

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 10-1-85			
Company Amoco Production Company				Connection					
Pool Bravo Dome Carbon Dioxide Gas Unit 640 Acre Area				Formation Tubb				Unit BDCDGU	
Completion Date 5-14-81		Total Depth 2505		Plug Back TD 2392		Elevation 4540		Farm or Lease Name	
Csg. Size 5-1/2	Wt. 14	d 	Set At 2498	Perforations: From 2036 To 2210		Well No. 1935 331 F			
Tbg. Size 2-7/8	Wt. 6.5	d 	Set At 1902	Perforations: From To		Unit Sec. Twp. Rge. F 33 19 35			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single						Packer Set At 1871		County Union	
Producing Thru Tubing		Reservoir Temp. °F 90 @ 2123		Mean Annual Temp. °F 50		Baro. Press. - P _a 12.2		State New Mexico	
L 2132	H 2132	Gg 1.529	% CO ₂ 100	% N ₂ 0	% H ₂ S 0	Prover	Meter Run 4.0	Taps Flange	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
SI							328			
1.	4.026 x 2.125			220	38	55	220	50		
2.	" "			241	25	55	241	"		
3.	" "			255	15	53	255	"		
4.	" "			277	7	52	277	"		
5.										

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1.							1808
2.							1588
3.							1100
4.							978
5.							

NO.	R _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c 340.2	P _c ² 115,736	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.87$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.80$	
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²
1.		232.2		61.819
2.		253.2		51.626
3.		267.2		46.987
4.		289.2		32.099
5.				

$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3260$

Absolute Open Flow	3260	Mcf/d @ 15.025	Angle of Slope @	Slope, n, .94
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Remarks:

Approved By Commission:	Conducted By:	Calculated By: D. D. Kimble	Checked By:
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