

**NEW MEXICO OIL CONSERVATION COMMISSION  
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL**

Form C-122  
Revised 9-1-65

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special			Test Date 9-2-93		20-059-2012S	
Company AMOCO PRODUCTION COMPANY			Connection			
Pool BRAVO DOME CARBON DIOXIDE GAS UNIT			Formation TUBB		Unit BDCDGL	
Completion Date 7/7/93		Total Depth 3455		Plug Back TD 2460-	Elevation 4885	Farm or Lease Name
Csg. Size 4 1/2" FG	Wt. 4.49	d 3.95	Set At 3463	Perforations: From 2420 To 2450		Well No. 2233-261 F
Tub. Size -	Wt. -	d -	Set At -	Perforations: From To		Unit Sec. Twp. Rge. F 26 22N 33E

Type Well - Single - Bradenhead - G.C. or G.O. Multiple SINGLE				Packer Set At -		County UNION	
Producing Thru CASING		Reservoir Temp. °F 95 @ 2420'		Mean Annual Temp. °F 50		Baro. Press. - P <sub>a</sub> 12.2	
L -	H 3463	G <sub>g</sub> 1.529	% CO <sub>2</sub> 100	% N <sub>2</sub> 0	% H <sub>2</sub> S 0	Prover	Meter Run 4.0
							Taps FLANGE

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. In. H <sub>2</sub> O	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
51				320							
1.	4.026	x	0.25	225					225		1.5 HRS
2.	4.026	x	0.375	210					210		.6 HRS
3.	4.026	x	0.500	190					190		.5 HRS
4.	4.026	x	0.875	95					95		.5 HRS
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P <sub>m</sub>	Flow Temp. Factor Ft.	Gravity Factor F <sub>g</sub>	Super Compress. Factor, F <sub>pv</sub>	Rate of Flow Q, Mcfd
1							221
2							479
3							804
4							1388
5							

NO.	R <sub>w</sub>	Temp. °R	T <sub>w</sub>	Z	Gas Liquid Hydrocarbon Ratio <u>DRY</u> Mcf/bbl.
1					A.P.I. Gravity of Liquid Hydrocarbons <u>DRY</u> Deg.
2					Specific Gravity Separator Gas <u>1.529</u> XXXXXXXXXX
3					Specific Gravity Flowing Fluid <u>XXXXX</u>
4					Critical Pressure <u>1072</u> P.S.I.A. P.S.I.A.
5					Critical Temperature <u>547</u> R R

P <sub>c</sub> <u>332.2 P<sub>c</sub><sup>2</sup> 110.356</u>				(1) $\frac{P_c^2}{P_c^2 - R_w^2} = 2.043$		(2) $\left[ \frac{P_c^2}{P_c^2 - R_w^2} \right]^n = 1.610$	
NO	P <sub>w</sub>	R <sub>w</sub> <sup>2</sup>	P <sub>c</sub> <sup>2</sup> - R <sub>w</sub> <sup>2</sup>	AOF = 0 $\left[ \frac{P_c^2}{P_c^2 - R_w^2} \right]^n = 1.61$			
1	237.2	56.264	54.092				
2	222.2	49.373	60.983				
3	202.2	40.885	69.471				
4	107.2	11.492	98.864				
5							

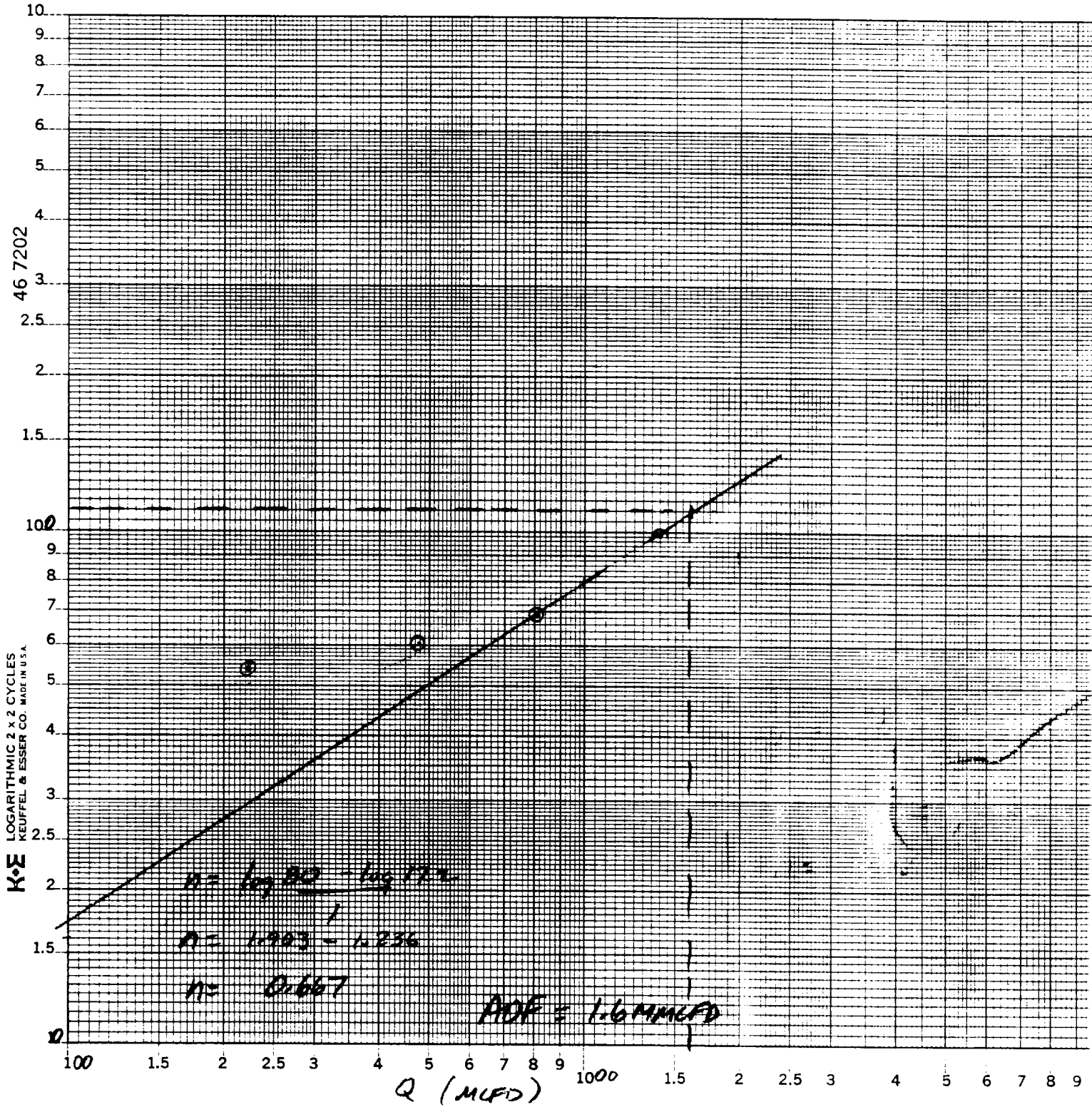
Absolute Open Flow <u>1.6 MMCFD</u>	Mcfd @ 15.025	Angle of Slope @	Slope, n <u>0.667</u>
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Remarks: WELL MAKING WATER

Approved by Commission:	Connected By:	Calculated By:	Checked By:
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2233-261F

$P_e^2 - P_w^2$



NOTE: WELL LOADING UP AT LOWER RATES WITH WATER.