UNITED STATES DEPARTMENT OF THE INTERIOR FORM APPROVED OMB NO. 1004-0137 Expires: January 31, 2018

D.	UREAU OF LAND MANAGEN	MENT	Expires.	January 31, 2016
	NOTICES AND REPORTS		5. Lease Serial No. NMLC065750/	Ą
Do not use th	is form for proposals to dril II. Use form 3160-3 (APD) f	ll or to re-enter an	6. If Indian, Allottee	or Tribe Name
SUBMIT IN	TRIPLICATE - Other instruc	tions on page 2	7. If Unit or CA/Agr 891000326X	reement, Name and/or No.
1. Type of Well			8. Well Name and No	o. TDI BB JABBA 104H
Oil Well ☐ Gas Well ☐ Oth 2. Name of Operator		LY KARDOS	9. API Well No.	——————————————————————————————————————
XTO PERMIAN OPERATING			30-025-47270-	-00-X1
3a. Address 6401 HOLIDAY HILL ROAD, MIDLAND, TX 79707		. Phone No. (include area code) n: 432-620-4374	10. Field and Pool of BONE SPRING	r Exploratory Area 3S
4. Location of Well (Footage, Sec., T	., R., M., or Survey Description)		11. County or Parish	, State
Sec 22 T20S R32E SWSW 27 32.552200 N Lat, 103.760582			LEA COUNTY	, NM
12. CHECK THE AI	PPROPRIATE BOX(ES) TO	INDICATE NATURE OF	F NOTICE, REPORT, OR OT	HER DATA
TYPE OF SUBMISSION		TYPE OF	ACTION	
— N. C.	☐ Acidize	☐ Deepen	☐ Production (Start/Resume)	☐ Water Shut-Off
☑ Notice of Intent	☐ Alter Casing	☐ Hydraulic Fracturing	□ Reclamation	■ Well Integrity
☐ Subsequent Report	☐ Casing Repair	☐ New Construction	☐ Recomplete	Other
☐ Final Abandonment Notice	☐ Change Plans	☐ Plug and Abandon	□ Temporarily Abandon	Change to Original A PD
	☐ Convert to Injection	☐ Plug Back	■ Water Disposal	15
If the proposal is to deepen directions Attach the Bond under which the wo following completion of the involved testing has been completed. Final Aldetermined that the site is ready for f XTO Permian Operating, LLC ***Sundry submitted on 06/16 915FWL *NO SURFACE DISTED Casing/Cement design per the XTO also requests the following Approval to utilize a spudder roperations.	rk will be performed or provide the Id operations. If the operation results bandonment Notices must be filed or inal inspection. The requests permission to make 1/20 (WIS: 519057) to change TURBANCE* Turn attached drilling program. The requests permission to make 1/20 (WIS: 519057) to change 1/20 (WIS:	Bond No. on file with BLM/BIA. in a multiple completion or recordly after all requirements, including the following changes to the SHL from 270FSL & 6	Required subsequent reports must be impletion in a new interval, a Form 31 ng reclamation, have been completed the original APD: 40FWL to 270FSL &	be filed within 30 days 160-4 must be filed once
Con	Electronic Submission #5223 For XTO PERMIAN nmitted to AFMSS for procession	l OPERAT <mark>I</mark> NG LLC, sent to ng by PRI <mark>SCILLA PEREZ</mark> on	the Hobbs 07/20/2020 (20PP3078SE)	
Name(Printed/Typed) KELLY KA	ARDOS	Title REGULA	ATORY COORDINATOR	
Signature (Electronic S	Submission)	Date 07/20/20	020	
	THIS SPACE FOR I	FEDERAL OR STATE (OFFICE USE	
_Approved_By_CQDY_LAYTON			T FIELD MANAGER	Date 08/11/2020
Conditions of approval, if any, are attache certify that the applicant holds legal or equ which would entitle the applicant to condu	uitable title to those rights in the sub			

Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

Additional data for EC transaction #522376 that would not fit on the form

32. Additional remarks, continued

Batch drill this well if necessary. In doing so, XTO will set each casing string and ensure that the well is cemented properly and the well is static. With floats holding, no pressure on the csg annulus, and the installation of a 10K TA cap as per GE recommendations, XTO will contact the BLM to skid the rig to drill the remaining wells on the pad. Once surface and intermediate strings are all completed, XTO will begin drilling the production hole on each of the wells.

ONLY test broken pressure seals on the BOP equipment per the attached procedure.

A variance is requested to cement offline for the surface and intermediate casing strings.

Attachments:
Drilling Program
Direction Drill Plan
Spudder Rig Description of Operations
BOP Break Test Procedure
Offline Cement Variance
SHL Submitted Sundry (WIS: 519057)

Revisions to Operator-Submitted EC Data for Sundry Notice #522376

Operator Submitted

APDCH APDCH Sundry Type: NOI NOI

NMNM33955 Lease: NMLC065750A

Agreement: 891000326X (NMNM68294X)

XTO PERMIAN OPERATING LLC 6401 HOLIDAY HILL ROAD, BLDG 5 MIDLAND, TX 79707 Ph: 4326828873 Operator: XTO PERMIAN OPERATING, LLC

6401 HOLIDAY HILL RD BLDG 5 MIDLAND, TX 79707 Ph: 432-620-4374

KELLY KARDOS Admin Contact:

KELLY KARDOS REGULATORY COORDINATOR REGULATORY COORDINATOR E-Mail: kelly_kardos@xtoenergy.com E-Mail: kelly_kardos@xtoenergy.com

Ph: 432-620-4374 Ph: 432-620-4374

Tech Contact:

KELLY KARDOS REGULATORY COORDINATOR KELLY KARDOS REGULATORY COORDINATOR E-Mail: kelly_kardos@xtoenergy.com E-Mail: kelly_kardos@xtoenergy.com

Ph: 432-620-4374 Ph: 432-620-4374

Location:

State: NMNM County: LEA LEA

Field/Pool: SALT LAKE BONE SPRING **BONE SPRINGS**

BIG EDDY UNIT DI BB JABBA 104H BIG EDDY UNIT DI BB JABBA 104H Well/Facility:

Sec 22 T20S R32E SWSW 270FSL 915FWL Sec 22 T20S R32E Mer NMP SWSW 270FSL 915FWL

32.552200 N Lat, 103.760582 W Lon

BLM Revised (AFMSS)

Big Eddy Unit DI BB 104H

Projected TD: 26779' MD / 9812' TVD
SHL: 270' FSL & 915' FWL , Section 22, T20S, R32E
BHL: 1980' FSL & 50' FWL , Section 30, T20S, R32E
Lea County, NM

Casing Design

The surface fresh water sands will be protected by setting 18-5/8 inch casing @ 1080' (147' above the salt) and circulating cement back to surface. The salt will be isolated by setting 13-3/8 inch casing at 2620' and circulating cement to surface. The Capitan Reef zone will be isolated by setting 9-5/8 inch casing at 4820'. An 8-3/4 inch curve and 8-1/2 inch lateral hole will be drilled to MD/TD and 5-1/2 inch casing will be set at TD and cemented back up to the 13-3/8 inch casing shoe depth.

men racera.	men lateral note will be armed to mby 15 and 5 1/2 men casing will be set at 15 and centented back up to the 15 3/5 men casing since depart									
Hole :	Size	Depth	OD Csg	Weight	Collar	Grade	New/Used	SF Burst	SF Collapse	SF Tension
24	"	0' – 1080'	18-5/8"	87.5#	STC	H-40	New	2.00	1.27	5.92
17-1,	/2"	0' - 2620'	13-3/8"	54.5#	STC	J-55	New	2.44	1.37	3.60
12-1,	/4"	0' - 4820'	9-5/8"	36#	LTC	J-55	New	1.36	1.77	2.61
8-3/4" x	8-1/2"	0' – 26779'	5-1/2"	17#	BTC	P-110	New	1.12	1.58	1.94

XTO requests to not utilize centralizers in the curve and lateral

13-3/8 & 9-5/8" Collapse analyzed using 50% evacuation based on regional experience.

5-1/2" tension calculated using vertical hanging weight plus the lateral weight multiplied by a friction factor of 0.35.

WELLHEAD:

Temporary Wellhead

· 18-5/8" SOW bottom x 21-1/4" 2M top flange.

Permanent Wellhead – GE RSH Multibowl System

- A. Starting Head: 13-5/8" 5M top flange x 13-3/8" SOW bottom
- B. Tubing Head: 13-5/8" 5M bottom flange x 7-1/16" 10M top flange
 - $\cdot \ \mbox{Wellhead will be installed by manufacturer's representatives}.$
 - $\cdot \ \ \text{Manufacturer will monitor welding process to ensure appropriate temperature of seal.}$
 - $\cdot\,$ Operator will test the 9-5/8" casing per Onshore Order 2.
 - \cdot Wellhead manufacturer representative may not be present for BOP test plug installation

Cement Program

Surface Casing:

Lead: 1040 sxs EconoCem-HLTRRC (mixed at 12.9 ppg, 1.87 ft3/sx, 10.13 gal/sx water)
Tail: 550 sxs Halcem-C + 2% CaCl (mixed at 14.8 ppg, 1.35 ft3/sx, 6.39 gal/sx water)
Compressives: 12-hr = 900 psi 24 hr = 1500 psi

1st Intermediate Casing:

 Lead: 1510 sxs EconoCem-HLTRRC (mixed at 12.9 ppg, 1.87 ft3/sx, 10.13 gal/sx water)

 Tail: 590 sxs Halcem-C + 2% CaCl (mixed at 14.8 ppg, 1.35 ft3/sx, 6.39 gal/sx water)

 Compressives:
 12-hr =
 900 psi
 24 hr = 1500 psi

2nd Intermediate Casing:

ECP/DV Tool to be set at 3150'

1st Stage

Lead: 220 sxs Halcem-C + 2% CaCl (mixed at 12.9 ppg, 1.88 ft3/sx, 9.61 gal/sx water)
Tail: 470 sxs Halcem-C + 2% CaCl (mixed at 14.8 ppg, 1.33 ft3/sx, 6.39 gal/sx water)
Compressives: 12-hr = 900 psi 24 hr = 1500 psi

2nd Stage

Lead: 170 sxs Halcem-C + 2% CaCl (mixed at 12.9 ppg, 1.88 ft3/sx, 9.61 gal/sx water)
Tail: 230 sxs Halcem-C + 2% CaCl (mixed at 14.8 ppg, 1.33 ft3/sx, 6.39 gal/sx water)
Compressives: 12-hr = 900 psi 24 hr = 1500 psi

Production Casing:

Lead: 880 sxs NeoCem (mixed at 10.5 ppg, 2.69 ft3/sx, 12.26 gal/sx water)

Tail: 3180 sxs VersaCem (mixed at 13.2 ppg, 1.61 ft3/sx, 8.38 gal/sx water)

Compressives: 12-hr = 1375 psi 24 hr = 2285 psi

Mud Circulation Program

INTERVAL	Hole Size	Mud Type	MW (ppg)	Viscosity (sec/qt)	Fluid Loss (cc)
0' - 1080'	24"	FW/Native	8.3 - 9.5	35-40	NC
1080' - 2620'	17-1/2"	Brine	9.8-10.2	30-35	NC
2620' to 4820'	12-1/4"	FW / Cut Brine	8.3-9.0	30-32	NC
4820' to 26779'	8-3/4" x 8-1/2"	FW / Cut Brine / Polymer	9 - 9.3	29-32	NC - 20

DRILLING PLAN: BLM COMPLIANCE (Supplement to BLM 3160-3)

XTO Energy Inc. BEU BB Jabba 104H

Projected TD: 26779' MD / 9812' TVD

SHL: 270' FSL & 915' FWL , Section 22, T20S, R32E BHL: 1980' FSL & 50' FWL , Section 30, T20S, R32E Lea County, NM

1. Geologic Name of Surface Formation

A. Quaternary

2. Estimated Tops of Geological Markers & Depths of Anticipated Fresh Water, Oil or Gas:

Formation	Well Depth (TVD)	Water/Oil/Gas
Rustler	952'	Water
Top of Salt	1227'	Water
Base of Salt	2572'	Water
Capitan	3225'	Water
Delaware	4719'	Water
Bone Spring	7722'	Water/Oil/Gas
1st Bone Spring Ss	8802'	Water/Oil/Gas
2nd Bone Spring Ss	9356'	Water/Oil/Gas
2nd Bone Spring Ss B	9727'	Water/Oil/Gas
Target/Land Curve	9812'	Water/Oil/Gas

^{***} Hydrocarbons @ Brushy Canyon

No other formations are expected to yield oil, gas or fresh water in measurable volumes. The surface fresh water sands will be protected by setting 18-5/8 inch casing @ 1080' (147' above the salt) and circulating cement back to surface. The salt will be isolated by setting 13-3/8 inch casing at 2620' and circulating cement to surface. The Capitan Reef zone will be isolated by setting 9-5/8 inch casing at 4820'. An 8-3/4 inch curve and 8-1/2 inch lateral hole will be drilled to MD/TD and 5-1/2 inch casing will be set at TD and cemented back up to the 13-3/8 inch casing shoe depth.

Casing Design

Hole Size	Depth	OD Csg	Weight	Collar	Grade	New/Used	SF Burst	SF Collapse	SF Tension
24"	0' - 1080'	18-5/8"	87.5#	STC	H-40	New	2.00	1.27	5.92
17-1/2"	0' - 2620'	13-3/8"	54.5#	STC	J-55	New	2.44	1.37	3.60
12-1/4"	0' - 4820'	9-5/8"	36#	LTC	J-55	New	1.36	1.77	2.61
8-3/4" x 8-1/2"	0' – 26779'	5-1/2"	17#	BTC	P-110	New	1.12	1.58	1.94

- XTO requests to not utilize centralizers in the curve and lateral.
- 13-3/8" & 9-5/8" Collapse analyzed using 50% evacuation based on regional experience.
- 5-1/2" tension calculated using vertical hanging weight plus the lateral weight multiplied by a friction factor of 0.35

WELLHEAD:

Temporary Wellhead

• 18-5/8" SOW bottom x 21-1/4" 2M top flange.

Permanent Wellhead – GE RSH Multibowl System

- A. Starting Head: 13-5/8" 5M top flange x 13-3/8" SOW bottom
- B. Tubing Head: 13-5/8" 5M bottom flange x 7-1/16" 10M top flange
 - Wellhead will be installed by manufacturer's representatives.
 - Manufacturer will monitor welding process to ensure appropriate temperature of seal.
 - Operator will test the 9-5/8" casing per BLM Onshore Order 2
 - Wellhead manufacturer representative will not be present for BOP test plug installation

^{***} Groundwater depth 40' (per NM State Engineers Office).

4. Cement Program

Surface Casing: 18-5/8", 87.5# New H-40, STC casing to be set at +/- 1080'

Lead: 1040 sxs EconoCem-HLTRRC (mixed at 12.9 ppg, 1.87 ft3/sx, 10.13 gal/sx water)

Tail: 550 sxs Halcem-C + 2% CaCl (mixed at 14.8 ppg, 1.35 ft3/sx, 6.39 gal/sx water)

Compressives: 12-hr = 900 psi 24 hr = 1500 psi

1st Intermediate Casing: 13-3/8", 54.5# New J-55, STC casing to be set at +/- 2620'

Lead: 1510 sxs EconoCem-HLTRRC (mixed at 12.9 ppg, 1.87 ft3/sx, 10.13 gal/sx water)

Tail: 590 sxs Halcem-C + 2% CaCl (mixed at 14.8 ppg, 1.35 ft3/sx, 6.39 gal/sx water)

Compressives: 12-hr = 900 psi 24 hr = 1500 psi

2nd Intermediate Casing: 9-5/8", 36# New J-55, LTC casing to be set at +/- 4820' ECP/DV Tool to be set at 3150'

1st Stage

Lead: 220 sxs Halcem-C + 2% CaCl (mixed at 12.9 ppg, 1.88 ft3/sx, 9.61 gal/sx water)

Tail: 470 sxs Halcem-C + 2% CaCl (mixed at 14.8 ppg, 1.33 ft3/sx, 6.39 gal/sx water)

Compressives: 12-hr = 900 psi 24 hr = 1500 psi

2nd Stage

Lead: 170 sxs Halcem-C + 2% CaCl (mixed at 12.9 ppg, 1.88 ft3/sx, 9.61 gal/sx water)

Tail: 230 sxs Halcem-C + 2% CaCl (mixed at 14.8 ppg, 1.33 ft3/sx, 6.39 gal/sx water)

Compressives: 12-hr = 900 psi 24 hr = 1500 psi

Production Casing: 5-1/2", 17# New P-110, BTC casing to be set at +/- 26779'

Lead: 880 sxs NeoCem (mixed at 10.5 ppg, 2.69 ft3/sx, 12.26 gal/sx water)
Tail: 3180 sxs VersaCem (mixed at 13.2 ppg, 1.61 ft3/sx, 8.38 gal/sx water)
Compressives: 12-hr = 1375 psi 24 hr = 2285 psi

5. Pressure Control Equipment

The blow out preventer equipment (BOP) for surf casing / temp. wellhead will consist of a 21-1/4" minimum 2M Hydril. MASP should not exceed 813 psi.

Once the permanent WH is installed on the 13-3/8 casing, the blow out preventer equipment (BOP) will consist of a 13-5/8" minimum 3M Hydril and a 13-5/8" minimum 3M 3-Ram BOP. MASP should not exceed 2586 psi. In any instance where 10M BOP is required by BLM, XTO requests a variance to utilize 5M annular with 10M ram preventers (a common BOP configuration, which allows use of 10M rams in unlikely event that pressures exceed 5M).

All BOP testing will be done by an independent service company. Annular pressure tests will be limited to 50% of the working pressure but no greater than casing 70% burst. When nippling up on the 13-5/8" 3M bradenhead and flange, the BOP test will be limited to 3000 psi. When nippling up on the 9-5/8", the BOP will be tested to a minimum of 3000 psi. All BOP tests will include a low pressure test as per BLM regulations. The 3M BOP diagrams are attached. Blind rams will be functioned tested each trip, pipe rams will be functioned tested each day.

A variance is requested to allow use of a flex hose as the choke line from the BOP to the Choke Manifold. If this hose is used, a copy of the manufacturer's certification and pressure test chart will be kept on the rig. Attached is an example of a certification and pressure test chart. The manufacturer does not require anchors.

6. Proposed Mud Circulation System

INTERVAL	Hole Size	Mud Type	MW (ppg)	Viscosity (sec/qt)	Fluid Loss (cc)
0' - 1080'	24"	FW/Native	8.3 - 9.5	35-40	NC
1080' - 2620'	17-1/2"	Brine	9.8-10.2	30-35	NC
2620' to 4820'	12-1/4"	FW / Cut Brine	8.3-9.0	30-32	NC
4820' to 26779'	8-3/4" x 8-1/2"	FW / Cut Brine / Polymer	9 - 9.3	29-32	NC - 20

The necessary mud products for weight addition and fluid loss control will be on location at all times.

Spud with fresh water/native mud. Drill out from under 18-5/8" surface casing with brine solution. A 9.8ppg-10.2ppg brine mud will be used while drilling through the salt formation. Use fibrous materials as needed to control seepage and lost circulation. Pump viscous sweeps as needed for hole cleaning. Pump speed will be recorded on a daily drilling report after mudding up. A Pason or Totco will be used to detect changes in loss or gain of mud volume. A mud test will be performed every 24 hours to determine: density, viscosity, strength, filtration and pH as necessary. Use available solids controls equipment to help keep mud weight down after mud up. Rig up solids control equipment to operate as a closed loop system.

Delaware Basin Asset - Clean

Lea County, NM (NAD27)
Bluebird
BEU BB JABBA 104H - Slot BEU BB JABBA 104H

BEU BB JABBA 104H

Plan: BEU BB JABBA 104H

Standard Planning Report

, 19 May, 2020

Halliburton

Planning Report

Database: EDM 5000.1 Single User Db Local Co-ordinate Reference: Well BEU BB JABBA

104H

Company:Delaware Basin Asset - CleanTVD Reference:BEU BB JABBA 104IProject:Lea County, NM (NAD27)MD Reference:BEU BB JABBA 104I

Site: Bluebird North Reference: Grid

Well: BEU BB JABBA 104H Survey Calculation Method: Minimum Curvature Wellbore: BEU BB JABBA 104H

Design: BEU BB JABBA 104H

Lea County, NM (NAD27)

Map System: US State Plane 1927 (Exact solution) System Datum: Mean Sea Level

Geo Datum: NAD 1927 (NADCON CONUS)

Map Zone: New Mexico East 3001

Site Bluebird

Project

Site Position: Northing: 565,233.62 usft Latitude:

From: Map Easting: 676,601.60 usft Longitude:

Position Uncertainty: 0.0 usft Slot Radius: 13-3/16 " Grid Convergence:

Well BEU BB JABBA 104H - Slot BEU BB JABBA 104H

Well Position +N/-S -207.2 usft **Northing**: 565,026.45 usft **Latitude**: 32° 3:

+E/-W 289.6 usft **Easting**: 676,891.16 usft **Longitude**: 103° 45'

Position Uncertainty 0.0 usft Wellhead Elevation: Ground Level: 3,

Wellbore BEU BB JABBA 104H

Magnetics Model Name Sample Date Declination Dip Angle Fig. (°) (°)

IGRF2000 12/31/2004 8.68 60.71

Design BEU BB JABBA 104H

Audit Notes:

Version: PLAN Tie On Depth: 0.0

Vertical Section: Depth From (TVD) +N/-S +E/-W Direction (usft) (usft) (usft) (°)

0.0 0.0 0.0 257.71

Plan Survey Tool Program Date 5/19/2020

Depth From Depth To
(usft) (usft) Survey (Wellbore) Tool Name Remarks

1 0.0 4,000.0 BEU BB JABBA 104H (BEU BB J ADK 105

AdK w/ Gyrocompass HS refere

2 4,000.0 26,779.7 BEU BB JABBA 104H (BEU BB J MWD+IFR1+MS

OWSG MWD + IFR1 + Multi-Sta

Plan Sections

Measured			Dogleg			
Depth (usft)	Inclination (°)	Azimuth (°)	(usft)	+N/-S (usft)	+E/-W (usft)	Rate (°/100usft)
0.0	0.00	0.00	0.0	0.0	0.0	0.00
2,750.0	0.00	0.00	2,750.0	0.0	0.0	0.00
2,900.0	3.00	160.00	2,899.9	-3.7	1.3	2.00
4,265.3	29.93	187.65	4,197.9	-382.0	-32.4	2.00
10,200.2	29.93	187.65	9,341.3	-3,316.9	-426.5	0.00

11,061.1	90.00	269.78	9,805.0	-3,583.6	-997.1	10.00
26,779.7	90.00	269.78	9,805.0	-3,642.9	-16,715.6	0.00

Measured Depth	Inclination	Azimuth	Vertical Depth (usft)	+N/-S	+E/-W	Vert Sec
(usft)	(°)	(°)	-	(usft)	(usft)	(us
0.0	0.00	0.00	0.0	0.0	0.0	
100.0	0.00	0.00	100.0	0.0	0.0	
200.0	0.00	0.00	200.0	0.0	0.0	
300.0	0.00	0.00	300.0	0.0	0.0	
400.0	0.00	0.00	400.0	0.0	0.0	
500.0	0.00	0.00	500.0	0.0	0.0	
600.0	0.00	0.00	600.0	0.0	0.0	
700.0	0.00	0.00	700.0	0.0	0.0	
800.0	0.00	0.00	800.0	0.0	0.0	
900.0	0.00	0.00	900.0	0.0	0.0	
1,000.0	0.00	0.00	1,000.0	0.0	0.0	
1,100.0	0.00	0.00	1,100.0	0.0	0.0	
1,200.0	0.00	0.00	1,200.0	0.0	0.0	
1,300.0	0.00	0.00	1,300.0	0.0	0.0	
1,400.0	0.00	0.00	1,400.0	0.0	0.0	
			·			
1,500.0 1,600.0	0.00 0.00	0.00 0.00	1,500.0 1,600.0	0.0 0.0	0.0 0.0	
1,700.0	0.00	0.00	1,700.0	0.0	0.0	
1,800.0	0.00	0.00	1,800.0	0.0	0.0	
1,900.0	0.00	0.00	1,900.0	0.0	0.0	
2,000.0	0.00	0.00	2,000.0	0.0	0.0	
2,100.0	0.00	0.00	2,100.0	0.0	0.0	
2,200.0	0.00	0.00	2,200.0	0.0	0.0	
2,300.0	0.00 0.00	0.00 0.00	2,300.0	0.0 0.0	0.0 0.0	
2,400.0		0.00	2,400.0	0.0		
2,500.0	0.00	0.00	2,500.0	0.0	0.0	
2,600.0	0.00	0.00	2,600.0	0.0	0.0	
2,700.0	0.00	0.00	2,700.0	0.0	0.0	
2,750.0	0.00	0.00	2,750.0	0.0	0.0	
2,800.0	1.00	160.00	2,800.0	-0.4	0.1	
2,900.0	3.00	160.00	2,899.9	-3.7	1.3	
3,000.0	4.83	172.07	2,999.7	-10.3	2.8	
3,100.0	6.76	177.40	3,099.2	-20.4	3.7	
3,200.0	8.72	180.36	3,198.3	-33.8	3.9	
3,300.0	10.70	182.24	3,296.8	-50.7	3.5	
3,400.0	12.68	183.53	3,394.7	-70.9	2.4	
3,500.0	14.67	184.48	3,491.9	-94.5	0.8	
3,600.0	16.66	185.21	3,588.2	-121.4	-1.5	
3,700.0	18.65	185.79	3,683.5	-151.6	-4.4	
3,800.0	20.64	186.26	3,777.7	-185.0	-8.0	
3,900.0	22.64	186.65	3,870.6	-221.7	-12.1	
4,000.0	24.63	186.97	3,962.2	-261.5	-16.9	
4,100.0	26.63	187.26	4,052.4	-304.4	-22.2	
4,200.0	28.63	187.50	4,141.0	-350.4	-28.2	
4,265.3	29.93	187.65	4,197.9	-382.0	-32.4	
4,300.0	29.93	187.65	4,228.0	-399.2	-34.7	
4,400.0	29.93	187.65	4,314.6	-448.6	-41.4	
4,500.0	29.93	187.65	4,401.3	-498.1	-48.0	
4,600.0	29.93	187.65	4,488.0	-547.5	-54.6	
4,700.0	29.93	187.65	4,574.6	-597.0	-61.3	
4,800.0	29.93	187.65	4,661.3	-646.5	-67.9	
4,900.0	29.93	187.65	4,748.0	-695.9	-74.6	
5,000.0	29.93	187.65	4,834.6	-745.4	-81.2	
rvey						

Measured	Vertical Depth						
Depth (usft)	Inclination (°)	Azimuth (°)	(usft)	+N/-S (usft)	+E/-W (usft)	Sec (us	
5,100.0	29.93	187.65	4,921.3	-794.8	-87.8		
5,200.0	29.93	187.65	5,007.9	-844.3	-94.5		
5,300.0	29.93	187.65	5,094.6	-893.7	-101.1		

5,400.0	29.93	187.65	5,181.3	-943.2	-107.8
5,500.0	29.93	187.65	5,267.9	-992.6	-114.4
5,600.0	29.93	187.65	5,354.6	-1,042.1	-121.0
5,700.0	29.93	187.65	5,441.3	-1,091.5	-127.7
•				·	
5,800.0	29.93	187.65	5,527.9	-1,141.0	-134.3
5,900.0	29.93	187.65	5,614.6	-1,190.4	-141.0
6,000.0	29.93	187.65	5,701.3	-1,239.9	-147.6
6,100.0	29.93	187.65	5,787.9	-1,289.3	-154.2
6,200.0	29.93	187.65	5,874.6	-1,338.8	-160.9
	00.00	407.05			407.5
6,300.0	29.93	187.65	5,961.2	-1,388.2	-167.5
6,400.0	29.93	187.65	6,047.9	-1,437.7	-174.2
6,500.0	29.93	187.65	6,134.6	-1,487.1	-180.8
6,600.0	29.93	187.65	6,221.2	-1,536.6	-187.4
6,700.0	29.93	187.65	6,307.9	-1,586.0	-194.1
6,800.0	29.93	187.65	6,394.6	-1,635.5	-200.7
6,900.0	29.93	187.65	6,481.2	-1,684.9	-207.4
			·		
7,000.0	29.93	187.65	6,567.9	-1,734.4	-214.0
7,100.0	29.93	187.65	6,654.5	-1,783.8	-220.6
7,200.0	29.93	187.65	6,741.2	-1,833.3	-227.3
7,300.0	29.93	187.65	6,827.9	-1,882.7	-233.9
7,400.0	29.93	187.65	6,914.5	-1,932.2	-240.6
7,500.0	29.93	187.65	7,001.2	-1,981.6	-247.2
7,600.0	29.93	187.65	7,087.9	-2,031.1	-253.8
7,700.0	29.93	187.65	7,174.5	-2,080.5	-260.5
	29.93	107.03	7,174.5	-2,000.3	-200.5
7,800.0	29.93	187.65	7,261.2	-2,130.0	-267.1
7,900.0	29.93	187.65	7,347.8	-2,179.4	-273.8
8,000.0	29.93	187.65	7,434.5	-2,228.9	-280.4
8,100.0	29.93	187.65	7,521.2	-2,278.3	-287.0
8,200.0	29.93	187.65	7,607.8	-2,327.8	-293.7
8,300.0	29.93	187.65	7,694.5	-2,377.2	-300.3
8,400.0	29.93	187.65	7,781.2	-2,426.7	-307.0
8,500.0	29.93	187.65	7,867.8	-2,476.2	-313.6
8,600.0	29.93	187.65	7,954.5	-2,525.6	-320.2
8,700.0	29.93	187.65	8,041.2	-2,575.1	-326.9
8,800.0	29.93	187.65	8,127.8	-2,624.5	-333.5
	29.93				-340.2
8,900.0		187.65	8,214.5	-2,674.0	
9,000.0	29.93	187.65	8,301.1	-2,723.4	-346.8
9,100.0	29.93	187.65	8,387.8	-2,772.9	-353.4
9,200.0	29.93	187.65	8,474.5	-2,822.3	-360.1
9,300.0	29.93	187.65	8,561.1	-2,871.8	-366.7
9,400.0	29.93	187.65	8,647.8	-2,921.2	-373.4
9,500.0	29.93	187.65	8,734.5	-2,970.7	-380.0
9,600.0	29.93	187.65	8,821.1	-3,020.1	-386.6
9,700.0	29.93	187.65	8,907.8	-3,069.6	-393.3
	20.00	107.03			
9,800.0	29.93	187.65	8,994.4	-3,119.0	-399.9
9,900.0	29.93	187.65	9,081.1	-3,168.5	-406.6
10,000.0	29.93	187.65	9,167.8	-3,217.9	-413.2
10,100.0	29.93	187.65	9,254.4	-3,267.4	-419.8
10,200.0	29.93	187.65	9,341.1	-3,316.8	-426.5
10,200.2	29.93	187.65	9,341.3	-3,316.9	-426.5

Measured			Vertical Depth			Vert
Depth	Inclination	Azimuth	(usft)	+N/-S	+E/-W	Sec
(usft)	(°)	(°)		(usft)	(usft)	(us
10,300.0	32.52	206.32	9,426.8	-3,365.8	-441.7	
10,400.0	37.42	221.59	9,508.9	-3,412.7	-473.9	
10,500.0	43.86	233.38	9,584.8	-3,456.2	-522.0	
10,600.0	51.25	242.54	9,652.4	-3,494.9	-584.6	
10,700.0	59.21	249.92	9,709.4	-3,527.8	-659.7	
10,800.0	67.53	256.14	9,754.2	-3,553.6	-745.1	
10,900.0	76.06	261.64	9,785.5	-3,571.8	-838.2	
11,000.0	84.70	266.75	9,802.2	-3,581.7	-936.2	
11,061.1	90.00	269.78	9,805.0	-3,583.6	-997.1	
11,100.0	90.00	269.78	9,805.0	-3,583.7	-1,036.0	
11,200.0	90.00	269.78	9,805.0	-3,584.1	-1,136.0	
11,300.0	90.00	269.78	9,805.0	-3,584.5	-1,236.0	
11,400.0	90.00	269.78	9,805.0	-3,584.8	-1,336.0	
11,500.0	90.00	269.78	9,805.0	-3,585.2	-1,436.0	

11,600.0	90.00	269.78	9,805.0	-3,585.6	-1,536.0
11,700.0	90.00	269.78	9,805.0	-3,586.0	-1,636.0
11,800.0	90.00	269.78	9,805.0	-3,586.4	-1,736.0
11,900.0	90.00	269.78	9,805.0	-3,586.7	-1,836.0
12,000.0	90.00	269.78	9,805.0	-3,587.1	-1,936.0
12,100.0	90.00	269.78	9,805.0	-3,587.5	-2,036.0
12,700.0	90.00	269.78	9,805.0	-3,587.9	-2,136.0
12,300.0	90.00	269.78	9,805.0	-3,588.2	-2,236.0
12,400.0	90.00	269.78	9,805.0	-3,588.6	-2,336.0
12,400.0	90.00	269.78			
12,500.0	90.00	209.76	9,805.0	-3,589.0	-2,436.0
12,600.0	90.00	269.78	9,805.0	-3,589.4	-2,536.0
12,700.0	90.00	269.78	9,805.0	-3,589.8	-2,636.0
12,800.0	90.00	269.78	9,805.0	-3,590.1	-2,736.0
12,900.0	90.00	269.78	9,805.0	-3,590.5	-2,836.0
13,000.0	90.00	269.78	9,805.0	-3,590.9	-2,936.0
13,100.0	90.00	269.78	9,805.0	-3,591.3	-3,036.0
13,200.0	90.00	269.78	9,805.0	-3,591.7	-3,136.0
13,300.0	90.00	269.78	9,805.0	-3,592.0	-3,236.0
13,400.0	90.00	269.78	9,805.0	-3,592.4	-3,336.0
13,500.0	90.00	269.78	9,805.0	-3,592.8	-3,436.0
13,600.0	90.00	269.78	9,805.0	-3,593.2	-3,536.0
13,700.0	90.00	269.78	9,805.0	-3,593.5	-3,636.0
13,800.0	90.00	269.78	9,805.0	-3,593.9	-3,736.0
13,900.0	90.00	269.78	9,805.0	-3,594.3	-3,836.0
14,000.0	90.00	269.78	9,805.0	-3,594.7	-3,936.0
				•	
14,100.0	90.00	269.78	9,805.0	-3,595.1	-4,036.0
14,200.0	90.00	269.78	9,805.0	-3,595.4	-4,136.0
14,300.0	90.00	269.78	9,805.0	-3,595.8	-4,236.0
14,400.0	90.00	269.78	9,805.0	-3,596.2	-4,336.0
14,500.0	90.00	269.78	9,805.0	-3,596.6	-4,436.0
14,600.0	90.00	269.78	9,805.0	-3,596.9	-4,536.0
14,700.0	90.00	269.78	9,805.0	-3,597.3	-4,636.0
14,800.0	90.00	269.78	9,805.0	-3,597.7	-4,736.0
14,900.0	90.00	269.78	9,805.0	-3,598.1	-4,836.0
15,000.0	90.00	269.78	9,805.0	-3,598.5	-4,936.0
15,100.0	90.00	269.78	9,805.0	-3,598.8	-5,036.0
15,200.0	90.00	269.78	9,805.0	-3,599.2	-5,136.0
15,300.0	90.00	269.78	9,805.0	-3,599.6	-5,236.0
15,400.0	90.00	269.78	9,805.0	-3,600.0	-5,336.0
-,			-,	-,	2,230.0

Measured		•	/ertical Depth			Vert
Depth	Inclination	Azimuth	(usft)	+N/-S	+E/-W	Sec
(usft)	(°)	(°)		(usft)	(usft)	(us
15,500.0	90.00	269.78	9,805.0	-3,600.4	-5,436.0	
15,600.0	90.00	269.78	9,805.0	-3,600.7	-5,536.0	
15,700.0	90.00	269.78	9,805.0	-3,601.1	-5,636.0	
15,800.0	90.00	269.78	9,805.0	-3,601.5	-5,736.0	
15,900.0	90.00	269.78	9,805.0	-3,601.9	-5,836.0	
16,000.0	90.00	269.78	9,805.0	-3,602.2	-5,936.0	
16,100.0	90.00	269.78	9,805.0	-3,602.6	-6,036.0	
16,200.0	90.00	269.78	9,805.0	-3,603.0	-6,136.0	
16,300.0	90.00	269.78	9,805.0	-3,603.4	-6,236.0	
16,400.0	90.00	269.78	9,805.0	-3,603.8	-6,336.0	
16,500.0	90.00	269.78	9,805.0	-3,604.1	-6,436.0	
16,600.0	90.00	269.78	9,805.0	-3,604.5	-6,536.0	
16,700.0	90.00	269.78	9,805.0	-3,604.9	-6,636.0	
16,800.0	90.00	269.78	9,805.0	-3,605.3	-6,736.0	
16,900.0	90.00	269.78	9,805.0	-3,605.6	-6,836.0	
17,000.0	90.00	269.78	9,805.0	-3,606.0	-6,936.0	
17,100.0	90.00	269.78	9,805.0	-3,606.4	-7,036.0	
17,200.0	90.00	269.78	9,805.0	-3,606.8	-7,136.0	
17,300.0	90.00	269.78	9,805.0	-3,607.2	-7,236.0	
17,400.0	90.00	269.78	9,805.0	-3,607.5	-7,336.0	
17,500.0	90.00	269.78	9,805.0	-3,607.9	-7,436.0	
17,600.0	90.00	269.78	9,805.0	-3,608.3	-7,536.0	
17,700.0	90.00	269.78	9,805.0	-3,608.7	-7,636.0	
17,800.0	90.00	269.78	9,805.0	-3,609.1	-7,736.0	
17,900.0	90.00	269.78	9,805.0	-3,609.4	-7,836.0	

18,000.0	90.00	269.78	9,805.0	-3,609.8	-7,936.0
18,100.0	90.00	269.78	9,805.0	-3,610.2	-8,036.0
18,200.0	90.00	269.78	9,805.0	-3,610.6	-8,136.0
18,300.0	90.00	269.78	9,805.0	-3,610.9	-8,236.0
18,400.0	90.00	269.78	9,805.0	-3,611.3	-8,336.0
18,500.0	90.00	269.78	9,805.0	-3,611.7	-8,436.0
18,600.0	90.00	269.78	9,805.0	-3,612.1	-8,536.0
18,700.0	90.00	269.78	9,805.0	-3,612.5	-8,636.0
18,800.0	90.00	269.78	9,805.0	-3,612.8	-8,736.0
18,900.0	90.00	269.78	9,805.0	-3,613.2	-8,836.0
19,000.0	90.00	269.78	9,805.0	-3,613.6	-8,936.0
19,100.0	90.00	269.78	9,805.0	-3,614.0	-9,036.0
19,200.0	90.00	269.78	9,805.0	-3,614.3	-9,136.0
19,300.0	90.00	269.78	9,805.0	-3,614.7	-9,236.0
19,400.0	90.00	269.78	9,805.0	-3,615.1	-9,336.0
19,500.0	90.00	269.78	9,805.0	-3,615.5	-9,436.0
19,600.0	90.00	269.78	9,805.0	-3,615.9	-9,536.0
19,700.0	90.00	269.78	9,805.0	-3,616.2	-9,636.0
19,800.0	90.00	269.78	9,805.0	-3,616.6	-9,736.0
19,900.0	90.00	269.78	9,805.0	-3,617.0	-9,836.0
20,000.0	90.00	269.78	9,805.0	-3,617.4	-9,936.0
20,100.0	90.00	269.78	9,805.0	-3,617.8	-10,036.0
20,200.0	90.00	269.78	9,805.0	-3,618.1	-10,136.0
20,300.0	90.00	269.78	9,805.0	-3,618.5	-10,236.0
20,400.0	90.00	269.78	9,805.0	-3,618.9	-10,336.0
20,500.0	90.00	269.78	9,805.0	-3,619.3	-10,436.0
20,600.0	90.00	269.78	9,805.0	-3,619.6	-10,536.0
20,700.0	90.00	269.78	9,805.0	-3,620.0	-10,636.0

Measured		V	ertical Depth			Vert
Depth	Inclination	Azimuth	(usft)	+N/-S	+E/-W	Sec
(usft)	(°)	(°)		(usft)	(usft)	(us
20,800.0	90.00	269.78	9,805.0	-3,620.4	-10,736.0	
20,900.0	90.00	269.78	9,805.0	-3,620.8	-10,836.0	
21,000.0	90.00	269.78	9,805.0	-3,621.2	-10,936.0	
21,100.0	90.00	269.78	9,805.0	-3,621.5	-11,036.0	
21,200.0	90.00	269.78	9,805.0	-3,621.9	-11,136.0	
21,300.0	90.00	269.78	9,805.0	-3,622.3	-11,236.0	
21,400.0	90.00	269.78	9,805.0	-3,622.7	-11,336.0	
21,500.0	90.00	269.78	9,805.0	-3,623.0	-11,436.0	
21,600.0	90.00	269.78	9,805.0	-3,623.4	-11,536.0	
21,700.0	90.00	269.78	9,805.0	-3,623.8	-11,636.0	
21,800.0	90.00	269.78	9,805.0	-3,624.2	-11,736.0	
21,900.0	90.00	269.78	9,805.0	-3,624.6	-11,836.0	
22,000.0	90.00	269.78	9,805.0	-3,624.9	-11,936.0	
22,100.0	90.00	269.78	9,805.0	-3,625.3	-12,036.0	
22,200.0	90.00	269.78	9,805.0	-3,625.7	-12,136.0	
22,300.0	90.00	269.78	9,805.0	-3,626.1	-12,236.0	
22,400.0	90.00	269.78	9,805.0	-3,626.5	-12,336.0	
22,500.0	90.00	269.78	9,805.0	-3,626.8	-12,436.0	
22,600.0	90.00	269.78	9,805.0	-3,627.2	-12,536.0	
22,700.0	90.00	269.78	9,805.0	-3,627.6	-12,636.0	
22,800.0	90.00	269.78	9,805.0	-3,628.0	-12,736.0	
22,900.0	90.00	269.78	9,805.0	-3,628.3	-12,836.0	
23,000.0	90.00	269.78	9,805.0	-3,628.7	-12,936.0	
23,100.0	90.00	269.78	9,805.0	-3,629.1	-13,036.0	
23,200.0	90.00	269.78	9,805.0	-3,629.5	-13,136.0	
23,300.0	90.00	269.78	9,805.0	-3,629.9	-13,236.0	
23,400.0	90.00	269.78	9,805.0	-3,630.2	-13,336.0	
23,500.0	90.00	269.78	9,805.0	-3,630.6	-13,436.0	
23,600.0	90.00	269.78	9,805.0	-3,631.0	-13,536.0	
23,700.0	90.00	269.78	9,805.0	-3,631.4	-13,636.0	
23,800.0	90.00	269.78	9,805.0	-3,631.8	-13,736.0	
23,900.0	90.00	269.78	9,805.0	-3,632.1	-13,836.0	
24,000.0	90.00	269.78	9,805.0	-3,632.5	-13,936.0	
24,100.0	90.00	269.78	9,805.0	-3,632.9	-14,036.0	
24,200.0	90.00	269.78	9,805.0	-3,633.3	-14,136.0	
24,300.0	90.00	269.78	9,805.0	-3,633.6	-14,236.0	

24,400.0	90.00	269.78	9,805.0	-3,634.0	-14,336.0
24,500.0	90.00	269.78	9,805.0	-3,634.4	-14,436.0
24,600.0	90.00	269.78	9,805.0	-3,634.8	-14,535.9
24,700.0	90.00	269.78	9,805.0	-3,635.2	-14,635.9
24,800.0	90.00	269.78	9,805.0	-3,635.5	-14,735.9
24,900.0	90.00	269.78	9,805.0	-3,635.9	-14,835.9
25,000.0	90.00	269.78	9,805.0	-3,636.3	-14,935.9
25,100.0	90.00	269.78	9,805.0	-3,636.7	-15,035.9
25,200.0	90.00	269.78	9,805.0	-3,637.0	-15,135.9
25,300.0	90.00	269.78	9,805.0	-3,637.4	-15,235.9
25,400.0	90.00	269.78	9,805.0	-3,637.8	-15,335.9
25,500.0	90.00	269.78	9,805.0	-3,638.2	-15,435.9
25,600.0	90.00	269.78	9,805.0	-3,638.6	-15,535.9
25,700.0	90.00	269.78	9,805.0	-3,638.9	-15,635.9
25,800.0	90.00	269.78	9,805.0	-3,639.3	-15,735.9
25,900.0	90.00	269.78	9,805.0	-3,639.7	-15,835.9
26,000.0	90.00	269.78	9,805.0	-3,640.1	-15,935.9

Measured		,	Vertical Depth			Vert
Depth	Inclination	Azimuth	(usft)	+N/-S	+E/-W	Sec
(usft)	(°)	(°)		(usft)	(usft)	(us
26,100.0	90.00	269.78	9,805.0	-3,640.5	-16,035.9	
26,200.0	90.00	269.78	9,805.0	-3,640.8	-16,135.9	
26,300.0	90.00	269.78	9,805.0	-3,641.2	-16,235.9	
26,400.0	90.00	269.78	9,805.0	-3,641.6	-16,335.9	
26,500.0	90.00	269.78	9,805.0	-3,642.0	-16,435.9	
26,600.0	90.00	269.78	9,805.0	-3,642.3	-16,535.9	
26,700.0	90.00	269.78	9,805.0	-3,642.7	-16,635.9	
26,779.7	90.00	269.78	9,805.0	-3,642.9	-16,715.6	

Design Targets

Target Name

- h	et Name it/miss target Shape	Dip Angle (°)	Dip Dir. (°)	TVD (usft)	+N/-S (usft)	+E/-W (usft)	Northing (usft)	East (us
FTP	2-4-1 - plan hits target center - Rectangle (sides W200	90.00 0.0 H50.0 D0.0)	9.96	9,805.0	-3,583.6	-997.1	561,442.89	6
BHL	2-4-1	90.00	76.25	9,805.0	-3,642.9	-16,715.6	561,383.58	6

Casing Points

Measured Depth (usft)	Vertical Depth (usft)		Casing Diameter
		Name	(")
1,100.0	1,100.0 18.75		18-3/4

plan hits target centerRectangle (sides W200.0 H50.0 D0.0)

5/19/2020 12:30:08PM

BA 104H - Slot BEU BB JABB

04H Default @ 3543.0u 04H Default @ 3543.0u

> 32° 33' 9.463 N 103° 45' 36.651 W 0.31 °

3' 7.397 N I5' 33.281 513.0 usft

eld Strength (nT)

49,626.25494017

Build Rate (°/100usft)	Turn Rate (°/100usft)	TFO (°)	Target
0.00	0.00	0.00	
0.00	0.00	0.00	
2.00	0.00	160.00	
1.97	2.03	30.31	
0.00	0.00	0.00	

6.98	9.54	83.17 FTP	2-4-1
0.00	0.00	0.00 BHL	2-4-1

ical	Dogleg	Build	Turn
tion	Rate	Rate	Rate
ift)	(°/100usft)	(°/100usft)	(°/100usft)
0.0	0.00	0.00	0.00
0.0	0.00	0.00	0.00
0.0	0.00	0.00	0.00
0.0	0.00	0.00	0.00
0.0	0.00	0.00	0.00
0.0	0.00	0.00	0.00
0.0	0.00	0.00	0.00
0.0	0.00	0.00	0.00
0.0	0.00	0.00	0.00
0.0	0.00	0.00	0.00
0.0	0.00	0.00	0.00
0.0	0.00	0.00	0.00
0.0	0.00	0.00	0.00
0.0	0.00	0.00	0.00
0.0	0.00	0.00	0.00
0.0	0.00	0.00	0.00
0.0	0.00	0.00	0.00
0.0	0.00	0.00	0.00
0.0	0.00	0.00	0.00
0.0	0.00	0.00	0.00
0.0	0.00	0.00	0.00
0.0	0.00	0.00	0.00
0.0	0.00	0.00	0.00
0.0	0.00	0.00	0.00
0.0	0.00	0.00	0.00
0.0	0.00	0.00	0.00
0.0	0.00	0.00	0.00
0.0	0.00	0.00	0.00
0.0	0.00	0.00	0.00
-0.1	2.00	2.00	0.00
-0.5 -0.6 0.8 3.4 7.4	2.00 2.00 2.00 2.00 2.00 2.00	2.00 1.83 1.93 1.96 1.98	0.00 12.07 5.33 2.96 1.88
12.7 19.4 27.3 36.6 47.2	2.00 2.00 2.00 2.00 2.00 2.00	1.98 1.99 1.99 1.99 1.99	1.30 0.95 0.73 0.58 0.47
59.0 72.2 86.5 102.2 113.0	2.00 2.00 2.00 2.00 2.00 2.00	1.99 2.00 2.00 2.00 2.00 2.00	0.39 0.33 0.28 0.25 0.22
118.9	0.00	0.00	0.00
135.9	0.00	0.00	0.00
153.0	0.00	0.00	0.00
170.0	0.00	0.00	0.00
187.0	0.00	0.00	0.00
204.0	0.00	0.00	0.00
221.0	0.00	0.00	0.00
238.0	0.00	0.00	0.00
ical	Dogleg	Build	Turn
tion	Rate	Rate	Rate
ift)	(°/100usft)	(°/100usft)	(°/100usft)
255.1	0.00	0.00	0.00
272.1	0.00	0.00	0.00

289.1

0.00

0.00

0.00

306.1	0.00	0.00	0.00
323.1	0.00	0.00	0.00
340.1	0.00	0.00	0.00
357.2	0.00	0.00	0.00
374.2	0.00	0.00	0.00
391.2	0.00	0.00	0.00
408.2	0.00	0.00	0.00
425.2	0.00	0.00	0.00
442.3	0.00	0.00	0.00
459.3	0.00	0.00	0.00
476.3	0.00	0.00	0.00
493.3	0.00	0.00	0.00
510.3	0.00	0.00	0.00
527.3	0.00	0.00	0.00
544.4	0.00	0.00	0.00
561.4	0.00	0.00	0.00
578.4	0.00	0.00	0.00
595.4	0.00	0.00	0.00
612.4	0.00	0.00	0.00
629.4	0.00	0.00	0.00
646.5	0.00	0.00	0.00
663.5	0.00	0.00	0.00
680.5	0.00	0.00	0.00
697.5	0.00	0.00	0.00
714.5	0.00	0.00	0.00
731.6	0.00	0.00	0.00
748.6	0.00	0.00	0.00
765.6	0.00	0.00	0.00
782.6	0.00	0.00	0.00
799.6	0.00	0.00	0.00
816.6	0.00	0.00	0.00
833.7	0.00	0.00	0.00
850.7	0.00	0.00	0.00
867.7	0.00	0.00	0.00
884.7	0.00	0.00	0.00
901.7	0.00	0.00	0.00
918.7	0.00	0.00	0.00
935.8	0.00	0.00	0.00
952.8	0.00	0.00	0.00
969.8	0.00	0.00	0.00
986.8	0.00	0.00	0.00
1,003.8	0.00	0.00	0.00
1,020.9	0.00	0.00	0.00
1,037.9	0.00	0.00	0.00
1,054.9	0.00	0.00	0.00
1,071.9	0.00	0.00	0.00
1,088.9	0.00	0.00	0.00
1,105.9	0.00	0.00	0.00
1,123.0	0.00	0.00	0.00
1,123.0	0.00	0.00	0.00

ical tion ift)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
1,148.3	10.00	2.59	18.71
1,189.7	10.00	4.90	15.27
1,246.0	10.00	6.44	11.79
1,315.3	10.00	7.39	9.16
1,395.7	10.00	7.96	7.38
1,484.7	10.00	8.32	6.22
1,579.5	10.00	8.53	5.50
1,677.4	10.00	8.64	5.11
1,737.3	10.00	8.68	4.97
1,775.4	0.00	0.00	0.00
1,873.2	0.00	0.00	0.00
1,971.0	0.00	0.00	0.00
2,068.7	0.00	0.00	0.00
2,166.5	0.00	0.00	0.00

2,3 2,4 2,5	264.3 262.1 159.9 557.7 555.5	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00
2,8 2,9 3,0	753.2 951.0 948.8 946.6 44.4	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00
3,3 3,4 3,5	242.2 340.0 337.8 335.5 333.3	0.00 0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00
3,8 3,9 4,0	731.1 128.9 126.7 124.5 22.3	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00
4,3 4,4 4,5	220.0 117.8 115.6 113.4 111.2	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00
4,8 4,9 5,0	709.0 306.8 304.5 302.3 00.1	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00
5,2 5,3 5,4	97.9 295.7 393.5 191.3 589.1	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00
5,7 5,8	886.8 84.6 882.4 980.2	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00

ical	Dogleg	Build	Turn
tion	Rate	Rate	Rate
ift)	(°/100usft)	(°/100usft)	(°/100usft)
6,078.0	0.00	0.00	0.00
6,175.8	0.00	0.00	0.00
6,273.6	0.00	0.00	0.00
6,371.3	0.00	0.00	0.00
6,469.1	0.00	0.00	0.00
6,566.9	0.00	0.00	0.00
6,664.7	0.00	0.00	0.00
6,762.5	0.00	0.00	0.00
6,860.3	0.00	0.00	0.00
6,958.1	0.00	0.00	0.00
7,055.9	0.00	0.00	0.00
7,153.6	0.00	0.00	0.00
7,251.4	0.00	0.00	0.00
7,349.2	0.00	0.00	0.00
7,447.0	0.00	0.00	0.00
7,544.8	0.00	0.00	0.00
7,642.6	0.00	0.00	0.00
7,740.4	0.00	0.00	0.00
7,838.1	0.00	0.00	0.00
7,935.9	0.00	0.00	0.00
8,033.7	0.00	0.00	0.00
8,131.5	0.00	0.00	0.00
8,229.3	0.00	0.00	0.00
8,327.1	0.00	0.00	0.00
8,424.9	0.00	0.00	0.00

8,522.6	0.00	0.00	0.00
8,620.4	0.00	0.00	0.00
8,718.2	0.00	0.00	0.00
8,816.0	0.00	0.00	0.00
8,913.8	0.00	0.00	0.00
9,011.6	0.00	0.00	0.00
9,109.4	0.00	0.00	0.00
9,207.2	0.00	0.00	0.00
9,304.9	0.00	0.00	0.00
9,402.7	0.00	0.00	0.00
9,500.5	0.00	0.00	0.00
9,598.3	0.00	0.00	0.00
9,696.1	0.00	0.00	0.00
9,793.9	0.00	0.00	0.00
9,891.7	0.00	0.00	0.00
9,989.4	0.00	0.00	0.00
10,087.2	0.00	0.00	0.00
10,185.0	0.00	0.00	0.00
10,282.8	0.00	0.00	0.00
10,380.6	0.00	0.00	0.00
10,478.4	0.00	0.00	0.00
10,576.2	0.00	0.00	0.00
10,674.0	0.00	0.00	0.00
10,771.7	0.00	0.00	0.00
10,869.5	0.00	0.00	0.00
10,967.3	0.00	0.00	0.00
11,065.1	0.00	0.00	0.00
11,162.9	0.00	0.00	0.00

ical	Dogleg	Build	Turn
tion	Rate	Rate	Rate
sft)	(°/100usft)	(°/100usft)	(°/100usft)
11,260.7	0.00	0.00	0.00
11,358.5	0.00	0.00	0.00
11,456.2	0.00	0.00	0.00
11,554.0	0.00	0.00	0.00
11,651.8	0.00	0.00	0.00
11,749.6	0.00	0.00	0.00
11,847.4	0.00	0.00	0.00
11,945.2	0.00	0.00	0.00
12,043.0	0.00	0.00	0.00
12,140.7	0.00	0.00	0.00
12,238.5	0.00	0.00	0.00
12,336.3	0.00	0.00	0.00
12,434.1	0.00	0.00	0.00
12,531.9	0.00	0.00	0.00
12,629.7	0.00	0.00	0.00
12,727.5	0.00	0.00	0.00
12,825.3	0.00	0.00	0.00
12,923.0	0.00	0.00	0.00
13,020.8	0.00	0.00	0.00
13,118.6	0.00	0.00	0.00
13,216.4	0.00	0.00	0.00
13,314.2	0.00	0.00	0.00
13,412.0	0.00	0.00	0.00
13,509.8	0.00	0.00	0.00
13,607.5	0.00	0.00	0.00
13,705.3	0.00	0.00	0.00
13,803.1	0.00	0.00	0.00
13,900.9	0.00	0.00	0.00
13,998.7	0.00	0.00	0.00
14,096.5	0.00	0.00	0.00
14,194.3	0.00	0.00	0.00
14,292.1	0.00	0.00	0.00
14,389.8	0.00	0.00	0.00
14,487.6	0.00	0.00	0.00
14,585.4	0.00	0.00	0.00
14,683.2	0.00	0.00	0.00

14,781.0	0.00	0.00	0.00
14,878.8	0.00	0.00	0.00
14,976.6	0.00	0.00	0.00
15.074.3	0.00	0.00	0.00
15,172.1	0.00	0.00	0.00
15,269.9	0.00	0.00	0.00
15,367.7	0.00	0.00	0.00
45 405 5	0.00	0.00	0.00
15,465.5	0.00	0.00	0.00
15,563.3	0.00	0.00	0.00
15,661.1	0.00	0.00	0.00
15,758.9	0.00	0.00	0.00
15,856.6	0.00	0.00	0.00
15,954.4	0.00	0.00	0.00
16,052.2	0.00	0.00	0.00
,			
16,150.0	0.00	0.00	0.00
16,247.8	0.00	0.00	0.00
16,345.6	0.00	0.00	0.00

ical tion ift)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
16,443.4	0.00	0.00	0.00
16,541.1	0.00	0.00	0.00
16,638.9	0.00	0.00	0.00
16,736.7	0.00	0.00	0.00
16,834.5	0.00	0.00	0.00
16,932.3	0.00	0.00	0.00
17,030.1	0.00	0.00	0.00
17,108.0	0.00	0.00	0.00

ting
ift) Latitude Longitude

75,894.06 32° 32' 31.990 N 103° 45' 45.155 W

60,175.53 32° 32' 32.199 N 103° 48' 48.780 W

Hole Diameter (")

18-3/4

COMPASS 5000.15 Build 90

XTO respectfully requests approval to utilize a spudder rig to pre-set surface casing.

Description of Operations:

- 1. Spudder rig will move in to drill the surface hole and pre-set surface casing on the well.
 - a. After drilling the surface hole section, the spudder rig will run casing and cement following all of the applicable rules and regulations (OnShore Order 2, all COAs and NMOCD regulations).
 - b. The spudder rig will utilize fresh water-based mud to drill the surface hole to TD. Solids control will be handled entirely on a closed loop basis. No earth pits will be used.
- 2. The wellhead will be installed and tested as soon as the surface casing is cut off and WOC time has been reached.
- 3. A blind flange at the same pressure rating as the wellhead will be installed to seal the wellbore. Pressure will be monitored with needle valves installed on two wing valves.
 - a. A means for intervention will be maintained while the drilling rig is not over the well.
- 4. Spudder rig operations are expected to take 2-3 days per well on the pad.
- 5. The BLM will be contacted and notified 24 hours prior to commencing spudder rig operations.
- 6. Drilling Operations will begin with a larger rig and a BOP stack equal to or greater than the pressure rating that was permitted will be nippled up and tested on the wellhead before drilling operations resume on each well.
 - a. The larger rig will move back onto the location within 180 days from the point at which the wells are secured and the spudder rig is moved off location.
 - b. The BLM will be notified 24 hours before the larger rig moves back on the pre-set locations
- 7. XTO will have supervision on the rig to ensure compliance with all BLM and NMOCD regulations and to oversee operations.
- 8. Once the rig is removed, XTO will secure the wellhead area by placing a guard rail around the cellar area.

Subject: Request for a Variance Allowing break Testing of the Blowout Preventer Equipment (BOPE)

XTO Energy requests a variance to ONLY test broken pressure seals on the BOPE and function test BOP when skidding a drilling rig between multiple wells on a pad.

Background

Onshore Oil and Gas Order (OOGO) No. 2, Drilling Operations, Sections III.A.2.i.iv.B states that the BOP test must be performed whenever any seal subject to test pressure is broken. The current interpretation of the Bureau of Land Management (BLM) requires a complete BOP test and not just a test of the affected component. OOGO No. 2, Section I.D.2 states, "Some situation may exist either on a well-by-well basis or field-wide basis whereby it is commonly accepted practice to vary a particular minimum standard(s) established in this order. This situation can be resolved by requesting a variance...". XTO Energy feels the break testing the BOPE is such a situation. Therefore, as per OOGO No. 2, Section IV., XTO Energy submits this request for the variance.

Supporting Documentation

OOGO No. 2 became effective on December 19, 1988 and has remained the standard for regulating BLM onshore drilling operations for over 30 years. During this time there have been significant changes in drilling technology. BLM continues to use the variance request process to allow for the use of modern technology and acceptable engineering practices that have arisen since OOGO No. 2 was originally released. The XTO Energy drilling rig fleet has many modern upgrades that allow the intact BOP stack to be moved between well slots on a multi-well pad, as well as, wellhead designs that incorporate quick connects facilitating release of the BOP from the wellhead without breaking any BOP stack components apart. These technologies have been used extensively offshore, and other regulators, API, and many operators around the world have endorsed break testing as safe and reliable.



Figure 1: Winch System attached to BOP Stack



Figure 2: BOP Winch System

American Petroleum Institute (API) standards, specification and recommended practices are considered the industry standard and are consistently utilized and referenced by the industry. OOGO No. 2 recognizes API recommended Practices (RP) 53 in its original development. API Standard 53, *Well Control Equipment Systems for Drilling Wells* (Fifth Edition, December 2018, Annex C, Table C.4) recognizes break testing as an acceptable practice. Specifically, API Standard 53, Section 5.3.7.1 states "A pressure test of the pressure containing component shall be performed following the disconnection or repair, limited to the affected component." See Table C.4 below for reference.

	Pressure Test—Low	Pressure Test—	-High Pressure ^{ac}	
Component to be Pressure Tested	Pressure ^{ac} psig (MPa)	Change Out of Component, Elastomer, or Ring Gasket	No Change Out of Component, Elastomer, or Ring Gasket	
Annular preventer ^b	250 to 350 (1.72 to 2.41)	RWP of annular preventer	MASP or 70% annular RWP, whichever is lower.	
Fixed pipe, variable bore, blind, and BSR preventers ^{bd}	250 to 350 (1.72 to 2.41)	RWP of ram preventer or wellhead system, whichever is lower	ITP	
Choke and kill line and BOP side outlet valves below ram preventers (both sides)	250 to 350 (1.72 to 2.41)	RWP of side outlet valve or wellhead system, whichever is lower	ITP	
Choke manifold—upstream of chokes ^e	250 to 350 (1.72 to 2.41)	RWP of ram preventers or wellhead system, whichever is lower	ITP	
Choke manifold—downstream of chokese	250 to 350 (1.72 to 2.41)	RWP of valve(s), line(s), or M whichever is lower	MASP for the well program,	
Kelly, kelly valves, drill pipe safety valves, IBOPs	250 to 350 (1.72 to 2.41)	MASP for the well program		
	during the evaluation period. The p	pressure shall not decrease below the		
		n the 21 days, pressure testing is req		

The Bureau of Safety and Environmental Enforcement (BSEE), Department of Interior, has also utilized the API standards, specification and best practices in the development of its offshore oil and gas regulations and incorporates them by reference within its regulations.

Break testing has been approved by the BLM in the past with other operators based on the detailed information provided in this document.

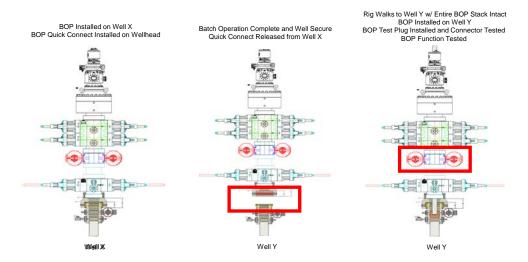
XTO Energy feels break testing and our current procedures meet the intent of OOGO No. 2 and often exceed it. There has been no evidence that break testing results in more components failing than seen on full BOP tests. XTO Energy's internal standards requires complete BOPE tests more often than that of OOGO No. 2 (Every 21 days). In addition to function testing the annular, pipe rams and blind rams after each BOP nipple up, XTO Energy performs a choke drill with the rig crew prior to drilling out every casing shoe. This is additional training for the rig crew that exceeds the requirements of the OOGO No. 2.

Procedures

- XTO Energy will use this document for our break testing plan for New Mexico Delaware basin.
 The summary below will be referenced in the APD or Sundry Notice and receive approval prior
 to implementing this variance.
- 2. XTO Energy will perform BOP break testing on multi-wells pads where multiple intermediate sections can be drilled and cased within the 21-day BOP test window.
 - a. A full BOP test will be conducted on the first well on the pad.
 - b. The first intermediate hole section drilled on the pad will be the deepest. All of the remaining hole sections will be the same depth or shallower.
 - i. Our Lower WC targets set the intermediate casing shoe no deeper than the Wolfcamp B.
 - ii. Our Upper WC targets set the intermediate casing shoe shallower than the Wolfcamp B.
 - c. A Full BOP test will be required if the intermediate hole section being drilled has a MASP over 5M.
 - d. A full BOP test will be required prior to drilling any production hole.
- 3. After performing a complete BOP test on the first well, the intermediate hole section will be drilled and cased, two breaks would be made on the BOP equipment.
 - a. Between the HCV valve and choke line connection
 - b. Between the BOP quick connect and the wellhead
- 4. The BOP is then lifted and removed from the wellhead by a hydraulic system.
- 5. After skidding to the next well, the BOP is moved to the wellhead by the same hydraulic system and installed.
- 6. The connections mentioned in 3a and 3b will then be reconnected.
- 7. Install test plug into the wellhead using test joint or drill pipe.
- 8. A shell test is performed against the upper pipe rams testing the two breaks.
- 9. The shell test will consist of a 250 psi low test and a high test to the value submitted in the APD or Sundry (e.g. 5,000 psi or 10,000psi).
- 10. Function test will be performed on the following components: lower pipe rams, blind rams, and annular.

- 11. For a multi-well pad the same two breaks on the BOP would be made and on the next wells and steps 4 through 10 would be repeated.
- 12. A second break test would only be done if the intermediate hole section being drilled could not be completed within the 21 day BOP test window.

Note: Picture below highlights BOP components that will be tested during batch operations



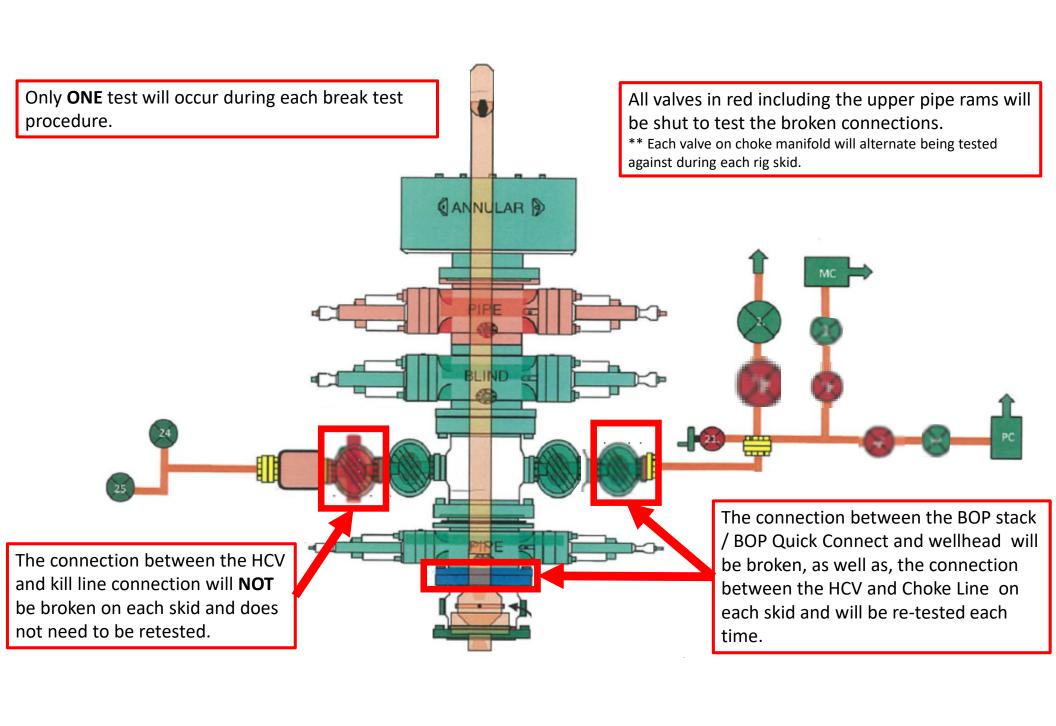
Summary

A variance is requested to **ONLY** test broken pressure seals on the BOP equipment when moving from wellhead to wellhead which is in compliance with API Standard 53. API Standard 53 states, that for pad drilling operation, moving from one wellhead to another within 21 days, pressure testing is required for pressure-containing and pressure-controlling connections when the integrity of a pressure seal is broken.

The BOP will be secured by a hydraulic carrier or cradle. The BLM will be contacted if a Well Control event occurs prior to the commencement of a BOPE Break Testing operation.

Based on discussions with the BLM on February 27th 2020 and the supporting documentation submitted to the BLM, we will request permission to ONLY retest broken pressure seals if the following conditions are met:

- 1. After a full BOP test is conducted on the first well on the pad.
- 2. The first intermediate hole section drilled on the pad will be the deepest. All of the remaining hole sections will be the same depth or shallower.
- 3. Full BOP test will be required if the intermediate hole section being drilled has a MASP over 5M.
- 4. Full BOP test will be required prior to drilling the production hole.



XTO Permian Operating, LLC Offline Cementing Variance Request

XTO requests the option to cement the surface and intermediate casing strings offline as a prudent batch drilling efficiency of acreage development.

1. Cement Program

No changes to the cement program will take place for offline cementing.

2. Offline Cementing Procedure

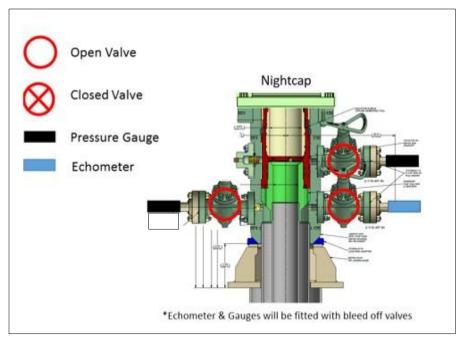
The operational sequence will be as follows. If a well control event occurs, the BLM will be contacted for approval prior to conducting offline cementing operations.

- 1. Run casing as per normal operations. While running casing, conduct negative pressure test and confirm integrity of the float equipment (float collar and shoe)
- 2. Land casing with mandrel
- 3. Fill pipe with kill weight fluid, do not circulate through floats and confirm well is static
- 4. Set annular packoff shown below and pressure test to confirm integrity of the seal. Pressure ratings of wellhead components and valves is 5,000 psi.
- 5. After confirmation of both annular barriers and internal barriers, nipple down BOP and install cap flange.
 - a. If any barrier fails to test, the BOP stack will not be nippled down until after the cement job is completed with cement 500ft above the highest formation capable of flow with kill weight mud above or after it has achieved 50-psi compressive strength if kill weight fluid cannot be verified.



Annular packoff with both external and internal seals

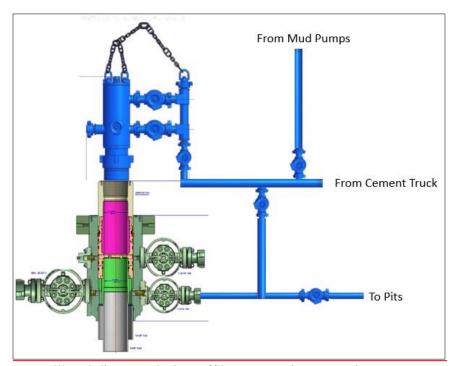
XTO Permian Operating, LLC Offline Cementing Variance Request



Wellhead diagram during skidding operations

- 6. Skid rig to next well on pad.
- 7. Confirm well is static before removing cap flange, flange will not be removed and offline cementing operations will not commence until well is under control. If well is not static, casing outlet valves will provide access to both the casing ID and annulus. Rig or third party pump truck will kill well prior to cementing or nippling up for further remediation.
 - a. Well Control Plan
 - i. The Drillers Method will be the primary well control method to regain control of the wellbore prior to cementing, if wellbore conditions do not permit the drillers method other methods of well control may be used
 - ii. Rig pumps or a 3rd party pump will be tied into the upper casing valve to pump down the casing ID
 - iii. A high pressure return line will be rigged up to lower casing valve and run to choke manifold to control annular pressure
 - iv. Once influx is circulated out of the hole, kill weight mud will be circulated
 - v. Well will be confirmed static
 - vi. Once confirmed static, cap flange will be removed to allow for offline cementing operations to commence
- 8. Install offline cement tool
- 9. Rig up cement equipment

XTO Permian Operating, LLC Offline Cementing Variance Request



Wellhead diagram during offline cementing operations

- 10. Circulate bottoms up with cement truck
 - a. If gas is present on bottoms up, well will be shut in and returns rerouted through gas buster to handle entrained gas
 - b. Max anticipated time before circulating with cement truck is 6 hrs
- 11. Perform cement job taking returns from the annulus wellhead valve
- 12. Confirm well is static and floats are holding after cement job
- 13. Remove cement equipment, offline cement tools and install night cap with pressure gauge for monitoring.

Form 3160-5 (June 2015)

UNITED STATES DEPARTMENT OF THE INTERIOR BUREAU OF LAND MANAGEMENT

FORM APPROVED OMB NO. 1004-0137 Expires: January 31, 2018 5. Lease Serial No. NMNM33955

SUNDRY NOTICES AND REPORTS ON WELLS

Do not use the abandoned we	6. If Indian, Allottee o	6. If Indian, Allottee or Tribe Name				
SUBMIT IN	TRIPLICATE - Other instruction	s on page 2	7. If Unit or CA/Agree	ement, Name and/or No.		
1. Type of Well			8. Well Name and No. BIG EDDY UNIT I	DI BB JABBA 104H		
2. Name of Operator XTO PERMIAN OPERATING	Contact: KELLY		9. API Well No. 30-025-47270	9. API Well No. 30-025-47270		
3a. Address 6401 HOLIDAY HILL RD BLD	3b. Pho	one No. (include area code) 32-620-4374	10. Field and Pool or I SALT LAKE BO	Exploratory Area NE SPRING		
MIDLAND, TX 79707 4. Location of Well (Footage, Sec., T	T., R., M., or Survey Description)		11. County or Parish,	State		
Sec 22 T20S R32E Mer NMP	SWSW 270FSL 640FWL		LEA COUNTY,	NM		
12. CHECK THE AI	PPROPRIATE BOX(ES) TO INC	DICATE NATURE OF	F NOTICE, REPORT, OR OTH	HER DATA		
TYPE OF SUBMISSION		TYPE OF	ACTION			
Notice of Intent ■	☐ Acidize ☐] Deepen	☐ Production (Start/Resume)	☐ Water Shut-Off		
_	☐ Alter Casing ☐	Hydraulic Fracturing	☐ Reclamation	■ Well Integrity		
☐ Subsequent Report	☐ Casing Repair ☐	New Construction	☐ Recomplete	⊠ Other		
☐ Final Abandonment Notice	☐ Change Plans	Plug and Abandon	□ Temporarily Abandon	Change to Original A PD		
	☐ Convert to Injection ☐	Plug Back	■ Water Disposal			
determined that the site is ready for f XTO Permian Operating, LLC Change the SHL from 270FSI Attachments: C102 & Supplement	requests permission to make the	following changes to	the original APD:	·		
14. I hereby certify that the foregoing is	strue and correct. Electronic Submission #519057 v For XTO PERMIAN OPE					
Name(Printed/Typed) KELLY KA	ARDOS	Title REGUL	ATORY COORDINATOR			
Signature (Electronic S	Submission) THIS SPACE FOR FED	Date 06/16/20				
	THIS SPACE FOR FED	TERAL OR STATE (
_Approved By		Title		Date		
Conditions of approval, if any, are attache certify that the applicant holds legal or equivalent would entitle the applicant to conduct the conductive conductive the applicant to conduct the conductive conductin conductive conductive conductive conductive conductive conducti	uitable title to those rights in the subject le					
Title 18 U.S.C. Section 1001 and Title 43 States any false, fictitious or fraudulent	U.S.C. Section 1212, make it a crime for statements or representations as to any ma		willfully to make to any department or	agency of the United		

District I

District IV

1625 N. French Dr., Hobbs, NM 88240 Phone: (575) 393-6161 Fax: (575) 393-0720 District II

811 S. First St., Artesia, NM 88210 Phone: (575) 748-1283 Fax: (575) 748-9720

District III 1000 Rio Brazos Road, Aztec, NM 87410 Phone: (505) 334-6178 Fax: (505) 334-6170

1220 S. St. Francis Dr. Santa Fe. NM 87505 Phone: (505) 476-3460 Fax: (505) 476-3462

State of New Mexico Energy, Minerals & Natural Resources Department

1220 South St. Francis Dr. Santa Fe, NM 87505

OIL CONSERVATION DIVISION

Form C-102 Revised August 1, 2011 Submit one copy to appropriate District Office

☐ AMENDED REPORT

WELL LOCATION AND ACREAGE DEDICATION PLAT

¹ API Number 30-025-4		² Pool Code	Pool Code ³ Pool Name	
⁴ Property Code		⁵ Pr	operty Name	⁶ Well Number
	BIG EDDY UNIT BB JABBA			104H
⁷ OGRID No.		8 O _l	perator Name	⁹ Elevation
373075		XTO PERMIAN OPERATING, LLC.		
		10 Care	face Leastion	

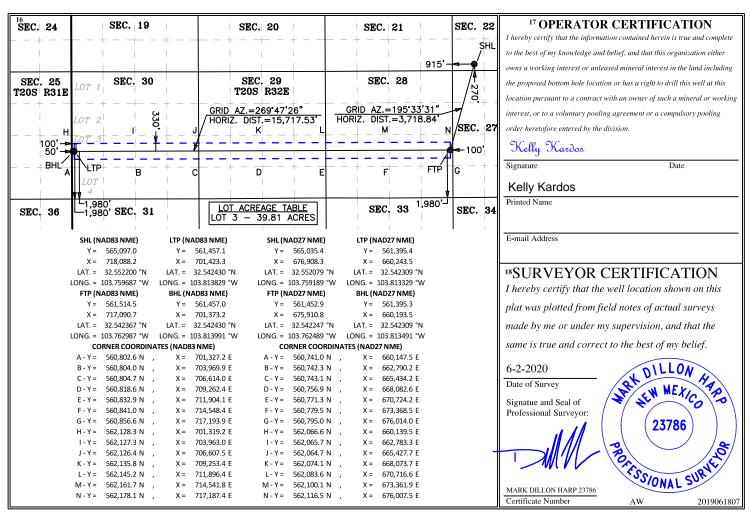
¹⁰ Surface Location

UL or lot no.	Section	Township	Range	Lot Idn	Feet from the	North/South line	Feet from the	East/West line	County
M	22	20 S	32 E		270	SOUTH	915	WEST	LEA
11 Pottom Hola Logation If Different From Surface									

Bottom Hole Location If Different From Surface

Bottom Hote Econtion in Billionia Tom Surface											
UL or lot no.	Section	Township	Range	Lot Idn	Feet from the	North/South line	Feet from the	East/West line	County		
3	30	20 S	32 E		1,980	SOUTH	50	WEST	LEA		
12 Dedicated Acres	¹³ Joint o	r Infill 14 C	Consolidation	Code 15 Or	der No.			•			

No allowable will be assigned to this completion until all interests have been consolidated or a non-standard unit has been approved by the division.



Inten	t	As Dril	led											
API#	†]											
Operator Name:						Property Name:							Well Number	
Kick (Off Point	(KOP)												
UL	Section	Township	Range	Lot	Feet	From N/S			Feet		From E/W		County	
Latit	Latitude					Longitude							NAD	
First T	Take Poir	nt (FTP)	Range	Lot	Feet		From N	ı/S	Feet	1	From I	E/W	County	
Latit					Longitude							NAD		
Latit	Latitude					Longitude								
Last 1	Гake Poin	t (LTP)												
UL	Section	tion Township Range Lot Feet From N/S Feet From E/W County								У				
Latit	ude	Longitu	Longitude NAD											
Is this well the defining well for the Horizontal Spacing Unit?														
Is this	s well an	infill well?												
	ll is yes p ng Unit.	lease provi	de API if	availal	ole, Ope	rator I	Name	and v	vell nı	umber f	or De	efinir	ng well fo	or Horizontal
API#	ŧ													
Operator Name:						Property Name:							Well Number	