Dis	rice	Ì
013	1104	

1625 N. French Dr., Hobbs, NM \$8240 Phone: (575) 393-6161 Fax: (575) 393-0720 District II 811 S. First St., Artesia, NM 88210 Phone: (575) 748-1283 Fax: (575) 748-9720 District III 1000 Rio Brazos Road. Aztec. NM-\$7410 Phone: (505) 334-6178 Fax: (505) 334-6170 District IV 1220 S. St. Francis Dr., Santa Fe, NM 87505 Phone: (505) 476-3460 Fax: (505) 476-3462

HOBBS OCD State of New Mexico Energy, Minerals & Natural Resources Department MAR 1 2 2010 IL CONSERVATION DIVISION 1220 South St. Francis Dr.

Form C-102 Revised August 1, 2011 Submit one copy to appropriate District Office

Santa Fe, NM 87505

AMENDED REPORT

RECEIVED

WELL LOCATION AND ACREACE DEDICATION DLAT

WELL LOCATION AND ACKEAGE DEDICATION FEAT										
· ·	r		² Pool Code	• . <i> </i>	OBBS CH	ANNE Pool Na	ime			
30-02	5-41	715		3170	>5	HUM	BLE CITY; BOI	NE SPRING		
⁺ Property (Code				⁵ Property	Name		6	Well Number	
404	+52				WEISSBI	EIR 23			1H	
⁷ OGRID	No.				* Operator	Name			⁹ Elevation	
6137			DEV	ON ENEF	RGY PRODU	CTION COMPA	NY, L.P.		3728.7	
	¹⁰ Surface Location									
UL or lot no.	Section	Township	Range	Lot Idn	Feet from the	North/South line	Feet from the	East/West line	County	
0	14	17 S	37 E		265	SOUTH	1350	EAST	LEA	
"Bottom Hole Location If Different From Surface										
UL or lot no.	Section	Township	Range	Lot ldn	Feet from the	North/South line	Feet from the	East/West line	County	
0	23	17 S	37 E		330	SOUTH	1980	EAST	LEA	
12 Dedicated Acres	¹³ Joint o	r Infill ¹⁴ C	onsolidation	Code 13 Or	der No.	•				
160										

No allowable will be assigned to this completion until all interests have been consolidated or a non-standard unit has been approved by the division.

N89'32'28'T 2641.86 /T N89'32'06'T N89'32'06'T	2640.15 FT	" OPERATOR CERTIFICATION
NW CORNER SEC. 14 I N O CORNER SEC. 14 LAT. = 32.84202657N, LAT. = 32.8420087N	HE CORNER SEC. 14 IAT. = 32.84199101N	I hereby certify that the information contained herein is true and complete
LONG. = 103.23075257W LONG. = 103.22215297W L = NUSP FAST (FT) NOVSP FAST (FT)	UNG = 103.2135588 W HWSP EAST (FT) 12	to the best of my knowledge and belief, and that this organization either
R H = 671829.55 N = 671850.71 ⇒ E = 879972.67 E = 882614.11	4 = 671872.14 C E = 885253.82	owns a working interest or unleased mineral interest in the land including
		the proposed bottom hole location or has a right to drill this well at this
ARE SHOW USAGING CONSTRUCT S	14	location musuant to a contract with an owner of such a mineral or working
Concentration of the second state proved by the second state provided by the second state second	15 17	interest, or to a voluntary pooling agreement or a compulsory pooling
W Q CORVER SCC. 14	E & CORNER SEC. 14	order beretofore entered by the division
LAT. = 32.8347646N LONG. = 103.23073657NWEJSSBEUR _ 2841H1	UT. = 32.8347416N OHG. = 103.2135461W	
$\begin{array}{llllllllllllllllllllllllllllllllllll$	NMSP EAST (FT) N = 659234.53	J C 3/11/2014
E = 880005.11 UONG = 103.21/9311W	E = 885285.67	Signature Date
₩ 66664325 ± E = 883963(61	<u>7-672</u>	David H. Caak
	-SE CORDER SEE. IF	Printed Name
	LAT. = 32.877483171 8	
C SW CONVEX SCC. 14 SQ CONVEX SCC. 14 Y	NMSP EAST (FT) 2 N = 566593.61 □	david.cook@dvn.com
	E = 885316.72 1350	E-mail Address
E = 880037.36 E = 882677.05	1	
569-3042 W 254013 H - 365 2003 W		SURVEYOR CERTIFICATION
ž III	1 8	I hereby certify that the well location shown on this
5 SEC. 23	42'12	
₹ ,		plat was plotted from field holes of actual surveys
	Y	made by me or under my supervision, and that the
ר אין		same is true and correct to the best of my belief.
w 0 CORDER SEC. 23;	E O CORNER SEC. 23 LAT. = 32.8202246 N	FEBRUARY 17, 2014
1040. • 103.23070837W (0.000 HOLE	LONG. = 103.2133216 W NUSP EAST (FT)	3/27 0/21
N = 663905.56 LAT. = 32.8138835 N E = 58068.85 LONG. = 103.2199559 W	N = 663352.66 E = 885349.15	Date of Survey (12797)
$\dot{\mathbf{g}}$ NMSP EAST (FT) $\mathbf{N} = 661624162$	500	
± E ≈ 883396;71	11'02'6	
	SE-COPINER SEC: 23-	Stoke WAS Man I all a
SIN CORNER SEC. 23 5 Q CORRER SEC. 23	LONG. = 103.21351017N =	
CHI = 32.8129926N LAT. = 32.8129795N V S CAI LONG. = 103.2306945W LONG. = 103.2221022W	N = 661311.97	Signautorandi Sealior Projetsionan Surveyor:
NASP EAST (FT) NAUSP EAST (FT) N = 661265.96 N = 661288.93	-1980'	Certificate Number: 74 FikiMOVF, JARAMILLO, PLS 12707
E = 880100.50 , E = 882740.73 S89'30'05'W 2640.57 FT \$\$\$89'30'00'	2640.38 FT	SURVEY NO. 2708

MAR 1 8 2014











Devon Energy, Inc.

Lea County (NAD83)	
Weissbeir 23	HOBBS OCD
Weissbeir "23" 1H - Slot 1H	HUBBS
Original Hole	MAR 1 2 2014

RECEIVED

Plan: Design #1

Standard Planning Report

10 March, 2014

Pathfinder - A Schlumberger Company

Planning Report

Database: Company: Project: Site: Well: Well: Wellbore: Design:	EDM 5 Devon Lea Co Weiss Weiss Origin Design	5000.1 Single U I Energy, Inc. ounty (NAD83) beir 23 beir "23" 1H al Hole n #1	ser Db		Local Co- TVD Refer MD Refere North Ref Survey Ca	ordinate Refe rence: ence: erence: alculation Met	rence: , ,	Well Weissbeir WELL @ 3755. WELL @ 3755. Grid Minimum Curva	"23" 1H - Slot 70usft (Origina 70usft (Origina ture	1H I Well Elev) I Well Elev)
Project	Lea Co	unty (NAD83)			· · · · · ·			· · · · · ·	· · · · · · ·	• • • • • • • • • •
Map System: Geo Datum: Map Zone:	US State North An New Me	e Plane 1983 nerican Datum xico Eastern Zo	1983 ne		System Dat	tum:	M	ean Sea Level		
Site	Weissb	eir 23			•••••••••••••••••••••••••••••••••••••••		······································			• • · · · · · · · · · • • • • • • • • •
Site Position: From: Position Uncertain	Map nty:	0.00	No Ea:) usft Sic	rthing: sting: ot Radius:	666 883	,845.25 usft ,963.81 usft 13-3/16 "	Latitude: Longitude: Grid Converg	jence:		32° 49' 41.570 N 103° 13' 4.552 W 0.60 °
Well	Weissb	eir "23" 1H - Slo	ot 1H		· · · · ·					· · · · · · · · · · · · · · · · · · ·
Well Position	+N/-S +E/-W	0.0 0.0	00 usft 00 usft	Northing: Easting:		666,845.25 883,963.81	5 usft Lat I usft Lor	itude: ngitude:		32° 49' 41.570 N 103° 13' 4.552 W
Position Uncertain	nty	0.0	0 usft	Wellhead Elevation	on:	3,755.70) usft Gro	ound Level:		3,728.70 usft
Wellbore	Origina	al Hole		••••••••••••••••••••••••••••••••••••••		01. 1	· · · · · · ·			
Magnetics	Мо	del Name	Sar	nple Date	Declina (°)	tion	Dip A ((ngle °)	Field \$ (Strength nT)
		BGGM2012		3/4/2014		7.24		60.70		48,699
Design	Design	#1		anti-ranan yere a yere a yere a			· · · · · · · · ·		·	
Audit Notes:										
Version:			Ph	nase: PF	ROTOTYPE	Tie	e On Depth:		0.00	
Vertical Section:		Ď	epth From	(TVD)	+N/-S (usft)	+8	E/-W	Dii	rection (°)	
			0.00		0.00	0	0.00	1	86.20	
Plan Sections		••••••••••••••••••••••••••••••••••••••			· ·				· · · · ·	· · · · · · · · · · · · · · · · · · ·
Measured Depth Ir (usft)	nclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)	TFO (°)	Target
0.00	0.00	0.00	0.0	0.00	0.00	0.00	0.00	0.00	0.00	
8,610.00	0.00	0.00	8,610.0	0 0.00	0.00	0.00	0.00	0.00	0.00	
9,581.80	38.91 89.03	183.20	0,937.1 9,216.4	-528.63	-96.03 -304.78	11.00	8.11	-8.87	-61.84	
14,281.80	89.03	183.20	9,296.0	0 -5,220.63	-567.10	0.00	0.00	0.00	0.00	Toe - Weissbeir 23 1⊦

Pathfinder - A Schlumberger Company

Planning Report

Database:	, EDM 5000.1 Single User Db	Local Co-ordinate Reference:	Well Weissbeir "23" 1H - Slot 1H
Company:	Devon Energy, Inc.	TVD Reference:	، WELL @ 3755.70usft (Original Well Elev)
Project:	Lea County (NAD83)	MD Reference:	WELL @ 3755.70usft (Original Well Elev)
Site:	Weissbeir 23	North Reference:	Grid
Well:	Weissbeir "23" 1H	Survey Calculation Method:	Minimum Curvature
Wellbore:	Original Hole	1 · · · ·	
Design:	° ⁷ Design #1		anna an the second s
Planned Survey	and the second	an a the second s	
	and the second	سیده اطور میشهد، ۲۰ د. د. د. س. م	angangan perior saya barka salar ketara ketar keta Ter

1 0 0	۰.	Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)	,
8,010 CD 0.00 8,010 CD 0.00 0.00 0.00 0.00 0.00 0.00 9,020 CD 9,00 220 CD 4,40 227 11.00 11.00 0.00 9,000 CD 9,00 228 CD 8,996.55 -18.14 -29.07 21.76 11.00 11.00 0.00 8,000 CD 31.80 8,995.55 -18.14 -29.07 21.76 11.00 11.00 0.00 8,000 CD 43.90 228.03 8,995.55 -14.14 -28.07 21.76 11.00 11.00 0.00 8,000 CD 43.92 228.68 8,945.95 -74.42 -117.14 86.64 11.00 54.4 -12.82 9,000 CD 43.52 220.68 8,945.95 -74.44 -117.14 86.64 11.00 8.41 -12.82 9,000 CD 72.51 194.65 9,147.27 -276.34 -286.84 -70.12 -276.84 -30.12 11.00 8.45 -7.11 -286.84 -70.01		8.600.00	0.00	0.00	8,600.00	0.00	0.00	0.00	0.00	0.00	0.00	
Self 259 E.0.00 Self 260 Self 260 Self 260 Self 27 Self 28		9 610 00	0.00	0.00	9 610 00	0.00	0.00	0.00	0.00	. 0.00	0.00	
10 00 00<		8,610.00	0.00	0.00	8,610.00	2.80	-4.49	0.00	11.00	11.00	0.00	
NR 157 5 Jun 9,50 288.03 8.89.55 -4.11 -5.58 4.79 11.00 11.00 0.00 8,700.00 23.60 23.80.3 8.95.5.2 -18.14 -23.07 21.18 11.00 11.00 0.00 8,900.00 31.80 238.03 8.95.72 3.861 238.03 8.95.71 -41.15 -46.63 48.61 11.00 11.00 0.00 9,000.00 47.24 22.01.3 5.03.87.5 -122.66 -167.06 140.01 11.00 6.33 -122.63 9,000.00 47.24 220.03 6.03.87.5 -122.66 -167.06 140.01 11.00 6.33 -122.63 9,000.00 63.99 201.75 3.149.97 -244.63 230.52.01 11.00 8.41 -824 9,300.00 80.31 132.20 9.216.43 -226.69 477.02 11.00 9.57 -7.41 9,600.00 80.03 183.20 9.221.13 -744.46 -316.59 757.64 0.00	, <u> </u>	0,004.29	0.17	236.03	0,004.04	-2.00		5.27	1.00		0.00	
5,00.00 20,00 238,03 8,96,02 18,14 -28,07 21,18 11,00 11,00 0.00 8,960,00 31,90 238,03 8,956,25 -41,65 -66,73 48,61 11,00 11,00 0.00 9,000,00 40,92 232,86 8,94,99 -74,42 -117,14 86,66,71 11,00 7,33 -10,23 9,000,00 47,54 220,00 55,28 209,99 3,099,17 -186,72 -214,74 208,47 11,00 7,73 -10,03 9,300,00 63,25 200,40 9,157,73 -279,34 -246,74 208,47 11,00 8,46 -7,44 9,400,00 72,51 114,65 9,167,27 -322,22 -277,50 300,12 11,00 8,45 -7,01 9,400,00 72,51 114,65 9,167,27 -322,22 -277,50 300,12 110,0 8,45 -7,01 9,400,00 80,03 1183,20 9,216,43 -586,45 -9,017 0,00	L	15t B5PG 5a		220 02	9 600 55	4 11	6.59	4 70	11 00	11 00	0.00	
S.BB00 3.0.0 2.0.0 2.0.0 6.895.27 3.0.0 11.00 11.00 10.00 0.00 9.000.00 41.05 -41.15 -96.673 44.851 11.00 11.00 0.00 9.000.00 40.22 222.66 8.964.99 -74.42 -117.14 86.64 11.00 5.54 -12.63 9.100.00 57.26 20.99 9.099.17 -186.72 -271.47 22.064.7 11.00 6.63 -12.63 9.300.00 55.25 20.04 9.167.73 -279.34 -244.59 305.20 11.00 8.41 -8.24 9.310.10 65.55 20.04 9.167.73 -277.50 380.12 11.00 8.65 -7.01 9.500.00 81.55 188.22 9.209.72 -447.60 -266.69 477.02 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 <td< td=""><td></td><td>8,700.00</td><td>9.90</td><td>238.03</td><td>0,099.00 9,705.90</td><td>-4.11</td><td>-0.50</td><td>4./9</td><td>11.00</td><td>11.00</td><td>0.00</td><td></td></td<>		8,700.00	9.90	238.03	0,099.00 9,705.90	-4.11	-0.50	4./9	11.00	11.00	0.00	
0.0000 0.000 <t< td=""><td></td><td>8,800.00</td><td>20.90</td><td>238.03</td><td>8 885 25</td><td>-10.14</td><td>-29.07</td><td>48.61</td><td>11.00</td><td>11.00</td><td>0.00</td><td></td></t<>		8,800.00	20.90	238.03	8 885 25	-10.14	-29.07	48.61	11.00	11.00	0.00	
8,963.72 38,91 238,03 8,97,16 -61,18 -98,03 71,41 11.00 11.00 1.00 0.00 9,100,00 47,24 220,03 9,096,75 -122,26 -167,06 140,01 11.00 6,63 -122,33 -10,00 7,74 26,73 -10,03 -10,00 7,74 -10,03 -10,00 7,74 -10,03 -10,00 6,63 -122,63 -10,00 6,63 -7,49 2,318,01 65,25 200,40 9,167,73 -279,44 -246,46 -200,01 6,86 -7,49 2,818,01 80,03 183,22 9,216,74 -566,69 -477,02 10,00 8,65 -643 9,500,00 81,03 183,20 9,216,44 -566,69 -767,52 0,00		0,000.00	51.50	200.00	0,000.20	-41.00	-00.70	40.01	11.00	11.00	0.00	
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		8,963.72	38.91	238.03	8,937.16	-61.18	-98.03	71.41	11.00	11.00	0.00	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		9,000.00	40.92	232.66	8,964.99	-74.42	-117.14	86.64	11.00	5.54	-14.82	
9.200.00 52.28 209.99 9.099.17 -18.72 -211.47 200.47 11.00 7.73 -10.03 9.318.01 65.25 200.40 9.157.73 -279.34 -284.58 305.20 11.00 8.68 -7.48 9.400.00 72.51 18.46 9.167.73 -279.34 -284.58 305.20 11.00 8.68 -7.48 9.400.00 81.55 188.22 9.216.43 -526.63 -304.78 654.45 11.00 9.14 -614 9.600.00 89.03 183.20 9.221.67 -526.63 -304.78 657.63 0.00 <t< td=""><td></td><td>9,100.00</td><td>47.54</td><td>220.03</td><td>9,036.75</td><td>-122.69</td><td>-167.06</td><td>140.01</td><td>11.00</td><td>6.63</td><td>-12.63</td><td></td></t<>		9,100.00	47.54	220.03	9,036.75	-122.69	-167.06	140.01	11.00	6.63	-12.63	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		9,200.00	55.28	209.99	9,099.17	-186.72	-211.47	208.47	11.00	7.73	-10.03	
9.318.01 65.25 200.40 9.157.73 -279.34 -224.58 305.20 11.00 8.68 -7.48 9.400.00 72.51 194.65 9.187.27 -352.22 -277.50 380.12 11.00 8.65 -7.01 9.500.00 81.05 188.20 9.216.43 -528.63 -300.78 655.45 11.00 9.05 -6.43 9.600.00 89.03 183.20 9.216.44 -646.63 -311.37 676.48 0.00 0.00 0.00 9.800.00 89.03 183.20 9.221.51 -746.46 -316.96 776.32 0.00 0.00 0.00 0.00 10.000 89.03 183.20 9.222.51 -946.12 -232.14 876.71 0.00 0.00 0.00 10.000 89.03 183.20 9.226.59 -1.145.76 -333.70 1.075.87 0.00 0.00 0.00 10.300.00 89.03 183.20 9.226.59 -1.245.61 -344.86 1.275.71 0.00		9,300.00	63.69	201.75	9,149.97	-204.10	-240.74	269.50	11.00	0.41	-0.24	
2nd BSPG Sand		9,318.01	65.25	200.40	9,157.73	-279.34	-254.58	305.20	11.00	8.68	-7.48	
9,400.00 72,51 194.65 9,167.27 -352.22 -277.50 380.12 11.00 8.85 -7.01 9,501.00 81.55 183.20 9,216.43 -528.63 -304.78 658.45 11.00 9.14 -6.14 9,600.00 89.03 183.20 9,216.44 -546.60 -305.79 576.63 0.00 0.00 0.00 9,700.00 89.03 183.20 9,216.44 -646.63 -311.37 675.64 0.00		2nd BSPG S	and									
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$		9,400.00	72.51	194.65	9,187.27	-352.22	-277.50	380.12	11.00	8.85	-7.01	
9,561,80 89,03 183,20 9,216,43 -528,63 -304,78 556,45 11,00 9,14 -6,14 9,600,00 89,03 183,20 9,216,44 -646,63 -311,37 676,48 0,00 0,00 0,00 9,900,00 89,03 183,20 9,218,24 -646,69 -322,54 876,17 0,00 0,00 0,00 9,900,00 89,03 183,20 9,223,51 -946,12 -328,12 976,02 0,00 0,00 0,00 10,000,0 89,03 183,20 9,226,50 -1,145,78 -339,28 1,175,72 0,00 0,00 0,00 10,000,0 89,03 183,20 9,233,67 -1,545,41 -350,44 1,375,42 0,00 0,00 0,00 10,000,0 89,03 183,20 9,233,67 -1,545,41 -356,02 1,475,27 0,00 0,00 0,00 10,600,00 89,03 183,20 9,235,36 -1,644,93 -367,19 1,674,96 0,00 0,0		9,500.00	81.55	188.22	9,209.72	-447.60	-296.69	477.02	11.00	9.05	-6.43	
9 600 00 89 03 183 20 9 .216 74 -546 60 -305 79 576 63 0.00 0.00 0.00 9 700 00 88 03 183 20 9 .210 13 -746 46 -316 56 776 52 0.00 0.00 0.00 9 900 00 88 03 183 20 9 .221 13 -746 46 -316 56 776 52 0.00 0.00 0.00 10 000 00 89 03 183 20 9 .222 51 -946 29 -322 54 1976 17 0.00 0.00 0.00 10 000 00 89 03 183 20 9 .225 51 -146 12 -333 70 1.075 87 0.00 0.00 0.00 10 000 00 89 03 183 20 9 .228 59 -1.245 61 -344 66 1.275 57 0.00 0.00 0.00 1.050 00 0.00 0.00 0.00 1.050 00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 <td></td> <td>9,581.80</td> <td>89.03</td> <td>183.20</td> <td>9,216.43</td> <td>-528.63</td> <td>-304.78</td> <td>558.45</td> <td>11.00</td> <td>9.14</td> <td>-6.14</td> <td></td>		9,581.80	89.03	183.20	9,216.43	-528.63	-304.78	558.45	11.00	9.14	-6.14	
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		9,600.00	89.03	183.20	9,216.74	-546.80	-305.79	576.63	0.00	0.00	0.00	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		9,700.00	89.03	183.20	9,218.44	-646.63	-311.37	676.48	0.00	0.00	0.00	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		9,800.00	89.03	183.20	9,220.13	-746.46	-316.96	776.32	0.00	0.00	0.00	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		9,900.00	89.03	183.20	9,221.82	-846.29	-322.54	876.17	0.00	0.00	0.00	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		10,000.00	89.03	183.20	9,223.51	-946.12	-328.12	976.02	0.00	0.00	0.00	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		10,100.00	89.03	183.20	9,225.21	-1,045.95	-333.70	1,075.87	0.00	0.00	0.00	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1	10 200 00	89.03	183 20	9 226 90	-1 145 78	-339.28	1 175 72	0.00	0.00	0.00	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	l	10,200.00	89.03	183.20	9 228 59	-1 245 61	-344.86	1 275 57	0.00	0.00	0.00	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	Í	10,400,00	89.03	183.20	9 230 29	-1 345 44	-350.44	1 375 42	0.00	0.00	0.00	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		10,500.00	89.03	183.20	9 231 98	-1 445 27	-356 02	1 475 27	0 00	0.00	0.00	
10,700.00 89.03 183.20 9.235.36 -1,644.93 -367.19 1,674.96 0.00 0.00 0.00 10,800.00 89.03 183.20 9.237.06 -1,744.76 -372.77 1,774.81 0.00 0.00 0.00 10,900.00 88.03 183.20 9.238.75 -1,844.59 -378.35 1,874.66 0.00 0.00 0.00 11,000.00 88.03 183.20 9.240.44 -1,944.42 -383.93 1,974.51 0.00 0.00 0.00 11,000.00 89.03 183.20 9.242.14 -2.044.25 -389.51 2.074.36 0.00 0.00 0.00 11,200.00 89.03 183.20 9.247.21 -2.343.74 -406.26 2.373.90 0.00 0.00 0.00 11,600.00 89.03 183.20 9.247.21 -2.343.74 -406.26 2.373.90 0.00 0.00 0.00 11,600.00 89.03 183.20 9.250.60 -2.643.23 -417.42 2.573.60 0.00		10.600.00	89.03	183.20	9,233.67	-1,545.10	-361.61	1,575.11	0.00	0.00	0.00	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		40,700,00	00.00	400.00	0,005,00	4 6 4 4 0 2	207.40	1 674 06	0.00	0.00	0.00	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		10,700.00	89.03	183.20	9,235.36	-1,044.93	-307.19	1,074.90	0.00	0.00	0.00	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		10,800.00	89.03	183.20	9,237.00	-1,744.70	-378 35	1,774.01	0.00	0.00	0.00	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		11,000,00	89.03	183.20	9,230.73	-1 944 42	-383.93	1 974 51	0.00	0.00	0.00	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		11 100 00	89.03	183.20	9 242 14	-2 044 25	-389 51	2 074 36	0.00	0.00	0.00	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			00.00	100.20	0,2 (2.1)	2,0 1 1 20		2,07,004	0.00	0.00	0.00	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1	11,200.00	89.03	183.20	9,243.83	-2,144.08	-395.09	2,1/4.21	0.00	0.00	0.00	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		11,300.00	89.03	183.20	9,245.52	-2,243.91	-400.66	2,274.05	0.00	0.00	0.00	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		11,400.00	89.03	183.20	9,247.21	-2,343.74	-400.20	2,373.90	0.00	0.00	0.00	
11,700.00 89.03 183.20 9,252.29 -2,643.23 -423.00 2,673.45 0.00 0.00 0.00 11,800.00 89.03 183.20 9,255.68 -2,842.89 -434.16 2,873.15 0.00 0.00 0.00 11,900.00 89.03 183.20 9,255.68 -2,842.89 -434.16 2,873.15 0.00 0.00 0.00 12,000.00 89.03 183.20 9,257.37 -2,942.72 -439.74 2,973.00 0.00 0.00 0.00 12,00.00 89.03 183.20 9,259.06 -3,042.55 -445.33 3,072.84 0.00 0.00 0.00 12,200.00 89.03 183.20 9,260.76 -3,142.38 -450.91 3,172.69 0.00 0.00 0.00 12,300.00 89.03 183.20 9,264.14 -3,342.04 -462.07 3,372.39 0.00 0.00 0.00 12,400.00 89.03 183.20 9,267.53 -3,541.70 -473.23 3,572.09 0.00 0.00 0.00 12,600.00 89.03 183.20 9,26		11 600 00	89.03	183.20	9,250.60	-2.543.40	-417.42	2,573.60	0.00	0.00	0.00	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$							100.00	0.070.45	0.00	0.00	0.00	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		11,700.00	89,03	183.20	9,252.29	-2,643.23	-423.00	2,673.45	0.00	0.00	0.00	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		11,800.00	89.03	183.20	9,203.99	-2,743.00	-420.00	2,773.30	0.00	0.00	0.00	
12,000.00 89.03 183.20 9,259.06 -3,042.55 -445.33 3,072.84 0.00 0.00 0.00 12,200.00 89.03 183.20 9,260.76 -3,142.38 -450.91 3,172.69 0.00 0.00 0.00 12,200.00 89.03 183.20 9,262.45 -3,242.21 -456.49 3,272.54 0.00 0.00 0.00 12,400.00 89.03 183.20 9,264.14 -3,342.04 -462.07 3,372.39 0.00 0.00 0.00 12,500.00 89.03 183.20 9,265.84 -3,441.87 -467.65 3,472.24 0.00 0.00 0.00 12,500.00 89.03 183.20 9,267.53 -3,541.70 -473.23 3,572.09 0.00 0.00 0.00 12,600.00 89.03 183.20 9,267.92 -3,641.52 -478.81 3,671.94 0.00 0.00 0.00 12,600.00 89.03 183.20 9,272.61 -3,641.52 -478.81 3,671.94 0.00 0.00 0.00 12,600.00 89.03 183.20 9,2		12,000,00	89.03	183.20	9,255.00	-2,042.09	-434.10	2,873.13	0.00	0.00	0.00	
12,00.00 89.03 183.20 9,260.76 -3,142.38 -450.91 3,172.69 0.00 0.00 0.00 12,300.00 89.03 183.20 9,262.45 -3,242.21 -456.49 3,272.54 0.00 0.00 0.00 0.00 12,400.00 89.03 183.20 9,264.14 -3,342.04 -462.07 3,372.39 0.00 0.00 0.00 12,500.00 89.03 183.20 9,265.84 -3,441.87 -467.65 3,472.24 0.00 0.00 0.00 12,600.00 89.03 183.20 9,267.53 -3,541.70 -473.23 3,572.09 0.00 0.00 0.00 12,600.00 89.03 183.20 9,269.22 -3,641.52 -478.81 3,671.94 0.00 0.00 0.00 12,600.00 89.03 183.20 9,270.92 -3,741.35 -484.40 3,771.79 0.00 0.00 0.00 12,900.00 89.03 183.20 9,272.61 -3,841.18 -489.98 3,871.63 0.00 0.00 0.00 12,900.00 89.03 183.20		12,000.00	89.03	183.20	9,259.06	-2,942.72	-445.33	3 072 84	0.00	0.00	0.00	
12,200.00 89.03 183.20 9,260.76 -3,142.38 -450.91 3,172.69 0.00 0.00 0.00 12,300.00 89.03 183.20 9,262.45 -3,242.21 -456.49 3,272.54 0.00 0.00 0.00 0.00 12,400.00 89.03 183.20 9,264.14 -3,342.04 -462.07 3,372.39 0.00 0.00 0.00 12,500.00 89.03 183.20 9,265.84 -3,441.87 -467.65 3,472.24 0.00 0.00 0.00 12,600.00 89.03 183.20 9,267.53 -3,541.70 -473.23 3,572.09 0.00 0.00 0.00 12,600.00 89.03 183.20 9,269.22 -3,641.52 -478.81 3,671.94 0.00 0.00 0.00 12,800.00 89.03 183.20 9,270.92 -3,741.35 -484.40 3,771.79 0.00 0.00 0.00 12,900.00 89.03 183.20 9,272.61 -3,841.18 -489.98 3,871.63 0.00 0.00 0.00 12,900.00 89.03 183.2		12,100.00	00.00	100.20	5,205.00	0,042.00	110.00	0,072.01	0.00	0.00	0.00	
12,300,00 89,03 183,20 9,262,45 -3,242,21 -456,49 3,272,54 0.00 0.00 0.00 12,400,00 89,03 183,20 9,264,14 -3,342,04 -462,07 3,372,39 0.00 0.00 0.00 12,500,00 89,03 183,20 9,265,84 -3,441,87 -467,65 3,472,24 0.00 0.00 0.00 12,600,00 89,03 183,20 9,267,53 -3,541,70 -473,23 3,572,09 0.00 0.00 0.00 12,600,00 89,03 183,20 9,269,22 -3,641,52 -478,81 3,671,94 0.00 0.00 0.00 12,800,00 89,03 183,20 9,270,92 -3,741,35 -484,40 3,771,79 0.00 0.00 0.00 12,900,00 89,03 183,20 9,272,61 -3,841,18 -489,98 3,871,63 0.00 0.00 0.00 12,900,00 89,03 183,20 9,274,30 -3,941,01 -495,56 3,971,48 0.00 0.00 0.00 13,000,00 89,03 183,20 9,2		12,200.00	89.03	183.20	9,260.76	-3,142.38	-450.91	3,172.69	0.00	0.00	0.00	
12,400.00 89.03 183.20 9,204.14 -3,342.04 -402.07 3,372.39 0.00 0.00 0.00 12,500.00 89.03 183.20 9,265.84 -3,441.87 -467.65 3,472.24 0.00 0.00 0.00 0.00 12,600.00 89.03 183.20 9,267.53 -3,541.70 -473.23 3,572.09 0.00 0.00 0.00 12,700.00 89.03 183.20 9,269.22 -3,641.52 -478.81 3,671.94 0.00 0.00 0.00 12,800.00 89.03 183.20 9,270.92 -3,741.35 -484.40 3,771.79 0.00 0.00 0.00 12,800.00 89.03 183.20 9,272.61 -3,841.18 -489.98 3,871.63 0.00 0.00 0.00 12,900.00 89.03 183.20 9,274.30 -3,941.01 -495.66 3,971.48 0.00 0.00 0.00 13,000.00 89.03 183.20 9,275.99 -4,040.84 -501.14 4,071.33		12,300.00	89.03	183.20	9,262.45	-3,242.21	-456.49	3,2/2.54	0.00	0.00	0.00	
12,00.00 69,03 163.20 9,263.64 -3,441.67 -407.65 3,472.24 0.00 0.00 0.00 12,600.00 89.03 183.20 9,267.53 -3,541.70 -473.23 3,572.09 0.00 0.00 0.00 0.00 12,700.00 89.03 183.20 9,269.22 -3,641.52 -478.81 3,671.94 0.00 0.00 0.00 12,800.00 89.03 183.20 9,270.92 -3,741.35 -484.40 3,771.79 0.00 0.00 0.00 12,900.00 89.03 183.20 9,272.61 -3,841.18 -489.98 3,871.63 0.00 0.00 0.00 13,000.00 89.03 183.20 9,272.61 -3,941.01 -495.66 3,971.48 0.00 0.00 0.00 13,000.00 89.03 183.20 9,275.99 -4,040.84 -501.14 4,071.33 0.00 0.00 0.00		12,400.00	89.03	103.20	9,204.14 0.265.04	-3,342.04 3 111 07	-402.U/	3,312.39	0.00	0.00	0.00	
12,00.00 89.03 183.20 9,269.22 -3,641.70 -473.23 3,572.09 0.00 0.00 0.00 12,700.00 89.03 183.20 9,269.22 -3,641.52 -478.81 3,671.94 0.00 0.00 0.00 0.00 12,800.00 89.03 183.20 9,270.92 -3,741.35 -484.40 3,771.79 0.00 0.00 0.00 12,900.00 89.03 183.20 9,272.61 -3,841.18 -489.98 3,871.63 0.00 0.00 0.00 13,000.00 89.03 183.20 9,272.430 -3,941.01 -495.56 3,971.48 0.00 0.00 0.00 13,100.00 89.03 183.20 9,275.99 -4,040.84 -501.14 4,071.33 0.00 0.00 0.00		12,500.00	89.03	183.20 193.20	9,∠00.04 0,267.52	-3,441.8/ -3.5/1.70	-401.05 _173.00	3,412.24	0.00	0.00	0.00	
12,700.00 89.03 183.20 9,269.22 -3,641.52 -478.81 3,671.94 0.00 0.00 0.00 12,800.00 89.03 183.20 9,270.92 -3,741.35 -484.40 3,771.79 0.00 0.00 0.00 12,900.00 89.03 183.20 9,272.91 -3,841.18 -489.98 3,871.63 0.00 0.00 0.00 13,000.00 89.03 183.20 9,272.43 -3,941.01 -495.56 3,971.48 0.00 0.00 0.00 13,000.00 89.03 183.20 9,275.99 -4,040.84 -501.14 4,071.33 0.00 0.00 0.00		12,000.00	09.03	103.20	3,207.00	-3,341.70	-413.23	3,372.08	0.00	0.00	0.00	
12,800.00 89.03 183.20 9,270.92 -3,741.35 -484.40 3,771.79 0.00 0.00 0.00 12,900.00 89.03 183.20 9,272.61 -3,841.18 -489.98 3,871.63 0.00 0.00 0.00 13,000.00 89.03 183.20 9,274.30 -3,941.01 -495.56 3,971.48 0.00 0.00 0.00 13,100.00 89.03 183.20 9,275.99 -4,040.84 -501.14 4,071.33 0.00 0.00 0.00		12,700.00	89.03	183.20	9,269.22	-3,641.52	-478.81	3,671.94	0.00	0.00	0.00	
12,900.00 89.03 183.20 9,272.61 -3,841.18 -489.98 3,871.63 0.00 0.00 0.00 13,000.00 89.03 183.20 9,274.30 -3,941.01 -495.56 3,971.48 0.00 0.00 0.00 13,100.00 89.03 183.20 9,275.99 -4,040.84 -501.14 4,071.33 0.00 0.00 0.00		12,800.00	89.03	183.20	9,270.92	-3,741.35	-484.40	3,771.79	0.00	0.00	0.00	
13,000.00 89.03 183.20 9,274.30 -3,941.01 -495.56 3,971.48 0.00 0.00 0.00 13,100.00 89.03 183.20 9,275.99 -4,040.84 -501.14 4,071.33 0.00 0.00 0.00	{	12,900.00	89.03	183.20	9,272.61	-3,841.18	-489.98	3,871.63	0.00	0.00	0.00	
ן דאָדעט.טט צאַטאָד 183.20 אָן 183.20 אָן 12,5.99 -4,040.84 -501.14 4,071.33 0.00 0.00 0.00	.	13,000.00	89.03	183.20	9,274.30	-3,941.01	-495.56	3,971.48	0.00	0.00	0.00	
		13,100.00	89.03	183.20	9,275.99	-4,040.84	-501.14	4,0/1.33	0.00	0.00	0.00	

COMPASS 5000.1 Build 56

Pathfinder - A Schlumberger Company

Planning Report

(usft)	(°)	Azimutn (°)	(usft)	+r (u	v/-5 isft)	+E/-VV (usft)	(usft)	(°/100usft)	(°/100usft)	(°/100usft)
13,200.00	89.03	183.20	9,277.6	59 -4	,140.67	-506.72	4,171.18	0.00	0.00	0.00
13,300.00	89.03	183.20	9,279.3	38 -4	,240.50	-512.30	4,271.03	0.00	0.00	0.00
13,400.00	89.03	183.20	9,281.0	07 -4	,340.33	-517.88	4,370.88	0.00	0.00	0.00
13,500.00	89.03	183.20	9,282.	-4	,440.16	-523.47	4,470.73	0.00	0.00	0.00
13,600.00	89.03	183.20	9,284.4	+6 -4	,538.88	-529.05	4,570.57	0.00	0.00	0.00
13,700.00	89.03	183.20	9,286.1	15 -4	,639.82	-534.63	4,670.42	0.00	0.00	0.00
13,800.00	89.03	183.20	9,287.8	34 -4	,739.65	-540.21	4,770.27	0.00	0.00	0.00
13,900.00	89.03	183.20	9,289.5	54 -4	,839.48	-545.79	4,870.12	0.00	0.00	0.00
14,000.00	89.03	183.20	9,291.2	23 -4	,939.31	-551.37	4,969.97	0.00	0.00	0.00
14,100.00	89.03	183.20	9,292.9	92 -5	,039.14	-556.95	5,069.82	0.00	0.00	0.00
14,200.00	89.03	183.20	9,294.6	52 -5	,138.97	-562.53	5,169.67	0.00	0.00	0.00
14,281.80	89.03	183.20	9,296.0	00 -5	,220.63	-567.10	5,251.34	0.00	0.00	0.00
Design Targets	· · · ·	· ·			*				· ··· ·	
Target Name										
- hit/miss target	Dip Angle	Dip Dir.	TVD	+N/-S	+E/-W	Northin	ig Ea	sting		
- Shape	(°)	(°)	(usft)	(usft)	(usft)	(usft)	(1	usft)	Latitude	Longitude
LP - 1H	0.00	0.01	9,207.00	0.00	0.00	666,8	845.25 8	83,963.81	32° 49' 41.570 N	103° 13' 4.552 W
- plan misses tar - Point	get center by 266	.64usft at 907	9.51usft MD (9022.72 T	™D, -111.44 N	l, -157.22 Ej)			
Toe - Weissbeir 23 1 - plan hits target - Point	H 0.00 center	0.00	9,296.00	-5,220.63	-567.10	661,6	624.62 8	83,396.71	32° 48' 49.981 N	103° 13' 11.841 W
L'amation-	,- ·									
Formations						- N - 4		. .	-	· ·

,	Measured Depth (usft)	Vertical Depth (usft)	Name	Lithology	Dip (°)	Dip Direction (°)	
	2,218.00	2,218.00	Rustler		0.70	186.20	
	2,344.00	2,344.00	Top of Salt		0.70	186.20	
	3,504.00	3,504.00	Base of Salt		0.70	186.20	
	3,544.00	3,544.00	Yates		0.70	186.20	
	4,574.00	4,574.00	Queen		0.70	186.20	
	5,377.00	5,377.00	Grayburg		0.70	186.20	
	6,464.00	6,464.00	Brushy Canyon		0.70	186.20	
	6,779.00	6,779.00	1st BSPG Lime		0.70	186.20	
	8,684.29	8,684.04	1st BSPG Sand		0.70	186.20	
	9,318.01	9,157.73	2nd BSPG Sand		0.70	186.20	



HOBBS OCD

MAR 1 2 2014

RECEIVED

Commitment Runs Deep



Design Plan Operation and Maintenance Plan Closure Plan

SENM - Closed Loop Systems February 2014

I. Design Plan

Devon uses MI SWACO closed loop system (CLS). The MI SWACO CLS is designed to maintain drill solids at or below 5%. The equipment is arranged to progressively remove solids from the largest to the smallest size. Drilling fluids can thus be reused and savings is realized on mud and disposal costs. Dewatering may be required with the centrifuges to insure removal of ultra fine solids.

The drilling location is constructed to allow storm water to flow to a central sump normally the cellar. This insures no contamination leaves the drilling pad in the event of a spill. Storm water is reused in the mud system or stored in a reserve fluid tank farm until it can be reused. All lubricants, oils, or chemicals are removed immediately from the ground to prevent the contamination of storm water. An oil trap is normally installed on the sump if an oil spill occurs during a storm.

A tank farm is utilized to store drilling fluids including fresh water and brine fluids. The tank farm is constructed on a 20 ml plastic lined, bermed pad to prevent the contamination of the drilling site during a spill. Fluids from other sites may be stored in these tanks for processing by the solids control equipment and reused in the mud system. At the end of the well the fluids are transported from the tank farm to an adjoining well or to the next well for the rig.

Prior to installing a closed-loop system on site, the topsoil, if present, will be stripped and stockpiled for use as the final cover or fill at the time of closure.

Signs will be posted on the fence surrounding the closed-loop system unless the closed-loop system is located on a site where there is an existing well, that is operated by Devon.

II. Operations and Maintenance Plan

Primary Shakers: The primary shakers make the first removal of drill solids from the drilling mud as it leaves the well bore. The shakers are sized to handle maximum drilling rate at optimal screen size. The shakers normally remove solids down to 74 microns.

Mud Cleaner: The Mud Cleaner cleans the fluid after it leaves the shakers. A set of hydrocyclones are sized to handle 1.25 to 1.5 times the maximum circulating rate. This ensures all the fluid is being processed to an average cut point of 25 microns. The wet discharged is dewatered on a shaker equipped with ultra fine mesh screens and generally cut at 40 microns.



Centrifuges: The centrifuges can be one or two in number depending on the well geometry or depth of well. The centrifuges are sized to maintain low gravity solids at 5% or below. They may or may not need a dewatering system to enhance the removal rates. The centrifuges can make a cut point of 8-10 microns depending on bowl speed, feed rate, solids loading and other factors.

The centrifuge system is designed to work on the active system and be flexible to process incoming fluids from other locations. This set-up is also dependent on well factors.

Dewatering System: The dewatering system is a chemical mixing and dosing system designed to enhance the solids removal of the centrifuge. Not commonly used in shallow wells. It may contain pH adjustment, coagulant mixing and dosing, and polymer mixing and dosing. Chemical flocculation binds ultra fine solids into a mass that is within the centrifuge operating design. The

dewatering system improves the centrifuge cut point to infinity or allows for the return of clear water or brine fluid. This ability allows for the ultimate control of low gravity solids.

Cuttings Boxes: Cuttings boxes are utilized to capture drill solids that are discarded from the solids control equipment. These boxes are set upon a rail system that allows for the removal and replacement of a full box of cuttings with an empty one. They are equipped with a cover that insures no product is spilled into the environment during the transportation phase.

Process Tank: (Optional) The process tank allows for the holding and process of fluids that are being transferred into the mud system. Additionally, during times of lost circulation the process tank may hold active fluids that are removed for additional treatment. It can further be used as a mixing tank during well control conditions.

Sump and Sump Pump: The sump is used to collect storm water and the pump is used to transfer this fluid to the active system or to the tank for to hold in reserve. It can also be used to collect fluids that may escape during spills. The location contains drainage ditches that allow the location fluids to drain to the sump.

Reserve Fluids (Tank Farm): A series of frac tanks are used to replace the reserve pit. These are steel tanks that are equipped with a manifold system and a transfer pump. These tanks can contain any number of fluids used during the drilling process. These can include fresh water, cut brine, and saturated salt fluid. The fluid can be from the active well or reclaimed fluid from other locations. A 20 ml liner and berm system is employed to ensure the fluids do not migrate to the environment during a spill.

If a leak develops, the appropriate division district office will be notified within 48 hours of the discovery and the leak will be addressed. Spill prevention is accomplished by maintaining pump packing, hoses, and pipe fittings to insure no leaks are occurring. During an upset condition the source of the spill is isolated and repaired as soon as it is discovered. Free liquid is removed by a diaphragm pump and returned to the mud system. Loose topsoil may be used to stabilize the spill and the contaminated soil is excavated and placed in the cuttings boxes. After the well is finished and the rig has moved, the entire location is scrapped and testing will be performed to determine if a release has occurred.

All trash is kept in a wire mesh enclosure and removed to an approved landfill when full. All spent motor oils are kept in separate containers and they are removed and sent to an approved recycling center. Any spilled lubricants, pipe dope, or regulated chemicals are removed from soil and sent to landfills approved for these products.

These operations are monitored by Mi Swaco service technicians. Daily logs are maintained to ensure optimal equipment operation and maintenance. Screen and chemical use is logged to maintain inventory control. Fluid properties are monitored and recorded and drilling mud volumes are accounted for in the mud storage farm. This data is kept for end of well review to insure performance goals are met. Lessons learned are logged and used to help with continuous improvement.

A MI SWACO field supervisor manages from 3-5 wells. They are responsible for training personnel, supervising installations, and inspecting sites for compliance of MI SWACO safety and operational policy.

III. Closure Plan

A maximum 340' X 340' caliche pad is built per well. All of the trucks and steel tanks fit on this pad. All fluid cuttings go to the steel tanks to be hauled by various trucking companies to an agency approved disposal.