BEFORE THE NEW MEXICO OIL CONSERVATION DIVISION

APPLICATION OF BEACH EXPLORATION, INC. FOR APPROVAL OF A WATERFLOOD PROJECT AND TO QUALIFY THE PROJECT FOR THE RECOVERED OIL TAX RATE, EDDY COUNTY, NEW MEXICO.

No			

APPLICATION

Beach Exploration, Inc. applies for an order approving a waterflood project for the proposed West High Lonesome Unit Area, and qualifying the project for the recovered oil tax rate. In support thereof, applicant states:

1. Applicant is the operator of the proposed West High Lonesome Unit Area (the "Unit Area"), which covers the following state and federal lands located in Eddy County, New Mexico:

TOWNSHIP 16 SOUTH, RANGE 29 EAST, N.M.P.M.

Section 17: S½NW¼, SW¼, and W½SE¼

Section 18: Lots 2, 3, 4, S½NE¼, SE½NW¼, E½SW¼, and

SE¼

Section 19: NE% and E%NW%

Section 20: NW¼NE¼, N½NW¼, and SW¼NW¼

Containing 1156.60 acres, more or less.

The unitized interval is the Penrose Sand member of the Queen formation, as further described in the unitization application filed concurrently herewith.

- 2. Applicant proposes to institute a waterflood project on the Unit Area. Applicant's address is Suite 200, 800 North Marienfeld, Midland, Texas 79701 (Attention: Robert N. Hinson).
- 3. Applicant proposes to inject water into the Penrose Sand member of the Queen formation through eighteen existing and planned injection wells. A plat outlining the Unit Area, and marking the locations of the initial and proposed injection and producing

wells, is attached hereto as Exhibit A.

- 4. Applicant requests that the waterflood project for the Unit Area be qualified for the recovered oil tax rate, pursuant to the Enhanced Oil Recovery Act (L. 1992, Ch. 38) and Division Rule 30. Project data includes:
 - (a) Number of initial producing wells:

Phase I: 14.

Phase II: 9

(b) Number of initial injection wells:

Phase I: 13.

Phase II: 18

- (c) Capital cost of additional facilities: \$929,000.00.
- (d) Estimated total project cost: \$6,400,000.00.
- (e) Estimated total value of incremental production recovered from the project: \$9,910,000.00.
- (f) Anticipated injection commencement date: September
 1, 2001.
- (g) Type of fluid injected: Produced and fresh water.
- (h) Anticipated injection volumes: 3600 BWPD maximum.
- 5. A Form C-108 for the injection wells and project is attached hereto as Exhibit B.

WHEREFORE, applicant requests that the Division (a) approve the injection application and waterflood project for the Unit Area, including a provision allowing administrative approval for expansion of the project area, (b) qualify the project as an enhanced oil recovery project, and (c) certify the project for the

recovered oil tax rate.

Respectfully submitted,

James Bruce

Post Office Box 1056

\$anta Fe, New Mexico 87504

(505) 982-2043

Attorney for Beach Exploration, Inc.

VERIFICATION

STATE OF TEXAS

COUNTY OF MIDLAND

Jack M. Rose, being duly sworn upon his cath, deposes and states: He is a petroleum engineer employed by Beach Exploration, Inc., he is familiar with the matters set forth in the foregoing Application, and the statements therein are true and correct to the best of his knowledge.

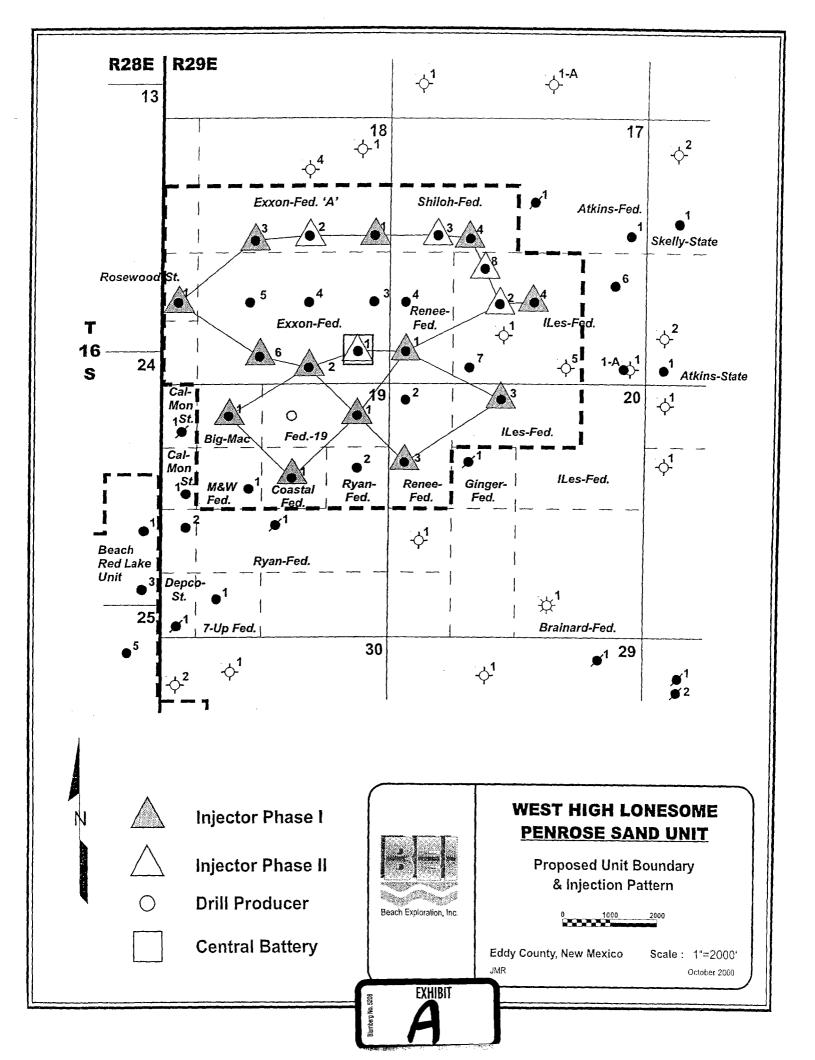
K M. Rose

SUBSCRIBED AND SWORN TO before me this 2001 by Jack M. Rose.

_ day of June,

BARBARA J. WATSON
Notary Public, State of Texas
My Commission Expires
February 16, 2064

2-16-200H



Oil Conservation Division 1220 South St. Francis Dr. Santa Fe, New Mexico 87505

FORM C-108 Revised 4-1-98

APPLICATION FOR AUTHORIZATION TO INJECT

I.	PURPOSE: X Secondary Recovery Pressure Maintenance Disposal Storage Application qualifies for administrative approval? Yes X No							
II.	OPERATOR: Beach Exploration, Inc.							
	ADDRESS: 800 N, Marienfeld Ste. 200 Midland, Texas 79701							
	CONTACT PARTY: Jack Rose PHONE: 915/683-6226							
III.	WELL DATA: Complete the data required on the reverse side of this form for each well proposed for injection. Additional sheets may be attached if necessary.							
IV.	Is this an expansion of an existing project? Yes X No If yes, give the Division order number authorizing the project:							
V.	Attach a map that identifies all wells and leases within two miles of any proposed injection well with a one-half mile radius circle drawn around each proposed injection well. This circle identifies the well's area of review.							
VI.	Attach a tabulation of data on all wells of public record within the area of review which penetrate the proposed injection zone. Such data shall include a description of each well's type, construction, date drilled, location, depth, record of completion, and a schematic of any plugged well illustrating all plugging detail.							
VII.	Attach data on the proposed operation, including:							
	 Proposed average and maximum daily rate and volume of fluids to be injected; Whether the system is open or closed; Proposed average and maximum injection pressure; Sources and an appropriate analysis of injection fluid and compatibility with the receiving formation if other than reinjected produced water; and, If injection is for disposal purposes into a zone not productive of oil or gas at or within one mile of the proposed well, attach a chemical analysis of the disposal zone formation water (may be measured or inferred from existing literature, studies, nearby wells, etc.). 							
*VIII.	Attach appropriate geologic data on the injection zone including appropriate lithologic detail, geologic name, thickness, and depth. Give the geologic name, and depth to bottom of all underground sources of drinking water (aquifers containing waters with total dissolved solids concentrations of 10,000 mg/l or less) overlying the proposed injection zone as well as any such sources known to be immediately underlying the injection interval.							
IX.	Describe the proposed stimulation program, if any.							
*X.	Attach appropriate logging and test data on the well. (If well logs have been filed with the Division, they need not be resubmitted).							
*XI.	Attach a chemical analysis of fresh water from two or more fresh water wells (if available and producing) within one mile of any injection or disposal well showing location of wells and dates samples were taken.							
XII.	Applicants for disposal wells must make an affirmative statement that they have examined available geologic and engineering data and find no evidence of open faults or any other hydrologic connection between the disposal zone and any underground sources of drinking water.							
XIII.	Applicants must complete the "Proof of Notice" section on the reverse side of this form.							
XIV.	Certification: I hereby certify that the information submitted with this application is true and correct to the best of my knowledge and belief.							
	NAME: Jack M. Rose TITLE: Engineer SIGNATURE: DATE: June 18, 2001							
	NAME: Jack M. Rose TITLE: Engineer SIGNATURE: DATE: June 18, 2001							
*	If the information required under Sections VI, VIII, X, and XI above has been previously submitted, it need not be resubmitted. Please show the date and circumstances of the earlier submittal:							
DIST	RIBUTION: Original and one copy to Santa Fe with one copy to the appropriate District Office							

Beach Exploration, Inc.

C-108 Application

<u>Proposed West High Lonesome Penrose Sand Unit</u> Eddy County, New Mexico

Form C108 – Item I. Purpose - Secondary Recovery

Form C108 – Item II. Operator - Beach Exploration, Inc.

Address - 800 N. Marienfeld, Suite 200

Midland, Texas 79701-3382

Contact - Jack M. Rose (915) 683-6226

Form C108 – Item III. Injection Well Data Sheets (attached 3 legal sheets)

Form C108 – Item IV. Expansion of existing project? NO

Form C108 – Item V. Large area map and Area of Review Detail map (attached)

Form C108 – Item VI. Area of Review – Well data tabulation & schematics

Unit Producing Wells – (attached 2 legal sheets)

Offset Well – (attached 1 legal sheet)

Plugged Wells – (attached 1 list, 11 schematics)

Form C108 – Item VII. Feasibility Study – (attached 25 pages)

Development Plat – (attached map)

Water Analyses – (attached 10 pages)

A feasibility study of the proposed unit was prepared by T. Scott Hickman & Associates in 1993. This study is the basis for our proposed operation and it indicates that additional reserves of 538,000 barrels can reasonably be expected to be recovered as a result of waterflooding. The engineering study with its related geological information is included for your review.

The proposed development of the waterflood is as shown on the attached plat. It consists of conversion of thirteen existing wells to Phase I water injectors, drilling one additional producer, installation of a (closed system) waterflood plant and distribution system, consolidation of twelve tank batteries to a central battery, and installation of a supply water pipeline. A subsequent conversion of five existing unit producing wells to Phase II water injectors is planned when water breakthrough occurs in these wells.

Make-up water volume requirements have been recalculated based on current cumulative production and is estimated to be 1.6 million barrels. Total make-up water requirements will be at least 1.6 million barrels and could range up to 2.4 million barrels depending on injection efficiency (67% estimated previously). The maximum monthly requirement would be 110,000 barrels initially and should decrease uniformly to little or no usage in a 3.5 to 4 year period with re-injection of produced water. On a daily basis, the targeted injection rate will be 200 BWPD for each well. Initially with thirteen injectors this would

be 2,600 BWPD and after Phase II water injectors have been converted (5 additional) the daily requirement would be 3,600 BWPD.

The maximum injection pressure is anticipated to be 1100 psi. Experience in four other Penrose floods in this area show that injection pressures can vary from a low of 280 BWPD at 700 psi to 150 BWPD at 1100 psi. The pay quality in the area of the proposed flood is expected to be on the tighter side and higher injection pressures are anticipated.

A four-township area surrounding the proposed flood was investigated for potential sources of makeup water. There are a few water wells in the area. One is indicated to be a saltwater well and the rest are fresh. The State Engineer's office has indicated that these wells are shallow, discontinuous water sources of very limited capacity and unsuitable for our purposes.

The City of Carlsbad Water Supply System has several fresh water pipelines in the area that have serviced waterflood operations. The closest is 3.24 miles to the east. This source is capable of delivering more than twice our maximum required daily makeup volume. The delivery point is uphill from our proposed flood and strong enough to flow by gravity to our proposed flood site.

Produced water is scarce in the area of the proposed flood but abundant to the south. The proposed flood is central to two townships. No saltwater disposal wells exist in these two townships and total water production is 175 barrels of water per day. Nine disposal wells exist in the north half of the two townships to the south of the proposed flood. Three of the nine wells are handling sufficient volumes of water to be considered as possible sources for makeup water. Two of these three are considered to be cost prohibitive, requiring seven plus miles of large diameter pipeline to be installed. The remaining disposal well, Mack Energy's Big George State #3, handles 6,500 barrels of water per day from Mack operated wells in the Paddock and Yeso. This well is 5.1 miles to the south and would require pumping by mechanical means to reach the proposed flood site.

Beach Exploration is requesting the use of Carlsbad Double Eagle fresh water as makeup water for the West High Lonesome Penrose Sand Unit. The Big George State #3 disposal water is extremely poor quality. This water has severe problems with suspended solids, oil carryover, scaling tendencies and bacteria. The water borders on being cost prohibitive from a chemical treating and facilities requirement standpoint but most significantly it is Beach's opinion that it would pose a significant long-term risk to the success of the flood.

City of Carlsbad fresh water has been successfully used in Penrose floods in the immediate vicinity of our proposed flood and should not create a problem with soluble salts or swelling clays.

Enclosed are individual analyses for the two potential make-up water sources: City of Carlsbad Double Eagle Fresh Water and Mack Energy's Big George State #3 disposal well. Also enclosed are water compatibility reports for the combination of these two waters with produced water from the proposed flood interval (source: Beach, Exxon Federal lease).

Form C108 - Item VIII.

The injection zone in the proposed unit is locally called the Penrose sand, a lower member of the Queen formation. The sand is generally a gray, fine grained, well sorted, and rounded to sub-rounded quartz sandstone. The sand ranges from 26 to 32 feet in thickness in the proposed unit area, and ranges in depth from 1,650 feet to 1,800 feet depending upon regional dip and surface elevation.

The office of the State Engineer has said that no fresh aquifers exist above or below the proposed injection zone. There are scattered but very limited shallow fresh water Triassic sands in the area down to approximately 100 feet. These are produced from occasional windmills. Only one such windmill exists within one mile of any of the proposed injection wells.

Form C108 – Item IX.

There is no stimulation program planned for this unit initially other than routine acid treatments for potential calcium carbonate scaling.

Form C108 – Item X.

All wells in the proposed flood are of public record and logs have been filed with the OCD.

Fresh water well water analysis – only one within one mile

Windmill located 900' FNL 400' FEL, Section 24,

T16S, R28E, Eddy County, New Mexico

Location Plat (attached)

Chemical analysis (attached – Water Well #2)

Form C108 – Item XII. Not applicable

Form C108 – Item XIII. "Proof of Notice" to be supplied later

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		X							<u> </u>	TYPICAL SCHEMATIC	
Total Depth Plug Back Depth	— Perforations	— Approx. Pkr Depth	Sacks of Cement Hole Size	PRODUCTION CASING: Top of Cement TOC Determined by Size & Depth of Csg	−2 3/8" Tubing (plastic coated)	Sacks of Cement Hole Size	TOC Determined by Size & Depth of Csg	SURFACE CASING: Top of Cement	∠G.L. Elev		Operator Lease & Well # Location SecUnit, Twp., Rge.
1800' 1784'	1714' - 1728'	1664'	450 7 7/8"	Surface Circulated 4 1/2" @ 1800'		250 12 1/4"	Circulated 8 5/8" @ 307'	Surface	3641'		Beach Expl Exxon Federal "A" #1 2310' FNL 330' FEL 18-H, 16S, 29E
1770' 1768'	1702' - 1722'	1652'	550 7 7/8"	Surface Circulated 4 1/2" @ 1770'		250 12 1/4"	Circulated 8 5/8" @ 295'	Surface	3654'		Beach Expl Exxon Federal "A" #2 2310' FNL 1650' FEL 18-G, 16S, 29E
1705' 1692'	1645' - 1655'	1595'	550 7 7/8"	Surface Circulated 4 1/2" @ 1705'		250 12 1/4"	Circulated 8 5/8" @ 330'	Surface	3621'		Beach Expl Exxon Federal "A" #3 2410' FNL 1932' FWL 18-F, 16S, 29E
1840' 1828'	1722' - 1756'	1672'	375 7 7/8"	Surface Circulated 4 1/2" @ 1840'		225 11"	Circulated 8 5/8" @ 302'	Surface	3650'		Beach Expl Exxon Federal #1 . 660' FSL 660' FEL 18-P, 16S, 29E
1820' 1800'	1713' - 1750'	1663'	400 7 7/8"	Surface Circulated 4 1/2" @ 1814'		475 12 1/4"	Circulated 8 5/8" @ 343'	Surface	3650'		Beach Expl Exxon Federal #2 330' FSL 1650' FEL 18-O, 16S, 29E
1780' 1772'	1708' - 1727'	1658'	500 7 7/8"	Surface Circulated 4 1/2" @ 1772'		250 12 1/4"	Circulated 8 5/8" @ 307'	Surface	3656'		Beach Expl Exxon Federal #6 560' FSL 2035' FWL 18-N, 16S, 29E

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2 3/8" Tubing internally plastic coated.

Model AD-1 Tension Packer set within 100' of top perf.

Injection formation: Penrose Sand member of Queen formation

Field: High Lonesome (Queen)

All wells were originally producers and will be converted to injection

There are no known overlying or underlying oil or gas zones.

Sec - I Init Two Rose	Location	Lease & Well #	Operator
18-1 16S 29F	1650' FSL 330' FWL	Rosewood St. "18" #1 Shiloh Federal #3	Beach Expl
17-F 165 29F	2310' FNL 988' FWL	Shiloh Federal #3	Beach Expl
17-F 165 29F	2210' FNL 1650' FWL	Shiloh Federal #4	Beach Expl
17-K 169 29F	. 1650' FSL 2310' FWL	lles Federal #2	Beach Expl
20-C 16S 29E	330' FNL 2310' FWL	lles Federal #3	Beach Expl
17.1 169	1650' FSI	lles Fede	Beach Ex

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_ Total Depth Plug Back Depth	— Perforations	Approx. Pkr Depth	PRODUCTION CASING: Top of Cement TOC Determined by Size & Depth of Csg Sacks of Cement Hole Size	−2 3/8" Tubing (plastic coated)	SURFACE CASING: Top of Cement TOC Determined by Size & Depth of Csg Sacks of Cement Hole Size	✓ G.L. Elev		Operator Lease & Well # Location SecUnit, Twp., Rge.
1750' 1681'	1576' - 1596'	1526'	Surface Circulated 5 1/2" @ 1733' 375 7 7/8"		Surface Circulated 8 5/8" @ 443' 270 12 1/4"	3578'		Beach Expl Rosewood St. "18" #1 1650' FSL 330' FWL 18-L, 16S, 29E
1850' 1844'	1730' - 1758'	1680'	Surface Calculated 4 1/2" @ 1850' 500 7 7/8" assumed		Surface Calculated 8 5/8" @ 311' 250 12 1/4" assumed	3640'		Beach Expl Shiloh Federal #3 2310' FNL 988' FWL 17-E, 16S, 29E
1850' 1840'	1752' - 1764'	1702'	Surface Calculated 4 1/2" @ 1850' 650 7 7/8" assumed		Surface Calculated 8 5/8" @ 309' 250 12 1/4" assumed	3649'		Beach Expl Shiloh Federal #4 2210' FNL 1650' FWL 17-F, 16S, 29E
1812'	1700' - 1812'(open hole)	1650'	1204' & Surf Calc@shoe & perf@250' 5 1/2" @ 1700' 100@1700' & 229@250' 7 7/8" assumed		Surface Calculated 8 1/4" @ 40 20 12 1/4" assumed	3643'		Beach Expl lles Federal #2 1650' FSL 2310' FWL 17-K, 16S, 29E
1820'	1700' - 1812'(open hole) 1590' - 1820'(open hole) 1740' - 1800' (open hole) 1760' - 1812' (open hole) 1760' nav intended	1580'	358')' Calculated 7" @ 1590' 100 7 7/8" assumed		141' Calculated 8" @ 328' 50 11" assumed	3649'		Beach Expl lles Federal #3 330' FNL 2310' FWL 20-C, 16S, 29E
1800'	1740' - 1800' (open ho	1717'	1105' Calculated 7" @ 1740' 50 thru perf @1725' 7 7/8" assumed		190' Calculated 8 5/8" @ 298' 50 12 1/4" assumed	3643'		Beach Expl lles Federal #4 1650' FSL 2310' FWL 17-J, 16S, 29E

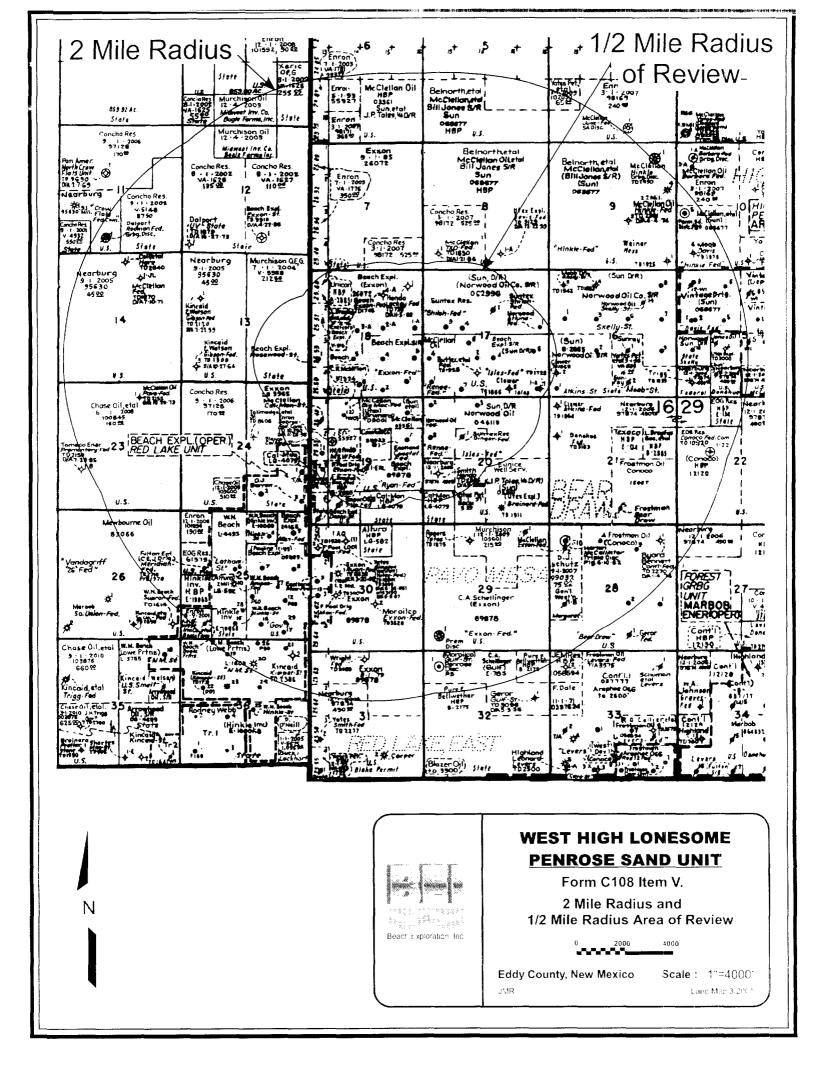
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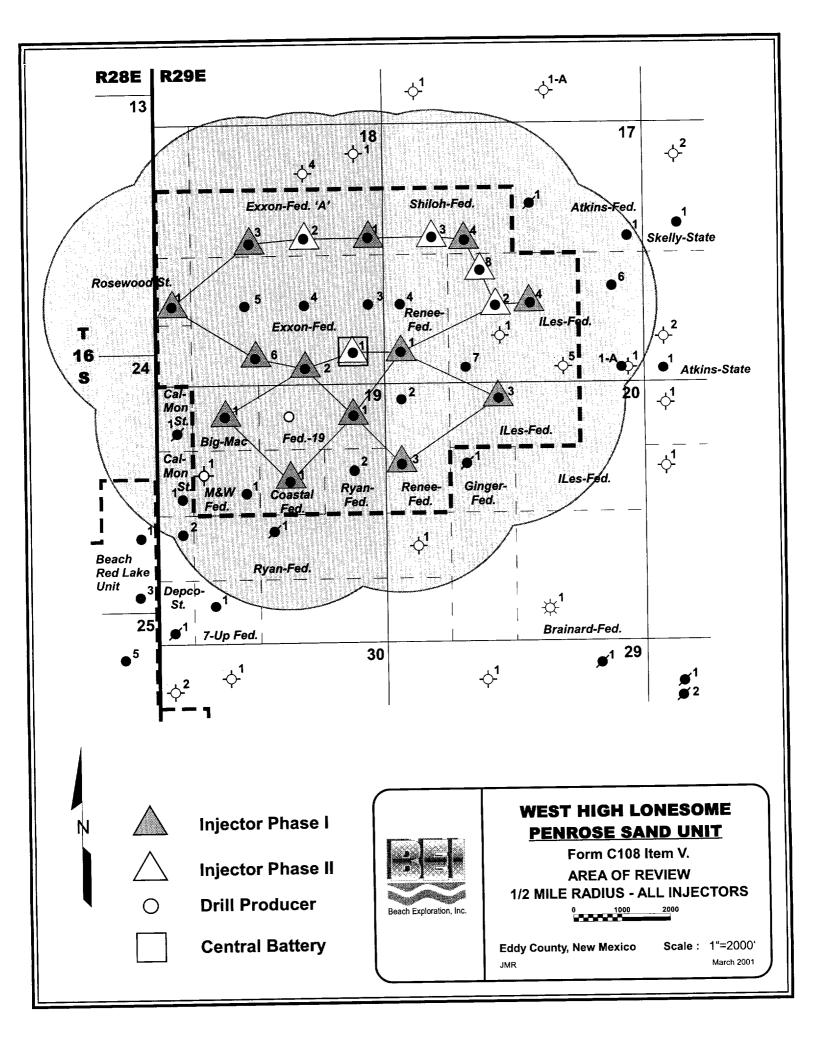
2 3/8" Tubing internally plastic coated.

Model AD-1 Tension Packer set within 100' of top perf.

Injection formation: Penrose Sand member of Queen formation All wells were originally producers and will be converted to injection Field: High Lonesome (Queen) There are no known overlying or underlying oil or gas zones.

ALL WELLS: 2 3/8" Tubing internally plastic coated. Model AD-1 Tension Packer set within 100' of top perf. Injection formation: Penrose Sand member of Queen formation Field: High Lonesome (Queen) All wells were originally producers and will be converted to injection There are no known overlying or underlying oil or gas zones.			M M				<u>a</u> _	TYPICAL SCHEMATIC	
100' of top perf. Imber of Queen formation will be converted to injection rlying oil or gas zones.	Total Depth Plug Back Depth	Perforations	— Approx. Pkr Depth	PRODUCTION CASING: Top of Cement TOC Determined by Size & Depth of Csg Sacks of Cement Hole Size	— 2 3/8" Tubing (plastic coated)	SURFACE CASING: Top of Cement TOC Determined by Size & Depth of Csg Sacks of Cement Hole Size	∕ G.L. Elev		Operator Lease & Well # Location SecUnit, Twp., Rge.
	1813 ¹ 1783 ¹	1740' - 1764'	1690'	Surface Circulated 4 1/2" @ 1809' 480 7 7/8"		Surface Circulated 8 5/8" @ 253' 190 12 1/4"	3642'		Beach Expl lles Federal #8 2310' FSL 1950' FWL 17-K, 16S, 29E
	1850' 1815'	1729' - 1750'	1679'	40' Calculated 5 1/2" @ 1815' 350 7 7/8"		Surrace Circulated 8 5/8" @ 300' 200 12 1/4"	3642'		Beach Expl Renee Federal #1 660' FSL 330' FWL 17-M, 16S, 29E
	1925' 1920'	1774' - 1793'	1724'	16' Calculated 5 1/2" @ 1920' 375 7 7/8"		Surface Circulated 8 5/8" @ 300' 280 12 1/4"	3638'		Beach Expl Renee Federal #3 1650' FNL 330' FWL 20-E, 16S, 29E
	1875 [,] 1846 [,]	1746' - 1772'	1696'	205' Calculated 4 1/2" @ 1874' 360 7 7/8"		Surface Circulated 8 5/8" @ 355' 250 12 1/4" assumed	3639'		Beach Expl Federal "19" #1 660' FNL 660' FEL 19-A, 16S, 29E
Well drilled to 3001' and P&A'd in 1956 No record of where plugs were set. Cleaned out to 2100' 8/85, 4 1/2" set at 1871'	3001' 1829'	1683' - 1699'	1633'	1112' Calculated 4 1/2" @ 1871' 200 7 7/8"		Surface Calculated 8 5/8" @ 202' 100 12 1/4" assumed	3597'		Beach Expl Big-Mac Federal #1 660' FNL 3300' FWL 19-C, 16S, 29E
	1877' 1834'	1747' - 1797'	1697'	Surface Circulated 5 1/2" @ 1877' 400 7 7/8"		Surface Circulated 8 5/8" @ 304' 200 12 1/4"	3637'		Beach Expl Coastal Federal #1 1980' FNL 1980' FEL 19-G, 16S, 29E





				TYPICAL SCHEMATIC	
				<u>HEMATIC</u>	
Total Depth Plug Back Depth	COMPLETION: Zone Perforations Stimulation POTENTIAL: Method BOPD BWPD MCFPD API gravity	Top of Cement TOC Determined by Size & Depth of Csg /Sacks of Cement Hole Size	SURFACE CASING: Top of Cement TOC Determined by Size & Depth of Csg Sacks of Cement Hole Size	Date Drilled G.L. Elev	Operator Lease & Well # Location SecUnit, Twp., Rge.
1820' 1793'	Penrose 1717' - 1741' Acidize w/1500gal Frac w/18,600gal gel+ 27,000# sand Pumping 80 0 48 32.6	Surface Circulated 4 1/2" @ 1818' 700 7 7/8"	Surface Circulated 8 5/8" @ 303' 235 12 1/4"	Nov-85 3642'	Beach Expl Exxon Federal #3 1650' FSL 330' FEL 18-I, 16S, 29E
1800' 1791'	Penrose 1714' - 1731' Acidize w/1200gal Frac w/20,000gal gel+ 42,000# sand Pumping 89 29 42 36.4	Surface Circulated 4 1/2" @ 1800' 500 7 7/8"	Surface Circulated 8 5/8" @ 333' 175 12 1/4"	Apr-86 3653'	Beach Expl Exxon Federal #4 1650' FSL 1650' FEL 18-J, 16S, 29E
1715' 1711'	Penrose 1639' - 1652' Acidize w/1200gal Frac w/20,000gal gel+ 42,000# sand Pumping 79 Trace 100	Surface Circulated 4 1/2" @ 1715' 450 7 7/8"	Surface Circulated 8 5/8" @ 303' 250 12 1/4"	Aug-86 3608'	Beach Expl Exxon Federal #5 1650' FSL 1835' FWL 18-K, 16S, 29E
1850' 1839'	Penrose 1721' - 1738' Acidize w/1000gal Frac w/30,000gal gel+ 50,000# sand Pumping 100 15 38	78' Calculated 5 1/2" @ 1839' 370 7 7/8"	Surface Circulated 8 5/8" @ 250' 250 12 1/4"	Jan-85 3626'	Beach Expl Renee Federal #4 1650' FSL 330' FWL 17-L, 16S, 29E
1850' 1841'	Penrose 1767' - 1787' Acidize w/1000gal Frac w/30,000gal gel+ 49,000# sand Pumping 84 13 TSTM	72' Calculated 5 1/2" @ 1842' 350 7 7/8"	Surface Circulated 8 5/8" @ 292' 250 12 1/4"	Mar-86 3648'	Beach Expl lles Federal #7 330' FSL 1650' FWL 17-N, 16S, 29E
1850' 1840'	Penrose 1760' - 1783' Acidize w/1000gal Frac w/30,000gal gel+ 43,000# sand Pumping 30 5 TSTM no record	63' Calculated 5 1/2" @ 1840' 350 7 7/8"	Surface Circulated 8 5/8" @ 300' 200 12 1/4"	Sep-85 3636'	Beach Expl Renee Federal #2 330' FNL 330' FWL 20-D, 16S, 29E

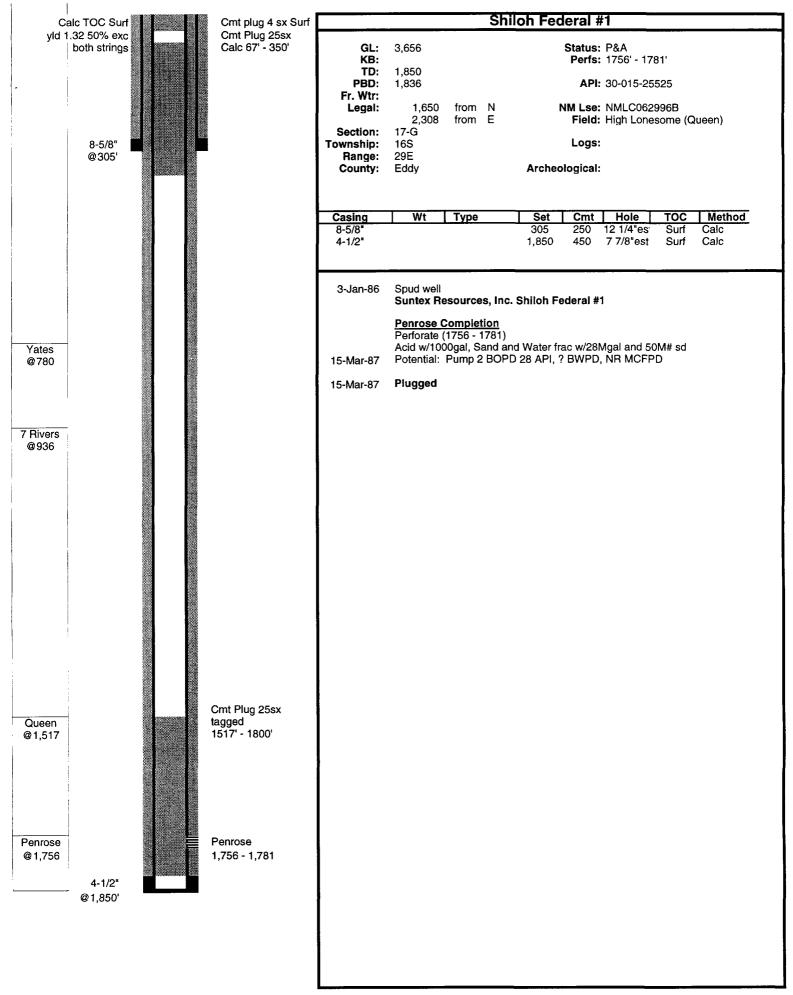
						TYPICAL SCHEMATIC	
Total Depth Plug Back Depth	POTENTIAL: Method BOPD BWPD MCFPD API gravity	COMPLETION: Zone Perforations Stimulation	Top of Cement TOC Determined by Size & Depth of Csg Sacks of Cement Hole Size	Top of Cement TOC Determined by Size & Depth of Csg Sacks of Cement Hole Size	G.L. Elev	Date Drilled	Operator Lease & Well # Location SecUnit, Twp., Rge.
1974' 1972'	Pumping 80 no record no record no record	Penrose 1734' - 1746' Acidize w/1000gal Frac w/17,000gal wtr+ 38,500# sand	Surface Calculated 5 1/2" @ 1972' 1000 7 7/8" assumed	Surface Calculated 8 5/8" @ 290' 175 12 1/4" assumed	3640'	Nov-85	Beach Expl M&W Federal #1 2210' FNL 1833' FWL 19-F, 16S, 29E
CIBPs @1645' & 1817' 2310' 2227'	Pumping 19 0 10 31.7	Penrose 1688' - 1804' Acidize w/1500gal Frac w/50,000gal gel+ 60,000# sand	500' Temp Survey 5 1/2" @ 2300' 650 7 7/8"	Surface Circulated 8 5/8" @ 348' 225 12 1/4"	3630'	Apr-82	Beach Expl Ryan Federal #2 1780' FNL 660' FEL 19-H, 16S, 29E

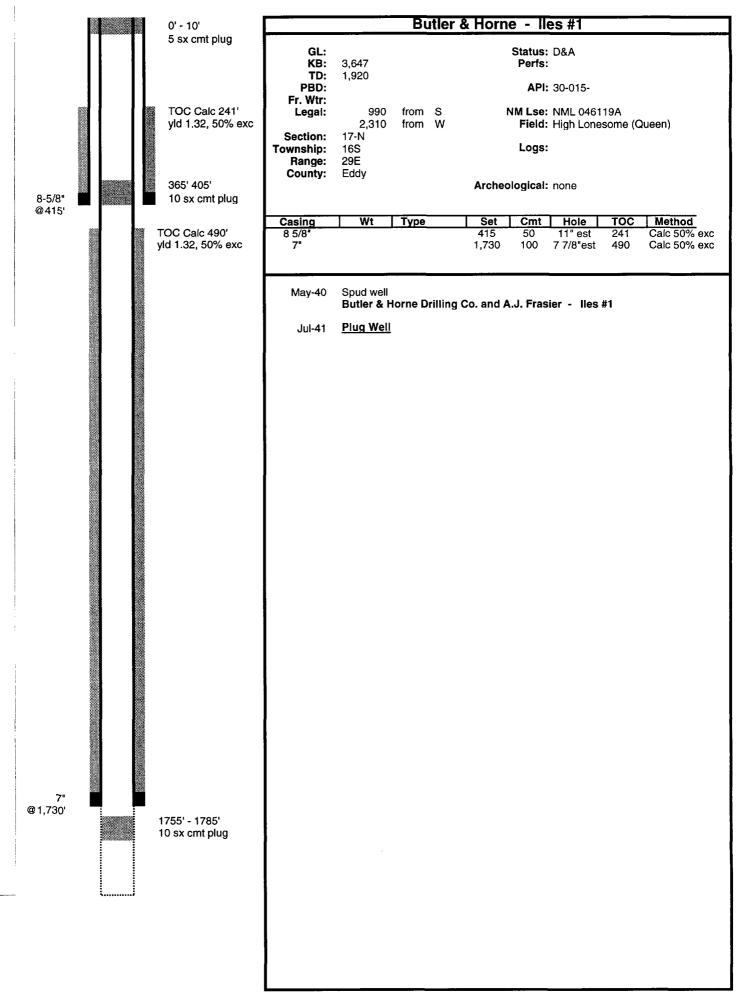
						TYPICAL SCHEMATIC	
					\	<u>IEMATIC</u>	
Total Depth Plug Back Depth	POTENTIAL: Method BOPD BWPD MCFPD MCFPD API gravity	COMPLETION: Zone Perforations Stimulation	PRODUCTION CASING: Top of Cement TOC Determined by Size & Depth of Csg /Sacks of Cement Hole Size	SURFACE CASING: Top of Cement TOC Determined by Size & Depth of Csg Sacks of Cement Hole Size	∕ G.L. Elev	Date Drilled	Operator Lease & Well # Location SecUnit, Twp., Rge.
1825' 1825'	Pumping 100 not reported not reported not reported	Penrose 1774' - 1799' Sand Frac w/10,000gal + assumed 10,000# sand	1317' Calculated 5 1/2" @ 1825' 100 7 7/8" assumed	Surface Circulated 8 5/8" @ 450' unknown 12 1/4" assurned	3653'	Apr-56	Mack Energy Corp. Atkins Federal #1 2310' FNL 330' FEL 17-H, 16S, 29E
1835' 1835'	Pumping 2 not reported not reported not reported	5 1/2" liner 1470' - 1735' cmt'd 85sx TOC 1540' by temp survey Penrose 1735'-1835' (open hole) 1801'-1821' pay interval Shot w/90 qts nitro		Surface Unknown 8 1/4" @ 291' 70 11" assumed	3655'	Aug-39	Beach Expl lles Federal #1-A 330' FSL 345' FEL 17-P, 16S, 29E
1825' 1810'	Pumping 20 not reported not reported not reported	Penrose 1778' - 1802' Sand Frac w/15,000 gal +15,000# sand	Surface Circulated 4 1/2" @ 1825' 800 7 7/8"	Surface Circulated 8 5/8" @ 315' 150 12 1/4"	3648'	Mar-57	Beach Expl lles Federal #6 1980' FNL 660' FEL 17-I, 16S, 29E
1678' 1678'	Pumping 7 0 TSTM not reported	Penrose 1658'-1678' (open hole) 1658'-1678' pay interval Natural completion	1271' Calculated 4 1/2" @ 1658' 100 7 7/8" assumed	Surface Calculated 10 3/4" @ 200' 100 12 1/4" assumed	3584'	Oct-87	Aspen Pumping Service Cal-Mon State #1 2310' FNL 512' FWL 19-E, 16S, 29E
1804' 1790'	Pumping 40 Trace TSTM not reported	Penrose 1719' - 1733' Natural completion	1021' Calculated 7" @ 1803' 200 9 1/2" assumed	Surface Calculated 10 3/4" @ 171' 60 12 1/4" assumed	3632'	Apr-88	Aspen Pumping Service Cal-Mon State #2 22260' FSL 512' FWL 19-L, 16S, 29E

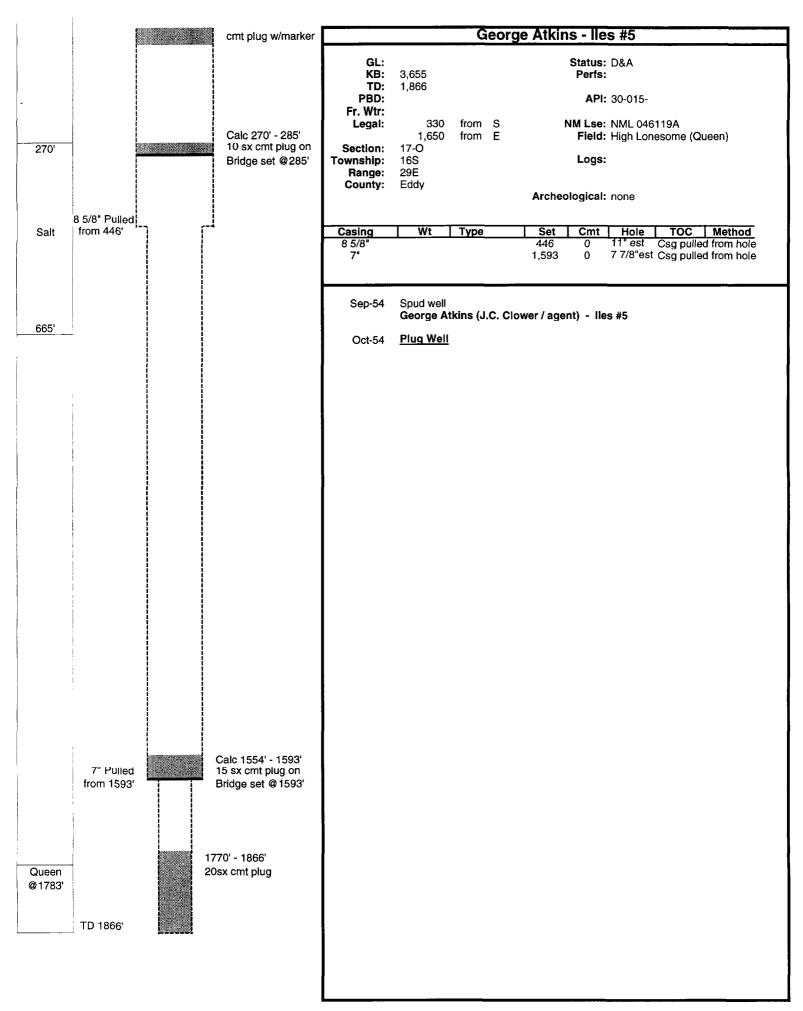
Beach Exploration, Inc.
Proposed West High Lonesome Penrose Sand Unit

<u>Area of Review - Plugged Wells (wellbore schematics attached)</u>
Form C-108, Item VI

	<u>Operator</u>	Lease & Well #	<u>Location</u>	SecUnit, Twp., Rge.
	1. Suntex Resources, Inc.	Shiloh Federal #1	1650' FNL 2308' FEL	17-G, 16S, 29E
	2. Butler & Horne	lles #1	990' FSL 2310' FWL	17-N, 16S, 29E
	3. George Atkins	lles #5	330' FSL 1650' FEL	17-O, 16S, 29E
	4. B.H. Nolen / George Atkins	s lles #1	330' FSL 330' FEL	17-P, 16S, 29E
	5. Hondo Oil & Gas	Lackey Federal	660' FNL 660 FEL	18-A, 16S, 29E
	6. Beach Exploration, Inc.	Exxon Federal "A" #4	990' FNL 1650' FEL	18-B, 16S, 29E
	7. McClellan Oil Corp.	Cal-Mon State #1	990' FNL 421' FWL	19-D, 16S, 29E
	8. Enron Oil & Gas Co.	Sabres "19" Fed. Com. #1	1846' FNL 926' FWL	19-F, 16S, 29E
	9. Upland Production Co.	Exxon ERL Federal #1	2310' FSL 2310 FEL	19-J, 16S, 29E
1	10. Suntex Resources, Inc.	Ginger Federal #1	1650' FNL 1650' FWL	20-F, 16S, 29E
1	11. Raymond Smith	Hondo #1	1980' FSL 660' FWL	20-L, 16S, 29E

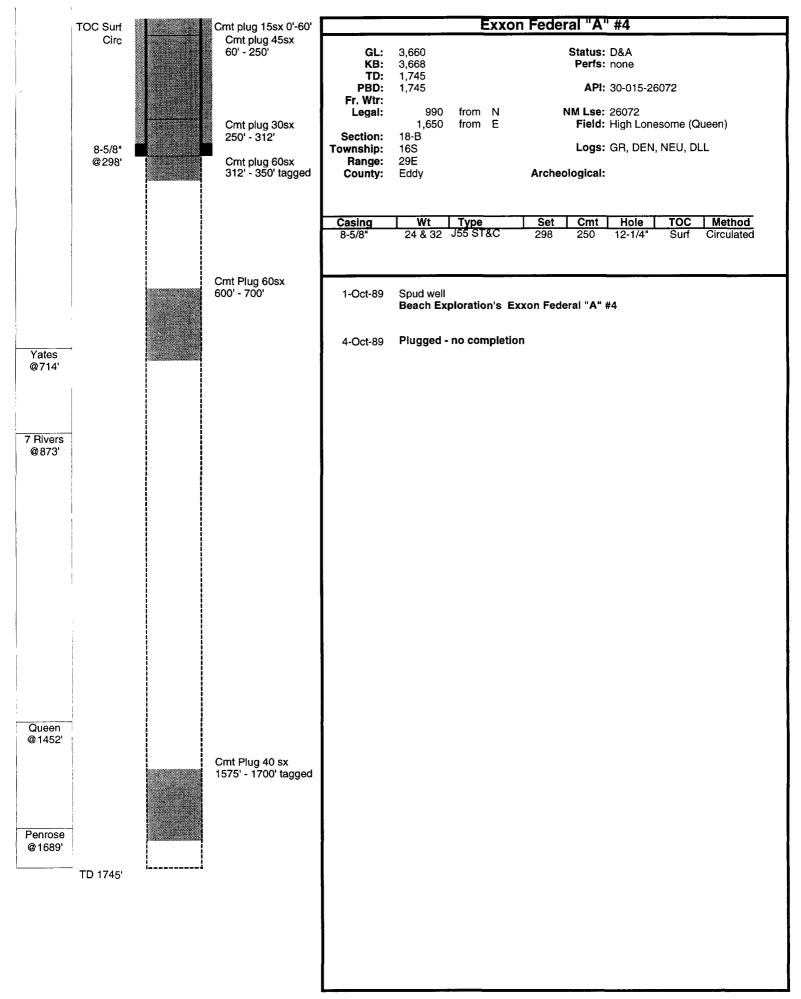


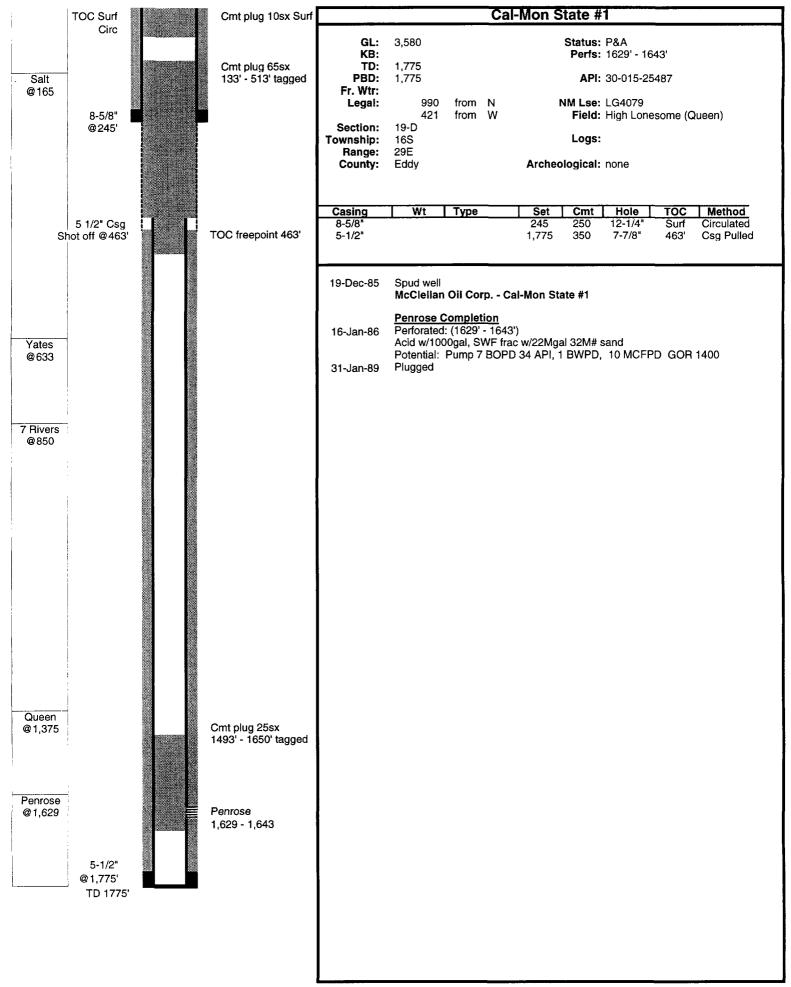


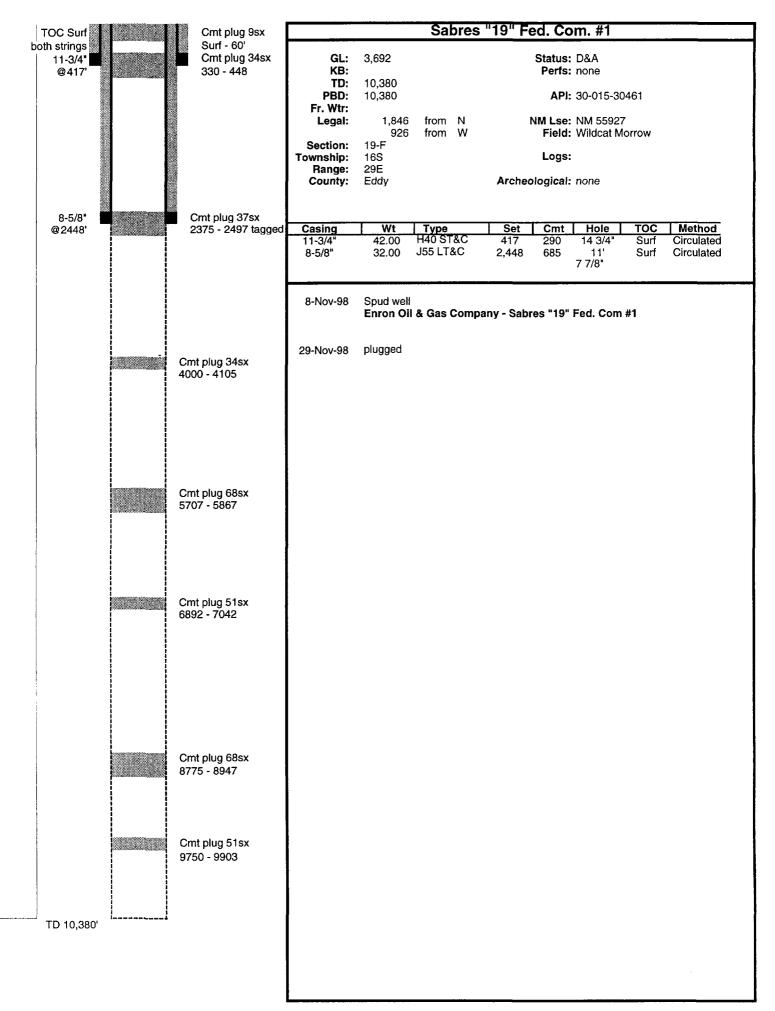


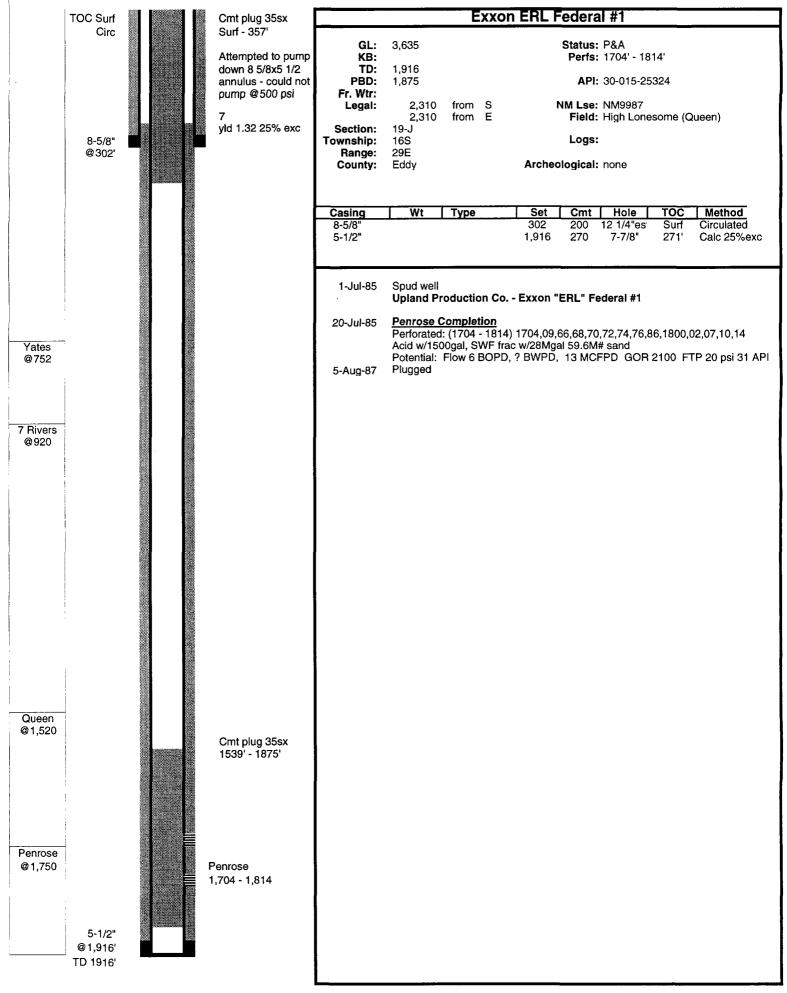
B.H. Nolen / George Atkins - Iles #1 cmt plug w/marker GL: Status: D&A 3,655 KB: Perfs: 1,630 TD: PBD: API: 30-015-Fr. Wtr: Legal: 330 from S NM Lse: NML 046119 from E 330 Field: High Lonesome (Queen) 250' - 275' 17-P Section: 10 sx cmt plug Township: **16S** Range: 29E 10" County: Eddy Archeological: none @305 Casing 10" Method Circulated Wt Type Set Cmt Hole TOC 305 Surf 40 11" est 8 1/4" Bottom 30' collapsed left in hole 1,630 remainder of 8 1/4" pulled Jul-39 Spud well B.H. Nolen (George Atkins) - Iles #1 Plug Well Oct-41 710' - 740' 10 sx cmt plug 1550' - 1600' 20 sx cmt plug Collapsed 8 1/4" Csg below 1600' TD 1630⁴

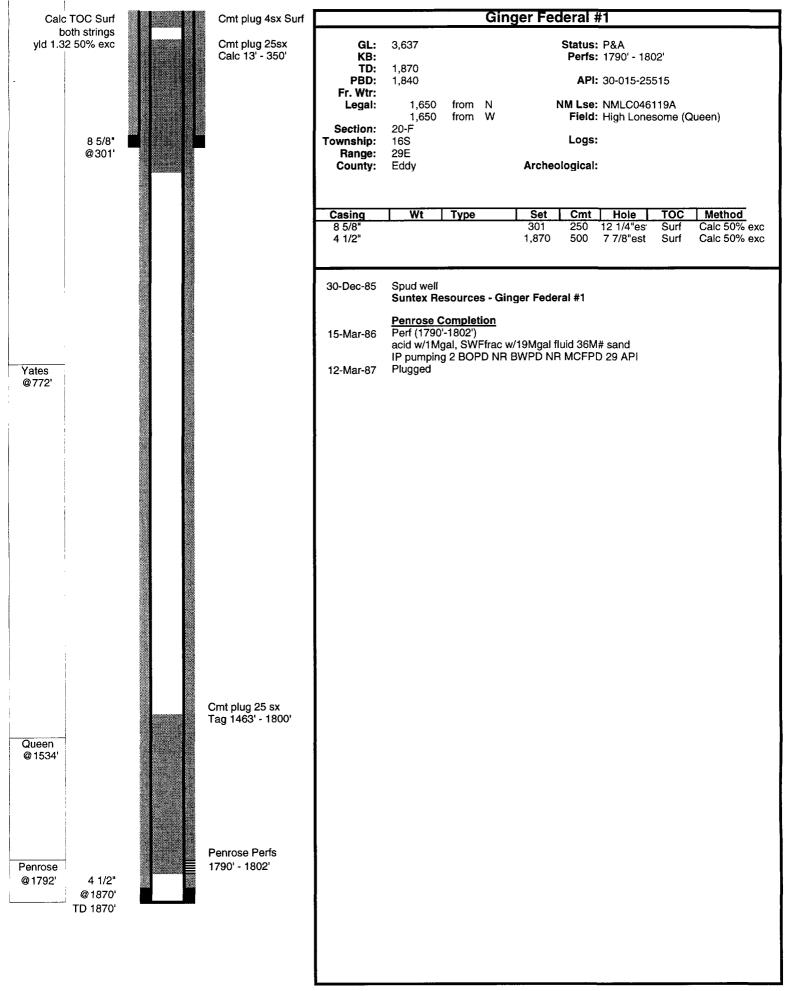
Lackey Federal #1 Cmt plug 10sx Surf 0' - 20' 3,653 Status: D&A GL: KB: TD: Perfs: none (open hole) Cmt plug 15sx 175' - 250' 755 PBD: 755 API: 30-015-Fr. Wtr: 660 NM Lse: Legal: from N 660 from E Field: Section: 18-A Township: Logs: 16\$ Range: 29E County: Eddy Archeological: Wt Set Cmt Hole TOC Method Casing Type no casing set 7 7/8" est 28-Oct-62 Spud well Hondo Oil & Gas - Lackey Federal #1 Plugged 5-Nov-62 Yates @725' TD 755'

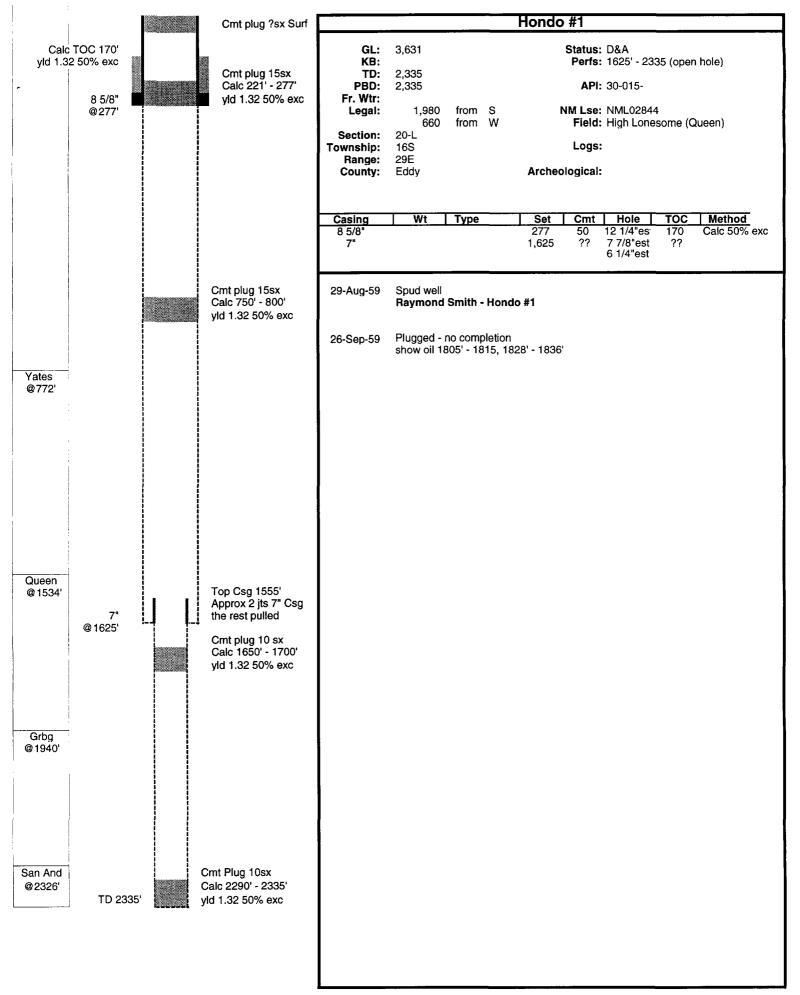












Waterflood Feasibility Study High Lonesome Queen Field Eddy County, New Mexico

Prepared For Beach Exploration, Inc.

T. SCOTT HICKMAN & ASSOCIATES. INC. PETROLEUM ENGINEERS January 27, 1993

Beach Exploration, Inc. 800 N. Marienfeld Suite 200 Midland, TX 79701

Attention: Mr. Hal Gill

Gentlemen:

Re: Waterflood Feasibility Study High Lonesome Queen Field Eddy County, New Mexico

In accordance with Mr. Gills' request, we have conducted a waterflood feasibility study of selected leases in the High Lonesome Queen Field, Eddy County, New Mexico. The results of this study along with the waterflood economics are discussed in the attached report.

Net oil and gas reserves shown on Tables 6 through 8 are estimated quantities of crude oil attributed to the composite revenue interests being evaluated after deduction of royalty and/or overriding royalty interests. The 1987 Oil and Gas Reserve Definitions, as endorsed by the SPE and SPEE, were used to classify the reserves. Future net revenue was adjusted for capital expenditures, operating costs, ad valorem taxes and wellhead taxes, but no consideration was given to Federal income taxes or any encumbrances that might exist against the evaluated interest. Present worth future net revenue shows the time value of money at certain discount rates, but does not represent our estimate of fair market value.

Oil reserves were determined using industry-accepted methods including extrapolation of established performance trends, volumetric calculations and analogy to similar producing zones. Since there are currently no gas sales from the leases, no gas reserves were assigned for the proposed unit area.

In the preparation of this report, we have reviewed for reasonableness, but accepted without independent verification information furnished by Beach Exploration, Inc. with respect to interest factors, current prices, operating costs,

Beach Exploration, Inc. January 27, 1993 Page 2

investments and various other data. We are qualified to perform engineering evaluations and do not claim any expertise in accounting, legal or environmental matters. As is customary in the profession, no field inspection was made of the properties nor have we verified that all operations are in compliance with any states and/or Federal conservation, pricing and environmental regulations that apply to them.

At the client's request, an oil price of \$18/BBL was held constant for the life of the project. Operating costs and capital investments were also held constant. No equipment salvage value or abandonment costs were included for the properties. The development and operating costs for the project were estimated by Beach Exploration based on the specifications furnished by us.

This study was performed using industry-accepted principles of engineering and evaluation that are predicated on established scientific concepts. However, the application of such principles involves extensive judgment and assumptions and is subject to changes in performance data, existing technical knowledge, economic conditions and/or statutory provisions. Consequently, our reserve estimates are furnished with the understanding that some revisions will probably be required in the future.

This report is solely for the information of and the assistance to Beach Exploration, their investors and others authorized by Beach in their evaluation of the waterflood potential in the High Lonesome Queen Field and is not to be used, circulated, quoted or otherwise referred to for any other purpose without the express written consent of the undersigned except as required by law. Persons other than those to whom this report is addressed or those authorized by the addressee shall not be entitled to rely upon the report unless it is accompanied by such consent. Data utilized in this report will be maintained in our files and are available for your use.

Yours very truly,

T. SCOTT HICKMAN & ASSOC., INC.

J. Louis Moseley, P.E.

glb attachments

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DISCUSSION

INTRODUCTION

The High Lonesome Queen Field, located approximately 11 miles northwest of Loco Hill, Eddy County, New Mexico was discovered in November 1939 with the completion of the B.H. Nolen #1 Iles. The field has produced approximately 4.5 MMBBL of oil and 1.5 BCF of gas to date from the Queen (Penrose) sand. The field currently includes 45 producing, 7 injection and 10 shut-in or temporarily abandoned wells.

Waterflood operations have been on going in the field in Sections 11 through 16 of T16S R39E, N.M.P.M. since 1957. The waterflood feasibility study area, covering the proposed West High Lonesome Penrose Sand Unit (WHLPSU), includes Sections 17 through 20.

CONCLUSIONS

- 1. The Queen (Penrose) sand is continuous throughout the field and the proposed Unit area.
- 2. Unitization is required to efficiently waterflood the reservoir.
- 3. Original oil-in-place (OOIP) for the proposed West High Lonesome Penrose Sand Unit area is estimated at 6119 MBBL.
- 4. Primary reserves are estimated at approximately 61 MBBL as of January 1, 1993.
- 5. Ultimate primary recovery is estimated at 538 MBBL or 8.8% of OOIP.
- 6. Waterflood reserves for the proposed unit are estimated at 538 MBBL based on a secondary/primary recovery ratio of 1.0.
- 7. Total waterflood development cost for the proposed unit is estimated at \$787,000.
- 8. Incremental BFIT waterflood economics for the proposed unit indicate unrisked future net revenue of \$1,511,000 discounted at 10%, payout of 3.2 years and an income to investment ratio of 4.6 undiscounted. The DCF ROR is estimated at 44%.

RECOMMENDATIONS

- 1. Unitize proposed unit area shown on Figure 8.
- 2. Drill and complete 1850' producing well in Unit B Section 19 T16S, R29E.
- 3. Install 80-acre, 5-spot waterflood pattern as shown on Figure 8.

- 4. Install supply line and purchase make-up water from the City of Carlsbad's Double Eagle fresh water system.
- 5. Install injection plant facilities and distribution lines and commence full-scale waterflood operations.
- 6. Monitor waterflood performance including balancing injection and withdrawals in each pattern to maximize waterflood economics.

GEOLOGY

The High Lonesome Queen Field produces from the Penrose sand at a depth of about 1700' (+1900' subsea). The Penrose is a relatively thin, blanket sand developed in the lower half of the Queen Formation (Guadalupian, Permian). The sand is widespread areally and is 26-32 feet thick in the study area. It dips to the southeast at 100-125 feet/mile (Figure 1).

The High Lonesome Queen Field is one of a series of fields trending northeast-southwest where hydrocarbons are stratigraphically trapped in the Penrose. Figures 2 and 3 illustrate the apparent continuity of the sand development and the long, narrow producing trend. The reservoir producing facies is a gray, very fine - medium grained, and subrounded quartz sandstone cemented with varying amounts of anhydrite and salt. This porous and permeable facies is sandwiched in between tight evaporitic sand in an updip direction and a red, shaley, and non-reservoir facies in the downdip direction. Along this producing trend, porosities average 12% and permeabilities nearly 14 md.

PRIMARY PERFORMANCE

Development drilling in the study area occurred mainly after mid 1985, the most recent being the Beach-Exxon A-Federal No. 3 well completed in June 1989 (Table 1). The wells were usually completed with 4 1/2" or 5 1/2" casing set through the Queen pay interval. The initial fracture treatments utilized 20,000-30,000 gallons gelled water with 1-2 lb/gal of sand concentration. Initial potentials ranged from 3 BOPD for the Norwood-Isles Federal No. 3 to 100 BOPD for the McClellan-Renee Federal No. 4.

The 10 leases and 26 wells within the proposed West High Lonesome Penrose Sand Unit have produced approximately 477 MBBL from the Queen (Penrose) sand as of January 1, 1993. Current production from the proposed unit averages approximately 2.1 BOPD per well. Individual lease production for 1992 year-to-date is shown on Table 2.

Primary reserves for the proposed W. High Lonesome Penrose Sand Unit are estimated at 61 MBBL as of January 1, 1993 based on individual well and composite decline curve analysis. Ultimate primary recovery is estimated at 538 MBBL. Primary performance for the proposed unit area is summarized on Table 2 and shown on Figures 4 and 5.

Declining fluid production associated with declining reservoir pressure, increasing GOR's and negligible water production over the life indicate the primary producing mechanism has been solution gas-drive. The maximum producing rate of approximately 11,000 BOPM occurred in 1986 from 21 producing wells. The composite GOR peaked at approximately 1300 SCF/BBL in 1991 before declining to the present level of less than 1000 SCF/BBL. Currently there are no gas sales from the study area based on available data. The reservoir fluid properties for the proposed unit area are summarized on Table 3.

A \$\phi\$ (porosity x net pay) isopach map of the Penrose sand was constructed for the proposed unit area and is shown as Figure 6. All available CNL-FDC wireline porosity logs as shown on Figure 7 were utilized to estimate net pay and \$\phi\$ for individual wells. Since core analysis data was not available to establish a porosity-permeability relationship, a 12% porosity cut-off was assumed. The average connate water saturation (Sw) for the Queen (Penrose) sand in the proposed Unit area was estimated to be 30% based on available wireline log data. Gross reservoir pore volume within the proposed unit area was estimated at 1374.55 ac-ft from the \$\phi\$h isopach map. The original oil-in-place (OOIP) volume calculated from the \$\phi\$h map appears reasonable based on the calculated primary recovery efficiency.

Volumetric calculations for the proposed area are as follows:

```
OOIP = 7,758 φ (1-Sw) Ah/Boi

Where OOIP = STB

7,758 = STB/Ac-Ft
φ Ah = PV, Ac-Ft
Sw = Connate Water Saturation, Frac of PV
Boi = RB/STB
= 7,758 (1-0.3)1374.55/1.22
= 6118.6 MBO
```

The primary recovery factor (PRF) for the proposed unit area is calculated as follows:

```
PRF = <u>538 MBBL</u> x 100 = 8.8% of OOIP
6118.6 MBBL
```

SECONDARY PERFORMANCE

A nominal 80-acre, 5-spot injection pattern utilizing 12 injection and 14 producing wells is recommended for the proposed W. High Lonesome Penrose Sand Unit based on analysis of other Queen (Penrose) waterfloods in the area (Table 4). This includes the proposed producing well to be drilled in Unit B of Section 19).

The proposed unit boundary as shown on Figure 8 should maximize the economics of secondary recovery for the study area. This optimization is achieved by excluding wells with very poor primary recovery (<8MBO) on the south and west side, minimizing the re-plugging liability to the south and east and installing the maximum number of 5-spot patterns utilizing existing wellbores.

The current average oil saturation in the proposed unit area is calculated as follows:

```
So (N-Np) Bo (1-Sw)
                       NBoi
      Where: So = Oil Saturation @ 1/1/93, fraction of Pore Volume (Vp)
               N = OOIP, MSTB
              Np = Cumulative Oil Production @ 1/1/93, MSTB
              Bo = Current Oil Formation Volume Factor, RB/STB
              Sw = Conate Water Saturation, Fraction of PV
             Boi = Initial oil Formation Volume Factor, RB/STB
              So _ (6118,6-477,5)1.05(1-0.3)
                         (6118.6)(1.22)
                 = 0.56
Pore Volume (Vp) <u>NBoi</u>
                  (6118.6)(1.22)
                       (1-0.3)
                 = 10,664 MBBL
   Free Gas Volume (FGV) = (1-So-Sw)Vp
                          = (1-0.56-0.3)(10,664 MBBL)
```

Fillup-time, assuming an average injection rate of 200 BPD/well, can be estimated as follows:

= 1493 MBBL

Fillup Time =
$$\frac{FGV}{Injection \ Rate}$$
= $\frac{1,493,000 \ BBL}{200 \ BPD/well \ x \ 12 \ wells \ x \ 30.4 \ days/month}$
= 20.5 months

Theoretical waterflood recovery based on volumetric calculations is as follows:

Waterflood Recovery <u>7758 ø Ah (So-Sor)(Ev x Ep)</u> Bo = <u>7758 (1374.55)(0.56-0.315)(0.5x0.67)</u> 1.22

= 717 MBBL

The estimated waterflood recovery utilizing volumetric calculations (717 MBBL) compares favorably with waterflood reserves of 538 MBBL based on a 1.0 S/P (Secondary/Primary Recovery) ratio by analogy. These reserves include those attributed to the proposed drilling well in Unit B of Section 19. Estimated recoveries for other Queen (Penrose) Sand Units on trend are summarized on Table 4.

Flood-start for the proposed unit is assumed to be July 1, 1993. The project effective injection rate is estimated at 48,000 BWPM or 0.67 x 72,000 BWPM. The effective injection rate factor of 0.67 is based on the areal confinment for the proposed injection plan which accounts for peripheral and east end injection losses in the proposed unit.

The estimated peak oil rate of 9000 BOPM or 23 BOPD per producing well was based on the observed performance of analogous Queen (Penrose) Waterfloods in the region adjusted for well spacing. Peak production, which is estimated to occur at fillup in March 1995, was held constant for 12 months before declining at approximately 20% per year for the life of the project (Figure 4).

In our opinion, the potential waterflood oil recovery for each of the leases within the proposed unit area can best be represented by ultimate primary

recovery and it should be utilized as the major parameter in the unit participation formula.

ECONOMICS

The total estimated waterflood development cost of \$787,000 for the proposed unit is summarized on Table 5. Operating costs were estimated at \$700/well-month for remaining primary operations and \$1240/well-month for waterflood operations based on 26 total wells. The estimate for waterflood operations includes the cost of make-up water estimated to be \$0.15/BBL. Operating costs were reduced to \$14,000/month near the end of waterflood operations to account for the elimination of make-up water and abandonment of uneconomic wells.

The initial injection rate is estimated to be 200 BWPD per well at a maximum wellhead pressure of 1100 psi based on analogy (Table 4). The initial make-up water volume (72,000 BPM) can be purchased from the city of Carlsbad's Double Eagle fresh water system approximately 3 miles from the proposed unit. The cost to install the water supply line from the system to the proposed unit is estimated at \$72,000 (Table 5). The cost of the make-up water volume, initially estimated at \$10,800/month, should decrease over the life of the project due to recycling produced water.

Tables 6, 7 and 8 are the respective cash flow projections for the Total Proved, Proved Developed Producing (PDP) and Proved Undeveloped (PUD) reserve categories. All economics were based on constant prices and costs.

Incremental waterflood (PUD) economics for the proposed unit indicate a rate of return of 44% and payout of 3.2 years on a total waterflood development cost of \$787,000.

TABLE 1 NELL DATA FROPUSED NEST HIGH LONESONE PENROSE SAND UNIT HIGH LONESONE QUEEN FIELD EDDY COUNTY, NEW REXICO

,			LECATION				IX	INITIAL POTENTIAL	TENT 191
OPERATOR LEASE	<u> </u>	KELL AO.	SEC THAN ROSE DATE	CASING RECORDS	Penfi	INITIAL INCHINENTS	EOF	是透	608-80F/80
BEACH EXPLORATION	EXXON FEDERAL	1 660 FSL 66	660 FEL 18-16-29 5/30/85	3 5/8-302-225 4 1/2-1840-373	1722-1756	4/950 8F/17,000 X 10,000#	F-7	m	1132
PEACH EXPLORATION	EXXON FEDERAL	2 330 FLS 16	1650 FEL 18-16-29 10/14/85	8 5/8-343-475	1713-1750	A/1500 SGF/18,000 X 15,0003	P-10	.	600
Beach exploration	EXXON PEDERAL	3 1650 F3L 3	330 FEL 18-16-29 11/29/85	8 5/8-304-235 4 1/2-1813-700	1717-1741	SGF/10,500 X 27,000€	g-7 8		009
BEACH EXPLOSATION	EUUN FEDERAL	4 1650 FSL 1	4 1650 F3L 1650 FEL 16-16-29 4/28/84	8 5/8-333-173 4 1/2-1300-500	1714-1731	4/1203 SGF/23.000 X 42.000#	F-63	8	472
BEACH EXPLOSATION	EXXON PEDERAL	5 1650 651 1	5 1650 FSL 1835 FKL 18-16-29 9/14/86	8 5/3-303-250 4 1/2-1715-450	1639-1652	4/1200 SGF/20,000 X 42,000#	ř-73		1266
BEACH EXPLORATION	EXXON FEDERAL	6 360 FSL 20	2035 Fig. 18-16-29 (277786	8 5/8-207-250 4 1/2-1772-500	1708-1727	4/1200 \$F/20.000 X 40.000#	P-50		ξύ <u>ύ</u>
БЕАСН ЕХРГОКАТІОМ	EXXON "A" FEDERAL	1 2316 FNL 3	330 FEL 18-16-29 10/2/88	8 5/8-311-350 4 1/2-1500-450	1714-1728	4/1200-83F/20+000 X-42+000-#	F-74	2	83
BEACH EXPLORATION	EXXON "A" FEDERAL	2 2310 FML 1	2 2810 FNL 1650 FEL 18-16-29 2/12/89	8 5/8-295-250 4 1/2-1770-550	1702-1722	A/1200 SAF/20,000 X 42,000#	P-28	64	1357
BEACH EXPLOSATION	EXXIN "A" FEDERAL	3 2410 FNL 1	3 2410 FNL 1932 FKL 18-16-29 6/9/89	8 5/8-330-250 4 1/2-1705-500	1645-1655	A/1260 S0F/20,000 X 42,666#	P-10		2000
BUTLER-HURN	।अह	1 990 FSL 23	2310 FWL 17-16-29 3/21/40	8 1/4-415 7-1735-100	F&A				
טרטאבעי איני	ISLES FETERAL	5 330 FSL 16	1650 FEL 17-16-29 10/1/54	8 5/8-446 7-1593	Fun				
EASTLAND	COASTAL FEDERAL	1 1980 FNL 1	1 1980 FNL 1980 FEL 19-16-29 6/20/85	8 5/8-304-200 5 1/2-1877-400	1747-1797	A/1500 SGF/36,540 X 87,900#	F-20	-	2500
HALE PETROLEUM	MAW FEDERAL	1 2210 FNL 1	1 2210 FNL 1833 FNL 19-16-29 5/19/86	8 5/8-290-175 5 1/2-1972-1040	1734-1745	A/1000 SGF/33,600 X 55,500#	P-80		
હેતી	RYBA FEDERAL	2 1750 FNL &	660 FEL 19-16-29 6/21/32	8 5/8-348-225 5 1/2-2310-650	1688-1804	A/1500 SF 50,000 X 60,000#	F-13	9	326
NGLELLAN GIL	BIG KAC FEDERAL	1 660 FM, 33	3300 FEL 19-16-29 973/85	4 1/2-1871-190	1883-1899	A7500 S0F/20.000 X 31,5003	F-14		
ETTELLAN GE	AENES FEDERAL	1 660 FLS 33	350 FIE 17-16-29 9716/85	8 5/8-300-200 5 1/2-1815-350	1729-1759	\$85731,000 X_50,0005	F-32	4	

TABLE 1 WELL DATA PROFOSED NEST HIGH LONESOME FENKOSE SAND UNIT HIGH LONESOME OVEEN FIELD EDDY COUNTY, NEW MEXICO

	! e	<u> </u>										
TENTIAL	COR-SOF/ED	24	292	375	4000					हर क्	500	4 50 50
INITIAL FOTENTIAL	17.6 17.6 18.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19	רוו	165	2	-				13	7	्	8
INI	EOPŪ	F-60	-8-3 -83	P-100	F-17	F-20	I	P-25	P-84	P-42	F-75	F-41
	INITIAL TREATHENTS	A/1000 SHF/30,060 X 43,000#	4/1000 SCF/30,000 X 49,000#	A/1000 SGF/30,000 X 50,000#	SNF/100,000 X 109,000#	100 GTS NITRO		SF/5000	A/1000 SGF/S0.000 X 49.000#	A/1000 SMF/30,000 X 49,0008	A/1000 SGF/28,000 X 50,000#	4/1000 SGF/10,200 X 24,000#
	PEÑFS	1760-83	1774-93	1721-1738	1746-1772	ÚH 1703-1813	GH 1590-1820	OH 1740-1800	1767-1757	1740-1764	1730-1758	1752-1764
	CASING RECORDS	8/56-300,250 5 1/2-1840-350	8 5/8-300-280 5 1/2-1920-375	8 5/8-250-250 5 1/2-1839-370	8 5/8-355-250 4 1/2-1874-380	8 1/4-43 5 1/2-1703-180	8 1/4-330-50 7-1590-100	8 5/3-275-50 7-1740-50	8 5/8-292-250 5 1/2-1842-350	8 5/8-253-190 4 1/2-1509-430	8 5/8-311-250 4 1/2-1350-500	8 5/8-309-250 4 1/2-1850-850
LUCATION	SEC THN RGE	2 330 FNL 330 FNL 20-16-29 9/25/65	3 1650 FML 330 Fix. 20-16-29 12/28/65	4 1650 FSL 330 FWL 17-16-29 1/15/86	1 660 FNL 660 FEL 19-16-29 9/30/85	2 1650 FSL 2310 Fil. 17-16-29 5/14/40	3 330 FM, 2310 FM, 20-16-29 6/1/40 8 1/4-330-50	4 1650 FSL 2310 FEL 17-16-29 3/9/53 2/12/54	7 330 FSL 1650 FWL 17-16-29 4/14/36	8 2310 FSL 1950 FML 17-16-29 9/16/37	3 2310 FML 938 FML 17-16-29 1/27/86	4 2310 FNL 1650 FNL 17-16-29 6/1786
	LEASE	NENEE FEDERAL	RENEE FEDERAL	स्टाटः स्टाटसम्	FEGGRAL "19"	ISLES FEIGRAL	ISLES FERERAL	isles feieral	ISLES PENERAL	ISLES FEDERAL	SHILOH FEDERAL	SHILON FEDERAL
	GPERATOR LES	אכנוברוש פון	MOCIELLAN OIL	MOLELLAN OIL	NORHOOD	NORMOOD	NORMOOD	หับสิงใดเอ	NORKOLD OIL	NORMOD OIL	SUNTEX RESOURCES	SUNTEX RESOURCES

TABLE 2

OPERATOR AND LEASE STATISTICS
PROPOSED W. HIGH LONESOME PENROSE SAND UNIT
HIGH LONESOME QUEEN FIELD
EDDY COUNTY, NEW MEXICO

OPERATOR LEASE	WELLS	% %	NOMINAL SURFACE ACRES TOTAL - %	ACRES	1992 01 YID (BBLS	1992 OIL PROD YID (8 MO) BBLS %	CUM OIL PROD 6 9-1-92 BBLS %	PROD 92	PRIMARY F BBLS	RESERVES 1-93	ULT IMATE RE BBLS	ULTIMATE PRIMARY RECOVERY BBLS %
Beach Exploration, inc. Exxon Federal	Q	24.0	240	22. 2	3677	28.9	156528	33.2	14140	22.9	172547	32. 1
Exxon Federal-A	ო	12.0	120	11.2	1994	15.7	25740	ss ss	1587	2.6	27971	5. 2
Total	. Gi	36.0	360	33.4	5671	44.6	182268	38.7	15727	25. 5	200518	37. 3
Eastland Oil Co. Coastal Federal	•••	7 0	Q	3.7	130	1.0	3043	9.0	0.0	0.0	3043	9
Haile Petroleum, LTD. M&W Federal		4.0	40	3.7	1135	83 6.	17435	3.7	12305	19.9	30291	ra O
JFG Enterprises Ryan Federal	-	4 .	9	3.7	0.0	0.0	9846	2.1	0.0	0.0	9846	
McClellan Oil Corp. Big Mac Federal		4.0	40	3.7	502	3.9	9745	2.0	2760	. 5	12780	2.4
Renee Federal	4	16.0	160	14.8	1897	14.9	90344	19. 2	3163	5. 1	94170	17. 5
Total		20.0	200	18.5	2399	18.8	100089	21. 2	5923	9.6	106950	19, 9
Norwood Oil Corp. Federal 19	-	4.0	80	7.4	22	0.2	4044	6.0	0.0	0.0	4044	0.7
Isles Federal	22	20.0	240	22.2	2181	17.1	115754	24.6	23763	38. 3	140347	26. 1
Total	9	24.0	320	29. 6	2203	17.3	119798	25. 5	23763	38.3	144391	26.8
Suntex Energy Corp. Shiloh Federal	~	8 0 .	80	7.4	1195	9.4	38757	8.2	4119	6.7	43257	0 · 80
Grand Total	52	100.0	1080	100.0	12733	100.0	471236	100.0	61837	100.0	538296	100.0

TABLE 3 Reservoir Fluid Properties Proposed West High Lonesome Unit High Lonesome Field Eddy County, New Mexico

Pi, Pb, Oil Gravity, Rsi, T,	740 psi est. 1800 psi est. 35° API 490 SCF/BBL 90° F
Boi,	1.22 RB/STB
Bo,	1.05 RB/STB @ current BHP est.@ 100 psi

~ • • • •

TABLE 4
Queen (Penrose) Sand Walerflood Projects
High Lonesome and Red Lake Fleids
Lea County, New Mexico

Project	Field Sestion. Township-Range	Area (Ac.)	Prim WBO	Primary EUR MBO MBO/Well	Secondary EUR MBO S/P	LY EUR	Injection Pallern	Maximum Wells	Floodstart Year	Average Maximum Injection Rate & Pressure
vintage Ufilling High Lonesome Penrose Ut.	High Lonesome (Queen) Sec. 15-7165-R29E	480	\$29	48.1	325	0.61	Partial 40	BP + 71	1957-65	150 BWPD
Aceco Petroleum High Lonesome Queen Sand Wf	High Lonesame (Queen) Sec. 16-716S-R29E	00	152	21.7	211	1. 39	40 Ac. 5-Spot	7P + 51	1957-59	@ 1100 ps; 150 BWPD
Armstrong Energy High Lonesome Brewer Bosworth	High Lonesame (Queen) Secs. 11, 12, 13 & 14. T165-R29f	1200	1361	45.4	1315	0.97	9 	+ 4 + 16	, 40 t	6 1100 ps.l
Kincald & Walson E. Redtake Ul.	Red Lake Queen Grayburg East						Line Drive			zau BWPu e 750 psi
,	Secs. 35 & 36-7165-R28E Secs. 1 & 2-7115-R28E	520	226	7.77	292	1.29	80 Ac, 5-Spot	6P + 71	1970	280 BWPD
			2268	37.2 Ave.	2143	0.94 WID. Ave. 1.07 Arith. Ave.	Ave. In. Ave.			
Proposed W. High Lonesome Penrose Sand Unit	High Lonesome (Queen) Secs. 17, 18, 19 & 20. T16S-R29E	1080	538	22.4	538 Est. 1.0 Est.	1. 0 Est.				

TABLE 5 Waterflood Development Cost Proposed W. High Lonesome Penrose Sand Unit High Lonesome Queen Field Eddy County, New Mexico

		Cost (M\$)
I.	Drill & Equip one (1) Producing Well	125
II.	Convert 12 Wells to Injection	140
III.	Install Water Supply Line	72
IV.	Install Waterflood Plant and Facilities	85
v.	Install Water Injection Lines	140
VI.	Production Facility Consolidation	120
VII.	Re-Plug 2 Abandoned Wells in Proposed Unit Area	_40
	Subtotal	722
	Pre Unitization Expense	_65
	Total	787

REMAINING PRIMARY & SECONDARY (PROVED)
PROPOSED W. HIGH LONESOME PENROSE SD UNIT
HIGH LONESOME QUEEN FIELD
EDDY COUNTY, NEW MEXICO

DATE: 01/20/93 TIME: 10:11.54

FILE: BEACH GET#: 96

RESERVES AND ECONOMICS

BEACH EXPLORATION INC CONSTANT OIL PRICE

AS OF JANUARY 1, 1993

T. SCOTT HICKMAN & ASSOC PETROLEUM ENGINEERS

ŧ					-PRICES	0	PERATIONS,	M\$			10.00 PCT
-END	GROSS PRO	DUCTION	NET PRO	DUCTION	DIL GAS	NET OPER	SEY+ADV+	NET OPER	CAPITAL	CASH FLOW	CUM. DISC
MO-Y	R OIL, MBBL (GAS, MANCF	OIL, MBBL	GAS, MMCF	\$/B \$/M	REVENUES	WF TAXES	EXPENSES	COSTS, M\$	STAX, M\$	BTAX, M\$
12-9	3 19. 204	. 000	15. 363	. 000 11	3.00 .0	276. 534	20. 351	372. 000	787. 000	-902.817	-860.844
12-9	4 50. 253	. 000	40. 202	. 000 18	3.000	723. 636	53. 255	372.000	. 000	298. 381	-602, 114
12-9	5 104.649	. 000	83.719	. 000 18	3.00 .0	1506. 942	110.901	372. 000	. 000	1024.041	205. 121
12-9	6 101.699	. 000	81, 359	. 000 18	3.00 .00	1464. 462	107.775	372.000	. 000	984.687	910. 769
12-9	7 82.309	. 000	65, 847	. 000 18	3.00 .00	1185. 246	87. 227	372.000	. 000	726. 019	1383. 752
12-9	8 66.126	. 000	52. 901	. 000 18	8. 00	952, 218	70. 077	372.000	. 000	510.141	1685. 883
12-9	9 53. 125	. 000	42. 500	. 000 18	. 00 . 00	765. 000	56, 300	372.000	. 000	336.700	1867. 165
12-	0 42.680	. 000	34, 144	.000 18	. 00 . 00	614. 592	45, 230	276. 000	. 000	293. 362	2010. 755
12-		. 000	27. 431	.000 18	. 00 . 00	493, 758	36. 338	276. 000	. 000	181. 420	2091. 481
12- 2	2 27. 547	. 000	22. 038	.000 18	.00 .00	396. 684	29. 194	276. 000	. 000	91. 490	2128. 490
12- 3 12- 4		. 000	13. 308	. 000 18	.00 .00	239, 544	17. 629	201. 616	. 000	20, 299.	2136.050
12- 5	i .										
12- 6	5										
12- 7	1										
s 101	598, 516	. 000	478. 812	. 000 18	. 00 . 00	8618.616	. 634, 277	3633. 616	787. 000	3563. 723	2136. 050
REM.	. 000	. 000	. 000	. 000	. 00 . 00	. 000	. 000	. 000	. 000	. 000	2136.050
TOTAL	598. 516	. 000	478.812	.000 18	. 00 . 00	8618.616	634. 277	3633. 616	787. 000	3563. 723	2136.050
CUM.	477. 484	. 000		NET OIL REV	ENUES (M\$)	8618.616		PRESENT WO	ORTH PROFIL	E
				NET GAS REVI	•		. 000	DIŞC	PW OF NET	DISC	PW OF NET
ULT.	10 76. 000	. 000		TOTAL REVI	ENUES (M\$)	8618.616	RATE	BTAX, M\$	RATE	BTAX, M\$
8TAX	RATE OF RETURN ((PCT)	68. 92	PROJECT LIFE	(YEARS)		10. 730	. 0	3563. 723	30. 0	812. 369
	PAYOUT YEARS		2. 59	DISCOUNT RAT			10.000	2.0	3205. 295	35. 0	631. 304
	PAYOUT YEARS (DI	SC)	2, 75	GROSS OIL WE	• •		25. 000	5. 0	2744. 439	40.0	483.313
	NET INCOME/INVES		5. 53	GROSS GAS WE			. 000	8.0	2358. 823	45. 0	361. 140
	NET INCOME/INVES		3. 85	GROSS WELLS			25. 000	10.0	2136.050	50. 0	259. 377
								12.0	1936. 505	60. 0	101. 703
INITI	AL W. I. FRACTION	†	1. 000000	INITIAL NET	OIL FRACT	TION	. 800000	15. 0	1674. 336	70.0	-12. 369
FINAL			1.000000		OIL FRACT		. 800000	18.0	1449. 570	80.0	-96.718
PRODU	CTION START DATE		8- 1-92	INITIAL NET			. 000000	20. 0	1317. 232	90.0	-160. 188
	S IN FIRST LINE		12.00		GAS FRACT		. 000000	25.0	1036. 420	100.0	-208.623

REMAINING PRIMARY-EXISTING OPERATIONS (PDP)
PROPOSED W. HIGH LONESOME PENROSE SD UNIT
HIGH LONESOME QUEEN FIELD
EDDY COUNTY, NEW MEXICO

DATE: 01/20/93 TIME: 10:11.54 FILE: BEACH GET#: 95

RESERVES AND ECONOMICS

BEACH EXPLORATION INC CONSTANT OIL PRICE

AS OF JANUARY 1, 1993

T. SCOTT HICKMAN & ASSOC PETROLEUM ENGINEERS

-END-	GROSS PR	PODUCTION	NET PRO	DUCTION	PRIC	ES GAS	OF	•	M\$ NET OPER	CAPITAL	CASH FLOW	10.00 PCT
MO-YR	OIL, MBBL		OIL, MBBL			\$/M	REVENUES		EXPENSES	COSTS, MS	BTAX, M\$	BTAX, MS

12-93	16. 214	. 000	12. 971	. 000	18.00	. 00	233. 478	17, 182	156, 600	. 000	59. 696	56, 939
12-94	13. 728	. 000	10.982	. 000	18.00	. 00	197.676	14. 548	120.000	. 000	63. 128	111.678
12-95	11.827	.000	9, 462	. 000	18.00	. 00	170.316	12.534	120.000	. 000	37. 782	141.461
12-96	10. 334	. 000	8. 267	. 000	18.00	. 00	148.806	10.951	120.000	. 000	17. 855	154.256
12-97	9. 136	. 000	7. 309	. 000	18.00	. 00	131.562	9. 683	120.000	. 000	1.879	155.480
- 10.00									•			
12-98 12-99												
12-33												
_ 12- 1												
12- 2												
12- 3												
12- 4												
12- 5												
12- 6												
12- 7												
TOT 2	61. 239	. 000	48. 991	. 000	18. 00	. 00	881.838	64.898	636, 600	. 000	180.340	155. 480
REM.	. 000	. 000	. 000	. 000	. 00	. 00	. 000	. 000	. 000	, 000	. 000	155. 480
TOTAL	61. 239	. 000	48. 991	. 000	18 NN	. 00	881. 838	64.898	636, 600	. 000	180. 340	155. 480
ľ	01. 233	. 000	40. 331	. 000	10.00	. 00	001.030	04. 638	636. 600	. 000	100. 340	133.460
CUM.	477.484	. 000		NET OIL RI	EVENUES	(M\$)		881.838		PRESENT WO	ORTH PROFIL	E
•				NET GAS RE	VENUES	(M\$)		. 000	DISC	PW OF NET	DISC	PW OF NET
ULT.	538. 723	. 000		TOTAL R	VENUES	(M\$)		881.838	RATE	BTAX, M\$	RATE	BTAX, M\$
	TE OF RETURN	I (PCT)	100.00	PROJECT L	FE (YE	ARS)		5. 000	. 0	180. 340	30.0	122.610
	YOUT YEARS		. 00	DISCOUNT F		CT)		10.000	2.0	174. 727	35.0	116.635
	YOUT YEARS (. 00	GROSS OIL				24.000	5.0	166. 952	40.0	111.289
	T INCOME/INV		. 00	GROSS GAS				. 000	8.0	159.864	45. Đ	106.480
RIYX NE	T INCOME/INV	EST (DISC)	. 00	GROSS WELL	2.			24.000	10.0	155.480	50.0	102.133
1817	W 1 == 1= 1	•••							12.0	151.346	60.0	94. 591
i	W. I. FRACTI		1.000000	INITIAL NE			,	. 800000	15.0	145. 564	70.0	88.280
	W. I. FRACTI		1.000000		TOIL			. 800000	18.0	140. 238	80.0	82. 923
	ION START DA		8 - 1 - 92	INITIAL NE				. 000000	2 0 . 0	136. 919	90.0	78. 326
MON 1 H2	IN FIRST LIN	Ł	12.00	FINAL NE	T GAS	FRACTI	ON	. 000000	25 . 0	129. 326	100.0	74.339

SECONDARY (PUD)
PROPOSED W. HIGH LONESOME PENROSE SD UNIT
HIGH LONESOME QUEEN FIELD
EDDY COUNTY, NEW MEXICO

DATE: 01/20/93 TIME: 10:11.54

FILE: BEACH
GET#: 0

RESERVES AND ECONOMICS

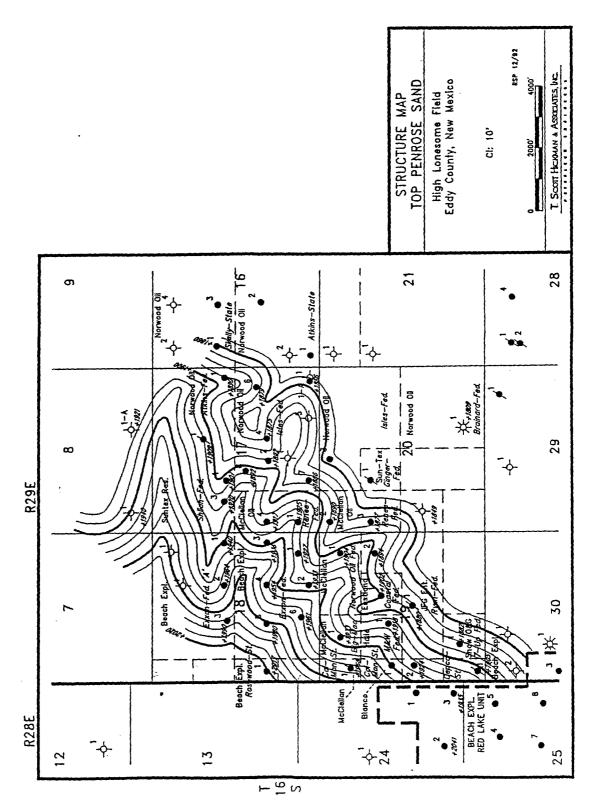
BEACH EXPLORATION INC CONSTANT OIL PRICE

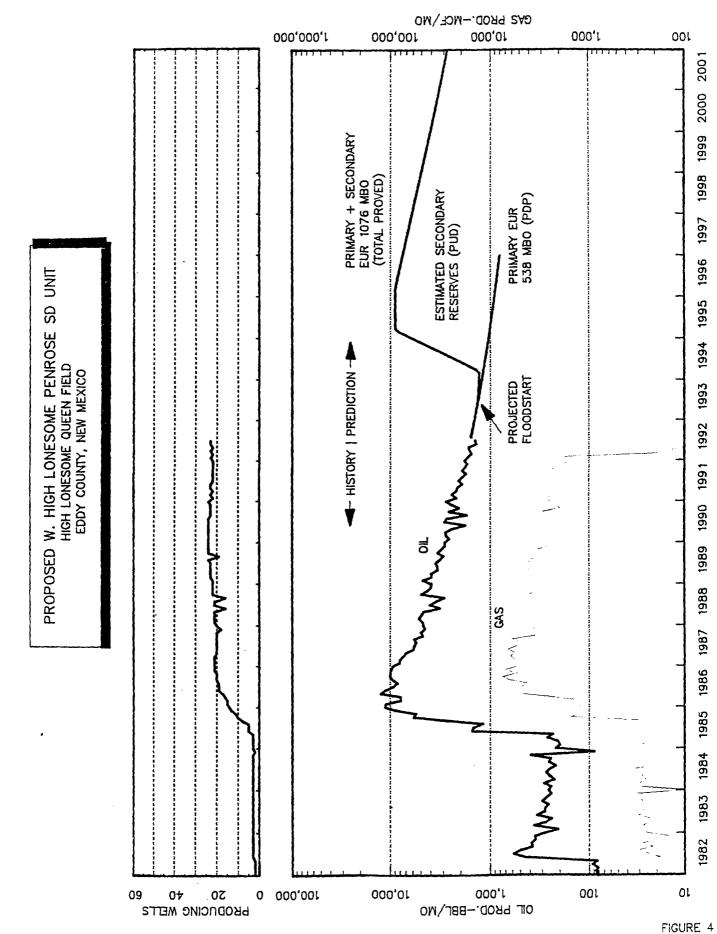
AS OF JANUARY 1, 1993

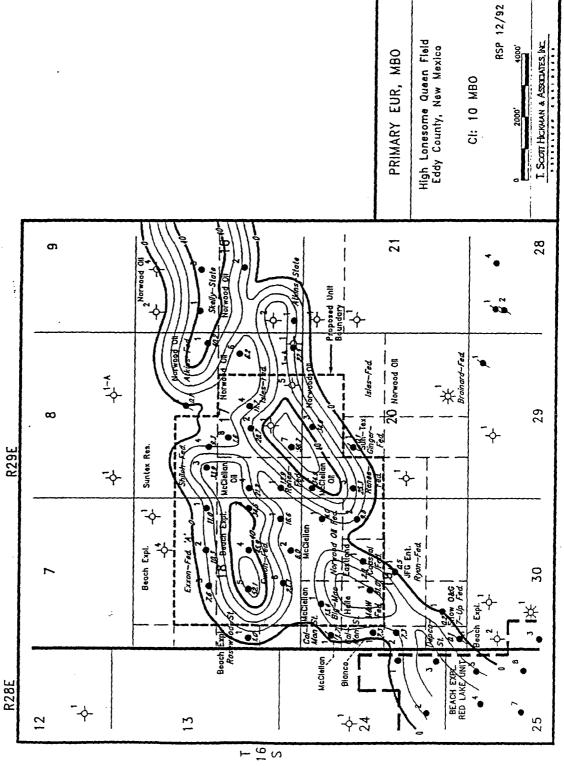
T. SCOTT HICKMAN & ASSOC PETROLEUM ENGINEERS

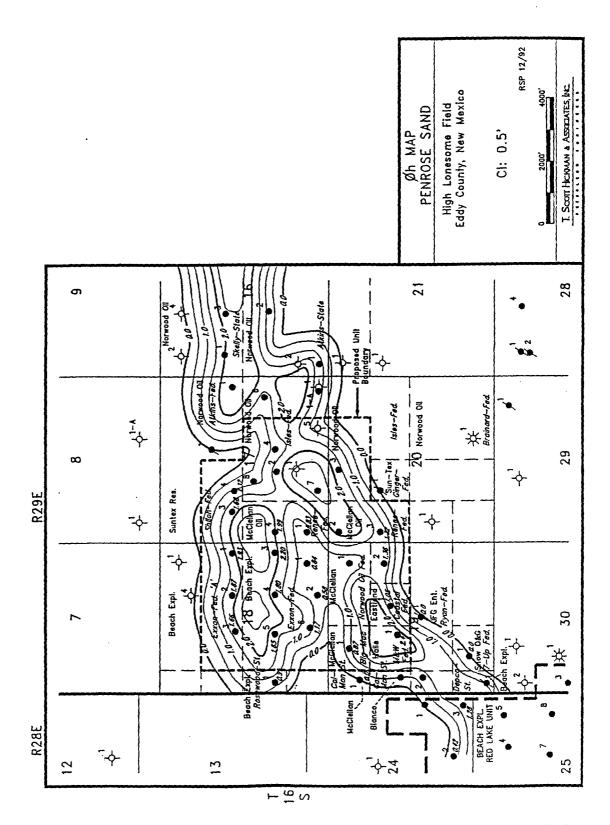
								0	•	•			10.00 PCT
	-ENO- MO-YR			NET PRO		_	GAS \$/M	NET OPER REVENUES	SEV+ADV+ WF TAXES	NET OPER EXPENSES	CAPITAL COSTS, M\$	CASH FLOW BTAX, M\$	CUM. DISC BTAX, M\$
_										•••••			,,
ľ	12-93	2. 990	. 000	2. 392	. 000	18. 00	. 00	43. 056	3, 169	215, 400	787.000	-962, 513	-917. 783
L	12-94	36. 525	. 000	29. 220	. 000	18.00	. 00	525. 960	38. 707	252. 000	. 000	235. 253	-713.792
	12-95	92. 822	, 000	74. 257	. 000	18.00	. 00	1336. 626	98. 367	252.000	. 000	986. 259	63 . 660
	12-96	91. 365	. 000	73. 092	. 000	18.00	. 00	1315. 656	96. 824	252. 000	. 000	966. 832	756. 513
	12-97	73. 173	. 000	58. 538	000	18.00	. 00	1053. 684	77. 544	252.000	. 000	724. 140	1228. 272
	12-98	66. 126	. 000	52. 901	. 000	18.00	. 00	952, 218	70.077	372: 000	. 000	510. 141	1530. 403
	12-99	53 . 125	. 000	42. 500	. 000	18.00	. 00	765. 000	56. 300	372.000	. 000	336. 700	1711. 685
	12- 0	42.680	. 000	34. 144	. 000	18.00	. 00	614. 592	45. 230	276.000	. 000	293. 362	1855. 275
_	12- 1	34. 289	. 000	27. 431	. 000	18. 00	. 00	493.758	36. 338	276.000	. 000	181. 420	1936. 001
	12- 2	27. 547	. 00 0	22. 038	. 000	18.00	. 00	396. 684	29. 194	276. 000	. 000	91.490	1973. 010
1	12- 3	16. 635	. 000	13. 308	. 000	18. 00	. 00	239. 544	17. 629	201.616	. 000	20. 299	1980.570
	12- 4												
	12- 5												
	12- 6												
, 1 	12 - 7												
s	TOT	537. 277	. 000	429. 821	. 000	18. 00	. 00	7736. 778	569. 379	2997. 016	787. 000	3383. 383	1980. 570
R	REM.	. 000	. 000	. 000	. 000	. 00	. 00	. 000	. 000	. 000	. 000	. 000	1980. 570
ī	OTAL	537. 277	000	429.821	. 000	18. 00	. 00	7736. 778	569. 379	2997. 016	787.000	3383. 383	1980.570
С	CUM.	. 000	. 000		NET OIL RI	EVENUES	(M\$)		7736. 778		PRESENT W	ORTH PROFIL	E
•					NET GAS RI	EVENUES	(M\$)		. 000	DISC	PW OF NET	DISC	PW OF NET
บ I	ILT.	537. 277	. 000		TOTAL RE	VENUES	(M\$)		7736. 778	RATE	BTAX, M\$	RATE	BTAX, M\$
		TE OF RETURN	(PCT)	60. 66	PROJECT LI	FE (YE	ARS)		10. 730	. 0	3383. 383	30.0	689. 759
		YOUT YEARS		2. 74	DISCOUNT	RATE (P	CT)		10.000	2.0	3030. 568	35.0	514.669
1		YOUT YEARS (2. 92	GROSS OIL	WELLS			25.000	5. 0	2577. 487	40.0	372.024
1		T INCOME/INVE		5. 30	GROSS GAS	WELLS			. 000	8.0	2198. 959	45.0	254.660
. B.	TAX NET	T INCOME/INVE	ST (DISC)	3. 64	GROSS WELL	.s			25.000	10.0	1980. 570	50.0	157. 244
										12.0	1785. 159	60.0	7. 112
										15.0	1528.772	70.0	-100.649
								7		18.0	1309. 332	80.0	-179.641
										20.0	1180.313	90.0	-238.514
										25. 0	907.094	100.0	-282.962

m.

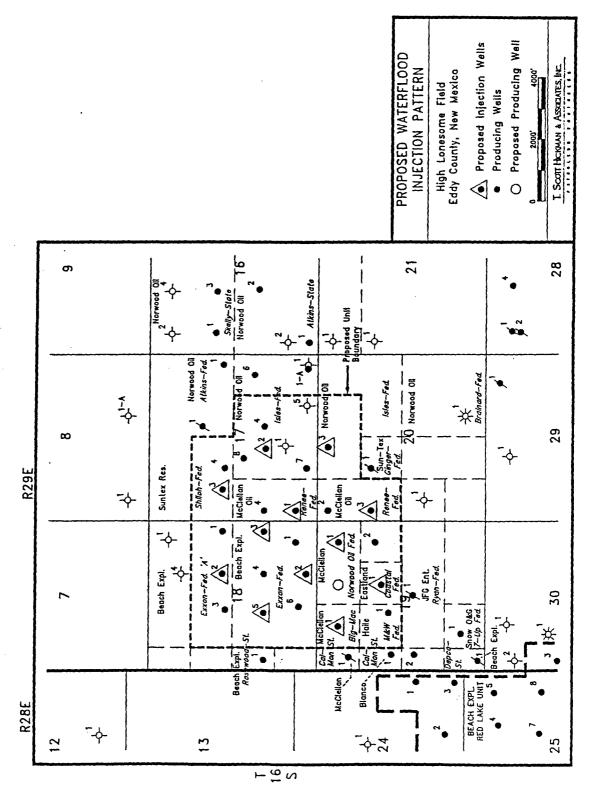


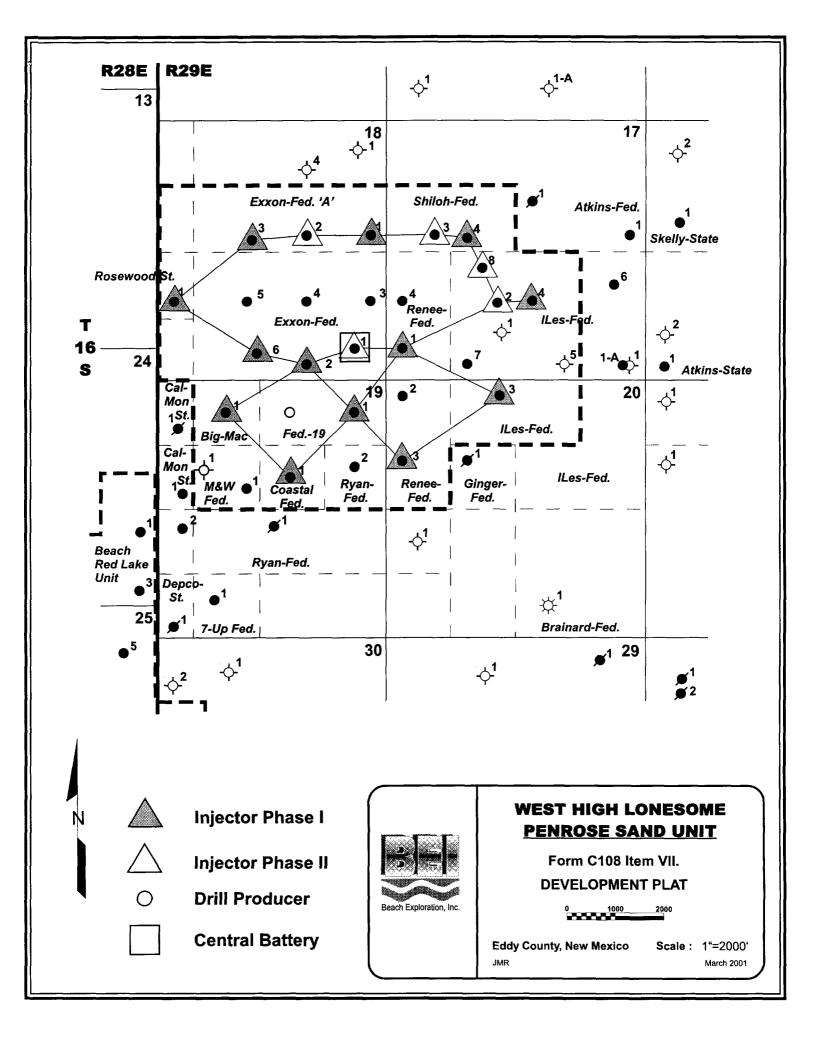






												POROSITY LOGS PENROSE SAND	High Lonesome Field Eddy County, New Mexico		Density/Neutron	○ Neutron	0 2000' 4000'	T. Scott Heiman & Associates, Inc.
	6			Norwood Oil	"•	Skelly-State Norwood Oll	~•	*- \				21				7		28
R29E	. 60		<u>*</u>	Suntex Res.	Shiloh-Fed. 1 Norwood	McClellan 7 Norwood			an O Norwood C		nee Sun-Tex Isles-Fed	(A) 20 Norwood Oil	- -	Brainard-Fed		<u></u>		29
			3	Beach Expl.	6	Expl. Beach Expl.		txxon-red.	Cal- McClellan	Col- Halle Eastland	Won St.	-	Depoco-	Srow Oses	Beach Expl.,	ф ₂	- 	30
R28E	12	-			13	Beach	7		McClellan	_	24	7	10	BEACH EXPL.	**		, 7 • B	25







InterChem, Inc

3803 Mankins

P. O. Box 13166

Odessa, Tx. 79768

Membrane Filter Evaluation

Monday, June 04, 2001

Pro Kem, Inc.

Oil Company Beach Exploration

Lease:

Double Eagle

Sample ID:

Fresh Water

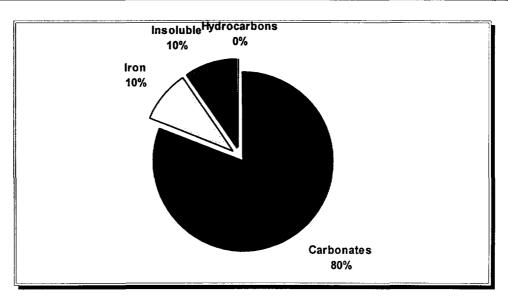
Location:

Test Date: 5/25/2001

Filter Size: 0.45 micron membrane filter

Volume/Time: 900 ccs in 4 minutes.

	mg/L.	Percent of Total
Hydrocarbons	0.00	0.00%
Carbonates	7.56	80.95%
Iron Oxide, Iron Sulfide, etc	0.89	9.52%
Acid Insolubles	0.89	9.52%
Total Suspended Solids	9.33	



Microscopic examination of the residues after leaching with 15% HCl revealed the presence of the following:

Small amounts of undissolved Iron Oxide, along with some sand.

Pro-Kem, Inc. WATER ANALYSIS REPORT

Oil Co. : Beach Exploration

Sample Loc. :

Lease : Double Eagle Well No.: Fresh Water

Date Analyzed: 5-June-2001 Date Sampled : 2-June-2001

Lab No. : F:\ANALYSES\jun0501.001

ANALYSIS

pH Specific Gravity 60/60 F. CaCO₃ Saturation Index @ 7.850 . 1.004 80 F. +0 140 F. +1

<u>D</u> :	issolved Gass	es		MG/L	EQ. WT.	*MEQ/L
4. 5. 6.	Hydrogen Sul Carbon Dioxi Dissolved Ox	fide de ygen		0 5 6.0		
Ca	ations					
7. 8. 9. 10.	Calcium Magnesium Sodium Barium	(Ca++) (Mg++) (Na+) (Ba++)	(Calculated)	39 36 168 Determined	/ 20.1 = / 12.2 = / 23.0 =	1.94 2.95 7.30
Aı	nions					
11. 12. 13. 14. 15.	Hydroxyl Carbonate Bicarbonate Sulfate Chloride	(OH-) (CO3=) (HCO3-) (SO4=) (C1-)		0 0 176 42 300	/ 17.0 = / 30.0 = / 61.1 = / 48.8 = / 35.5 =	0.00 0.00 2.88 0.86 8.45
16. 17. 18. 19.	Total Dissol Total Iron Total Hardne Resistivity	(Fe) ss As Ca	ıCO3	761 2 245 2.810 /cm.	/ 18.2 =	0.11

LOGARITHMIC WATER PATTERN *meq/L.

HCO3 S04 Mg 10000 1000 100 10 1 10 100 1000 10000

Calc:	ium	Su.	lfat	e S	oluk	<u>ili</u>	ty I	rof	ile
14 13 m 13 g 13 / 13 L 12	70 — 44 — 118 — 92 — 66 — 40 — 114 — 88 — 62 — 36 — 110 — 11								
	*F 5	a :	70 :	90	110	130	150	170	

PROBAB	LE M	INER	AL	COMPOS	ET?	ION	
COMPOUND	EQ.	WT.	X	*meq/L	=	mg/	/ L.

Ca (HCO ₃) ₂	81.04	1.94	157
CaSO ₄	68.07	0.00	0
CaCl ₂	55.50	0.00	0
$Mg(HCO_3)_2$	73.17	0.94	69
MgSO ₄	60.19	0.86	52
MgCL ₂	47.62	1.15	55
NaHCO3	84.00	0.00	0
NaSO4	71.03	0.00	0

*Milli Equivalents per Liter

7.30

58.46

This water is mildly corrosive due to the pH observed on analysis.

The corrosivity is increased by the content of mineral salts, and the presence of, CO2, Oxygen in solution.

NaCl



InterChem, Inc.

(915) 550-7027 P

P. O. Box 13166

Odessa, Tx. 79768

Water Quality Survey

20-April-2001

Pro-Kem, Inc. Beach Exploration - Big George SWD

Attached please find the printouts reflecting the results obtained from the survey conducted at the above water handling facilities on April 20, 2001. Following, for your perusal, is a detailed explanation of our findings, on a point-by-point basis.

Sample Locations

Listed below are the locations sampled for the purposes of this survey.

» Second Water Holding Tank

Water Analyses

Results indicate that the water handled by this system is moderately corrosive due to the content of dissolved mineral salts, reporting a TDS of 211,045 mg/L., in combination with the presence of H₂S and CO₂ in solution. In addition, the presence of small amounts of Oxygen will exacerbate the corrosion process on the tubular goods exposed to this water by the process of cathodic depolarization.

The Stiff and Davis Saturation Index predicts that this water should exhibit a moderate to severe Calcium Carbonate deposition tendency at 80° F., increasing in magnitude to a severe level at 140° F. A mild to moderate Calcium Sulfate scaling potential is expected from this water.

Dissolved Gasses

Listed below are the results obtained from the tests carried out on-site at the time of sampling. Results indicate minor amounts of CO₂ and H₂S in the produced water; however, we detected Oxygen in solution. Please review the following table.

Location	ppm.	ppm.	ppm.	
	O,	CO,	H,S	
Water Holding Tank	0.5	130	40	

Suspended Solids Test

Results of the 0.45 micron membrane filter tests carried out on-site at the time of sampling indicate that about 65% of the total suspended solids present in the injection water is composed of carbonates. The next highest figure is due to the hydrocarbons, which account for 19% of this water's suspended solids. The total

Water Quality Survey

Page 1

amount of suspended solids present is considered to be high, since it falls above the accepted lower limit of 50 mg/L. After leaching with 15% HCl, examination of the residues revealed small amounts of undissolved iron sulfide, along with what appears to be Calcium Sulfate. Please review the following table and graph outlining our results.

Location	mg/L.	mg/L.	mg/L.	mg/L.	mg/L.	
	Organic	Carbonates	Iron	Insolubles	Total	
Water Tank	37.00	129.50	29.00	2.50	198.00	

Suspended Oil Content

The TriChloro Ethane extraction carried out on the sample collected during this survey indicate that there were 2,518 ppm. of oil in suspension in the injection water at the time of collection.

Bacteria Counts

The results obtained from the bacteria culture bottles inoculated on-site at the time of sampling indicate moderate amounts of Sulfate-Reducing bacteria. Please review the following table.

	Col./ml.	Col./ml.
Location	Aerobic	SRB
Water Tank	Negative	10,000 <x<100,000< td=""></x<100,000<>

Observations and Recommendations

Based on the above observations, we feel that the system is operating above acceptable limits. The dissolved oxygen in these waters should be minimized by replacing the thiefhatch seals if necessary and installing a gas blanket with at least 2oz. of pressure on all water holding tanks. As you know, the presence of this gas in solution acts to further precipitate any solids still in solution, such as iron sulfide, as well as to increase the corrosive attack by hydrogen sulfide on any metal surfaces exposed to the injection water, by the mechanism of cathodic depolarization.

At the time of sampling, the bacteria tests indicate moderate amounts of sulfate-reducing bacteria present in suspension, such that we recommend that the producing wells be tested to determine those which may be candidates for cleaning and treatment with a bactericide.

Should there be an observed production drop in some of the producing wells, it may be that there is scale deposition downhole. Based on the results of the water analyses, as well as of the membrane filters, the majority of this scale should be Calcium Carbonate, with perhaps small amounts of Calcium Sulfate. Therefore, those producing wells which may have experienced a production drop may be acidized with 5% by volume of blend No. 1 to assist the acid in penetrating any hydrocarbon deposits downhole. These wells should also be considered candidates for squeezing with a scale inhibitor to extend the producing life of the well.

If we may further assist you in the interpretation of the above observations, please call at your convenience.

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Technical Services

Water Quality Survey

Page 2

Blend No. 1 Micellar Solvent for Acidizing

Product	Gals/55		
INC 901	55		

Pro-Kem, Inc. WATER ANALYSIS REPORT

File Name: c:\Waters\May1401.001

0.001 /cm.

SAMPLE

Oil Co.: **Beach Exploration** Date Sampled: 20-April-2001 Lease: Date Analyzed: Mack Energy 20-April-2001 Well No .: Big George SWD Lab ID Number: May1401.001-1

Location: Water Holding Tank Salesperson:

Attention:

ANALYSIS

1. 6.750 2. Specific Gravity 60/60 F. 1.148

3. CACO3 Saturation Index @ 80F 0.876 @140F 2.046

Dissolved Gasses		MG/L. EQ. WT. *MEQ/L
4.	Hydrogen Sulfide	40
5.	Carbon Dioxide	130
6.	Dissolved Oxygen	0.5

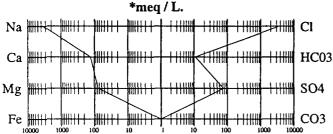
Cations

7.	Calcium	(Ca++)		2,467	/ 20.1 =	122.74
8.	Magnesium	(Mg++)		898	/ 12.2 =	73.61
9.	Sodium	(Na+)	(Calculated)	78,473	/ 23.0 =	3,411.87
10.	Barium	(Ba++)		Not Determined		,

£	<u>Anions</u>				
11.	Hydroxyl	(OH+)	0	/ 17.0 =	0.00
12.	Carbonate	(CO3=)	0	/ 30.0 =	0.00
13.	Bicarbonate	(HCO3-)	635	/ 61.1 =	10.39
14.	Sulfate	(SO4=)	3,600	/ 48.8 =	73.77
15.	Chloride	(Cl-)	124,972	/ 35.5 =	3,520.34
16.	Total Dissolved S	Solids	211,045		
17.	Total Iron	(Fe)	4	/ 18.2 =	0.22
18.	Total Hardness as	CaCO3	9.857		

19. Resistivity @ 75 F. (Calculated)

LOGARITHMIC WATER PATTERN



Calcium Sulfate Solubility Profile						
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4400		-				/
4390					- /	_
4380			_			
4370			_		\overline{A}	
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4350						
4340				-4		
4330	_		_			
4320		\rightarrow				
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PROBABLE MINERAL COMPOSITION

COMPOUND	EQ. WT.	X	*meq/L	=	mg/L.
Ca(HCO3)2	81.04		10.39		842
CaSO4	68.07		73.77		5,022
CaCl2	55.50		38.57		2,141
Mg(HCO3)2	73.17		0.00		0
MgSO4	60.19		0.00		0
MgC12	47.62		73.61		3,505
NaHCO3	84.00		0.00		0
NaSO4	71.03		0.00		0
NaCl	58.46		3,408.16		199,241



InterChem, Inc

3803 Mankins

P. O. Box 13166

Odessa, Tx. 79768

Suspended Oil Tests

Monday, May 14, 2001

Pro-Kem, Inc.

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	Oil Company, Beach Exploration Sample ID Collected Suspended Oil	
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Lease: Mack Energy

Big George SWD

Water Holding Tank

20-Apr-01

2518

José Luis Enriquez

Tech Services



InterChem, Inc

3803 Mankins

P. O. Box 13166

Odessa, Tx. 79768

Membrane Filter Evaluation

Monday, May 14, 2001

Pro Kem, Inc.

Oil Company Beach Exploration

Lease:

Mack Energy

Sample ID:

Big George SWD

Location:

Water Holding Tank

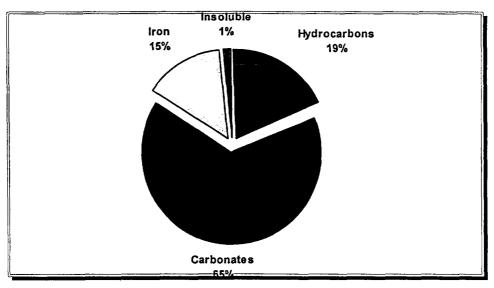
Test Date: 4/20/2001

Filter Size:

0.45 micron membrane filter

Volume/Time: 200 ccs in 5 minutes.

	mg/L.	Percent of Total
Hydrocarbons	37.00	18.69%
Carbonates Calcium Carbonate, etc.	129.50	65.40%
Iron Iron Oxide, Iron Sulfide, etc	29.00	14.65%
Acid Insolubles	2.50	1.26%
Total Suspended Solids	198.00	
And the second s		



Microscopic examination of the residues after leaching with 15% HCl revealed the presence of the following:

Small amounts of undissolved Iron Sulfide, along with

what appears to be Calcium Sulfate.

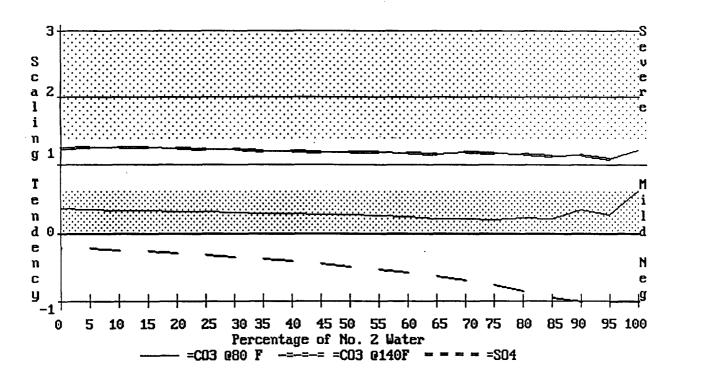
Comparison Between Two Waters

Pro-Kem, Inc.

Sample # 1
Beach Exploration
Exxon Federal
11-December-2000

Sample # 2
Beach Exploration
Double Eagle Fresh Water
11-December-2000

Percent of		TDS		Saturat	ion Index	Calcium Sulfate
#1 & #2	Hq	mg/L	SpGr	@80°F.	@140°F.	Scaling Potential
100 - 0	6.530	125966	1.093	+0.357	+1.247	Nil
95 - 5	6.590	119706	1.089	+0.346	+1.251	Nil
90 - 10	6.649	113446	1.084	+0.333	+1.258	Nil
85 - 15	6.709	107186	1.080	+0.328	+1.263	Nil
80 - 20	6.768	100926	1.075	+0.320	+1.240	Nil
75 - 25	6.828	94,666	1.071	+0.310	+1.230	Nil
70 - 30	6.887	88,406	1.066	+0.296	+1.226	Nil
65 - 35	6.947	82,146	1.062	+0.282	+1.200	Nil
60 - 40	7.006	75,886	1.057	+0.279	+1.199	Nil
55 - 45	7.066	69,626	1.053	+0.274	+1.184	Nil
50 - 50	7.125	63,367	1.048	+0.273	+1.183	Nil
45 - 55	7.185	57,107	1.044	+0.261	+1.186	Nil
40 - 60	7.244	50,847	1.039	+0.241	+1.171	Nil
35 - 65	7.304	44,587	1.035	+0.217	+1.157	Nil
30 - 70	7.363	38,327	1.030	+0.212	+1.182	Nil
25 - 75	7.423	32,067	1.026	+0.201	+1.171	Nil
20 - 80	7.482	25,807	1.021	+0.230	+1.160	Nil
15 - 85	7.542	19,547	1.017	+0.218	+1.128	Nil
10 - 90	7.601	13,287	1.012	+0.348	+1.138	Nil
5 - 95	7.661	7,027	1.008	+0.273	+1.083	Nil
0 - 100	7.720	767	1.003	+0.614	+1.214	Nil



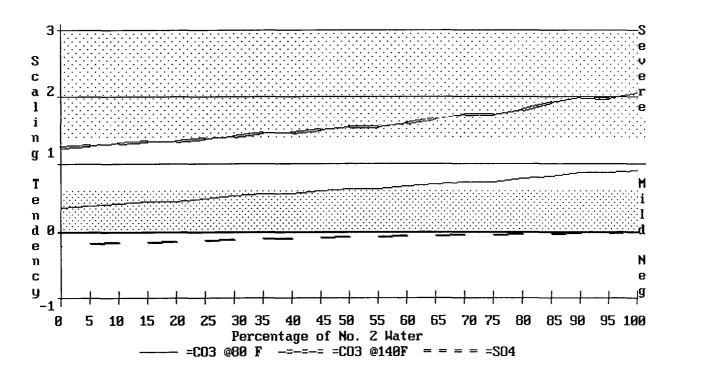
Comparison Between Two Waters

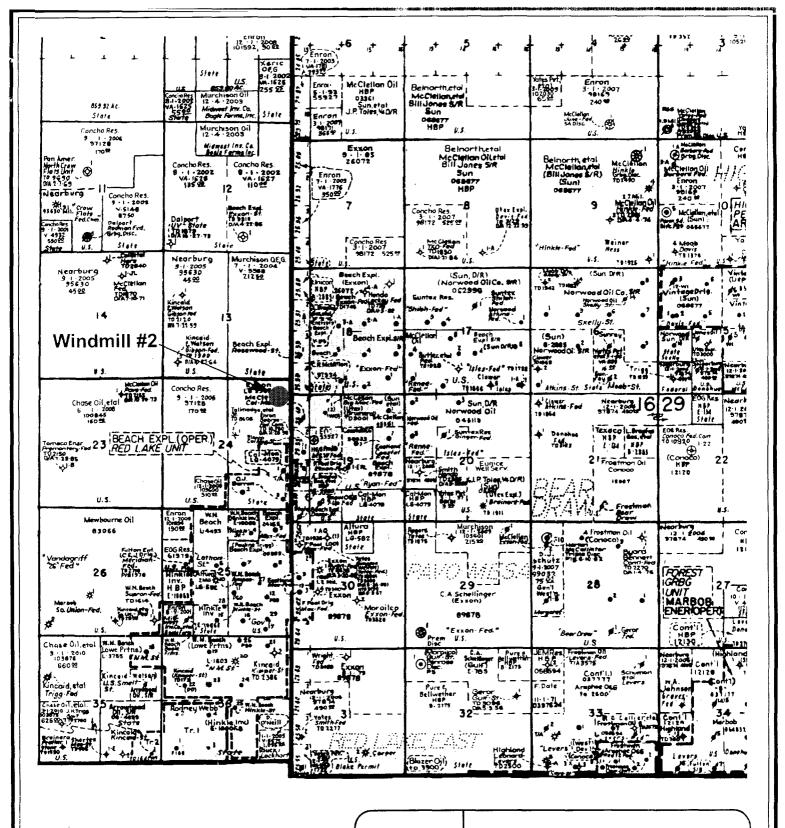
Pro-Kem, Inc.

Sample # 1
Beach Exploration
Exxon Federal Tank Battery
18-May-2001

Sample # 2 Mack Energy Big George SWD 18-May-2001 . 25:

Percent of	TDS			Saturation Index		Calcium Sulfate	
#1 & #2	рH	mg/L	SpGr	@80°F.	@140°F.	Scaling Potential	
100 - 0	6.530	125966	1.093	+0.357	+1.247	Nil	
95 - 5	6.541	130225	1.096	+0.389	+1.269	Nil	
90 - 10	6.552	134484	1.099	+0.411	+1.301	Nil	
85 - 15	6.563	138743	1.101	+0.443	+1.333	Nil	
80 - 20	6.574	143002	1.104	+0.444	+1.334	Nil	
75 - 25	6.585	147261	1.107	+0.486	<u>+1.366</u>	Nil	
70 - 30	6.596	151520	1.110	+0.527	+1.407	Nil	
65 - 35	6.607	155779	1.112	+0.558	+1.458	Nil	
60 - 40	6.618	160038	1.115	+0.558	+1.458	Nil	
55 - 45	6.629	164297	1.118	+0.598	+1.498	Nil	
50 - 50	6.640	168556	1.121	+0.628	+1.548	Nil	
45 55	6.651	172814	1.123	+0.628	+1.548	Nil_	
40 - 60	6.662	177073	1.126	+0.667	+1.607	Nil	
35 - 65	6.673	181332	1.129	+0.705	+1.665	Nil	
30 - 70	6.684	185591	1.132	+0.734	+1.724	Nil_	
25 - 75	6.695	189850	1.134	+0.732	+1.722	Nil	
20 - 80	6.706	194109	1.137	+0.779	+1.799	Nil	
<u> 15 -</u> 85	6.717	198368	1.140	+0.816	+1.916	Nil_	
10 - 90	6.728	202627	1.143	+0.872	+1.982	Nil	
5 - 95	6.739	206886	1.145	+0.868	+1.978	Nil	
0 - 100	6.750	211145	1.148	+0.893	+2.063	Nil	







WEST HIGH LONESOME PENROSE SAND UNIT

Form C-108 Item XI.

Fresh Water Wells Within 1 Mile of Injectors

0 2000 4000

Eddy County, New Mexico

Scale: 1'=4000'

Land Map 3:2001

N

Beach Exploration, INc.
Proposed West High Lonesome Penrose
Sand Unit
Fresh Water Well Analysis
Form C-108, Item XI

HALLIBURTON DIVISION LABOR ()RY

HALLIBURTON SERVICES ARTESIA DISTRICT

LABORATORY REPORT

No. W685, W686, & W687

TO Beach Explor	Beach Exploration			Date December 4, 1990				
P. O. Box 36	569			d 44.44				
Midland, TX	79701	The report is the property of Halifourion Services and neither 4 nor any pert shared; nor a copy thereof, is to be published or disclosed without first securing the express written approval of leboratory management, it may however, be used in the course of regular business operations by any person or concern and employees thereof receiving such report from Haliburton Services.						
Submitted by			_Date Rec	December 4, 1990				
Well No		_Depth	Fo:	rmation	_			
Field		_County	Son	urce				
	(CITY OF CARLSBAD) DOUBLE EAGLE WATER	(WATER) BOGLE	NELL # 1) MILL #1	(WATER WELL # 2) MILL #2	米			
Resistivity	12.55 @ 70°	3.41	@ 70°	12.55 @ 70°				
Specific Gravity	1.0011 @ 70°	1.002	@ 70°	1.0011 @ 70°	_			
рН Вq	8.1	7.6		7.7				
Calcium	1,571	1,675	•	1,152				
Magnesium	508	762		889	_			
Chlorides	300	1,000	· · · · · · · · · · · · · · · · · · ·	300				
Sulfates	Small	Heavy		Heavy	_			
Bicarbonates	214	214		214	_			
Soluble Iron	0	0		0				
			·	-	_			
					_			
					_			
Remarks:	•							
	$\subset \lambda$	0. 1.						
	Respect	fully submitte	ed .					

Analyst: Eric Jacobson - Field Engineer

HALLIBURTON SERVICES