

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special				Test Date: 4-9-85	
Company: Amoco Production Company			Connection:		
Pool: Bravo Dome Carbon Dioxide Unit - 640 acre area			Formation: Tubb		Unit: BDCDGU
Completion Date: 11-2-83		Total Depth: 2610		Plug Back TD: 2590	Elevation: 4990
Csg. Size: 7	Wt.: 20	d:	Set At: 2610	Perforations: From 2336 To 2470	
Tbg. Size: 3.5	Wt.: 9.3	d:	Set At: 2336	Perforations: From To	
Type Well - Single - Bradenhead - G.C. or G.O. Multiple: Single				Packer Set At: 2305	
Producing Thru: Tubing		Reservoir Temp. °F: 90° @ 2403		Mean Annual Temp. °F: 50	
Baro. Press. - P _a		County: Harding		State: New Mexico	
L: 2403	H: 2403	Gg: 1.529	% CO ₂ : 100	% N ₂ : 0	% H ₂ S: 0
Prover		Meter Run: 4.0		Taps: Flange	

FLOW DATA					TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							296		
1.	4.026 x 1.875			224	44	57	236.2	50	24 hr.
2.	4.026 x 1.875			252	20	58	254.2	50	24 hr.
3.	4.026 x 1.875			275	7	58	287.2	50	24 hr.
4.	4.026 x 1.875			290	1	58	302.2	50	24 hr.
5.									

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1.							1486
2.							1078
3.							662
4.							400
5.							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcl/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas 1.529 X X X X X X X X
3.					Specific Gravity Flowing Fluid X X X X X
4.					Critical Pressure 1072 P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature 547 R _____ R

P _c 308.2	P _c ² 94.987	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.42$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.63$
NO.	P _t ²	P _w	P _w ²
1		236.2	39.197
2		254.2	30.370
3		287.2	12.503
4		302.2	3.662
5			

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2418$

Absolute Open Flow 2418 Mcfd @ 15.025	Angle of Slope θ _____	Slope, n .55
Remarks: _____		
Approved By Commission:	Conducted By:	Calculated By: D. D. Kimble
		Checked By: