

CARPER

DRILLING COMPANY, INC.

O I L P R O D U C T I O N S A N D D R I L L I N G

EMERY CARPER, PRESIDENT
STANLEY CARPER, EXEC. VICE-PRES. & TREAS.
MARSHALL ROWLEY, VICE-PRES.
FRANCES BOOKER, SECRETARY
NELLE MILLER, ASST. TREAS.

ARTESIA, NEW MEXICO
CARPER BUILDING

SHERWOOD 6-2784
SHERWOOD 6-2785

September 17, 1960

New Mexico Oil Conservation Commission
P. O. Box 871
Santa Fe, New Mexico

Attention: Mr. A. L. Porter

Gentlemen:

Reference is made to Case 2078 which is an
Application of Chambers & Kennedy for an oil - oil dual completion .
This case is scheduled to be heard before an examiner on Wednesday,
September 21, 1960.

It is our understanding that if this case is approved,
it will be confined to the North Shugart Queen-Grayburg Pool and
if this is correct we have no objection.

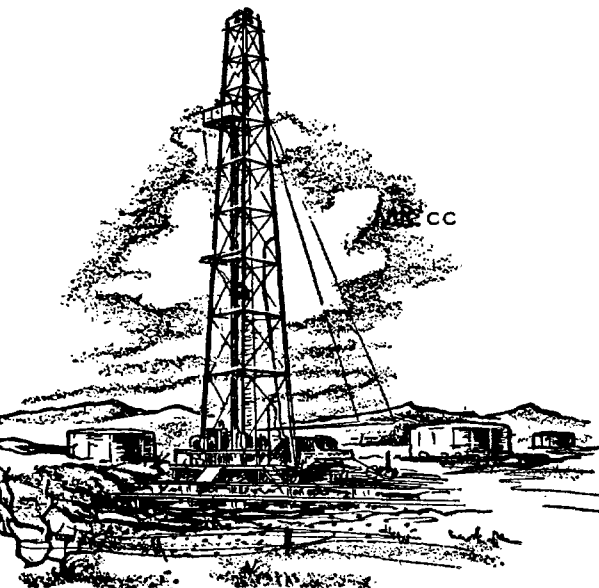
In the event this case should be extended to cover
wells in the Shugart Pool, we wish to register a vigorous protest before
such action is taken.

Yours very truly,

CARPER DRILLING COMPANY, INC.

Marshall Rowley

Marshall Rowley



C. FRED CHAMBERS
W. D. KENNEDY

Chambers & Kennedy
OFFICE SUITE 607
MIDLAND NATIONAL BANK BUILDING
MIDLAND, TEXAS
August 24, 1960
1960 AUG 25 AM 10:00

TELEPHONE
MU 34643

W. J. Alexander
W. J. Alexander
W. J. Alexander

Mr. Daniel S. Nutter
Oil Conservation Commission
P. O. Box 871
Santa Fe, New Mexico

Dear Mr. Nutter:

Attached you will find a diagrammatic sketch of the two pumping unit installation that Chambers & Kennedy proposes to use to dually complete their Monterey-State #2 well. In this installation each zone would have its own individual bottom hole pump, rod string and pumping unit.

If there is additional information that we could furnish you, we will be glad to do so.

Yours very truly,

CHAMBERS & KENNEDY

W. J. Alexander
W. J. Alexander
Engineer

WJA:aa
Encl.

W. J. Alexander
W. J. Alexander
W. J. Alexander

OIL CONSERVATION COMMISSION

P. O. BOX 871

SANTA FE, NEW MEXICO

Case 2078

August 11, 1960

**Chambers and Kennedy
Suite 607
Midland National Bank Building
Midland, Texas**

Gentlemen:

We are in receipt of your application for administrative approval to dually complete your Monterey State Well No. 2, located in Unit D, Section 32, Township 18 South, Range 31 East, Eddy County, New Mexico.

We regret to inform you that this application cannot be approved administratively, but must go to public hearing for a decision. This is necessary for two reasons: First, our rules require that any dual completion, to be eligible for administrative approval, must be within one mile of a similar dual completion which has previously been authorized after notice and hearing, or it must be within the horizontal limits of two pools which have been approved for dual completion after notice and hearing. Your well is not within one mile of a previously authorized dual completion in the same two zones nor is it within the horizontal limits of any pool producing from the Yates or the Queen formations, the formations in which you propose to complete.

Secondly, your request for dual completion cannot be handled administratively because of the dual zone pumping equipment which you propose to install. The Commission has never recognized this type of equipment as eligible for administrative approval and has in fact approved only one such application after hearing. This was the Cities Service case, which, after two hearings was finally approved on a temporary

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Chambers and Kennedy

August 11, 1960

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one-year basis, during which time a series of carefully controlled tests were to be made to evaluate the equipment. I might add that Cities Service found it necessary to replace the first pump so tested before the year was up and was then authorized, after a third hearing, to install a second pump under similar testing requirements. Cities Service recently removed this pump after approximately six-months service. This, according to our understanding of the matter, was necessitated by failure of the equipment to adapt itself to the conditions which were encountered in the well.

Please advise us as to whether or not you wish us to docket your application for hearing.

Very truly yours,

DANIEL S. NUTTER
Chief Engineer

DSN/eg

cc: Mr. Mose Armstrong
Oil Conservation Commission
Artesia, New Mexico

New Mexico Oil Conservation Commission
Santa Fe, New Mexico

W A I V E R

The undersigned, being an offset operator to the Chambers & Kennedy Monterey State in the N. Shugart Queen Grayburg field, Eddy County, New Mexico, hereby waives any right to protest the dual completion of the Monterey State #2 well with the understanding that the Penrose zone will be produced through 1½ inch tubing, and the Yates zone will be produced through two inch tubing.

TEXAS GULF PRODUCING COMPANY
MIDLAND, TEXAS

BY: Herb Hull

DATE: July 14, 1960

New Mexico Oil Conservation Commission
Santa Fe, New Mexico

W A I V E R

The undersigned, being an offset operator to the Chambers & Kennedy Monterey State in the N. Shugart Queen Grayburg field, Eddy County, New Mexico, hereby waives any right to protest the dual completion of the Monterey State #2 well with the understanding that the Penrose zone will be produced through 1½ inch tubing, and the Yates zone will be produced through two inch tubing.

Iverson & Welch
Artesia, New Mexico

BY: _____

L S Stileh

DATE: _____

7 - 19 - 60

New Mexico Oil Conservation Commission
Santa Fe, New Mexico

W A I V E R

The undersigned, being an offset operator to the Chambers & Kennedy Monterey State in the N. Shugart Queen Grayburg field, Eddy County, New Mexico, hereby waives any right to protest the dual completion of the Monterey State #2 well with the understanding that the Penrose zone will be produced through 1½ inch tubing, and the Yates zone will be produced through two inch tubing.

THE PURE OIL COMPANY
~~ROSWELL, - NEW-MEXICO-~~
Fort Worth, Texas

BY:

James L. Mann
Manager, Texas Producing Division

DATE: 7/18/60

New Mexico Oil Conservation Commission
Santa Fe, New Mexico

W A I V E R

The undersigned, being an offset operator to the Chambers & Kennedy Monterey State in the N. Shugart Queen Grayburg field, Eddy County, New Mexico, hereby waives any right to protest the dual completion of the Monterey State #2 well with the understanding that the Penrose zone will be produced through 1½ inch tubing, and the Yates zone will be produced through two inch tubing.

SUNRAY MID-CONTINENT OIL COMPANY
Hinkle Building
Roswell, New Mexico

BY: _____

E. J. Hinkle

DATE: _____

7/25/60

Chambers & Kennedy

SUITE 607
MIDLAND NATIONAL BANK BUILDING

MIDLAND, TEXAS

August 16, 1960

C. FRED CHAMBERS
W. D. KENNEDY

TELEPHONE
MU 3-4643

New Mexico Oil Conservation Commission
Santa Fe, New Mexico

Re: CHAMBERS & KENNEDY SUNRAY MID-CONTINENT #2
Eddy County, New Mexico

Gentlemen:

Please find enclosed additional waiver from
Yates Brothers, Artesia, New Mexico concerning the
dual completion of the CHAMBERS & KENNEDY SUNRAY
MID-CONTINENT #2

This signed waiver was received in our office
today.

Very truly yours,

CHAMBERS & KENNEDY

J. Davis
By: J. Davis,
Production Secretary

New Mexico Oil Conservation Commission
Santa Fe, New Mexico

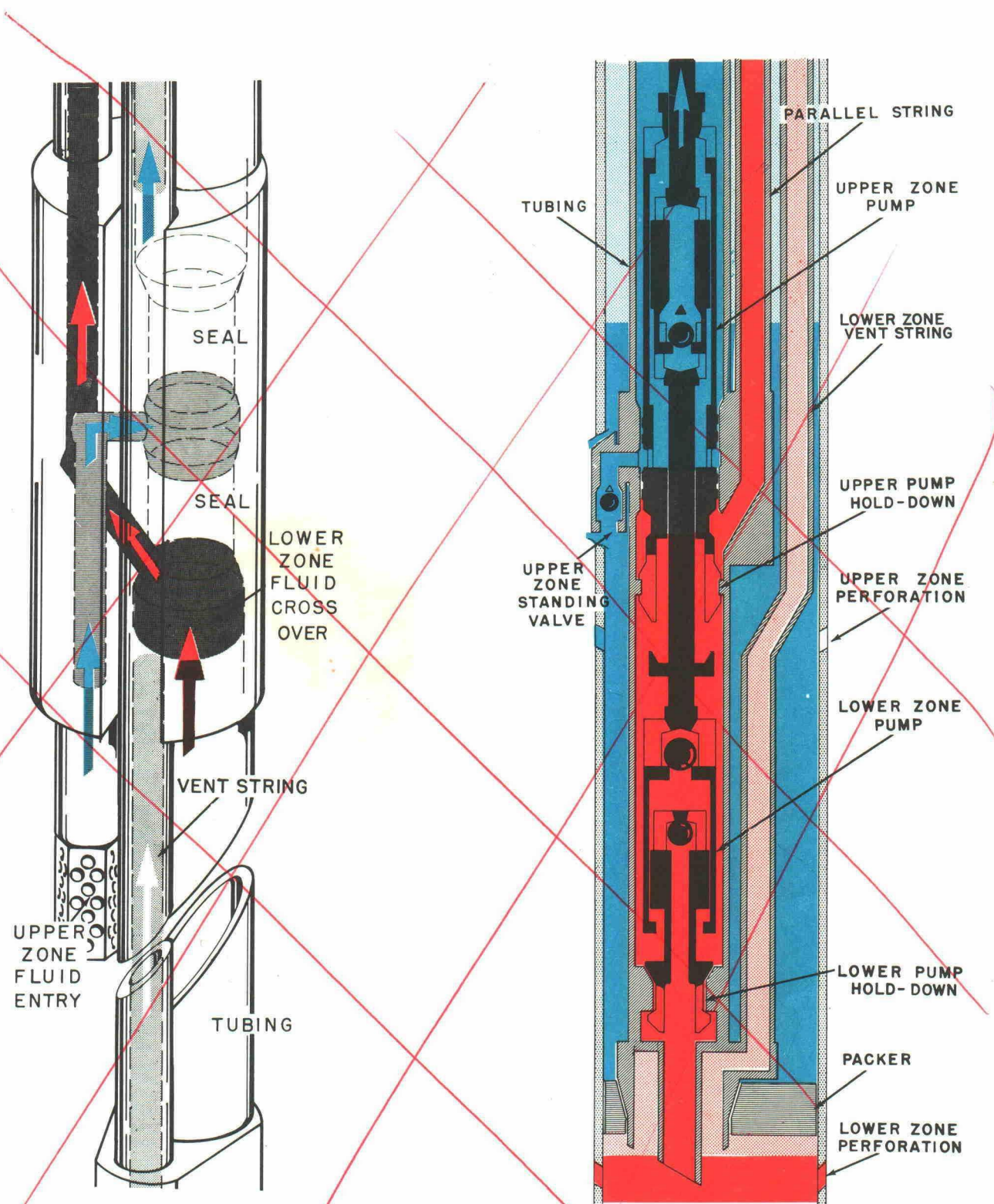
W A I V E R

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YATES BROTHERS
Artesia, New Mexico

BY: *D. Yates*

DATE: 8/16/50



In the **DZ2090** installation a packer separates the perforated intervals of the upper and lower zone. Both upper and lower zone pumps are positioned in the long string of tubing and are run in, operated, and pulled with a single string of rods. The long string conducts the upper zone production to the surface, a second string of tubing conducts the lower zone gas from below the packer to the surface, and a third string conducts the lower zone fluid from the crossover shoe to the surface. Gas from the upper zone is vented up the casing. The two shorter strings are clamped onto the long string and they are run into the well together. The vent string passes the crossover shoe in a slot provided for this purpose. The **DZ2090** is designed to run in 5½ in. casing.

FIG. 2
SINGLE PACKER TRIPLE STRING
Installation Typical of
DZT2090

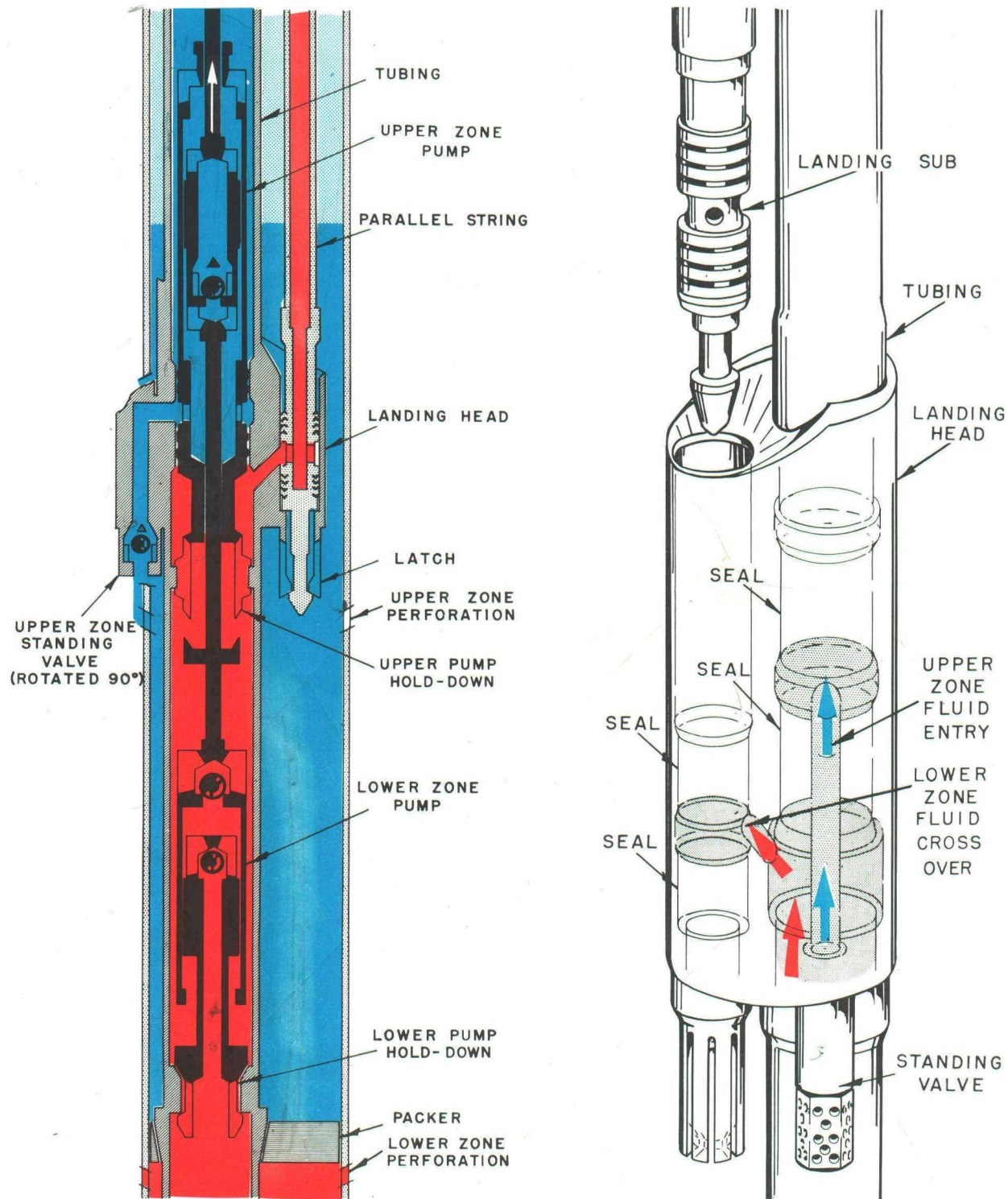
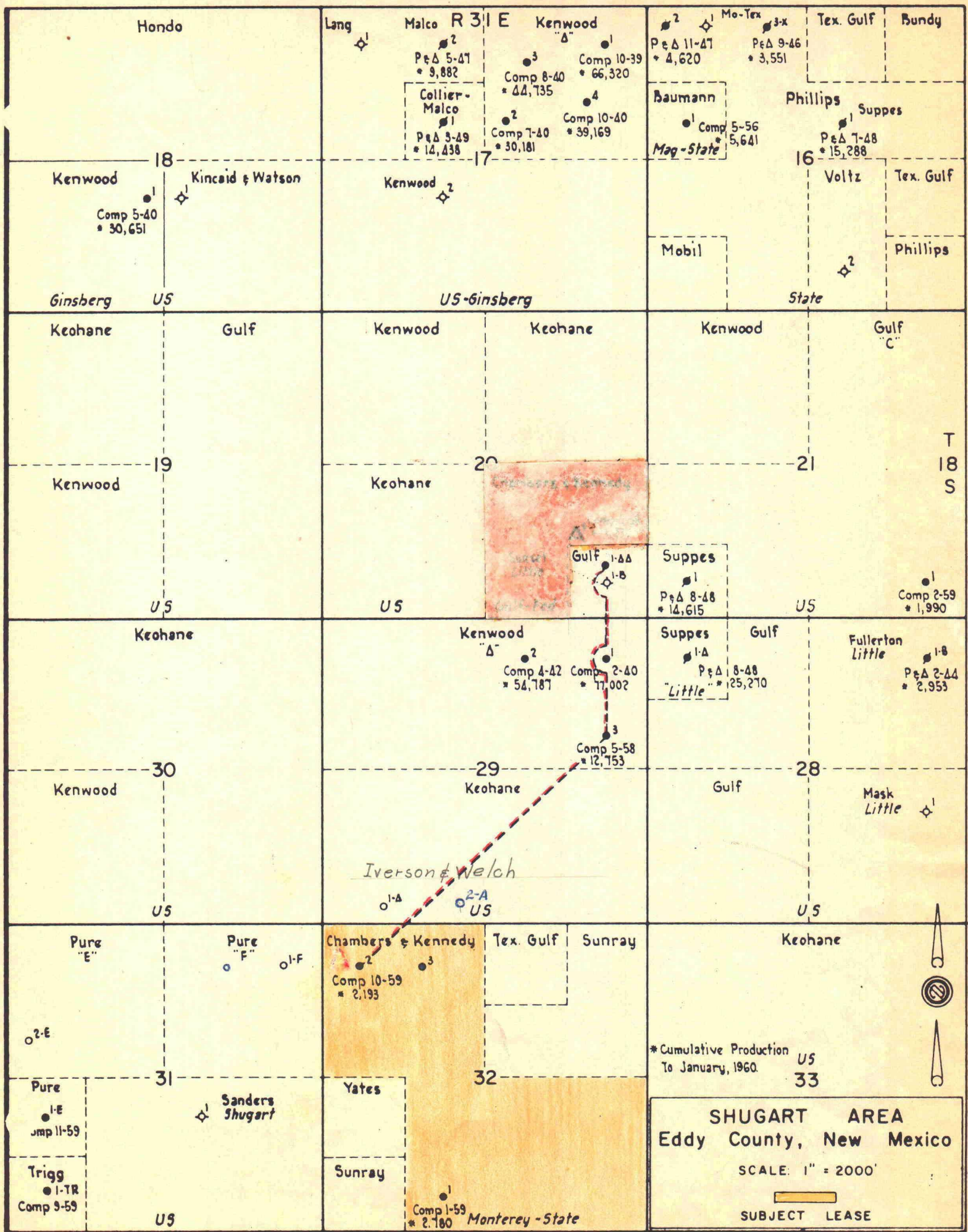


FIG. 3
SINGLE PACKER DOUBLE STRING
 Installation Typical of
 DZT2092-55 DZT2092-70
 DZT2592-70

In the DZ2092 and DZ2592 installations, a packer separates the perforated intervals of the upper and lower zone. Both upper and lower zone pumps are positioned in the long string of tubing, and are run in, operated, and pulled with a single string of rods. The long string conducts the upper zone production while a second string of tubing conducts the lower zone production to the surface. No gas is vented from the lower zone, but gas from the upper zone is vented up the casing. The two tubing strings are run independently. The crossover shoe with integral landing head is run in on the long string. A landing spear is run on the bottom of the short string. This spear is automatically guided into place by the landing head and the seal elements are properly positioned by a no-go ring and latch.



Chambers & Kennedy

SUITE 607
MIDLAND NATIONAL BANK BUILDING

MIDLAND, TEXAS

SEPTEMBER 19, 1960

C. FRED CHAMBERS
W. D. KENNEDY

BEFORE EXAMINER NUTTER	
OIL CONSERVATION COMMISSION	
EXHIBIT NO. <u>1</u>	TELEPHONE MU 3-4643
CASE NO. <u>2078</u>	

Chambers & Kennedy Monterey State #2
1-N, 32-18-31, Eddy Co., New Mexico

This well has 5½", 14# csg. with a drift dia. of 4.887" Cemented @ 3500'. To dual complete this well either of the following installations may be used.

Installation #1

Two strings of HYDRIL type "CS" tubing with a joint O.D. of 2.33" or a combined dimension of 4.66" and a clearance of 0.227" can be used. This tubing can be purchased @ \$1.339/ft.

Yates pay @ 2620 @ \$1.339/ft	:	3,408.18
Penrose pay @ 3430 @ 1.339/ft	:	<u>4,592.77</u>
		8,100.95

Installation #2

One string of Tex-Tube 1½" series 301 Integral joint tubing with a joint O.D. of 2.110". And one string of Tex-Tube 2 3/8" series 301 Integral joint tubing with a joint O.D. of 2.70" or a combined dimension of 4.81" and a clearance of 0.077 inches can be used. The 1½ tubing can be purchased @ \$0.501/ft and the 2 3/8" @ \$0.864/ft.

Yates Pay @ 2620 @ \$0.501/ft.	:	1,312.62
Penrose Pay @ 3430 @ \$0.864/ft.	:	<u>2,963.52</u>
		4,276.14

With installation No. 2 Chambers & Kennedy will be able to make a saving of \$3,842.81, or a difference of 89.45%.

With 1½" tubing in this well at 2620' it can be pumped with an 1¼" insert pump on ½" sucker rods, and a 25,000 inch-pound torque gear box pumping unit. The attached calculations by Continental-Emsco give the production that may be produced with reasonable loads for this unit. These production

rates are high enough to recover the allowable of this well for any rate that may be established in the foreseeable future. At the present time we do not anticipate much water in this zone, but should it become a factor we will be able to handle it because these calculations are for water at the pump level with no help from gas.

Since the lower zone of this well has been sand-fractured and it may be necessary from time to time to clean out the sand from the well bore for stimulation reasons, we propose to use a Brown Oil Tools By-Pass packer. This packer may be pulled so that cleanout work may be performed. This packer also has the added advantage that gas from below the packer may be vented into the 2 3/8" tubing string through which the lower zone will be producing whereby less gas locking trouble should be experienced by the lower pump.

WELL INSTALLATION WORK SHEET

Company Albuquerque 7 Lease _____ Well # _____ Date 9-19-60
 Plunger 1 1/2 Stroke 26 SPM 20 Pump Depth 2600 Desired Prod. Small Impulse Factor 1.15
1 1/2 5/8" Rods 100 % 2600 ft. 3/4" Rods _____ % _____ ft. 7/8" Rods _____ % _____ ft.
 1" Rods _____ % _____ ft. 1-1/8" Rods _____ % _____ ft.

Weight of Fluid: $W_f = (\text{Wt. per foot on Plunger}) \times (\text{Depth}) = \underline{1380}$ lbs.

SIZE	WT/FT	LENGTH	BUOY.	EFFECTIVE WT OF RODS	F	STRESS
<u>1 1/2</u> 5/8"	<u>7.2</u> (1.14)	<u>2600</u>	(.875)	<u>1640</u> lbs	<u>1.15</u>	<u>1880</u> lbs
						<u>3260</u> lbs ÷ .307 = <u>16.500</u> psi
3/4"	(1.62)	()	(.875)	() lbs	()	() lbs ÷
						Load on top 3/4" Rods = () lbs ÷ .442 = () psi
7/8"	(2.17)	()	(.875)	() lbs	()	() lbs ÷
						Load on top 7/8" Rods = () lbs ÷ .601 = () psi
1"	(2.88)	()	(.875)	() lbs	()	() lbs
						Load on top 1" Rods = () lbs ÷ .785 = () psi
1-1/8"	(3.67)	()	(.875)	() lbs	()	() lbs
						Load on top 1-1/8" Rods = () lbs ÷ .994 = () psi
Effective Weight of Rods: $EW_r =$				<u>1640</u> lbs	PPRL = <u>3260</u> lbs	

Minimum Polished Rod Load: $MPRL = EW_r (1.87 - F) = \underline{1640} (1.87 - \underline{.72}) = \underline{1185}$ lbs.

Load Ratio: $\frac{(PPRL - MPRL)}{(PPRL)} (100) = \frac{(\underline{2085})}{(\underline{3260})} (100) = \underline{64}$ %

Coefficient of Rod Stretch

$C_r = C_1 \%_1 + C_2 \%_2 + C_3 \%_3 = () () + () () + () () =$

Coefficient of Tubing Stretch ($C_t = 0$ if tubing anchored) Not Anchored: $C_t =$

Total Coefficient of Stretch: $C = C_r + C_t = + =$

Total Stretch: $E = C (D/1000)^2 = ()^2 = \underline{12}$ in.

Overtravel: $O = (1.41) (F-1) (D/1000)^2 = (1.41) (\underline{.15}) (\underline{6.02})^2 = \underline{1.5}$ in.

Plunger Stroke: $S_p = S - E + O = \underline{26} - \underline{12} + \underline{1.5} = \underline{15.5}$ in.

Theoretical Production (100%): $(K, \text{PLGR. Constant}) (S_p) (\text{SPM}) = (\underline{.182}) (\underline{15.5}) (\underline{20}) = \underline{56.5}$ bbls/day

Production at 80% Pump Efficiency: $.80 (\text{Theo. Prod.}) = .80 (\underline{56.5}) = \underline{45}$ bbls/day

Counterbalance Effect: $W_r + \frac{\text{Fluid Wt.}}{2} = \underline{1640} + \underline{640} = \underline{2330}$ lbs

Peak Torque: $(PPRL - CB) (S/2) = (\underline{930}) (\underline{13}) = \underline{12100}$ in. lbs.

Prime Mover Horsepower (Single Cylinder & CE Green ▲ Electric Motors)

$HP = \frac{\text{Depth} \times \text{Prod. (Based on 100\% PR Stroke)}}{85,000} = \frac{() ()}{85,000} =$

Non-Synchronous Pumping Speeds (Desirable) _____ SPM

Remarks: _____

ILLEGIBLE

WELL INSTALLATION WORK SHEET

Company Chapman & Company Lease _____ Well # _____ Date 4-17-60
 Plunger 1 1/8" Stroke 26 SPM 16.5 Pump Depth 7000 Desired Prod. 45 Impulse Factor 1.10
 1/2" Rods 100 % 2600 ft. 3/4" Rods _____ % _____ ft. 7/8" Rods _____ % _____ ft.
 1" Rods _____ % _____ ft. 1-1/8" Rods _____ % _____ ft.

Weight of Fluid: $W_f =$ (Wt. per foot on Plunger) Multiplied by (Depth) = 1380 lbs.

SIZE	WT/FT	LENGTH	BUOY.	EFFECTIVE WT OF RODS	F	STRESS
1-1/8"	(3.67)	(<u>2600</u>)	(.875)	(<u>1640</u> lbs)	(<u>1.10</u>)	= <u>1304</u> lbs
Load on top 1-1/8" Rods						= <u>3184</u> lbs ÷ <u>.197</u> = <u>16,160</u> psi
7/8"	(2.17)	(_____)	(.875)	(_____ lbs)	(_____)	= _____ lbs ÷ _____ = _____ psi
Load on top 7/8" Rods						= _____ lbs ÷ .601 = _____ psi
3/4"	(1.62)	(_____)	(.875)	(_____ lbs)	(_____)	= _____ lbs ÷ _____ = _____ psi
Load on top 3/4" Rods						= _____ lbs ÷ .442 = _____ psi
1"	(2.88)	(_____)	(.875)	(_____ lbs)	(_____)	= _____ lbs ÷ _____ = _____ psi
Load on top 1" Rods						= _____ lbs ÷ .785 = _____ psi
1-1/8"	(3.67)	(_____)	(.875)	(_____ lbs)	(_____)	= _____ lbs ÷ .994 = _____ psi
Load on top 1-1/8" Rods						= _____ lbs ÷ .994 = _____ psi
Effective Weight of Rods: $EW_r =$ (_____ lbs)				PPRL = <u>3184</u> lbs		

Minimum Polished Rod Load: $MPRL = EW_r (1.87 - F) =$ (1640) (.77) = 1270 lbs.

Load Ratio: $\frac{(PPRL - MPRL)}{(PPRL)} (100) =$ (1914) (3184) (100) = 60 %

Coefficient of Rod Stretch

$C_r = C_1 \%_1 + C_2 \%_2 + C_3 \%_3 =$ (_____) (_____) + (_____) (_____) + (_____) (_____) = _____

Coefficient of Tubing Stretch ($C_t = 0$ if tubing anchored) Not Anchored: C_t _____

Total Coefficient of Stretch: $C = C_r + C_t =$ _____ + _____ = _____

Total Stretch: $E = C (D/1000)^2 =$ _____ (_____) ² = 12 in.

Overtravel: $O = (1.41) (F-1) (D/1000)^2 =$ (1.41) (_____) (_____) ² = 1 in.

Plunger Stroke: $S_p = S - E + O =$ 26 - 12 + 1 = 15 in.

Theoretical Production (100%): (K, PLGR. Constant) (S_p) (SPM) = (182) (15) (16.5) = 45 bbls/day

Production at 80% Pump Efficiency: .80 (Theo. Prod.) = .80 (45) = 36 bbls/day

Counterbalance Effect: $W_r + \frac{\text{Fluid Wt.}}{2} =$ 1640 + 640 = 2280 lbs

Peak Torque: (PPRL -CB) ($S/2$) = (854) (13) = 11,100 in. lbs.

Prime Mover Horsepower (Single Cylinder & CE Green ▲ Electric Motors)

$HP = \frac{\text{Depth} \times \text{Prod. (Based on 100\% PR Stroke)}}{85,000} =$ (_____) (_____) = _____

Non-Synchronous Pumping Speeds (Desirable) _____ SPM

Remarks: _____

ILLEGIBLE

WELL INSTALLATION WORK SHEET

Company Shenandoah Kennedy Lease _____ Well # _____ Date 7-19-60
 Plunger 1 1/4" Stroke 26" SPM 140 Pump Depth 2600 Desired Prod. MAX Impulse Factor 1.01

1/2" Rods 100 % 2600 ft. 3/4" Rods _____ % _____ ft. 7/8" Rods _____ % _____ ft.
1" Rods _____ % _____ ft. 1-1/8" Rods _____ % _____ ft.

Weight of Fluid: $W_f =$ (Wt. per foot on Plunger) Multiplied by (Depth) = 1380 lbs.

SIZE	WT/FT	LENGTH	BUOY.	EFFECTIVE WT OF RODS	F	STRESS
<u>1/2"</u>	<u>(1.72)</u>	<u>(2600)</u>	<u>(.875)</u>	<u>= (1640) lbs</u>	<u>(.107)</u>	<u>= 1750 lbs</u>
						<u>Load on top 1/2" Rods = 3130 lbs ÷ .197 = 15,900 psi</u>
<u>3/4"</u>	<u>(1.62)</u>	<u>()</u>	<u>(.875)</u>	<u>= () lbs</u>	<u>()</u>	<u>= () lbs ÷</u>
						<u>Load on top 3/4" Rods = () lbs ÷ .442 = () psi</u>
<u>7/8"</u>	<u>(2.17)</u>	<u>()</u>	<u>(.875)</u>	<u>= () lbs</u>	<u>()</u>	<u>= () lbs ÷</u>
						<u>Load on top 7/8" Rods = () lbs ÷ .601 = () psi</u>
<u>1"</u>	<u>(2.88)</u>	<u>()</u>	<u>(.875)</u>	<u>= () lbs</u>	<u>()</u>	<u>= () lbs</u>
						<u>Load on top 1" Rods = () lbs ÷ .785 = () psi</u>
<u>1-1/8"</u>	<u>(3.67)</u>	<u>()</u>	<u>(.875)</u>	<u>= () lbs</u>	<u>()</u>	<u>= () lbs</u>
						<u>Load on top 1-1/8" Rods = () lbs ÷ .994 = () psi</u>

Effective Weight of Rods: $EW_r =$ () lbs PPRL = 3130 lbs

Minimum Polished Rod Load: $MPRL = EW_r (1.87 - F) = (1640) (.80) = 1312$ lbs.

Load Ratio: $\frac{(PPRL - MPRL)}{(PPRL)} (100) = \frac{(3130 - 1312)}{(3130)} (100) = 58\%$

Coefficient of Rod Stretch

$C_r = C_1 \% + C_2 \% + C_3 \% = () () + () () + () () = 12\%$

Coefficient of Tubing Stretch ($C_t = 0$ if tubing anchored)

Not Anchored: $C_t = 0$

Total Coefficient of Stretch: $C = C_r + C_t = () + () = ()$

Total Stretch: $E = C (D/1000)^2 = () ()^2 = 12$ in.

Overtravel: $O = (1.41) (F-1) (D/1000)^2 = (1.41) () ()^2 = 1$ in.

Plunger Stroke: $S_p = S - E + O = 26 - 12 + 1 = 15$ in.

Theoretical Production (100%): $(K, PLGR. Constant) (S_p) (SPM) = (.182) (15) (14) = 38.5$ bbls/day

Production at 80% Pump Efficiency: $.80$ (Theo. Prod.) = $.80 (38.5) = 30.8$ bbls/day

Counterbalance Effect: $W_r + \frac{\text{Fluid Wt.}}{2} = 1640 + 690 = 2330$ lbs

Peak Torque: $(PPRL - CB) (S/2) = (800) (13) = 10,400$ in. lbs.

Prime Mover Horsepower (Single Cylinder & CE Green ▲ Electric Motors)

$HP = \frac{\text{Depth} \times \text{Prod. (Based on 100\% PR Stroke)}}{85,000} = \frac{(2600) (66)}{85,000} = .8$

Non-Synchronous Pumping Speeds (Desirable) 14 - 16.5 - 20 SPM

Remarks: _____

ILLEGIBLE



BROWN OIL TOOLS, INC.

BROWN CAM-LOK PACKER

CAM-LOK is a weight set packer

a tension set packer

a tension tubing anchor

a tubing catcher

and it is convertible at the well . . .

CAM-LOK is a tough, compact, full-opening, retrievable, reliable tool. In its simplest application, **CAM-LOK** is used as a weight set packer. **CAM-LOK** is set in tension to take advantage of pressure from below when testing, water flooding, fracturing, acidizing, or in shallow wells where the tubing weight and casing fluid column may not be sufficient to hold the packer weight-set against high bottom hole pressure.

Use **CAM-LOK** as a packer during the flowing life of your well. When the well goes on the pump, convert **CAM-LOK** to a tubing anchor while you are working over the well and run it back. Thrifty? You bet it is!

AND POSITIVE, TOO . . .

CAM-LOK is the most controllable mechanical packer you can put in your well.

Less than one quarter turn of the tubing in either direction operates the unique Brown cam mechanism, to grip the casing like a pipe wrench working from the inside. This wrench grip, not friction springs or blocks, will lock the packer in place as long as torque is held in the tubing—to permit lifting or slack-off of the tubing to set or release the packer. **CAM-LOK** is the industry's best insurance against failure of a packer to release.

AND IT'S SIMPLE TO OPERATE . . .

TO SET WITH WEIGHT:

Make up **CAM-LOK** in the tubing string with its seal end up. Run in hole to setting depth, then pick up on tubing two or three inches (at the packer) to make sure jay pin is on top of slot. Manually torque tubing to the right to actuate the cam mechanism, and hold torque while lowering tubing to the desired setting weight.

TO RELEASE FROM WEIGHT SETTING:

Just pick up on tubing and come out of hole.

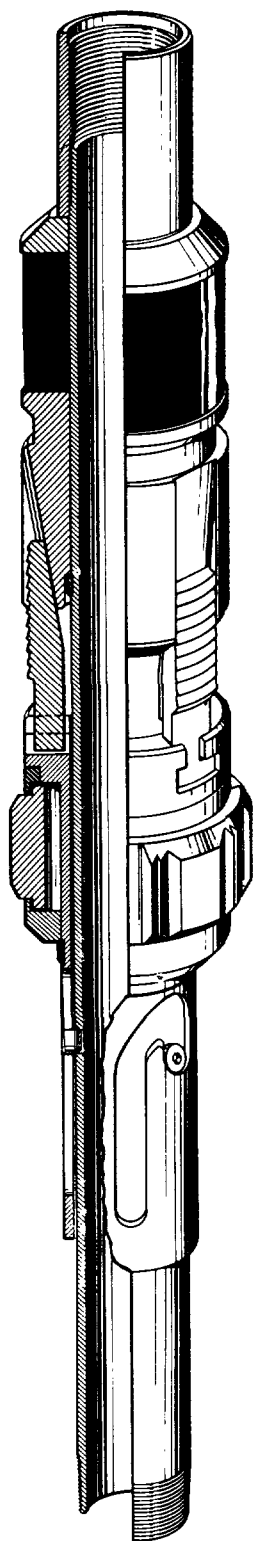
TO SET WITH TENSION:

Make up **CAM-LOK** in tubing string with seal end down. Set jay latch pin in short slot and run packer to setting depth. Apply torque to tubing. Cam mechanism will lock packer in position.

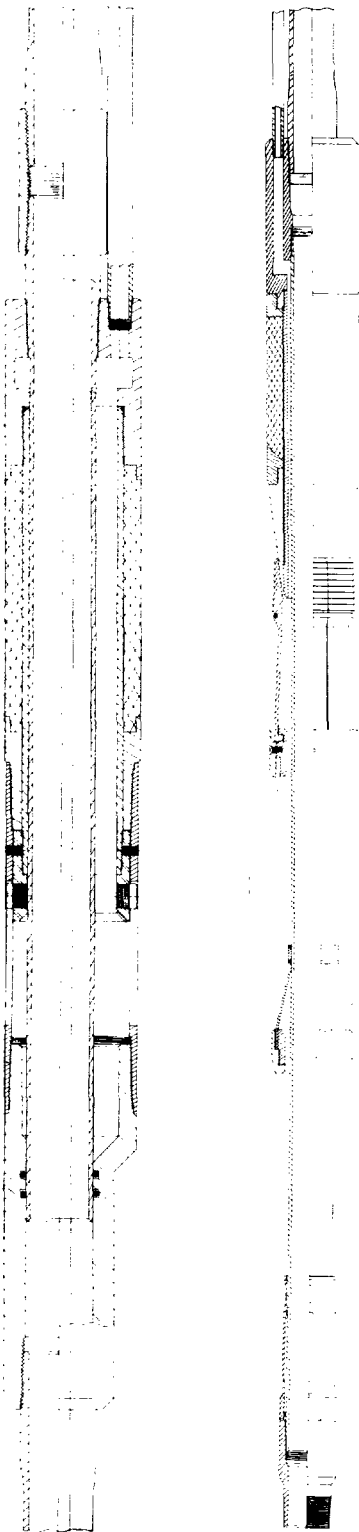
Hold left-hand torque while lowering tubing two or three inches to clear jay pin from short slot, then pick up to setting weight, and release torque.

TO RELEASE FROM TENSION SETTING:

Release tubing tension to set down on packer. Manually turn tubing to right with tongs. Lower another six inches (at the packer), then pick up on tubing. When torque is released, tubing and packer may be pulled out of the hole.



CAM-LOK
Weight Set Packer



Anchor
By-Pass
Packer

Boll Weevil
By-Pass
Packer

BROWN BY-PASS PACKERS

The Brown By-Pass Packers are designed for gas lift chamber installations and are ideally suited for both high and low productivity, low bottom hole pressure wells. In either type, the bottom hole pressure is not sufficient to support a column of fluid that can be efficiently intermitted by a conventional installation. In using the Brown By-Pass Packer as part of the chamber installation it assures increased slug volume, therefore more fluid per cycle, particularly in wells operated at maximum cycle rates. All By-Pass packers are furnished with a top by-pass connection. A bottom by-pass connection is furnished when specified. The Brown By-Pass Packers are furnished in two types which differ in the setting procedure. The Brown Boll Weevil By-Pass Packer has the standard Boll Weevil setting principle which requires only tubing reciprocation to set. This rugged, easy to set packer is especially applicable in deep or crooked holes where packers requiring rotation to set cannot be used successfully. The Brown Anchor By-Pass Packer is set by applying weight which shears the shear pins and compresses the seal.

ENGINEERING DATA ON BROWN BY-PASS PACKERS

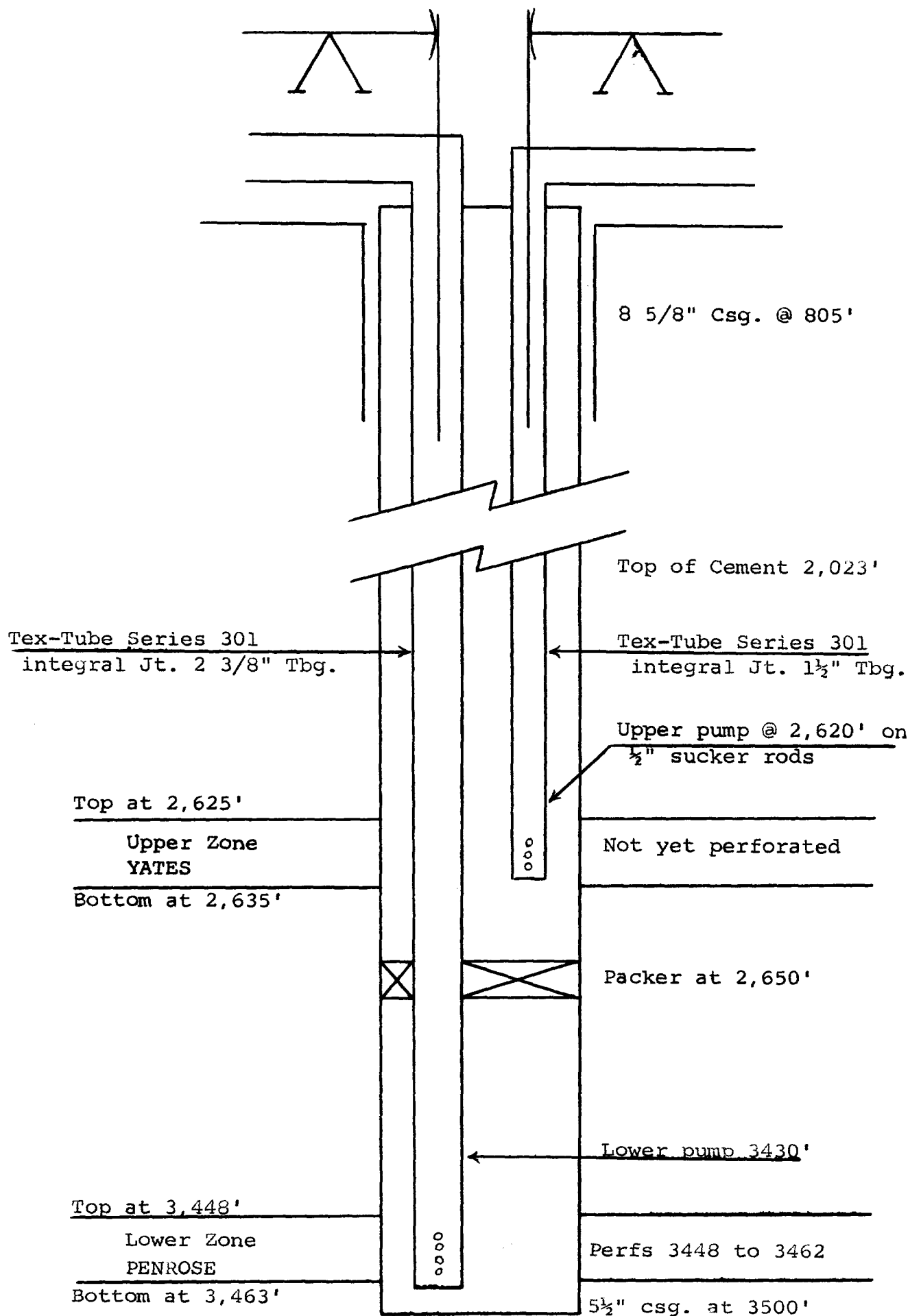
Shear Pin By-Pass	Casing		Packer O.D. in.	Overall Packer Length in.	Travel To Set in.	First String I.D. in.	Small String Connection	Total Packer Slip Area Sq. In.	Body Length in.
	O.D., In.	Lb/Ft							
2 x 5½	5½	13-17	4⅝	44	3	2	½ Line Pipe		6¼
2½ x 7	7	26	5¾	58	3	2⅞	½ Line Pipe		7
2½ x 7	7	32-35	5⅝	58	3	2⅞	½ Line Pipe		7
Boll Weevil By-Pass									
2 x 5½	5½	13-17	4⅝	85	14	2	½ Line Pipe	32	8¾
2 x 7	7	17-20	6	92	15	2	½ Line Pipe	63	8½
2 x 7	7	26	5¾	92	15	2	½ Line Pipe	63	8½
2½ x 7	7	17-20	6	92	15	2⅞	½ Line Pipe	63	8½
2½ x 7	7	26	5¾	92	15	2⅞	½ Line Pipe	60	8½

Parts, prices, and operating instructions for Brown production tools are contained in the general "Parts and Price List", and can be obtained by writing to Brown Oil Tools, Inc., P. O. Box 19236, Houston 24, Texas.

DIAGRAMMATIC SKETCH OF DUAL COMPLETION INSTALLATION

CHAMBERS & KENNEDY

Monterey-State Well No. 2
1-N, 32-18-31, Eddy Co., N. M.



NOTE: Well to be pumped with two strings of tools and two units. Tubing, packer, & pump depths are approximate.

3200	1000
1	1000
BEFORE EXAMINER MUSTER	
OF ONE THOUSAND AND NO	



THE WESTERN COMPANY

GAMMATRON

Simultaneous Radioactivity Log

COMPANY: CHAMBERS & KENNEDY
WELL: MONTEREY STATE # 2
FIELD: CULWIN
COUNTY: EDDY
STATE: N. MEX.
LOCATION: 660' FN & WL'S.
SEC. 32, T-18-S, R-31-E

COMPANY: CHAMBERS & KENNEDY

WELL: MONTEREY STATE # 2

FIELD: CULWIN

COUNTY: EDDY STATE: NEW, MEX

LOCATION: 660' FN & WL'S, SEC. 32,

T-18-S, R-31-E

LOCATION

FILE NO.

LOG NO. 95940

LOG MEAS. FROM: DERRICK FLOOR (G.L.+3') ELEV.

DRLG. MEAS. FROM: GROUND LEVEL ELEV.

PERM. DATUM: GROUND LEVEL ELEV.

TYPE OF LOG	G/R	N/N
RUN NO.	1-NW	1-NW
DATE	9-23-59	9-23-59
TOTAL DEPTH (DRILLER)	3501	3501
EFFECTIVE DEPTH (DRILLER)	3493	3493
EFFECTIVE DEPTH (WESTERN)	3492	3492
TOP OF LOGGED INTERVAL	SURF.	SURF.
BOTTOM OF LOGGED INTERVAL	3479	3490.5
TYPE OF FLUID IN HOLE	OIL	OIL
FLUID LEVEL		
SOURCE STRENGTH & TYPE		S10A3
SOURCE SPACING		13.5
DETECTOR CLASS	SCINT.	SCINT.
DETECTOR TYPE	D4G1	D6N1
DETECTOR LENGTH	4"	4"
O.D. OF INSTRUMENT IN.	3 5/8	3 5/8
TIME CONSTANT SEC.	2.0	2.0
LOGGING SPEED FT. MIN.	30	30
STATISTICAL VARIATION	RECORDED	RECORDED
SENSITIVITY REFERENCE	C-933	D-368
RECORDED BY	KIMBALL	
WITNESSED BY	MR. BERRY	

BEFORE EXAMINER NUTTER

OIL CONSERVATION COMMISSION

EXHIBIT NO.

CASE NO.

CASING RECORD INTERVAL

BIT SIZE	CASING	WT.-LB.	FROM WELL RECORD	FROM RA LOG
	5 1/2"		TO	TO
			SURF. TO 3493	TO
			TO	TO
			TO	TO