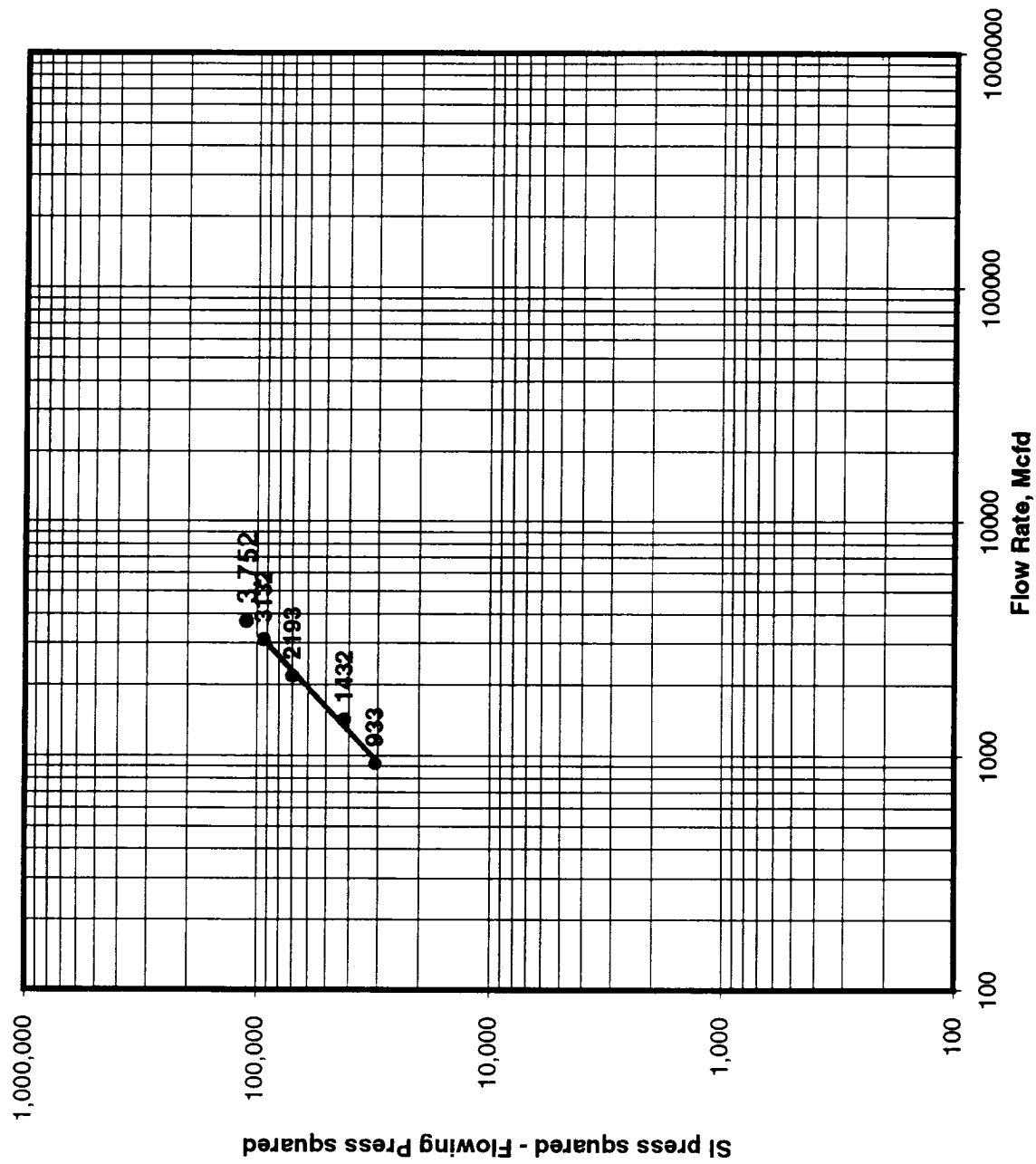


NEW MEXICO OIL CONSERVATION COMMISSION Form C-122
 MULTIPPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL Revised 9-1-63

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special				Test Date 8/29/95		API Number 30-059-20317				
Company Amoco Corporation				Connection Bravo Dome CO2 Plant		RTU Number 5070				
Pool N/A				Formation Tubb		Unit BDCDGU				
Completion Date 8/16/95		Total Depth 2206		Plug Back Depth 2196		Elevation 4665 GL				
Csg. Size 5.5	Wt. 15.5, 5.9	Csg. Inside Dia 4.75 FG	Set At 2206	Perforations From 2096 To 2195		Well Number 2135-071-K				
Tbg. Size n/a	Wt. n/a	Tbg. Inside Dia n/a	Set At n/a	Perforations From n/a To n/a		Unit Sec. Twp. Rge. sec 07, T-21, R-35				
Type well - Single-Bradenhead-G.G. or G.O. Multiple Single				Packer Set At n/a		County Union				
Producing Through Casing		Reservoir Temp. F 95		Mean Annual Temp. F 60		Baro. Press. - PSIA 12.2				
Flow Channel L 2196	Depth, H 2196	Gg 1.5192	%CO2 100	%N2 0	%H2S 0	Prover ORIFICE	Meter Run 4 inch			
						Taps FLANGE				
FLOW DATA				TUBING DATA		CASING DATA				
NO.	Prover Size	X	Stat. Press psig	Diff. Press. Hw	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI						320				24 hour
1.						270				60 MIN
2.						250				60 MIN
3.						190				60 MIN
4.						120				60 MIN
5.						0				
RATE OF FLOW CALCULATIONS										
NO.	Coefficient (24 Hours)		Pressure Pm	Flow Temp. Factor, Ft	Gravity Factor, Fg	Super Compressibility Factor, Fpv		Rate of Flow Q, Mcfd		
		$\frac{1}{hw \cdot Pm}$						Values	Log(10)	
SI								0		
1.								933	2.9699	
2.								1432	3.1559	
3.								2193	3.3410	
4.								3132	3.4958	
5.								3752	AOF	
NO.	Pr	Temp. °R	Tr	Z	Gas Liquid Hydrocarbon Ratio A. P. I. Gravity of Liquid Hydrocarbon		N/A Mcf/bbl N/A Deg.			
1.					Specific Gravity Separator Gas		N/A			
2.					Specific Gravity Flowing Fluid		1.5192			
3.					Critical Pressure		1072 P.S.I.A.			
4.					Critical Temperature		548 R			
5.										
Pc = 332.2		Pc^2 = 110,357				(1) 4th test point	(2) 4th test point			
NO.	Pw^2	Pw	Pw^2	Pc^2 - Pw^2	Pc^2 - Pw^2	$\frac{Pc^2}{Pc^2 - Pw^2}$	$\frac{Pc^2}{Pc^2 - Pw^2} \cdot n$	$\frac{Pc^2}{Pc^2 - Pw^2} \cdot n$	$\frac{Pc^2}{Pc^2 - Pw^2} \cdot n$	
SI		332.2	110,357	0	0	1.188			1.198	
1.		282.2	79,637	30,720	4.4874					
2.		262.2	68,749	41,608	4.6192					
3.		202.2	40,885	69,472	4.8418					
4.		132.2	17,477	92,880	4.9679					
5.										
Absolute Open Flow 3,752 Mcfd @ 15.025				Angle of Slope 43.65		Slope, n = 1.048 (Cotangent)				
Remarks: <u> </u> fiberglass casing to top of tubb. Steel casing set through tubb and perted.										
Approved By Commission:			Conducted By: Bill Prichard			Calculated By: Automation Software			Checked By: Gary Ford, Bill Prichard	

Handwritten signature/initials

GAS WELL BACK PRESSURE TEST - ABSOLUTE OPEN FLOW



GAS WELL BACK PRESSURE TEST INFLOW PERFORMANCE

