

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special				Test Date 6-9-85							
Company Amoco Production Company			Connection								
Pool Bravo Dome Carbon Dioxide Gas Unit 640 Acre Area			Formation Tubb		Unit BDCDGU						
Completion Date 4-29-81		Total Depth 2629'		Plug Back TD 2403'		Elevation 4520' GL	Farm or Lease Name				
Csq. Size 5-1/2"	Wt. 14#	d	Set At 2622	Perforations: From 2085' To 2180'		Well No. 1835 021J					
Tng. Size 2-3/8"	Wt. 4.7#	d	Set At 1924'	Perforations: From To		Unit J	Sec. Twp. Rge. 2 18 35				
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 1894'		County Union					
Producing Thru Tubing		Reservoir Temp. °F @ 2172'		Mean Annual Temp. °F 50		Baro. Press. - P _a 12.2	State New Mexico				
L 2172'	H 2172'	G _g 1.529	% CO ₂ 100	% N ₂ 0	% H ₂ S 0	Prover	Meter Run 4.0# Taps Flange				
FLOW DATA				TUBING DATA		CASING DATA		Duration of Flow			
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. °F	Press. p.s.i.g.		Temp. °F	Press. p.s.i.g.	Temp. °F
SI							337				
1.	4.026 x 2.375			276	18	61	288.2	50			24 hr.
2.	4.026 x 2.375			288	13	61	300.2	"			24 hr.
3.	4.026 x 2.375			310	5	60	322.2	"			24 hr.
4.	4.026 x 2.375			328	2	54	340.2	"			24 hr.
5.											
RATE OF FLOW CALCULATIONS											
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd				
1.							1734				
2.							1493				
3.							985				
4.											
5.											
NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ 0 _____ Mcf/bbl.						
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ 0 _____ Deg.						
2.					Specific Gravity Separator Gas _____ 1.529 _____ X X X X X X X X X X						
3.					Specific Gravity Flowing Fluid _____ X X X X X _____						
4.					Critical Pressure _____ 1072 _____ P.S.I.A. _____ P.S.I.A.						
5.					Critical Temperature _____ 547 _____ R _____ R						
P _c 349.2 P _c ² 121.940											
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 3.136$		(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.33$				
1		288.2		38.831							
2		300.2		31.821							
3		322.2		18.128							
4		340.2		6.205							
5											
Absolute Open Flow 4040					Mcf/d @ 15.025			Angle of Slope θ		Slope, n .74	
Remarks:											
Approved by Commission:			Conducted By:			Calculated By: D. D. Kimble			Checked By:		

1835 0215

46 7200

K_Σ LOGARITHMIC 2 x 2 CYCLES
KEUFFEL & ESSER CO. MADE IN U.S.A.

ADP = 40%

22 0 2

Q = MCF

