

NEW MEXICO OIL CONSERVATION COMMISSION  
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122  
Revised 9-1-65

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special				Test Date 4-29-85							
Company Amoco Production Company			Connection								
Pool Bravo Dome <b>Carbon Dioxide Gas Unit, 640 Acre Area</b>			Formation Tubb		Unit BDCDGU						
Completion Date 9/25/84		Total Depth 2814	Plug Back TD 2711	Elevation 4930	GL						
Csg. Size 7	Wt. 20	Set At 2814	Perforations: From 2327 To 2532		Well No. 1934 291G						
Thq. Size 3-1/2	Wt. 9.3	Set At 2203	Perforations: From                      To		Unit    Soc.    Twp.    Rge. G       29     19     34						
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single			Packer Set At 2172		County Union						
Producing Thru Tubing		Reservoir Temp. °F 90 @ 2430	Mean Annual Temp. °F 50	Baro. Press. - P <sub>a</sub> 12.2							
L 2430	H 2430	G <sub>g</sub> 1.529	% CO <sub>2</sub> 100	% N <sub>2</sub> 0	% H <sub>2</sub> S 0						
Prover				Meter Run 4.0	Taps Flange						
FLOW DATA											
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
1.	4.026 x 1.375			209	31	54	221.2	50			
2.	4.026 x 1.375			226	20	54	238.2	50			24 hr
3.	4.026 x 1.375			274	5	53	286.2	50			24 hr
4.	4.026 x 1.375			303	1	50	315.2	50			24 hr
5.											
RATE OF FLOW CALCULATIONS											
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P <sub>m</sub>	Flow Temp. Factor Ft.	Gravity Factor F <sub>g</sub>	Super Compress. Factor, F <sub>pv</sub>	Rate of Flow				
1.							Q, Mcid				
2.							592				
3.							528				
4.							312				
5.							163				
NO.	P <sub>t</sub>	Temp. °R	T <sub>r</sub>	Z	Gas Liquid Hydrocarbon Ratio _____ 0 _____ Mcf/bbl.						
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ 0 _____ Deg.						
2.					Specific Gravity Separator Gas _____ 1.529 _____ X X X X X X X X X						
3.					Specific Gravity Flowing Fluid _____ X X X X X _____						
4.					Critical Pressure _____ 1072 _____ P.S.I.A. _____ P.S.I.A.						
5.					Critical Temperature _____ 547 _____ R _____ R						
P <sub>c</sub> 326.2    P <sub>c</sub> <sup>2</sup> 106.4											
NO.	P <sub>t</sub> <sup>2</sup>	P <sub>w</sub>	P <sub>w</sub> <sup>2</sup>	P <sub>c</sub> <sup>2</sup> - P <sub>w</sub> <sup>2</sup>	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.851$ (2) $\left[ \frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.456$						
1.		221.2		57.477	AOF = Q $\left[ \frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 862$						
2.		238.2		49.667							
3.		286.2		24.496							
4.		315.2		7.055							
5.											
Absolute Open Flow _____ 862 _____ Mcid @ 15.025					Angle of Slope $\theta$ _____		Slope, n _____ .61 _____				
Remarks: _____											
Approved By Commission:			Conducted By:			Calculated By: D. D. Kimble			Checked By:		