

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 12/19/85			
Company Exxon Co. U.S.A.				Connection None					
Pool				Formation Strawn				Unit	
Completion Date 11/19/85		Total Depth 10377		Plug Back TD 10354		Elevation 3849		Farm or Lease Name Mary Federal	
Csg. Size 7	Wt. 26	d 6.276	Set At 10377	Perforations: From 9916 To 10349		Well No. 5			
Thq. Size 2 7/8	Wt. 6.5	d 2.441	Set At 9870	Perforations: From Open To End		Unit N	Sec. 11	Twp. 23S	Rge. 25E
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single						Packer Set At 9870		County Eddy	
Producing Thru TBG		Reservoir Temp. °F 173 @ 9870		Mean Annual Temp. °F 60		Base. Press. - P _g 13.2		State New Mexico	
L 9870	H 9870	Cg .6789	% CO ₂ 1.961	% N ₂ 1.673	% H ₂ S	Prover	Meter Run 3.826	Taps Flg	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							2990				
1.	3.826 X 1.00			300	11	86	2930				1 hr.
2.	3.826 X 1.00			300	20	90	2860				1 hr.
3.	3.826 X 1.00			300	40	92	2784				1 hr.
4.	3.826 X 1.00			300	80	92	2665				1 hr.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{sp}	Rate of Flow O, Mcfd
1	4.758	58.70	313.2	.9759	1.214	1.029	340
2	4.758	79.14	313.2	.9723	1.214	1.029	457
3	4.758	111.93	131.2	.9706	1.214	1.029	646
4	4.758	158.29	313.2	.9706	1.214	1.029	913
5							

NO.	R	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcl/bbl.	
1	.47	546	1.43	.944	A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.	
2	.47	550	1.44	.945	Specific Gravity Separator Gas .679 XXXXXXXXXX	
3	.47	552	1.44	.945	Specific Gravity Flowing Fluid XXXXX	
4	.47	552	1.44	.945	Critical Pressure 669 P.S.I.A. _____ P.S.I.A.	
5					Critical Temperature 382 R _____ R	

P _c 3003.2 P _c ² 9019.2				(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 4.906$		(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 4.086$	
NO.	P ₁ ²	P _w	P _w ²	P _c ² - P _w ²	AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3.730$		
1		2943.4	8663.6	355.6			
2		2860.1	8180.2	839.0			
3		2797.9	7828.2	1191.0			
4		2679.7	7180.8	1838.4			
5							

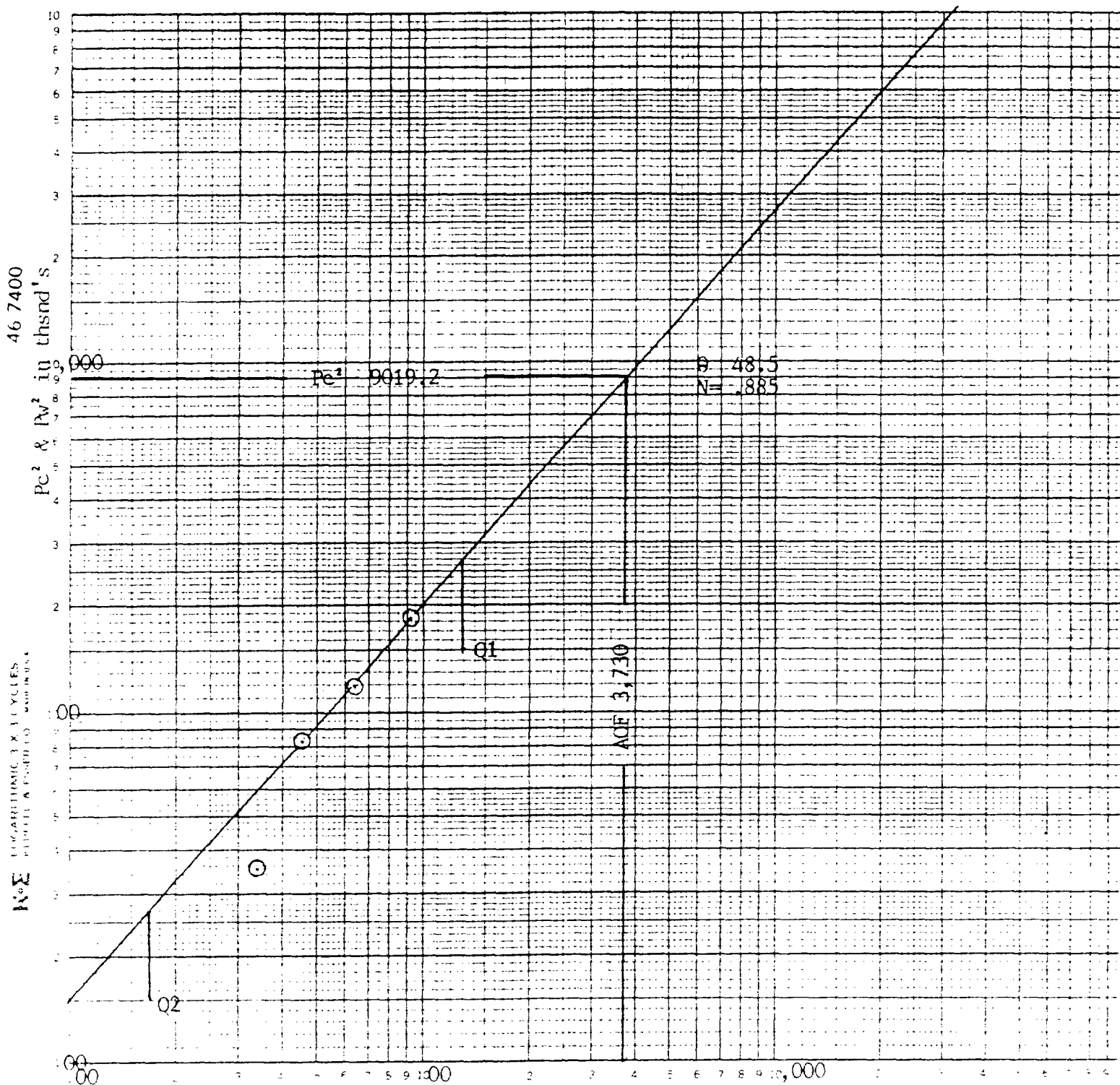
Absolute Open Flow 3.730		Mold @ 15.025	Angle of Slope 48.5	Slope, n .885
Remarks: Well made no fluid during test.				

Approved By Division	Conducted By: Duke Services, Inc.	Calculated By: R. Reston	EXH Checked By: 11
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DOCKET NO. 8858, 8842

HEARING DATE 3-19-86

COMPANY: Exxon Co. U.S.A.
 LEASE: Mary Federal # 5
 COUNTY: Eddy
 DATE: 12/19/85



Q=MCF/DAY

$$Q1 = 1300 = \log 3.113943$$

$$Q2 = 169 = \log 2.228943$$

$$N = .885000$$

$$CAOF = 913 \left(\frac{9019.2}{1838.4} \right)^{.885} = 3,730 \text{ MCF/D}$$