

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

| | | | |
|--|---|---|---|
| Type Test: <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special | | Test Date 4-23-85 | |
| Company Amoco Production Company | | Connection | |
| Pool Bravo Dome Carbon Dioxide Unit - 640 acre area | | Formation: Tubb | Unit BDCDGU |
| Completion Date 12-31-80 | Total Depth 2650 | Plug Back TD 2597 | Elevation 4915 |
| Farm or Lease Name | Csg. Size 5.5 | Wt. 14 | Set At 2650 |
| Perforations: From 2298 To 2552 | Well No. 1934 061G | Tbg. Size 2-7/8 | Wt. 6.5 |
| Set At 2104 | Perforations: From To | Unit G | Sec. 06 |
| Twp. 19 | Rge. 34 | County Union | State New Mexico |
| Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single | | Packer Set At 2118 | County Union |
| Producing Thru Tubing | Reservoir Temp. *F 90°@ 2425 | Mean Annual Temp. *F 50 | Baro. Press. - P _a 12.2 |
| L 2425 | H 2425 | G _g 1.529 | % CO ₂ 100 |
| % N ₂ 0 | % H ₂ S 0 | Prover | Meter Run 4.0 |
| Taps Flange | FLOW DATA | TUBING DATA | CASING DATA |
| NO. | Prover Line Size | X | Orifice Size |
| SI | Press. p.s.i.g. | Diff. h _w | Temp. *F |
| 1. | 4.026 x 2.125 | 209 | 32 |
| 2. | 4.026 x 2.125 | 242 | 13 |
| 3. | 4.026 x 2.125 | 265 | 5 |
| 4. | 4.026 x 2.125 | 293 | 1 |
| 5. | | | |
| Press. p.s.i.g. | Temp. *F | Press. p.s.i.g. | Temp. *F |
| 310 | 59 | 221.2 | 50 |
| 24 hr. | 24 hr. | 24 hr. | 24 hr. |
| 24 hr. | 24 hr. | 24 hr. | 24 hr. |
| 24 hr. | 24 hr. | 24 hr. | 24 hr. |
| 24 hr. | 24 hr. | 24 hr. | 24 hr. |
| RATE OF FLOW CALCULATIONS | NO. | Coefficient (24 Hour) | $\sqrt{h_w P_m}$ |
| Pressure P _m | Flow Temp. Factor Ft. | Gravity Factor F _g | Super Compress. Factor, F _{pv} |
| Rate of Flow Q, Mcfd | 1 | 2 | 3 |
| 1567 | 2 | 3 | 4 |
| 1105 | 4 | 5 | |
| 720 | | | |
| NO. | P _f | Temp. *R | T _f |
| Z | Gas Liquid Hydrocarbon Ratio | A.P.I. Gravity of Liquid Hydrocarbons | Specific Gravity Separator Gas |
| 1 | 0 | 0 | 1.529 |
| 2 | Mcf/bbl. | Deg. | X X X X X X X X |
| 3 | Specific Gravity Flowing Fluid | Critical Pressure | Critical Temperature |
| 4 | X X X X X | 1072 | 547 |
| 5 | P.S.I.A. | P.S.I.A. | R |
| P _c 322.2 | P _c ² 103.813 | | |
| NO. | P _f ² | P _w | P _w ² |
| 1 | 221.2 | 54.883 | |
| 2 | 235.2 | 48.494 | |
| 3 | 277.2 | 26.973 | |
| 4 | 305.2 | 10.666 | |
| 5 | | | |
| (1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.89$ | (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.89$ | AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2964$ | |
| Absolute Open Flow | 2964 | Mcf/d @ 15.025 | Angle of Slope θ |
| Slope, n | 1.00 | Remarks: | |
| Approved By Commission: | Conducted By: | Calculated By: D. D. Kimble | Checked By: |