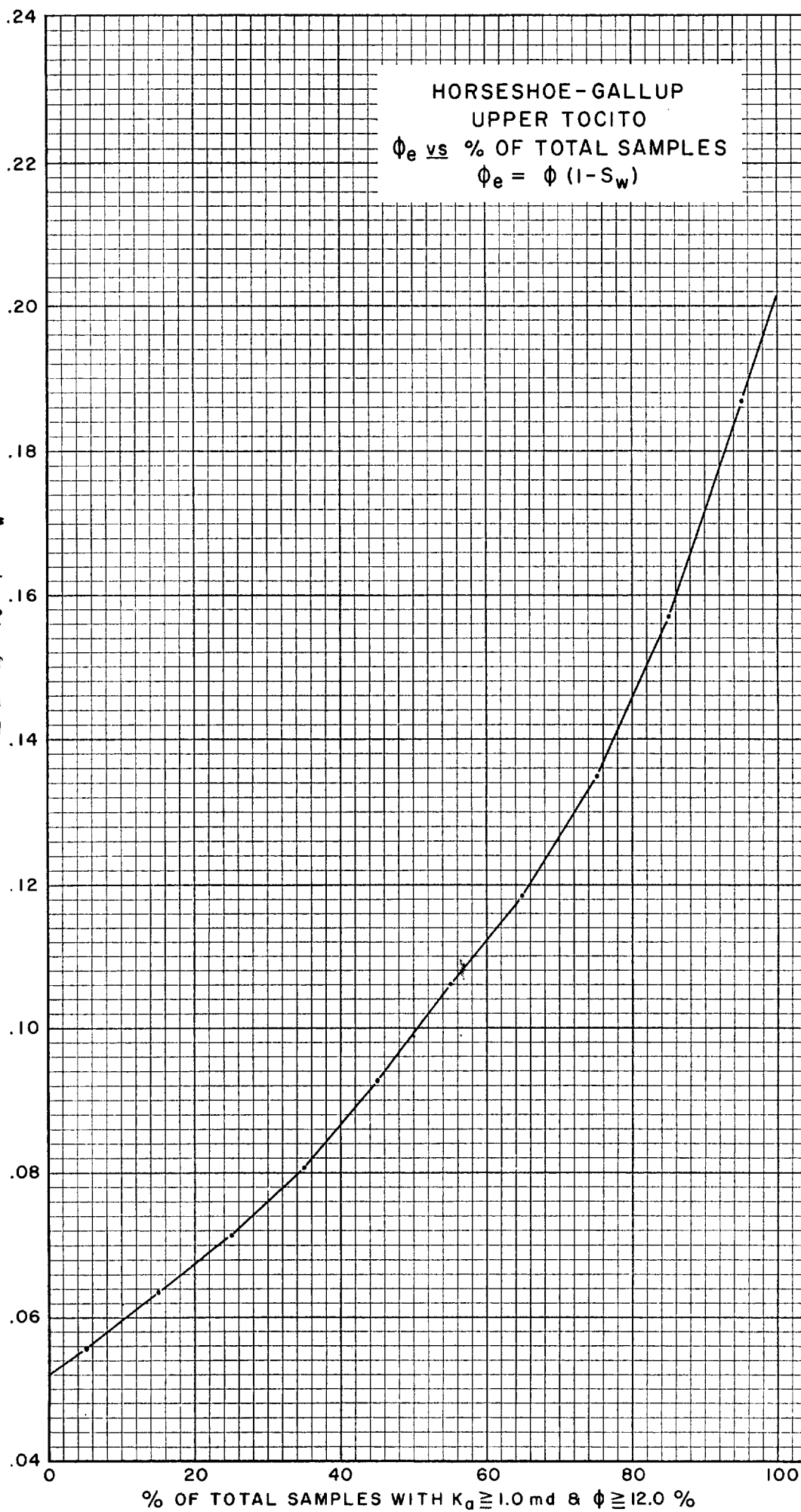






HORSESHOE-GALLUP
UPPER TOCITO
 ϕ_e vs % OF TOTAL SAMPLES
 $\phi_e = \phi (1 - S_w)$

POROSITY
EFFECTIVE $\phi_e = \phi (1 - S_w)$



CHEMICAL ENGINEERING GROUP
RELATIVE PERMEABILITY LABORATORY
DATA SUMMARY

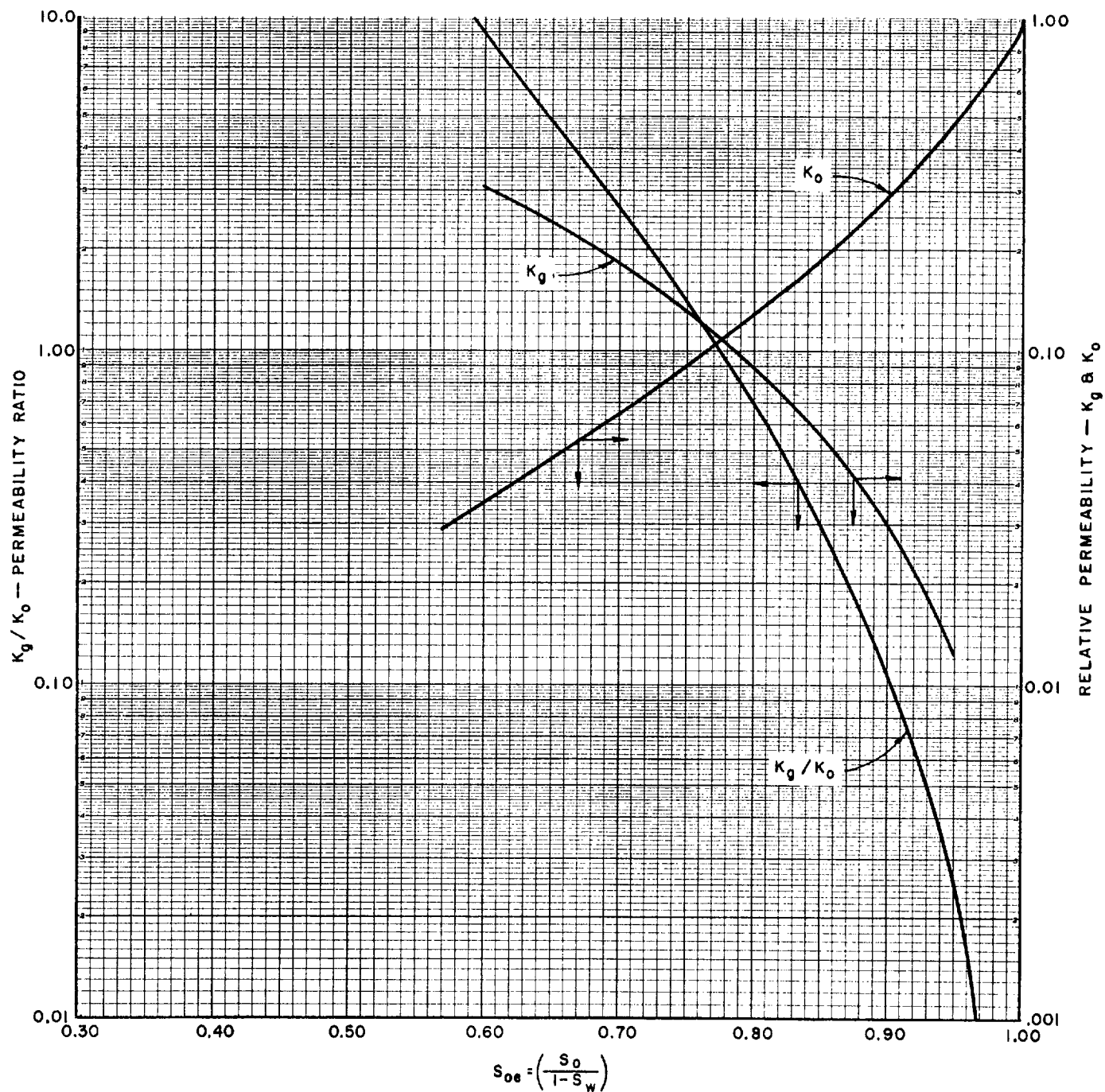
STUDY NO. F59-10
DATE: September 18, 1959

SUBJECT: Gas-Oil Relative Permeability
FIELD: Horseshoe-Gallup

COUNTY: San Juan STATE: New Mexico

Formation and Well	Depth, Ft.	<u>Permeability, Md.</u>		Porosity, %	Interstitial Water %, After Displacement By Oil at 200 Psi
		To Air	To Oil at Connate Water		
UPPER TOCITO					
Navajo #B-3	1295-96	15.0	10.3	9.4	36.7
Navajo #1	1111-12	57.5	33.5	11.6	22.3
Navajo #5	1178-79	296	251	17.2	21.9
Navajo #1	1117-18	725	641	18.9	25.5
LOWER TOCITO					
Navajo #1	1227-28	5.3	1.8	13.9	55.5
Navajo #1	1225-26	28.7	19.8	18.2	42.7
Navajo #1	1205-06	71.3	44.9	17.6	39.6
Navajo #1	1208-09	223	183	20.1	24.0
Navajo #1	1214-15	365	324	21.8	26.5

HORSESHOE GALLUP AVERAGE
RELATIVE PERMEABILITY CURVE
UPPER AND LOWER TOCITO

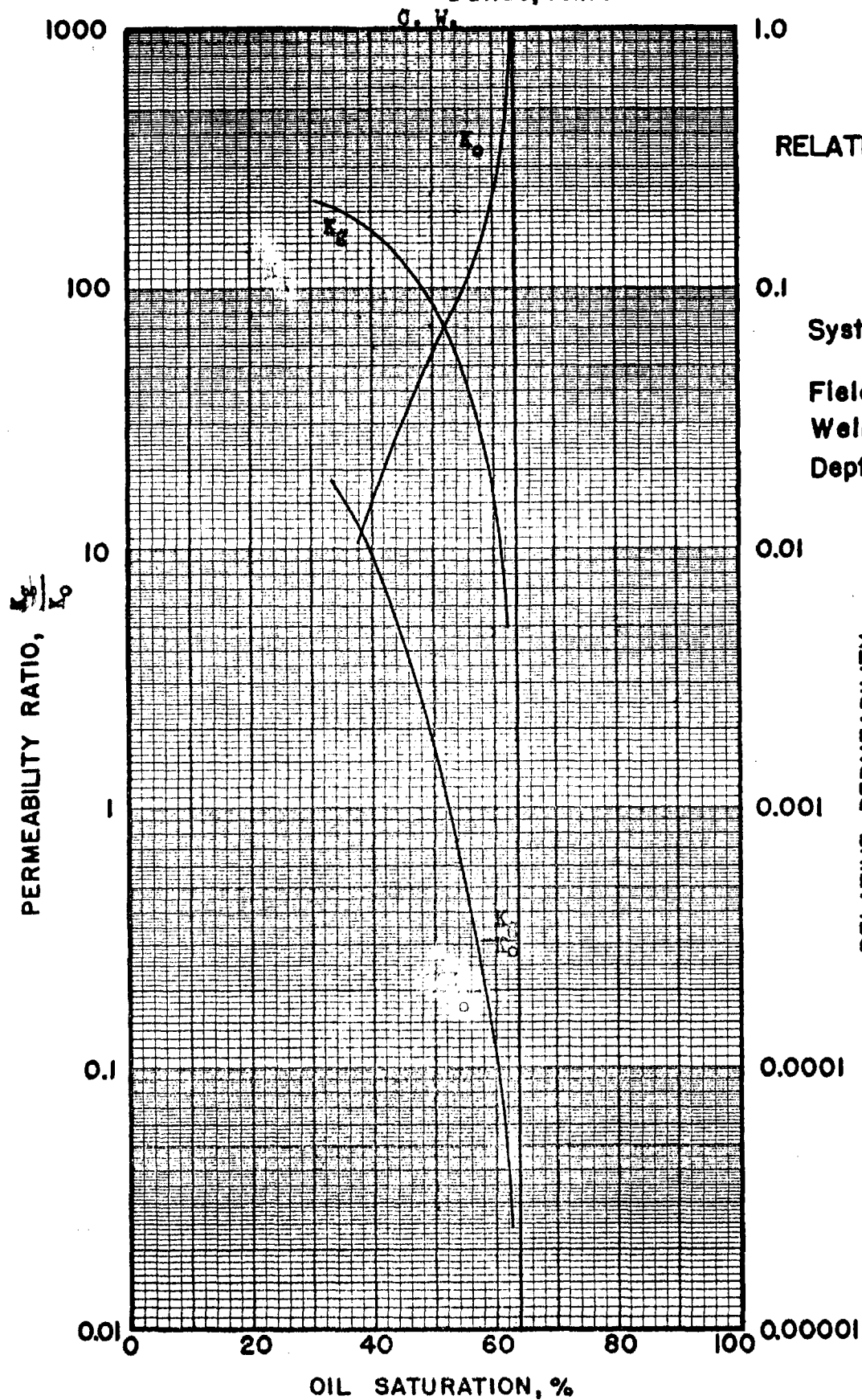


THE ATLANTIC REFINING COMPANY

PETROLEUM ENGINEERING SECTION

CHEMICAL ENGINEERING GROUP

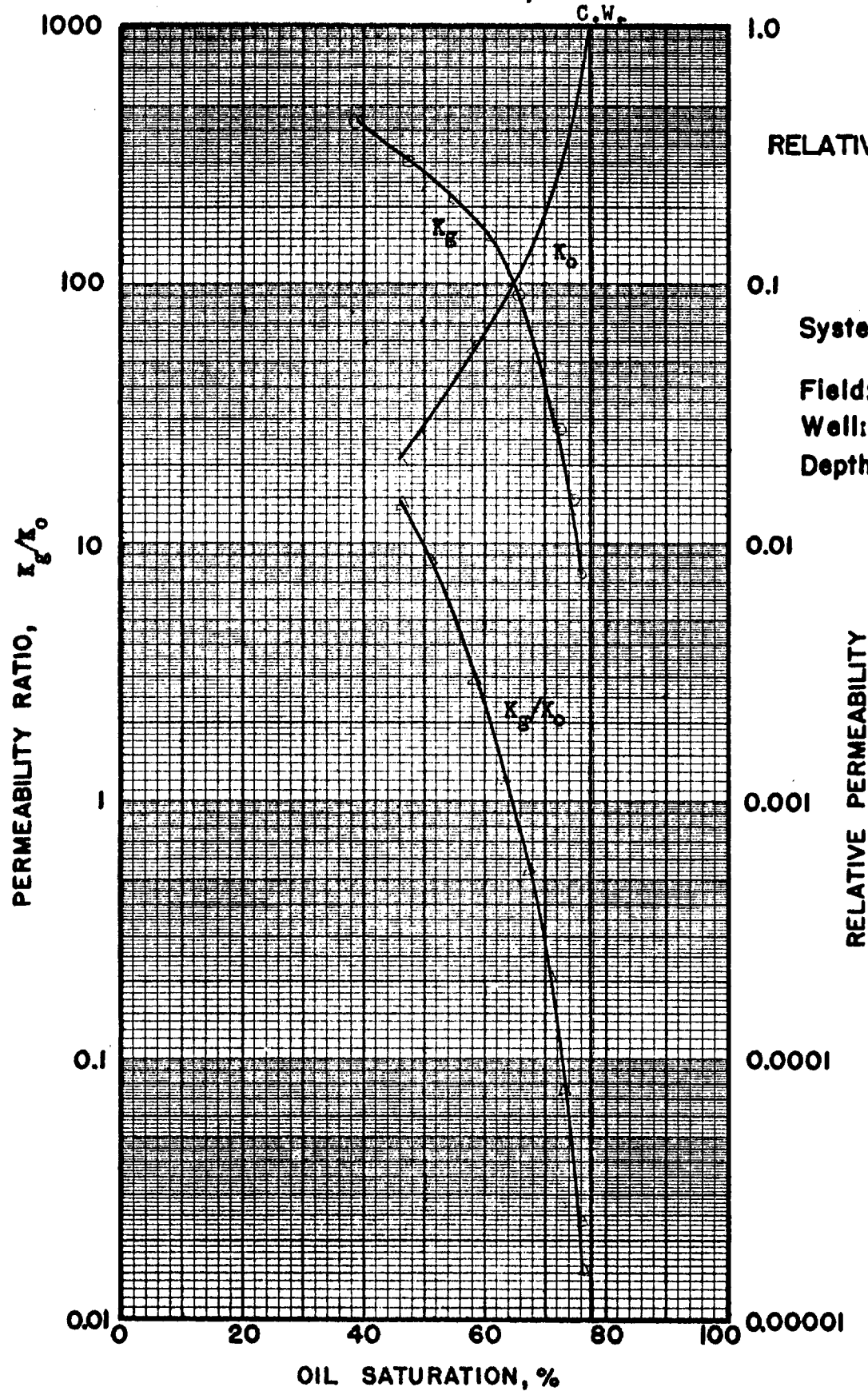
Dallas, Texas



THE ATLANTIC REFINING COMPANY

PETROLEUM ENGINEERING SECTION
CHEMICAL ENGINEERING GROUP

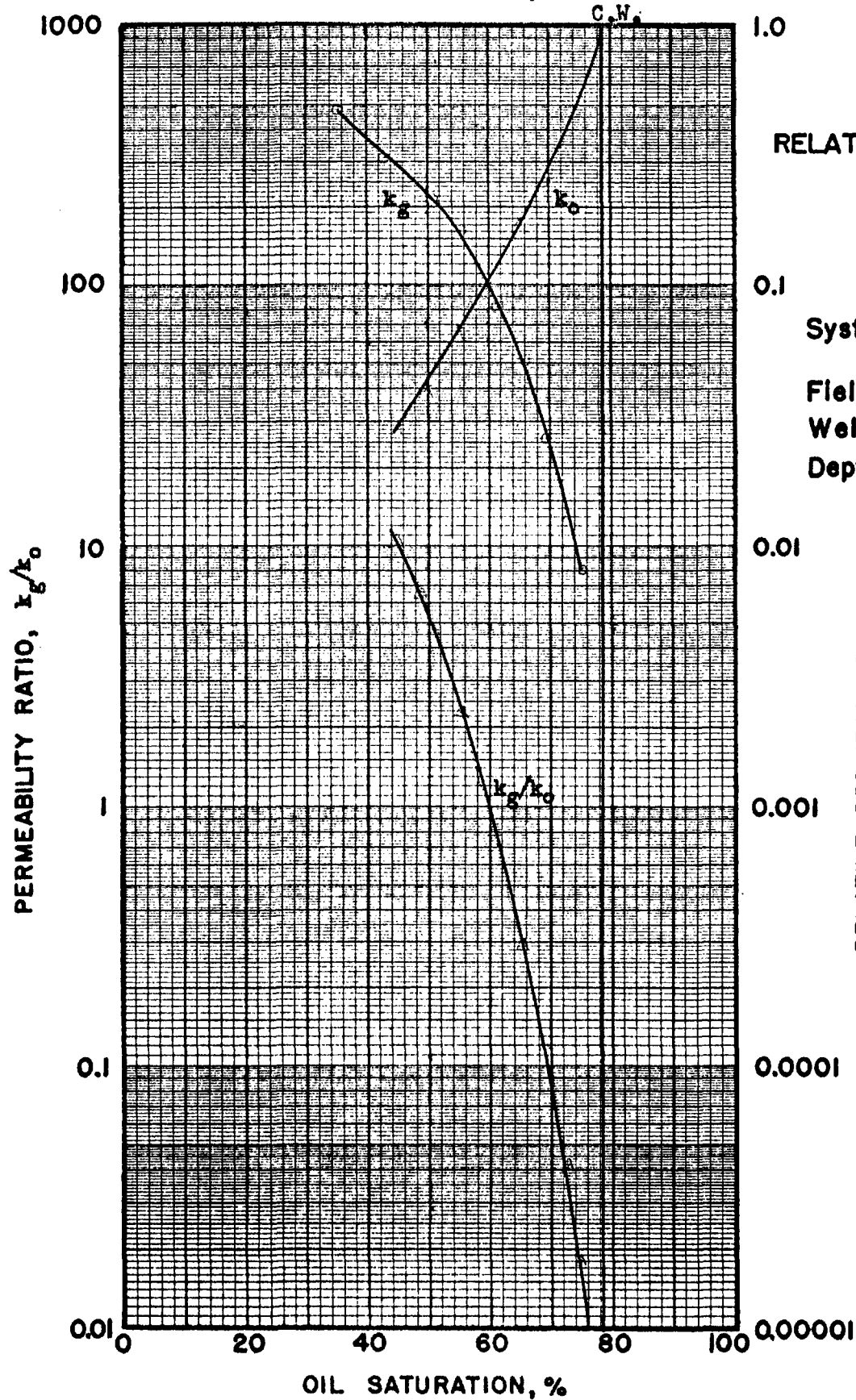
Dallas, Texas



THE ATLANTIC REFINING COMPANY

PETROLEUM ENGINEERING SECTION
CHEMICAL ENGINEERING GROUP

Dallas, Texas

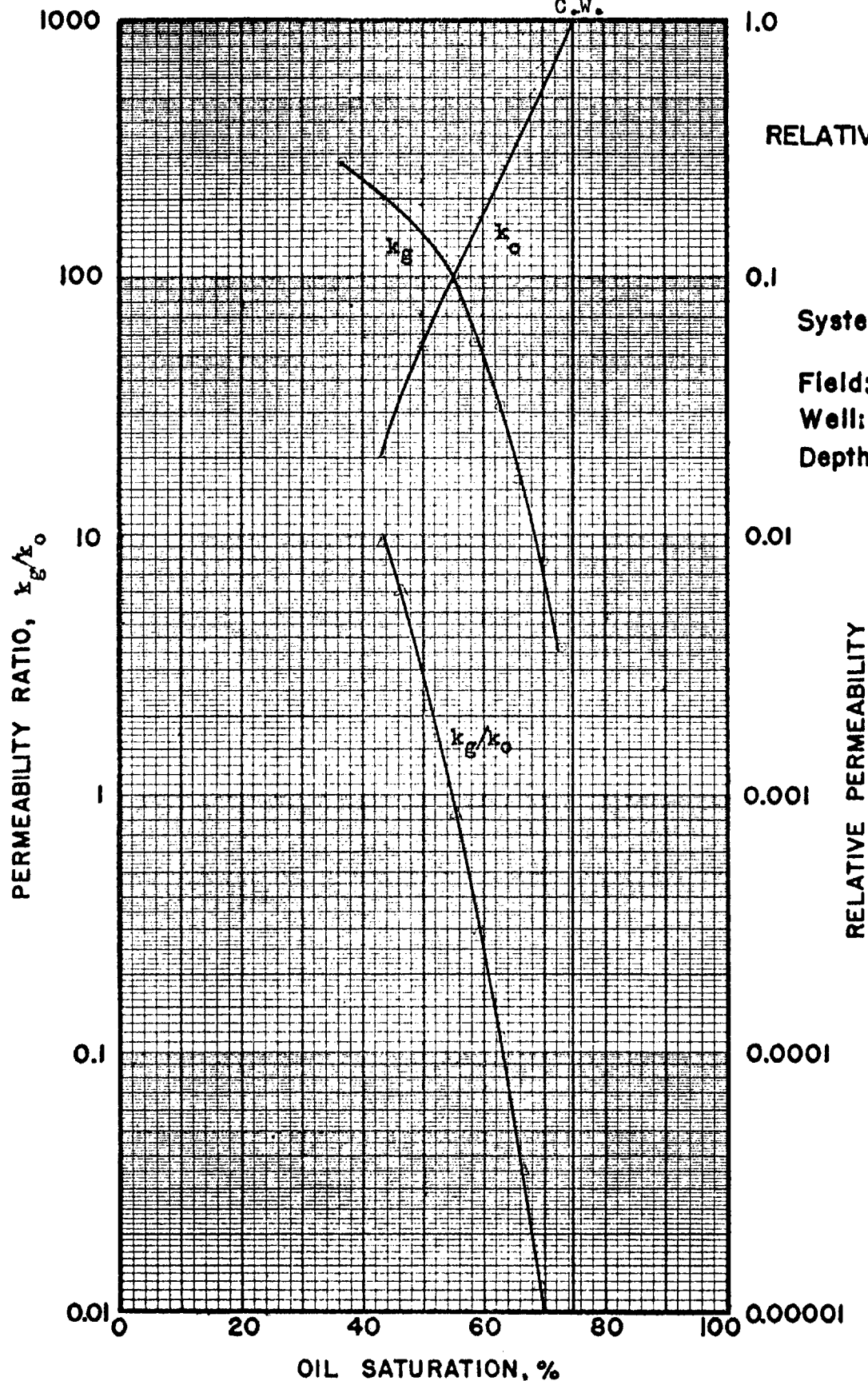


THE ATLANTIC REFINING COMPANY

PETROLEUM ENGINEERING SECTION
CHEMICAL ENGINEERING GROUP

Dallas, Texas

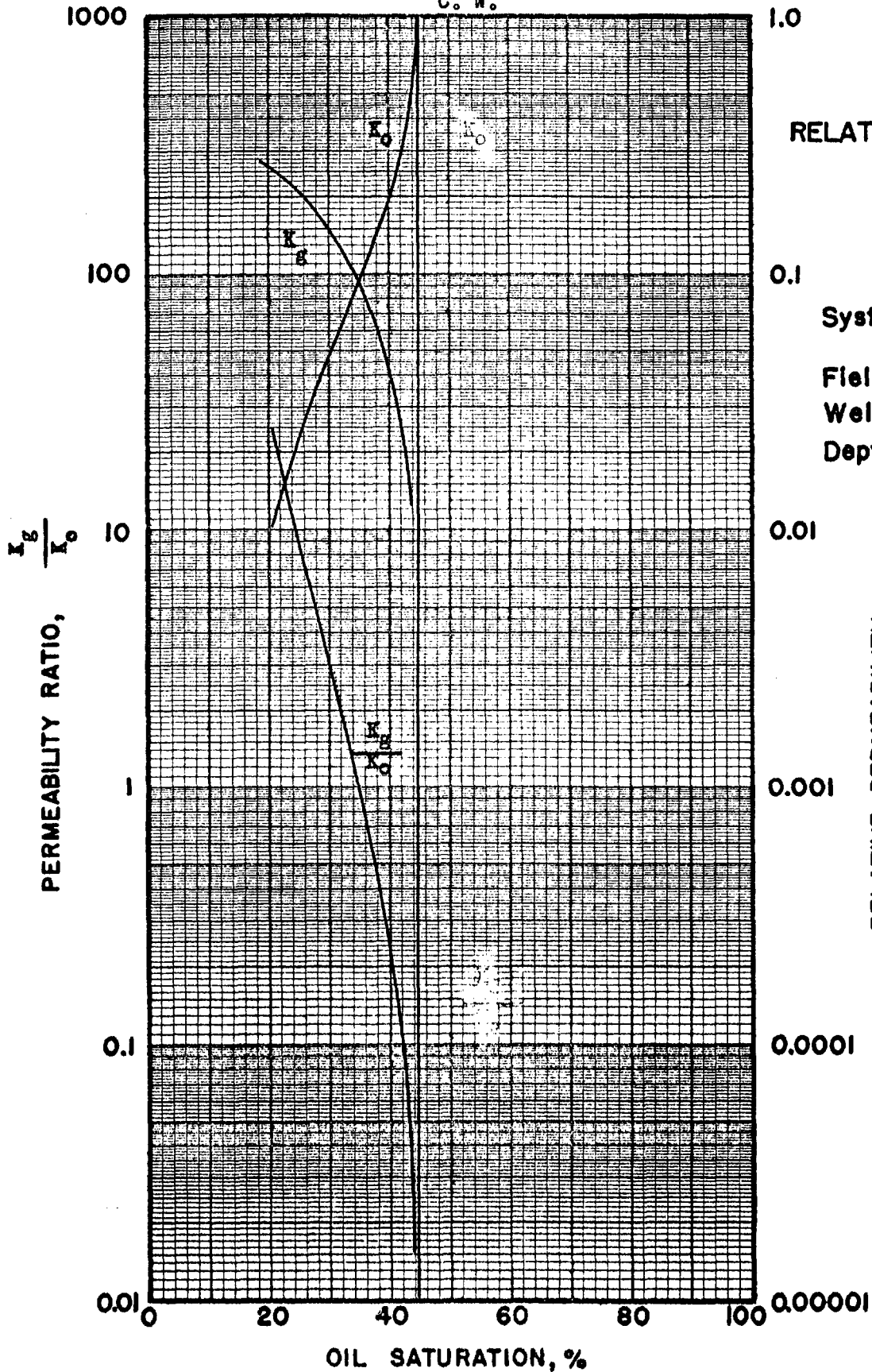
C.W.



THE ATLANTIC REFINING COMPANY

PETROLEUM ENGINEERING SECTION
CHEMICAL ENGINEERING GROUP

Dallas, Texas
C. W.



RELATIVE PERMEABILITY STUDIES

System: Gas-Oil

Field: Horseshoe-Gallup

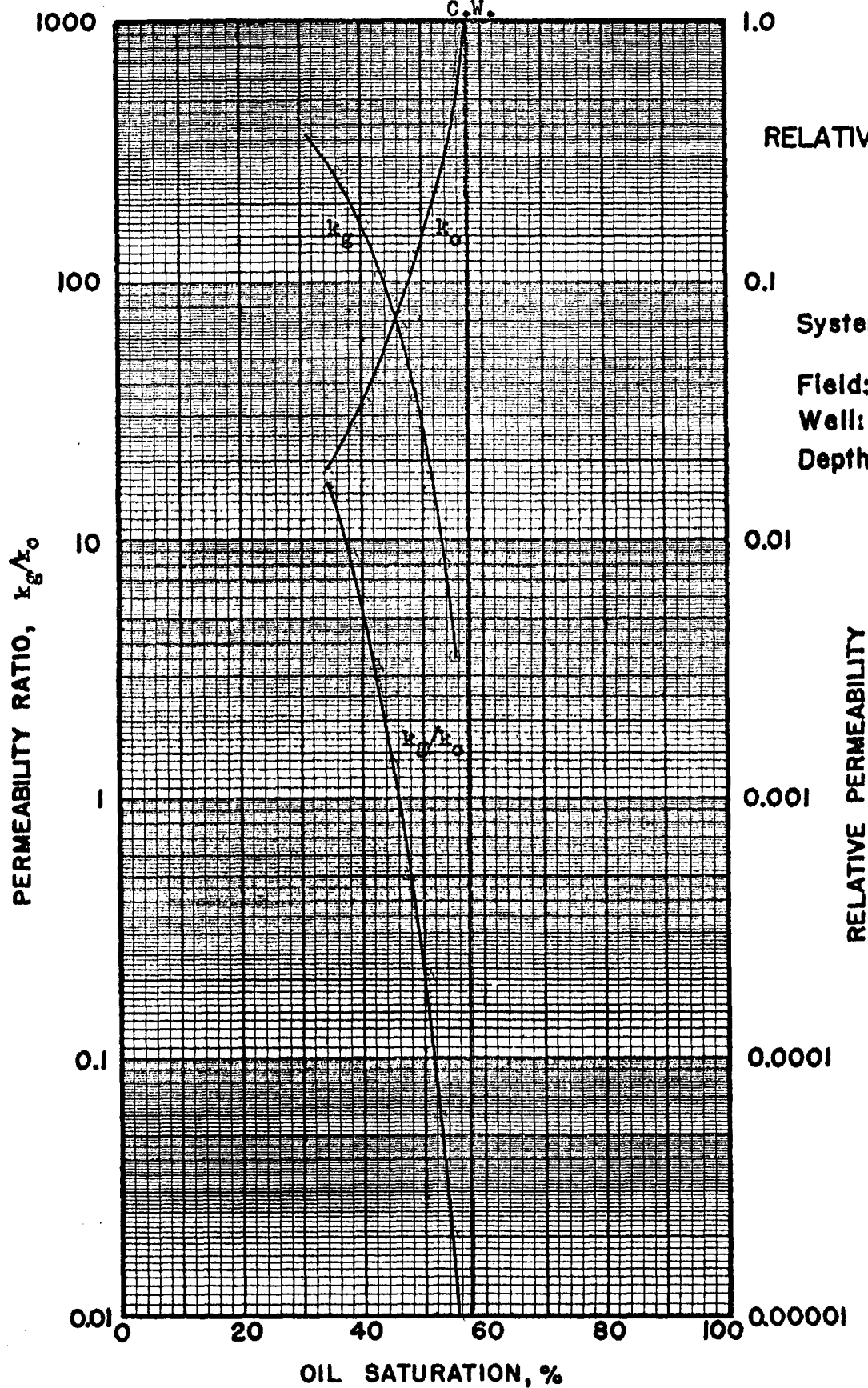
Well: Navajo No. 1

Depth: 1227-28

THE ATLANTIC REFINING COMPANY

PETROLEUM ENGINEERING SECTION
CHEMICAL ENGINEERING GROUP

Dallas, Texas

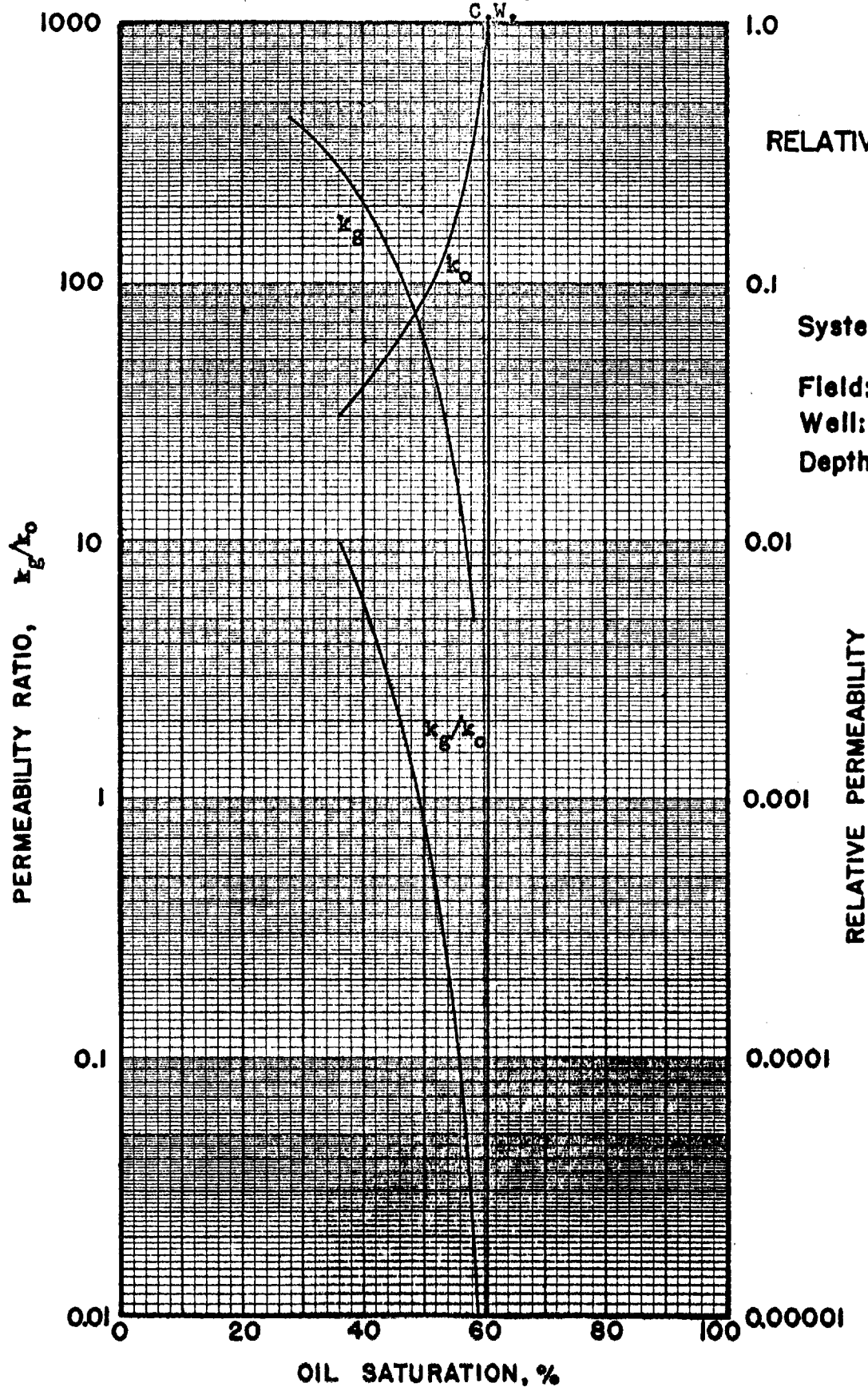


THE ATLANTIC REFINING COMPANY

PETROLEUM ENGINEERING SECTION

CHEMICAL ENGINEERING GROUP

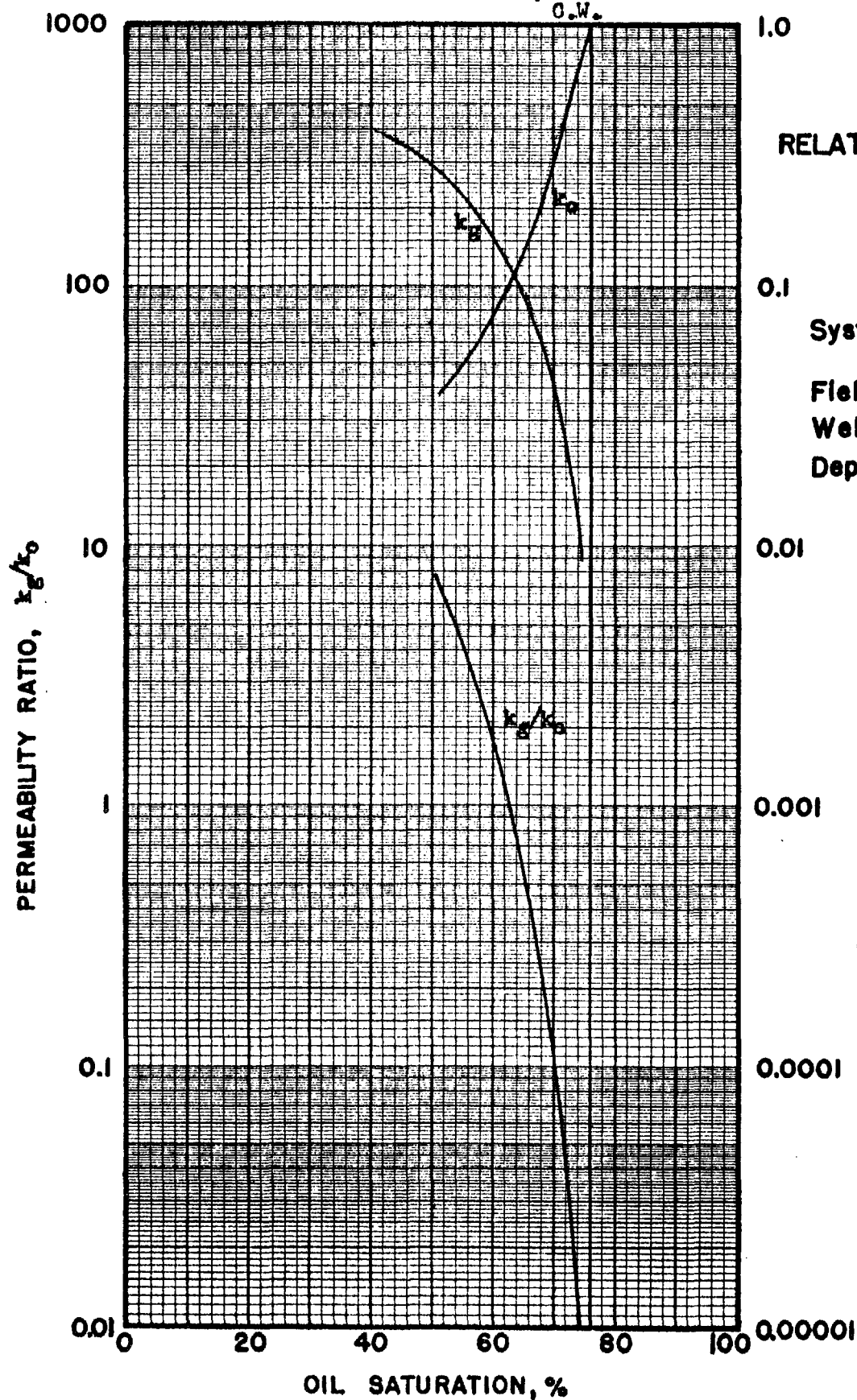
Dallas, Texas



THE ATLANTIC REFINING COMPANY

PETROLEUM ENGINEERING SECTION
CHEMICAL ENGINEERING GROUP

Dallas, Texas

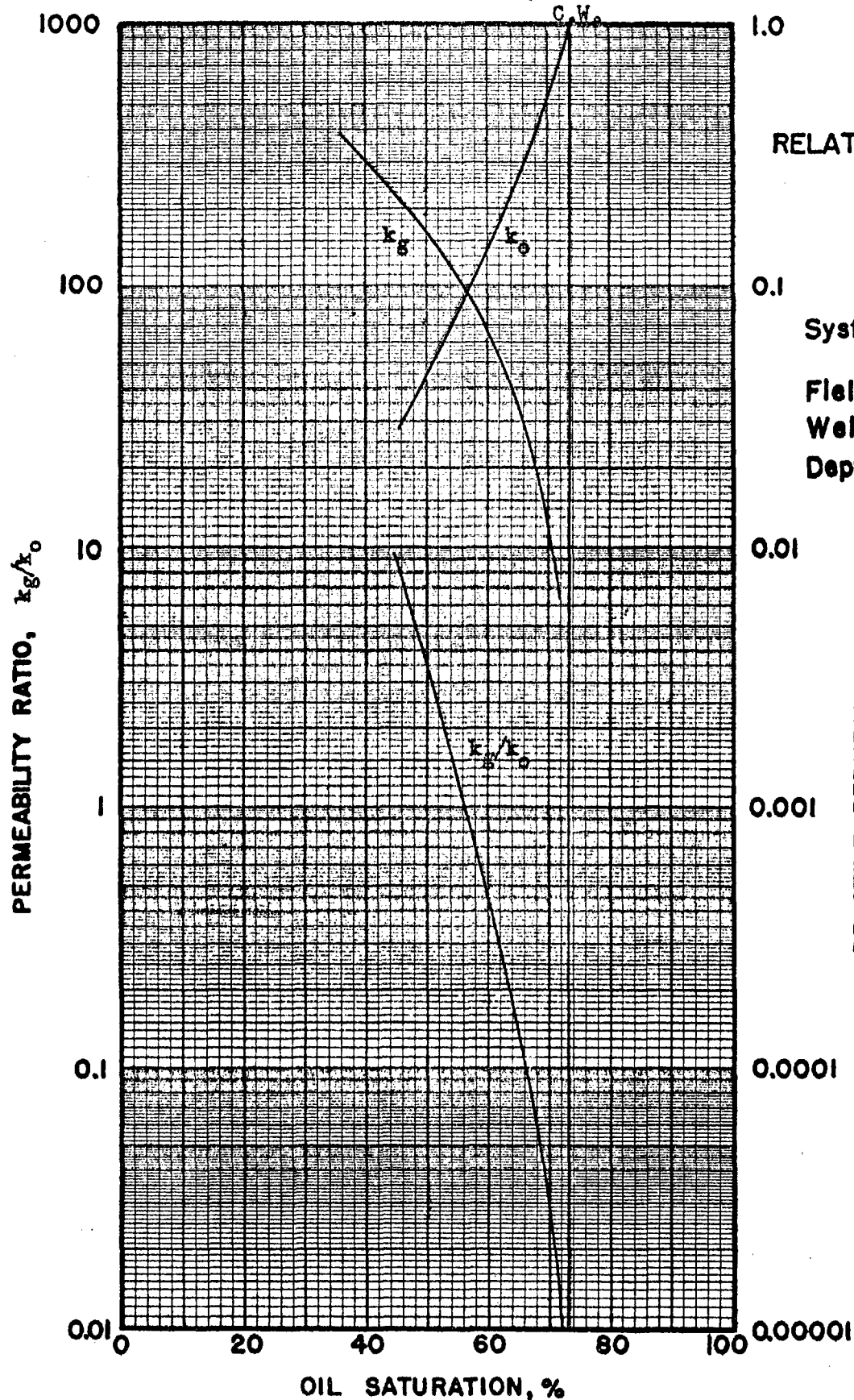


THE ATLANTIC REFINING COMPANY

PETROLEUM ENGINEERING SECTION

CHEMICAL ENGINEERING GROUP

Dallas, Texas



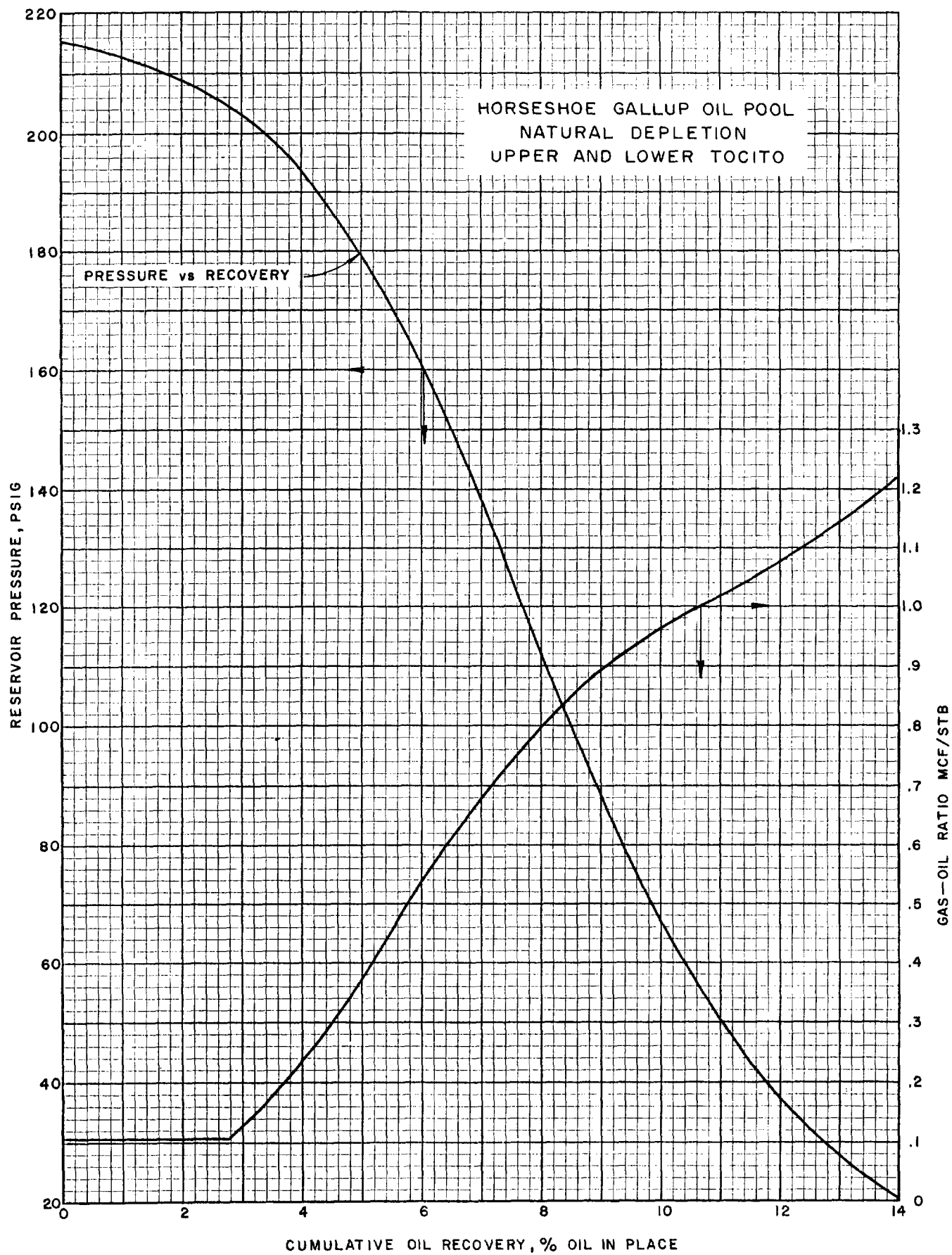
CHEMICAL ENGINEERING GROUP
RESTORED STATE LABORATORY
DATA SUMMARY

SUBJECT: Fresh Core Waterflood Results

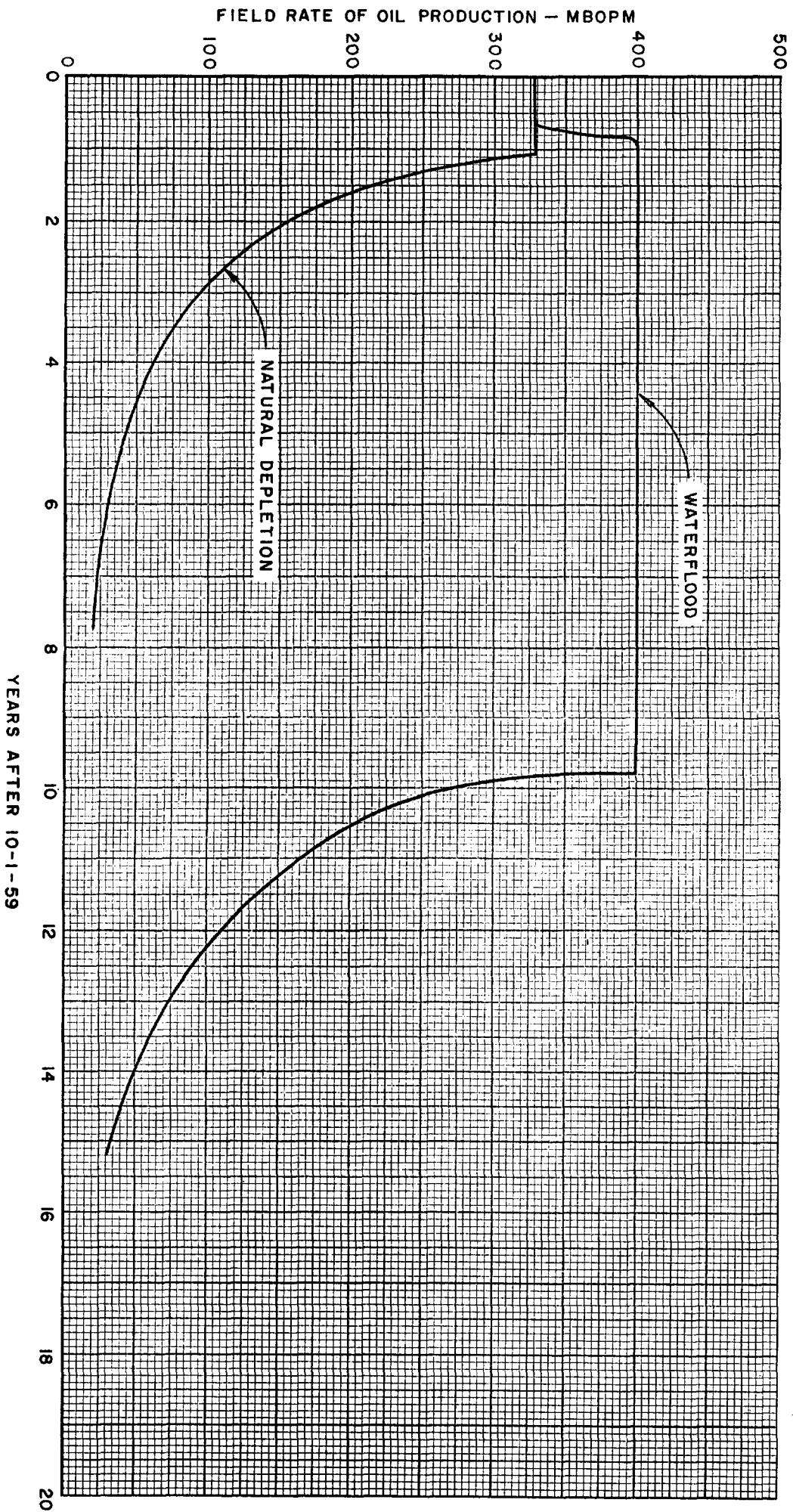
WELL: Navajo #5 STATE: New Mexico
FIELD: Horseshoe Gallup COUNTY: San Juan FORMATION: Tocito (Gallup)

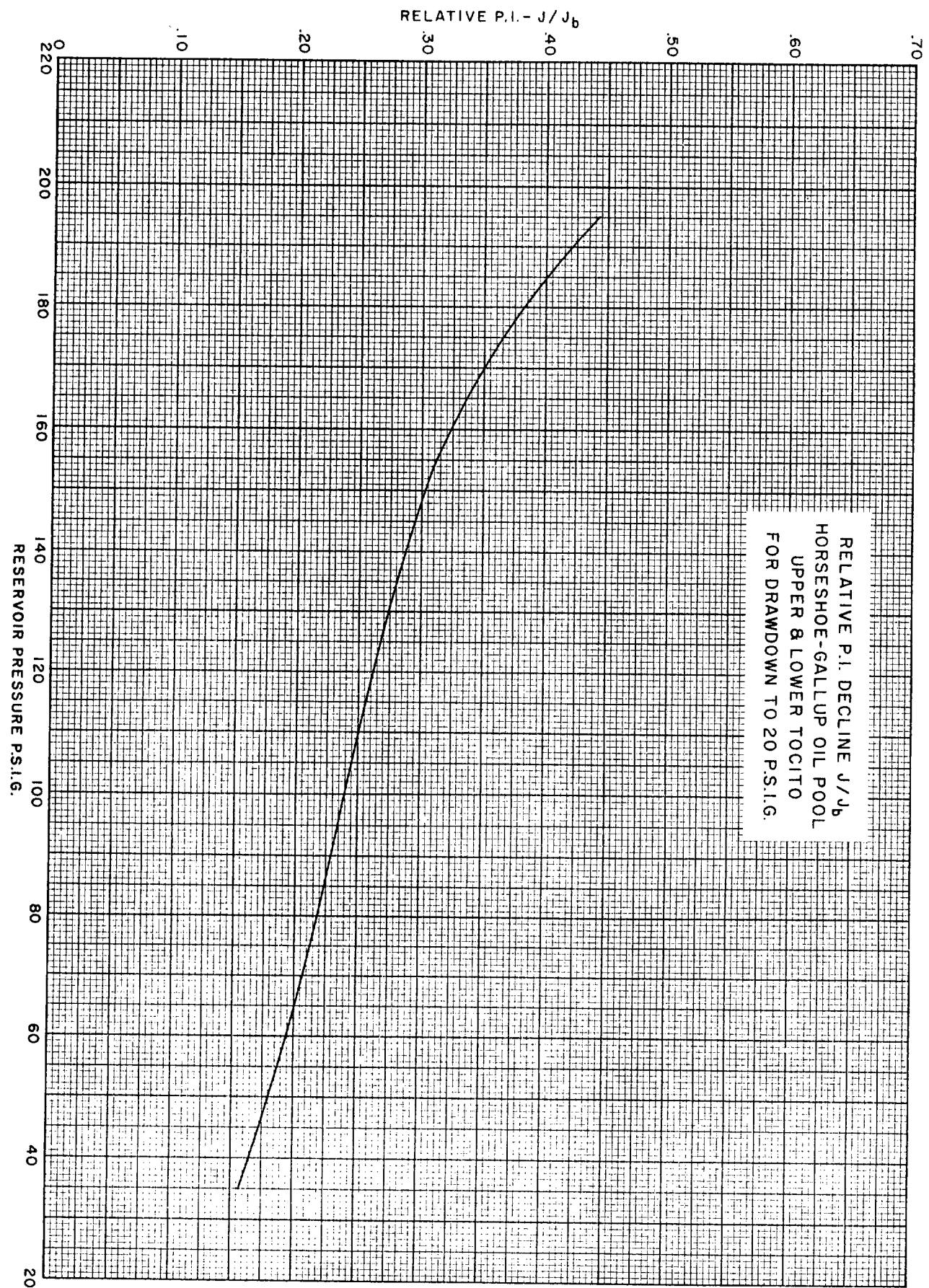
Depth, Ft.	Permeability, md.			Porosity, %	Interstitial Water %, After Centrifuge with Oil at 200 psi	Residual Oil to Waterflood % P. V.
	To Air	To Oil at C.W.	To Brine at R.O.			
<u>Upper Tocito</u>						
1165-66	4.6	2.3	.21	11.3	18.4	51.3
1177-78	1128	795	221	17.9	31.5	22.2
1177-78	287	210	72.3	14.2	40.7	29.7
1195-96	1.1	.33	.02	7.1	26.1	52.2
<u>Lower Tocito</u>						
1282-83	50.8	30.1	14.2	18.5	35.2	26.7
1291-92	87.2	47.5	29.3	20.3	31.7	25.1
1297-98	228	119	66.1	21.0	31.3	18.9
1301	260	163	70.3	22.9	36.4	20.7
1281-82	159	98.3	45.7	20.2	16.1	31.6
1286	133	75.5	34.1	21.0	26.7	23.5
1290-91	170	109	56.1	20.8	25.2	27.9
1296-97	147	76.3	44.2	18.0	34.3	26.5
1302	190	105	50.4	19.9	29.4	23.2

$$\gamma_w / \gamma_o = 1.86$$



FIELD OIL RATE vs TIME
 FUTURE PRIMARY AND SECONDARY
 HORSESHOE GALLUP OIL POOL
 UPPER AND LOWER TOCITO





PERFORMANCE SUMMARYPrimary

Estimated Primary Recovery % OIP	12.3%
Primary Recovery, bbl/acre-ft.	95
Estimated Primary Recovery to Start of Waterflood, bbl/acre-ft.	46

Secondary

Average Residual Oil	27.7% of pore volume
Estimated Gas Saturation at Start of Flood	4.8% of pore volume
Conformance Factor	88%
Added Oil Recovery by Waterflood, bbl/acre-ft.	297

CUMULATIVE OIL & WATER PRODUCED - MSTB
CUMULATIVE WATER INJECTED - MBBLs.

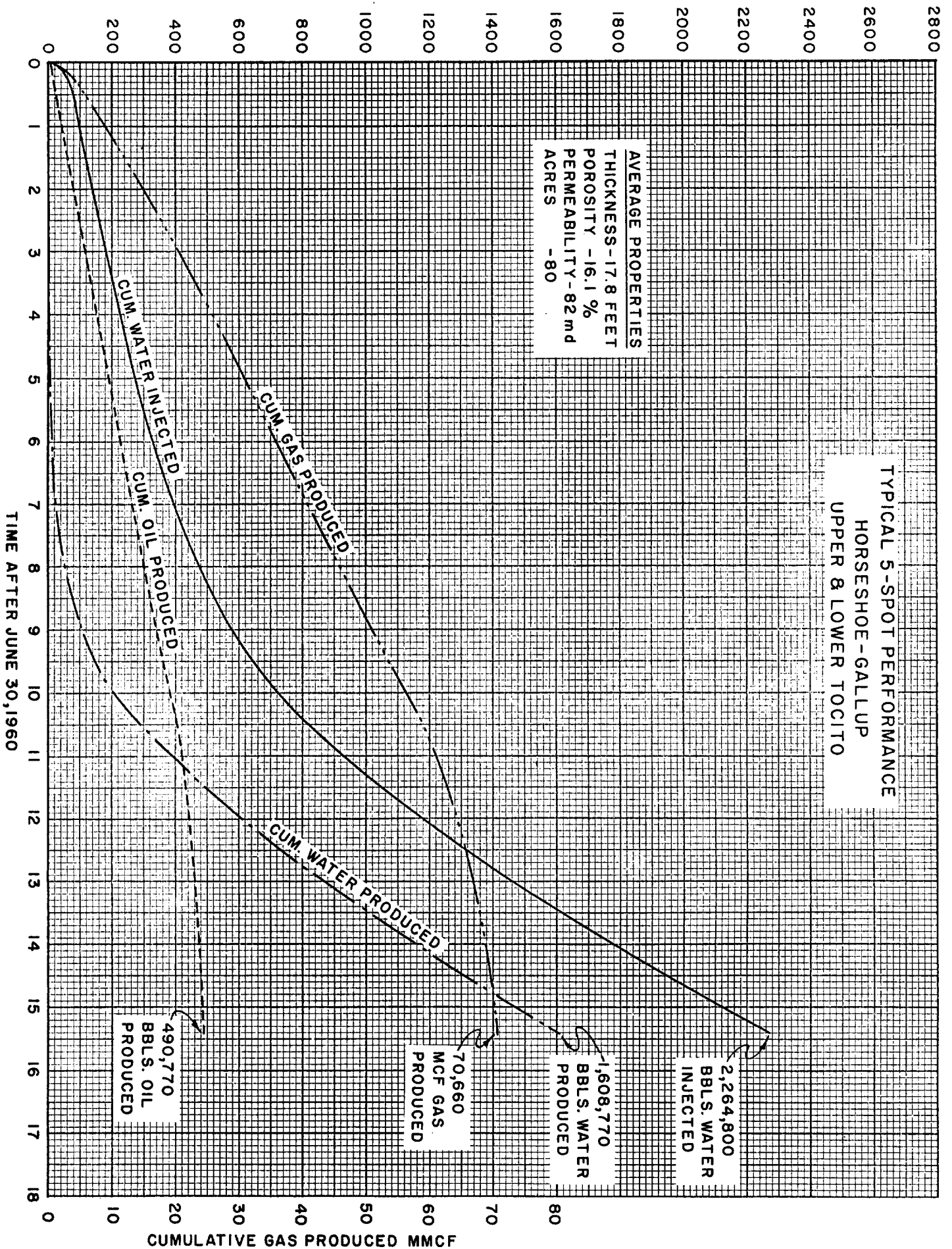


Exhibit B

P.I.

DENVER • CASPER
BILLINGS • BISMARCK
LOS ANGELES

LOG NO. 21628 S

**Distributed by
Petroleum Information**

COMPANY Atlantic Refining Company

WELL #9 Navajo

FIELD Horseshoe Canyon

C NW NE

LOC (P.I.) 30 31N 16W

San Juan, New Mexico

21628 S
30 31N 16W

 <i>Sonic Log</i> SCHLUMBERGER WELL SURVEYING CORPORATION		COUNTY <u>SAN JUAN, N.M.</u> FIELD or LOCATION <u>HORSESHOE GALLUP</u> WELL <u>NAVAJO #9</u>	
		COMPANY <u>ATLANTIC REFINING COMPANY</u>	
COMPANY ATLANTIC		Other Surveys	
REFINING COMPANY		NONE	
WELL <u>NAVAJO #9</u>		Location of Well <u>660' FR N/L</u> <u>1980' FR E/L</u> <u>SEC. 30-31N-16W</u>	
FIELD <u>HORSESHOE GALLUP</u>			
LOCATION <u>SEC. 30-31N-16W</u>			
COUNTY <u>SAN JUAN</u>	Elevation: K.B., <u>5546'</u> D.F., <u>5546'</u> or G.L., <u>5539'</u>		
STATE <u>NEW MEXICO</u>			
Log Depth Measured from <u>KB</u> Ft. above _____			
RUN No. <u>ONE</u>			
Date <u>11-5-58</u>			
First Reading <u>1450</u>			
Last Reading <u>1000</u>			
Feet Measured <u>450</u>			
Cat. Schlum. <u>--</u>			
Cog. Driller <u>102</u>			
Depth Reached <u>1453</u>			
Bottom Driller <u>1453</u>			
Mud Nat. <u>GEL CHEM</u>			
Dens. Visc. <u>9.1</u> <u>50</u> <u>of</u>			
Mud Resist. <u>2.7</u> <u>75</u> <u>of</u>			
" Res. BHT <u>1.9</u> <u>85</u> <u>of</u>			
" RH <u>8.5</u> <u>of</u>			
" Vfr. Loss <u>4.6</u> <u>CC 30 min</u> <u>of</u>			
" Kmif <u>--</u> <u>CC 30 min</u> <u>of</u>			
Bit Size <u>7 7/8"</u>			
Spcon <u>31</u>			
To <u>TO 1000'</u>			
Op'r. Rig Time <u>1 HR</u>			
Truck No. <u>2517 FARM</u>			
Recorded By <u>MATHIENS</u>			
Witness <u>JESSUP</u>			

REMARKS	VLC No.: _____
	VLS No.: _____
VIP No.: _____	
MUD FROM FLOW LINE CD USED	
Velocity (feet per second) = $\frac{1,000,000}{\text{Interval Transit Time (microseconds per foot)}}$	

SPONTANEOUS-POTENTIAL millivolts	DEPTHS	INTERVAL TRANSIT TIME microseconds per foot	
		Span: <u>3</u> Ft.; 2 Receivers	Increases
$+ \frac{\Delta V}{\Delta L}$ -	L.R. 1000'	106	66
		146	106
		86	
		126	

Exhibit B

LOG NO. 22891 S		Distributed by Petroleum Information	
COMPANY Atlantic Refining Company			
WELL #29 Navajo			
FIELD Horseshoe Canyon			
LOC (P.I.) 1724 S/N 2067 E/W			
SE NW 31 31N 16W			
San Juan, New Mexico			



DENVER · CASPER
BILLINGS · BISMARCK
LOS ANGELES

LOG NO. 22891 S
31 31N 16W

SCUMBERGER WELL SURVEYING CORPORATION 		COUNTY SAN JUAN, NEW MEX. FIELD or LOCATION HORSESHOE GALLUP WELL NAVAJO # 29																																													
COMPANY ATLANTIC REFINING COMPANY WELL NAVAJO # 29 FIELD HORSESHOE GALLUP LOCATION SEC. 31-31N-16W		Other Surveys NONE Location of Well 1724' FR N/L 2067' FR W/L SEC. 31-31N-16W																																													
COUNTY SAN JUAN STATE NEW MEXICO Elevation: K.B. 5561 D.F. 5554 or G.L. 5554		Log Depths Measured From KB -7 Ft. above GL																																													
<table border="1"> <tr> <td>RUN No.</td> <td>ONE</td> </tr> <tr> <td>Date</td> <td>2-10-59</td> </tr> <tr> <td>First Reading</td> <td>1366</td> </tr> <tr> <td>Last Reading</td> <td>1000</td> </tr> <tr> <td>Feet Measured</td> <td>366</td> </tr> <tr> <td>Gen. Schlum.</td> <td>--</td> </tr> <tr> <td>Gen. Driller</td> <td>100</td> </tr> <tr> <td>Depth Reached</td> <td>1320</td> </tr> <tr> <td>Bottom Driller</td> <td>1320</td> </tr> <tr> <td>Mud Not.</td> <td>GEI</td> </tr> <tr> <td>Dens. Visc.</td> <td>8.9 @ 72°F</td> </tr> <tr> <td>Mud Resist.</td> <td>1.6 @ 84°F</td> </tr> <tr> <td>" Res. BHT</td> <td>1.4 @ 84°F</td> </tr> <tr> <td>" pH</td> <td>-- @ 84°F</td> </tr> <tr> <td>" Vitr. Loss</td> <td>1.3 @ 84°F</td> </tr> <tr> <td>" Rmt</td> <td>7 7/8"</td> </tr> <tr> <td>Bit Size</td> <td>7 7/8"</td> </tr> <tr> <td>Spont.</td> <td>3'</td> </tr> <tr> <td>Op. Rig Time</td> <td>1000 To 10</td> </tr> <tr> <td>Truck No.</td> <td>1 HR. To 10</td> </tr> <tr> <td>Recorded by</td> <td>1559 F.A.P.M.</td> </tr> <tr> <td>Witness</td> <td>DILLI</td> </tr> </table>				RUN No.	ONE	Date	2-10-59	First Reading	1366	Last Reading	1000	Feet Measured	366	Gen. Schlum.	--	Gen. Driller	100	Depth Reached	1320	Bottom Driller	1320	Mud Not.	GEI	Dens. Visc.	8.9 @ 72°F	Mud Resist.	1.6 @ 84°F	" Res. BHT	1.4 @ 84°F	" pH	-- @ 84°F	" Vitr. Loss	1.3 @ 84°F	" Rmt	7 7/8"	Bit Size	7 7/8"	Spont.	3'	Op. Rig Time	1000 To 10	Truck No.	1 HR. To 10	Recorded by	1559 F.A.P.M.	Witness	DILLI
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Truck No.	1 HR. To 10																																														
Recorded by	1559 F.A.P.M.																																														
Witness	DILLI																																														
REMARKS VLC No.: 77A VLS No.: 99A VIP No.: 59A																																															
Velocity (feet per second) = $\frac{1,000,000}{\text{Interval Transit Time (microseconds per foot)}}$																																															
SPONTANEOUS-POTENTIAL millivolts		INTERVAL TRANSIT TIME microseconds per foot Increases Span: 3 Ft. 2 Receivers																																													

Exhibit B

Distributed by
Petroleum Information

LOG NO. 22895 IE

COMPANY Atlantic Refining Company

WELL #23 Navajo

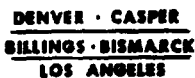
FIELD Horseshoe Canyon

LOC (P.I.) 2080 S/N 1980 E/W

SE NW 29 31N 16W

San Juan, New Mexico

29 31N 16W



Schlumberger Well Surveying Corporation

Production - Electrical Log

COUNTY SAN JUAN, NEW MEX.
FIELD or LOCATION HORSESHOE GALLUP
WELL NAVAJO # 23

COMPANY ATLANTIC REFINING COMPANY

COUNTY SAN JUAN
STATE NEW MEXICO

COMPANY ATLANTIC REFINING COMPANY
WELL NAVAJO # 23
FIELD HORSESHOE GALLUP
LOCATION SEC. 29-31N-16W

Other Surveys
SL
Location of Well
2080' FR N/L
1980' FR W/L
SEC. 29-31N-16W
Elevation D.F.
K.B. 5432
or G.L. 5432
FILING No.

RUN No.	DATE	FIRST READING	LAST READING	FEET MEASURED	COR. SLOTTING	COR. DRILLER	DEPTH REACHED	BOTTOM DRILLER	MUD NUT	MUD VISC.	RDS. BHT	TIME	PH	WTR. LOSS	BIT SIZE	SPECT. AM	AN	IND.	OPR. RIG TIME	TRUCK NO.	RECORDED BY	WITNESS
ONE	2-15-59	1373	104	1269	104	110	1379	1280	KB	DLL EMUL.	8.8 @ 70%	1.4 @ 83%	1.4 @ 83%	1.4 @ 83%	1.4 @ 83%	1.4 @ 83%	1.4 @ 83%	1.4 @ 83%	1.4 @ 83%	1.4 @ 83%	1.4 @ 83%	1.4 @ 83%

REMARKS C.D. USED : S.O. = 1 1/2"

Cartridge No. TRC-208C
Panel No. RP-260B
Sonde No. RS-121C

SPONTANEOUS-POTENTIAL millivolts	DEPTHS	CONDUCTIVITY millimhos/m = $\frac{1000}{\text{ohms. m}^2/\text{m}}$
$+ \frac{10}{\frac{1}{2} \times 1000}$	2"-100'	400
		600
		1000
		1000
	L.R. 104'	RESISTIVITY -ohms. m ² /m
		16" NORMAL
		0 100 1000

DENVER - CASPER
BILLINGS - BISMARCK
LOS ANGELES

Distributed by
Petroleum Information

LOG NO. 24706 IE

CO. Atlantic Refining
Company

WELL #8-B Navajo

FIELD Horseshoe Canyon

LOC (P.I.) 1924 N/S 576 E/W NW SW
20 31N 16W

San Juan, New Mexico

24706 IB
20 31N 16W

SCHUMBERGER WELL SURVEYING CORPORATION INCORPORATED IN TEXAS <i>Precision & Dependability</i>		COUNTY SAN JUAN, NEW MEX.	
		FIELD or LOCATION HORSESHOE GALLUP WELL NAVAJO # B-8	
		COMPANY ATLANTIC REFINING COMPANY	
		COMPANY ATLANTIC REFINING COMPANY	Other Surveys SL
		WELL NAVAJO # B-8	Location of Well
		FIELD HORSESHOE GALLUP	1980' ± c.d. 660' ± R.W./ SEC. 20-31N-16W 2 4 - 1
		LOCATION SEC. 20-31N-16W	Elevation D.F., K.B., or G.L. 5515
		COUNTY SAN JUAN	PLUG No.
		STATE NEW MEXICO	

RUN No.	DATE	TIME	DEPTH	TEMP.	S.P.	RESISTIVITY	INDUCTION
ONE	6-12-59						
	First Reading	1542					
	Last Reading	109					
	Total Measured	1533					
	Cat. Return	109					
	Cat. Driller	110					
	Depth Reached	1548					
	Bottom Driller	1550					
	Depth Bottom	KB					
	Mixed Test	Q.L. EQUL					
	Dens. Vis.	8.9 40					
	Mixed Resist.	1.6 85					
	Ros. RHT	1.6 85					
	Temp.	1.4 85					
	pH	-					
	" Wyr. Loss	-					
	Bit Size	7 7/8"					
	Speds. - AM	16"					
	AM						
	IND.	40"					
	Org. Rig Time	2 HRS.					
	Trawl Log	2515 EARN					
	Recorded by	KIMBALL					
	Witness	MR. SHEETS					

REMARKS C.D. USED S.O. = 13"

Cartridge No. 155C
Panel No. 4TB
Sonde No. 200E

SPONTANEOUS-POTENTIAL millivolts	DEPTH	CONDUCTIVITY millimhos/m = $\frac{1000}{\text{ohms. m}^2/\text{m}}$
$\frac{10}{4} +$ —	2" - 100' L.R. 109'	INDUCTION 400
		RESISTIVITY - ohms. m ² /m
		16" NORMAL 100
		INDUCTION 1000

Exhibit B

LOG NO. 23016 IE

Distributed by
Petroleum InformationLOG NO. 23016 IE
19 31N 16W**PI.**DENVER • CASPER
BILLINGS • BISMARCK
LOS ANGELES

COMPANY Atlantic Refining Company

WELL #1-B Navajo

FIELD Horseshoe Canyon

LOC (P.I.) 601 N/S 2002 E/W

SE SW 19 31N 16W

San Juan, New Mexico

SCHUMBERGER WELL SURVEYING CORPORATION Production - Electrical Log DALLAS, TEXAS		COUNTY SAN JUAN, NEW MEX. FIELD or LOCATION HORSESHOE GALLUP WELL NAVAJO B-1 COMPANY ATLANTIC REFG. CO.	
COMPANY ATLANTIC REFINING COMPANY NAVAJO B-1 FIELD HORSESHOE GALLUP LOCATION SEC. 19-31N-16W COUNTY SAN JUAN STATE NEW MEXICO		Other Surveys SL Location of Well 601' FR S/L 2002' FR W/L SEC. 19-31N-16W Elevation: D.F.: 5682 K.B.: 5675 or G.L.: 5675 FILING No.	
RUN No. Date First Reading Last Reading Feet Measured C.G. Driller Depth Reached Bottom Driller Depth Datum Mud No. Dens. Visc. Mud Resist. Res. BHT Rmf. Rmc. pH Wtr. Loss Bit Size Specs. - AM IN I.D. Op. Rig Time Truck No. Recorded By Witness	2-20-59 1563 102 1461 102 102 1569 1570 K.B. OIL 9.1 1.7 @ 70' 1.4 @ 85' 1.2 @ 85' 9 @ 85' 5 CC 30 min. 7 7/8" 16" 2 1/2" 40" 3/4" IR 3516 FARM HAMILTON MR. SIEETS	2-20-59 1563 102 1461 102 102 1569 1570 K.B. OIL 9.1 1.7 @ 70' 1.4 @ 85' 1.2 @ 85' 9 @ 85' 5 CC 30 min. 7 7/8" 16" 2 1/2" 40" 3/4" IR 3516 FARM HAMILTON MR. SIEETS	2-20-59 1563 102 1461 102 102 1569 1570 K.B. OIL 9.1 1.7 @ 70' 1.4 @ 85' 1.2 @ 85' 9 @ 85' 5 CC 30 min. 7 7/8" 16" 2 1/2" 40" 3/4" IR 3516 FARM HAMILTON MR. SIEETS
REMARKS C.D. USED S.O. - 1 1/2"			
Cartridge No. C 88 Penel No. B179 Sonde No. C214			
SPONTANEOUS-POTENTIAL millivolts 10, MV	DEPTHS 2"- 100' L.R. 102' 0-1000	CONDUCTIVITY millimhos/m = $\frac{1000}{\text{ohms. m/m}}$ INDUCTION 380 180 0 RESISTIVITY -ohms. m ² /m 16" NORMAL 100 INDUCTION 100	

EXHIBIT B

DENVER • CASPER
BELLINGHAM • BISMARCK
LOS ANGELES

LOO NO 22436 IS 31 31N 16W

SOLUNBERGER WELL SURVEYING CORPORATION					
COUNTY <u>SAN JUAN, N.M.</u> FIELD or LOCATION <u>HORSESHOE GALLUP</u> WELL <u>NAVAJO #28</u>		COMPANY <u>ATLANTIC REFINING COMPANY</u>		COMPANY <u>ATLANTIC REFINING COMPANY</u>	
STATE <u>N.M.</u>		COUNTY <u>SAN JUAN</u>		LOCATION <u>SEC. 31-31N-16W</u>	
RUN NO. <u>ONE</u> <u>-5558</u>		WEL <u>NAVAJO #28</u>		FIELD <u>HORSESHOE GALLUP</u>	
DATE <u>12/17/51</u>		LOCATION <u>SEC. 31-31N-16W</u>		OTHER SURVEYS SL	
TIME <u>1:30 PM</u>		LOCATION <u>SEC. 31-31N-16W</u>		Location of Well 1980' FR E/L 1989' FR S/L SEC. 31-31N-16W	
TIME <u>1:30 PM</u>		LOCATION <u>SEC. 31-31N-16W</u>		Direction D.F. 5468' E.L. 5468' or O.L. 5468'	
TIME <u>1:30 PM</u>		LOCATION <u>SEC. 31-31N-16W</u>		PLUNG No.	
TIME <u>1:30 PM</u>		LOCATION <u>SEC. 31-31N-16W</u>		PLUNG No.	
TIME <u>1:30 PM</u>		LOCATION <u>SEC. 31-31N-16W</u>		PLUNG No.	
TIME <u>1:30 PM</u>		LOCATION <u>SEC. 31-31N-16W</u>		PLUNG No.	
TIME <u>1:30 PM</u>		LOCATION <u>SEC. 31-31N-16W</u>		PLUNG No.	
TIME <u>1:30 PM</u>		LOCATION <u>SEC. 31-31N-16W</u>		PLUNG No.	
TIME <u>1:30 PM</u>		LOCATION <u>SEC. 31-31N-16W</u>		PLUNG No.	
TIME <u>1:30 PM</u>		LOCATION <u>SEC. 31-31N-16W</u>		PLUNG No.	
TIME <u>1:30 PM</u>		LOCATION <u>SEC. 31-31N-16W</u>		PLUNG No.	
TIME <u>1:30 PM</u>		LOCATION <u>SEC. 31-31N-16W</u>		PLUNG No.	
TIME <u>1:30 PM</u>		LOCATION <u>SEC. 31-31N-16W</u>		PLUNG No.	
TIME <u>1:30 PM</u>		LOCATION <u>SEC. 31-31N-16W</u>		PLUNG No.	
TIME <u>1:30 PM</u>		LOCATION <u>SEC. 31-31N-16W</u>		PLUNG No.	
TIME <u>1:30 PM</u>		LOCATION <u>SEC. 31-31N-16W</u>		PLUNG No.	
TIME <u>1:30 PM</u>		LOCATION <u>SEC. 31-31N-16W</u>		PLUNG No.	
TIME <u>1:30 PM</u>		LOCATION <u>SEC. 31-31N-16W</u>		PLUNG No.	
TIME <u>1:30 PM</u>		LOCATION <u>SEC. 31-31N-16W</u>		PLUNG No.	
TIME <u>1:30 PM</u>		LOCATION <u>SEC. 31-31N-16W</u>		PLUNG No.	
TIME <u>1:30 PM</u>		LOCATION <u>SEC. 31-31N-16W</u>		PLUNG No.	
TIME <u>1:30 PM</u>		LOCATION <u>SEC. 31-31N-16W</u>		PLUNG No.	
TIME <u>1:30 PM</u>		LOCATION <u>SEC. 31-31N-16W</u>		PLUNG No.	
TIME <u>1:30 PM</u>		LOCATION <u>SEC. 31-31N-16W</u>		PLUNG No.	
TIME <u>1:30 PM</u>		LOCATION <u>SEC. 31-31N-16W</u>		PLUNG No.	
TIME <u>1:30 PM</u>		LOCATION <u>SEC. 31-31N-16W</u>		PLUNG No.	
TIME <u>1:30 PM</u>		LOCATION <u>SEC. 31-31N-16W</u>		PLUNG No.	
TIME <u>1:30 PM</u>		LOCATION <u>SEC. 31-31N-16W</u>		PLUNG No.	
TIME <u>1:30 PM</u>		LOCATION <u>SEC. 31-31N-16W</u>		PLUNG No.	
TIME <u>1:30 PM</u>		LOCATION <u>SEC. 31-31N-16W</u>		PLUNG No.	
TIME <u>1:30 PM</u>		LOCATION <u>SEC. 31-31N-16W</u>		PLUNG No.	
TIME <u>1:30 PM</u>		LOCATION <u>SEC. 31-31N-16W</u>		PLUNG No.	
TIME <u>1:30 PM</u>		LOCATION <u>SEC. 31-31N-16W</u>		PLUNG No.	
TIME <u>1:30 PM</u>		LOCATION <u>SEC. 31-31N-16W</u>		PLUNG No.	
TIME <u></u>					

Exhibit B



DENVER - CASPER
BILLINGS - BISMARCK
LOS ANGELES

Distributed by
Petroleum Information

LOG NO. 23100 IE

COMPANY Atlantic Refining Company

WELL #24 Navajo

FIELD Horseshoe Canyon

LOC (P.1J) C NW NW

29 31N 16W

San Juan, New Mexico

LOG NO 23100 IE
29 31N 16W

COUNTY <u>SAN JUAN, NEW MEX.</u> FIELD or LOCATION <u>HORSESHOE GALLUP</u> WELL <u>NAVAJO # 24</u>		COMPANY <u>ATLANTIC REFINING COMPANY</u>		COMPANY <u>ATLANTIC REFINING COMPANY</u> WELL <u>NAVAJO # 24</u> FIELD <u>HORSESHOE GALLUP</u> LOCATION <u>SEC. 29-31N-16W</u>		Other Surveys SL Location of Well 660' FR N/L 660' FR W/L SEC. 29-31N-16W		Elevation D.F. K.B. 5485 or G.L.		FILING No.	
FOLD HERE											
REMARKS <u>C.D. USED : S.O. - 1 1/2"</u>											
Cartridge No. <u>208C</u> Panel No. <u>260B</u> Sonde No. <u>121C</u>											
SPONTANEOUS-POTENTIAL millivolts $\frac{10}{4} \text{ MV} +$			DEPTHS 2"-100' L.R. 97'		CONDUCTIVITY millimhos/m = $\frac{1000}{\text{ohms. m}^2/\text{m}}$						
					INDUCTION 400 1200 0						
					RESISTIVITY -ohms. m ² /m						
					16" NORMAL						
					INDUCTION						
					100						
					1000						

Exhibit B

P.I.DENVER • CASPER
BILLINGS • BISMARCK
LOS ANGELES

Distributed by	
LOG NO.	23763 IE Petroleum Information
CO.	Atlantic Refining
	Company
WELL	#26 Navajo
FIELD	Horseshoe Canyon
LOC (P.I.)	C NW NE
	29 31N 16W
	San Juan, New Mexico

LOG NO. 23763 IE
29 31N 16W**P.I. COMPLETION INFORMATION**

SAN JUAN CO.
ATLANTIC REFINING #26 NAVAJO, c nw ne 29-31n-16w, 660 s/a 1980 w/e.
Contr: Banner, NMB-1A.
Spud 3-8-58. Csg: 8-5/8" @ 100 w/115; 4 1/2" @ 1347 w/190. El: 5488 Gr. Log Tops: Upper
Tocito 1294, Sanassee 1434, 1447 TD, PB 1334. Perf 1296-1312; ad oil fract. Comp 3-12-58.
IPP 102 BOPD. Prod Zone: TOCITO, 1296-1312.

HORSESHOE
CANYON
31n-16w

(7)

COLUMBER WELL SURVEYING CORPORATION Production - Electrical Log AUSTIN, TEXAS		COUNTY <u>SAN JUAN, NEW MEX.</u> FIELD or LOCATION <u>HORSESHOE GALLUP</u> WELL <u>NAVAJO - 26</u> COMPANY <u>ATLANTIC REFINING COMPANY</u> STATE <u>NEW MEXICO</u> FILING No. _____	
COMPANY <u>ATLANTIC REFINING COMPANY</u> WELL <u>NAVAJO - 26</u> FIELD <u>HORSESHOE GALLUP</u> LOCATION <u>SEC. 29-31N-16W</u> Location of Well 660' FR N/L 1980' FR E/L SEC. 29-31N-16W Elevation: D.F.L. _____ K.B. 5495 or G.L. _____		Other Surveys SL _____	
RUN No. <u>3-11-59</u> Date First Reading <u>1441</u> Last Reading <u>100</u> Feet Measured <u>1241</u> Csg. Driller <u>100</u> Depth Reached <u>105</u> Bottom Driller <u>1445</u> Depth Bottom <u>KB</u> Mud No. <u>OIL EMUL.</u> Mud Visc. <u>8.9</u> Mud Resist. <u>1.25 @ 68"</u> Res. BHT <u>96 @ 84"</u> Rmc <u>7.2 @ 84"</u> pH <u>-- @ --</u> Wtr. Loss <u>-- CC30 min. --</u> Bit Size <u>7 7/8"</u> Spgrs. AM <u>16"</u> MN <u>27 2"</u> IND. <u>40"</u> Op. Rig Time <u>1 hr.</u> Truck No. <u>2516 L.A.M.</u> Recorded By <u>J.A.L. 10.31</u> Witness <u>MR. S.H. 11.5</u>			
REMARKS <u>C.D. USED ; S.O. = 11"</u> Cartridge No. <u>C80</u> Panel No. <u>B179</u> Sonde No. <u>C214</u>			
SPONTANEOUS-POTENTIAL millivolts 		CONDUCTIVITY millimhos/m = $\frac{1000}{\text{ohms, m/m}}$ INDUCTION 400 1200 3 600 400 RESISTIVITY 1200	

Exhibit B



LOG NO.	22112 S	Distributed by	Petroleum Information
COMPANY	Atlantic Refining Company		
WELL	#22 Navajo		
FIELD	Horseshoe Canyon		
LOC (P.I.)	C NW SE		
	29 31N 16W		
	San Juan, New Mexico		

LOG NO. 22112 S
29 31N 16W

SLUBBERGER WELL SURVEYING CORPORATION 		COUNTY SAN JUAN, N.M. FIELD or LOCATION HORSESHOE GALLUP WELL NAVAJO #22 COMPANY ATLANTIC REFINING COMPANY COUNTY SAN JUAN STATE NEW MEXICO Elevation: K.B., 5512' D.F., 5505' or G.L., 5505'																																													
COMPANY ATLANTIC REFINING COMPANY WELL NAVAJO #22 FIELD HORSESHOE GALLUP LOCATION SEC. 29-31N-16W Other Surveys NONE Location of Well 1980' FR S/L 1980' FR E/L SEC. 29-31N-16W		Log Depths Measured From: KB 1 Ft. above OF																																													
<table border="1"> <tr> <th>RUN No.</th> <th>ONE</th> </tr> <tr> <td>Depth</td> <td>12.8-58</td> </tr> <tr> <td>First Reading</td> <td>1345</td> </tr> <tr> <td>Last Reading</td> <td>1000</td> </tr> <tr> <td>Feet Measured</td> <td>345</td> </tr> <tr> <td>Cat. Schlum.</td> <td>102</td> </tr> <tr> <td>Cat. Driller</td> <td>1348</td> </tr> <tr> <td>Depth Reached</td> <td>1347</td> </tr> <tr> <td>Bottom Driller</td> <td>1347</td> </tr> <tr> <td>Mud Net</td> <td>OIL EMUL</td> </tr> <tr> <td>Dens. Visc.</td> <td>40</td> </tr> <tr> <td>Mud Resist.</td> <td>69 of</td> </tr> <tr> <td>Res. BHT</td> <td>83 of</td> </tr> <tr> <td>pH</td> <td>83 of</td> </tr> <tr> <td>Wtr. Loss</td> <td>CC 30 min</td> </tr> <tr> <td>Wtr. Loss</td> <td>83 of</td> </tr> <tr> <td>Bit Size</td> <td>7 7/8"</td> </tr> <tr> <td>Spdm.</td> <td>3'</td> </tr> <tr> <td>Op. Mfg Time</td> <td>1 HR</td> </tr> <tr> <td>Truck No.</td> <td>1588FARM</td> </tr> <tr> <td>Recorded By</td> <td>PARSON</td> </tr> <tr> <td>Witness</td> <td>JESSUP & SARTAIN</td> </tr> </table>				RUN No.	ONE	Depth	12.8-58	First Reading	1345	Last Reading	1000	Feet Measured	345	Cat. Schlum.	102	Cat. Driller	1348	Depth Reached	1347	Bottom Driller	1347	Mud Net	OIL EMUL	Dens. Visc.	40	Mud Resist.	69 of	Res. BHT	83 of	pH	83 of	Wtr. Loss	CC 30 min	Wtr. Loss	83 of	Bit Size	7 7/8"	Spdm.	3'	Op. Mfg Time	1 HR	Truck No.	1588FARM	Recorded By	PARSON	Witness	JESSUP & SARTAIN
RUN No.	ONE																																														
Depth	12.8-58																																														
First Reading	1345																																														
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Feet Measured	345																																														
Cat. Schlum.	102																																														
Cat. Driller	1348																																														
Depth Reached	1347																																														
Bottom Driller	1347																																														
Mud Net	OIL EMUL																																														
Dens. Visc.	40																																														
Mud Resist.	69 of																																														
Res. BHT	83 of																																														
pH	83 of																																														
Wtr. Loss	CC 30 min																																														
Wtr. Loss	83 of																																														
Bit Size	7 7/8"																																														
Spdm.	3'																																														
Op. Mfg Time	1 HR																																														
Truck No.	1588FARM																																														
Recorded By	PARSON																																														
Witness	JESSUP & SARTAIN																																														
REMARKS VIC No.: A-60 VIS No.: A-77 VIP No.: A-59 MUD FROM MUD PIT																																															
Velocity (feet per second) = $\frac{1,000,000}{\text{Interval Transit Time (microseconds per foot)}}$																																															
SPONTANEOUS-POTENTIAL millivolts -10 MV +		INTERVAL TRANSIT TIME microseconds per foot Increases Span 3 Ft. 2 Receivers																																													
DEPTHS 2"-100' L.R. 1000'		106 86 66																																													

Exhibit B



LOG NO.	23322 IE	Distributed by	Petroleum Information
COMPANY	Atlantic Refining Company		
WELL	#4-B Navajo		
FIELD	Horseshoe Canyon		
LOC (P.I.)	C NW SE		
	19 31N 16W		
	San Juan, New Mexico		

LOG NO. 23322 IE
19 31N 16W

SCHUMBERGER WELL SURVEYING CORPORATION Division - Electrical Log 10000 10th Street Denver, Colorado 80202		COUNTY <u>SAN JUAN, NEW MEX.</u> FIELD or LOCATION <u>HORSESHOE GALLUP</u> WELL <u>NAVAJO B-4</u> COMPANY <u>ATLANTIC REFINING COMPANY</u> COUNTY <u>SAN JUAN</u> STATE <u>NEW MEXICO</u> LOCATION <u>SEC. 19-31N-16W</u> WELL <u>NAVAJO B-4</u> FIELD <u>HORSESHOE GALLUP</u> LOCATION <u>SEC. 19-31N-16W</u> Other Surveys SL Location of Well 1980' FR S/L 1980' FR E/L SEC. 19-31N-16W Elevation: D.F. 5542 K.B. 5535 or G.L. 5535 FILING No.	
RUN No. <u>ONE</u> Date <u>3-15-59</u> First Reading <u>1456</u> Last Reading <u>97</u> Feet Measured <u>1359</u> Csg. Schlum. <u>97</u> Csg. Driller <u>97</u> Depth Reached <u>1462</u> Bottom Driller <u>1462</u> Depth Datum <u>DE</u> Mud Nat. <u>GEL-CHEN-DOLL</u> Dens. Visc. <u>8.91 45</u> Mud Resist. <u>1.8 @ 60"</u> Res. BHT <u>8 @ 85"</u> Rinf. <u>8 @ 85"</u> Rinc. <u>1.5 @ 85"</u> " W/L Loss <u>-- CC 30 min.</u> Bit Size <u>7 7/8"</u> Specs. <u>AM</u> MN IND. Oor. Rig Time Truck No. <u>1588 FARM</u> Recorded by <u>HANDLEY</u> Witness <u>MR. FLET</u>	REMARKS <u>C.D. USED</u> <u>S.O. = 1 1/2"</u> <u>MUD FROM FLOW LINE</u> Cartridge No. <u>C-182</u> Panel No. <u>B-138</u> Sonde No. <u>C-215</u>		
SPONTANEOUS-POTENTIAL millivolts $- \frac{10}{1} \text{ MV} +$	DEPTHS 2"- 100' L.R. 97'	CONDUCTIVITY millimhos/m = $\frac{1000}{\text{ohms. m}^2/\text{m}}$ INDUCTION 400 1200 0 600 400 RESISTIVITY -ohms. m ² /m 16" NORMAL 0 100 0 1000 INDUCTION 0 100 0 1000	

Exhibit B

LOG NO. 23491 IE Distributed by Petroleum Information

LOG NO. 23491 IE
19 31N 16W



DENVER - CASPER
BILLINGS - BISMARCK
LOS ANGELES

CO. Atlantic Refining Company

WELL #5-B Navajo

FIELD Horseshoe Canyon

LOC (P.I.) 1980 S/N 2023 E/W

SE NW 19 31N 16W

San Juan, New Mexico

SCHUMBERGER WELL SURVEYING CORPORATION Production - Electrical Log		COUNTY SAN JUAN, NEW MEX. FIELD or LOCATION HORSESHOE GALLUP WELL NAVAJO B-5 COMPANY ATLANTIC REFINING COMPANY	
COMPANY ATLANTIC REFINING COMPANY WELL NAVAJO B-5 FIELD HORSESHOE GALLUP LOCATION SEC. 19-31N-16W		Other Surveys NONE Location of Well 1980' FR N/L 2023' FR W/L SEC. 19-31N-16W Elevation: D.F. 5528 K.B. 5521 or G.L. 5521	
RUN No. ONE Date 3-20-59 First Reading 1467 Last Reading 102 Feet Measured 1365 Csg. Sclum. 102 Csg. Driller 102 Depth Reached 1473 Bottom Driller 1470 Mud Datum 1470 Mud No. 1470 Mud Test. 1470 Mud Resist. 1470 Res. BHT 1470 Rmt 1470 Rmc 1470 PH 1470 Wtr. Loss 1470 Bit Size 7 7/8" Specs. - AM 16" IND. 27'2" 40" 1 LIR. 1559 FARN. 1500 MR. SILETS		FOLD HERE REMARKS C.D. TAPED ; S.O. = Cartridge No. 250C Panel No. 237B Sonde No. 450C	
SPONTANEOUS-POTENTIAL millivolts 10 + - MV		CONDUCTIVITY millimhos/m = $\frac{1000}{\text{ohms. m}^2/\text{m}}$ INDUCTION 200 RESISTIVITY -ohms. m ² /m 16" NORMAL 100 1000	

Exhibit B

Distributed by
Petroleum Information

LOG NO. 23485 IE

CO. Atlantic Refining
Company

WELL #7-B Navajo

FIELD Horseshoe Canyon

LOC (P.I.) C SE SW
20 31N 16W

San Juan, New Mexico

LOG NO 23485 IE

20 31N 16W

 Schlumberger Well Surveying Corporation <i>Production - Electrical Log</i>		COUNTY SAN JUAN, N.M. FIELD or LOCATION HORSESHOE GALLUP WELL NAVAJO B #7	
		COMPANY ATLANTIC REFINING COMPANY	
COMPANY ATLANTIC REFINING COMPANY WELL NAVAJO B #7 FIELD HORSESHOE GALLUP LOCATION SEC. 20-31N-16W		Other Surveys NONE Location of "J" 660' FR S.L. 1980' FR W/L SEC. 20-31N-16W	
COUNTY SAN JUAN STATE NEW MEXICO		Elevation: D.F. K.A.: 5482' or G.L.: 5475'	
RUN No. _____ Date First Reading 3-26-59 Last Reading 1526 Feet Measured 98 Csg. Schlum. 1478 Csg. Driller 98 Depth Reached 1282 Bottom Driller 1586 Mud Nat. KB Dens. Nat. 8.8 @ 140' Mud Resist. 2.0 @ 79' Res. BHT 1.6 @ 87' Rmt. --- Rmc. --- pH --- Wtr. Loss 9.2 @ --- Bit Size 6 CC 30 min. Spgrs.—AM 7 7/8" IND. 16" Opr. Rig Time 1 HR Truck No. 2515EARM Recorded By JCL:mjs Witness TR. SA:ljl			
FOLD HERE			
REMARKS C.D. USED : S.O. = 11"			
Cartridge No. 155C Panel No. 41 P Sonde No. 164C			
SPONTANEOUS-POTENTIAL millivolts $\frac{10}{\pm MV} +$		CONDUCTIVITY millimhos/m — $\frac{1000}{ohms. m^2/m}$ INDUCTION 200 600 400 RESISTIVITY — ohms. m²/m 16" NORMAL 0 ————— 100 0 ————— 1000	

Exhibit B



DENVER - CASPER
BILLINGS - BISMARCK
LOS ANGELES

LOG NO. 22435 IE	Distributed by Petroleum Information
COMPANY Atlantic Refining Company	
WELL #17 Navajo	
FIELD Horseshoe Canyon	
LOC(P.I.) 660 S/N 1980 W/E	
31 31N 16W	
San Juan, New Mexico	

LOG NO. 22435 IE
31 31N 16W

COUNTY SAN JUAN, N.M. FIELD or LOCATION HORSESHOE CANYON WELL NAVAJO #17 COMPANY ATLANTIC REFINING COMPANY		COMPANY ATLANTIC REFINING COMPANY WELL NAVAJO #17 FIELD HORSESHOE CANYON LOCATION SEC. 31-31N-16W LOCATION OF WELL 660' FR N/L 1980' FR E/L SEC. 31-31N-16W Elevation D.F. K.A. 5457.1 or O.L. 5450.1 FILING No.	
RUN No. ONE Date 1-31-58 First Reading 1305 Last Reading 97 Total Measured 1202 Cor. Station 97 Cor. Driller 36 Depth Measured 1310 Bottom Driller 1310 Depth Datum 128 Fluid Test, 8.9 Density, 1.5 Visc. 7.4 App. Resist. 1.8 Res. BHT 1.5 Ref. 1.2 Bore 8.6 pH 8.6 Wt. Loss 6 Wt. Loss 6 Sp. Grav. 1.61 IN. 40 O.C. Log Time 1:58 Log No. 1587 Logged By HAMILTON Witness MR. SHEETS & MR. BAKER		Other Surveys SL Location of Well 660' FR N/L 1980' FR E/L SEC. 31-31N-16W Elevation D.F. K.A. 5457.1 or O.L. 5450.1 FILING No.	
REMARKS C.D. USED, S.O. = 1 1/2"			
Cartridge No. C 250 Panel No. B 237 Sonde No. C 450			
SPONTANEOUS-POTENTIAL millivolts 10 + - HV		CONDUCTIVITY millimhos/m - $\frac{1000}{\text{ohms} \cdot \text{m}^2/\text{m}}$ INDUCTION 400 200 0 600 400 RESISTIVITY -ohms. m ² /m 16" NORMAL 0 100 0 1000 INDUCTION 0 100 0 1000 2" 100' 400 600 800 97' 900	

Exhibit B



DENVER - CASPER
BILLINGS - BISMARCK
LOS ANGELES

Distributed by Petroleum Information	
LOG NO. 21838 IE	
COMPANY Atlantic Refining Company	
WELL #16 Navaajo	
FIELD Horseshoe Canyon	
LOC (P.I.) C SE NE	
31 31N 16W	
San Juan, New Mexico	

LOG NO. 21838 IE
31 31N 16W

SCHLUMBERGER WELL SURVEYING CORPORATION Production - Electrical Log		COUNTY SAN JUAN, N.M. FIELD or LOCATION HORSESHOE GALLUP WELL NAVAJO # 16 COMPANY ATLANTIC REFG. COMPANY COMPANY ATLANTIC REFINING COMPANY WELL NAVAJO # 16 FIELD HORSESHOE GALLUP LOCATION SEC. 31-31N-16W COUNTY SAN JUAN STATE NEW MEXICO FILING No.		Other Surveys Location of Well 1980' FR N/L 660' FR E/L SEC. 31-31N-16W Elevation D.F.: K.B.: 5432 or G.L.: 5425	
RUN No. ONE Date 11-20-58 First Reading 1304 Last Reading 1207 Feet Measured 97 Csg. Driller -- Depth Reached 97 Bottom Driller 1310 Depth Datum 1310 Mud Net KB Mud Visc. 9.61 46 Mud Resist. 2 @ 64 Res. BHT 1 @ 83 Rmc 1 @ 83 pH -- @ Wt. loss -- @ Bit Size 7 7/8" Specs. - AM 16" IND. 40" Opr. Rig Time 1552 AM Truck No. DILLI Recorded by CUMELLA Witness	FOLD HERE				
REMARKS MUD FROM FLOW LINE					
Cartridge No. 250 Panel No. 237 Sonde No. 450					
SPONTANEOUS-POTENTIAL millivolts		CONDUCTIVITY millimhos/m = $\frac{1000}{\text{ohms. m}^2/\text{m}}$			
		INDUCTION 400 200 0 600 400			
		RESISTIVITY -ohms. m ² /m			
		16" NORMAL 0 100 0 1000			
		INDUCTION 0 100 0 1000			
		0 100 0 1000			
		0 100 0 1000			



DENVER - CASPER
BILLINGS - BISMARCK
LOS ANGELES

LOG NO. 23223 1E		Distributed by Petroleum Information
COMPANY Atlantic Refining Company		
WELL #3-B Navajo		
FIELD Horseshoe Canyon		
LOC (P.I.) C SE SE		
19 31N 16W		
San Juan, New Mexico		

LOG NO. 23223 1E
19 31N 16W

		COUNTY SAN JUAN, N.M. FIELD or LOCATION HORSESHOE GALLUP WELL NAVAJO B #3 COMPANY ATLANTIC REFINING COMPANY COUNTY SAN JUAN STATE NEW MEXICO LOCATION SEC. 14-31N-16W FIELD HORSESHOE GALLUP LOCATION SEC. 14-31N-16W Other Surveys NONE Location of Well 660' FR S/L 660' FR F/L SEC. 14-31N-16W Elevation: D.F. 5512' K.B. 5512' or G.L. 5505'	
RUN No. ONE Date 3-7-55 First Reading 1441 Last Reading 105 Feet Measured 1336 Csg. Depth 105 Depth Reached 1447 Bottom Driller 1450 Mud Net 0.11 ENCL. Mud Visc. 8.8 42" Mud Resist. 2.2 @ 58" Res. BHT 1.5 @ 84" Rmt. --- @ ---" Rmt. --- @ ---" pH --- @ ---" Wtr. Loss --- @ ---" Bit Size 7 7/8" Spcgs. --- AM IND. 40" TIR. 2515 FARM Truck No. DILL Recorded by MR. SHEETS Witness		FOLD HERE REMARKS C.D. USED : S.O. = 12" Cartridge No. Panel No. Sonde No. C-214	
SPONTANEOUS-POTENTIAL millivolts $10 \frac{1}{V} +$		CONDUCTIVITY millimhos/m = $\frac{1000}{\text{ohms. m}^2/\text{m}}$ DEPTHS 2'-100' INDUCTION 400 200 RESISTIVITY -ohms. m ² /m 16" NORMAL 100 1000 INDUCTION 100 1000 Csg. 105'	