	•			
Submit 1 Copy To Appropriate District Office <u>District I</u> – (575) 393-6161 1625 N. French Dr., Hobbs, NM 88240 <u>District II</u> – (575) 748-1283 811 S. First St., Artesia, NM 88210 <u>District III</u> – (505) 334-6178 1000 Rio Brazos Rd., Aztec, NM 87410 DEC 2	State of New Mer	kico		Form C-103
District I $-$ (575) 393-6161	Energy Minerals and Natur	al Resources		ised August 1, 2011
1625 N. French Dr., Hobbs, NM 88240	00**		WELL API NO.	
<u>District II</u> – (575) 748-1283 811 S. First St., Artesia, NM 88210	OIL CONSERVATION	DIVISION	<u>30-025-40719</u>	
District III - (505) 334-6178	6201220 South St. Fran	cis Dr.	5. Indicate Type of Lease STATE 🛛	FEE
1625 N. French Dr., Hobbs, NM 88240 <u>District II</u> – (575) 748-1283 811 S. First St., Artesia, NM 88210 <u>District III</u> – (505) 334-6178 1000 Rio Brazos Rd., Aztec, NM 87410 <u>District IV</u> – (505) 476-3460 1220 S. St. Francis Dr., Santa Fe, NM	Santa Fe, NM 87:	505	6. State Oil & Gas Lease	
1220 S. St. Francis Dr., Santa Fe, NM	6201220 South St. France ENED ^{anta} Fe, NM 87:			
87505 PEV	ND REPORTS ON WELLS		7. Lease Name or Unit A	areement Name
(DO NOT USE THIS FORM FOR PROPOSALS T	O DRILL OR TO DEEPEN OR PLU		7. Lease Name of Omr A	greement rame
DIFFERENT RESERVOIR. USE "APPLICATION PROPOSALS.)	FOR PERMIT" (FORM C-101) FOI	R SUCH	THISTLE UNIT	
1. Type of Well: Oil Well 🛛 Gas W	/ell 🗍 Other		8. Well Number 34H	
2. Name of Operator	kernel		9. OGRID Number	
DEVON ENERGY PRODUCTION CO.,	<u>L</u> .P.		6137	
3. Address of Operator 333 W. SHERIDAN AVE., OKLAHOM	A CITY OF HACNAN 72100	5010	10. Pool name or Wildcat	
4. Well Location			BRINNINSTOOL; DELA	
	fact from the COUTH	11	foot for a dire . WE	
Unit Letter <u>N</u> : <u>350</u>	feet from the <u>SOUTH</u>		feet from the <u>_WES</u>	
Section 33	Township 23S Elevation (Show whether DR,	Range 33E	NMPM LEA	County
366		кк <i>д</i> , к <i>1</i> , Ок, <i>еіс.)</i>		
12. Check Appro	priate Box to Indicate Na	ture of Notice, I	Report or Other Data	
	•		*	
			SEQUENT REPORT	
		REMEDIAL WORK		
	NGE PLANS	COMMENCE DRIL CASING/CEMENT		A L
		CASING/GEMENT	JOD []	
OTHER: Surface Hole Re-Stake		OTHER: DRILLIN		
13. Describe proposed or completed or of starting any proposed work). S				
proposed completion or recomplet		For Multiple Con	npretions: Attach wendore	diagram of
proposed completion of recomple				
Designed and the Cold Designed full			a lugation within a sting 22. T	
Devon Energy Production Co., L.P. respectfully 33E from: 350 FSL & 2075 FWL to 355 FSL &	1525 FWL. Also, Devon respec	tfully requests approv	val to change the proposed der	oth from 12,316' to
13,363' and the target formation from Brinninst	ool; Delaware to Madera Sand.		······································	····, · · · · · · · · · · · · · · · · ·
See attached revised C-102, Drill Plan & Direct	ion Survey			
see attached revised C-102, Dim Fian & Direct	ion Survey.			
				·
I hereby certify that the information above is true and	complete to the best of my knowledg	e and belief.		
SIGNATURE / the Com	TITLE Regulatory Specialist	DATE1	2/26/2014	
Type or print name <u>David H. Cook</u>	E-mail address: <u>david.cook@dv</u>	n.com PHON	E: <u>(405) 552-7848</u>	
For State Use Only				
APPROVED BY:	TITLE Petroleum Engi	neer DATE	12/99/12	
Conditions of Approval (if any):		· · · · · · · · · · · · · · · · · · ·		
Les la company de				

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DEC 29 2014

Devon Energy, Thistle Unit 34H

1. Geologic Formations

TVD of target 8,734'		Pilot hole depth	N/A
MD at TD:	13,363'	Deepest expected fresh water:	

Basin

Formation	Depth (TVD) from KB	Water/Mineral Bearing/ Target Zone?	Hazards*
Rustler	1,300	Fresh Water	
Top of Salt	1,547		
Delaware	5,161	Oil/Gas	
Cherry Canyon	6,133	Oil/Gas	
Brushy Canyon	7,464	Oil/Gas	
Madera	8,707	Oil/Gas	

*H2S, water flows, loss of circulation, abnormal pressures, etc.

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Hole Size	Casing	Interval	Csg.	Weight	Grade	Conn	SF	SF Burst	SF
	From	То	Size .	(lbs)			Collapse		Tension.
17.5"	0	1,350'	13.375"	54.5	H-40	STC	1.25	2.80	4.97
12.25"	0	4,300'	9.625"	40	J-55	BTC	1.15	1.40	2.30
	4,300'	5,100'	9.625"	40	J-55	BTC	1.58	1.47	4.50
Option #1									
8.75"	0	8,220'	7"	29	HCP-110	BTC	2.34	2.86	3.32
8.75"	8,220'	13,363'	5.5"	17	HCP-110	BTC	2.05	2.55	6.48
Option #2									
8.75"	0	13,363'	5.5"	17	HCP-110	BTC	2.5	2.55	2.05
	•	· · · · · · · · · · · · · · · · · · ·		BLM Min	imum Safety	y Factor	1.125	1.00	1.6 Dry
									1.8 Wet

2. Casing Program

All casing strings will be tested in accordance with Onshore Oil and Gas Order #2 III.B.1.h

Must have table for contingency casing

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	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Does casing meet API specifications? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide	Y
justification (loading assumptions, casing design criteria).	
Will the intermediate pipe be kept at a minimum 1/3 fluid filled to avoid approaching	Y
the collapse pressure rating of the casing?	
Is well located within Capitan Reef?	<u>N</u>
If yes, does production casing cement tie back a minimum of 50' above the Reef?	
Is well within the designated 4 string boundary.	Section of the sector of the sector
Is well located in SOPA but not in R-111-P?	N
If yes, are the first 2 strings cemented to surface and 3 rd string cement tied back	
500' into previous casing?	
Is well located in R-111-P and SOPA?	l n
If yes, are the first three strings cemented to surface?	
Is 2 nd string set 100' to 600' below the base of salt?	
Is well located in high Cave/Karst?	N
If yes, are there two strings cemented to surface?	
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
La well located in critical Cave/Karst?	N
Is well located in critical Cave/Karst?	N
If yes, are there three strings cemented to surface?	

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2. Cementing Program

String	Number of sx	Weight Ibs/gal	Yield cf/sx	Water Volu me g/sx	500# Comp. Strength (hours)	Slurry Description				
13-3/8"	690	13.5	1.72	9.07	12	Class C Cement + 0.125 lbs/sack Pol-E-Flake + 4% bwoc Bentonite				
Surface	550	14.8	6.32	1.33	7	Class C Cement + 0.125 lbs/sack Poly-E-Flake				
13-3/8"	450	13.5	1.72	9.07	12	Class C Cement + 0.125 lbs/sack Pol-E-Flake + 4% bwoc Bentonite				
Surface	550	14.8	6.32	1.33	7	Class C Cement + 0.125 lbs/sack Poly-E-Flake				
Two Stage Option		DV Tool = 300ft								
	320	14.8	6.32	1.33	7	Class C Cement + 0.125 lbs/sack Poly-E-Flake + 63.5% Fresh Water				
9-5/8" Intermediate	1070	12.9	9.81	1.85	15	(65:35) Class C Cement: Poz (Fly Ash): 6% BWOC Bentonite + 5% BWOW Sodium Chloride + 0.125 Ibs/sack Poly-E-Flake				
	430	14.8	6.32	1.33	6	Class C Cement + 0.125 lbs/sack Poly-E-Flake +				
	960	12.9	9.81	1.85	15	(65:35) Class C Cement: Poz (Fly Ash): 6% BWOC Bentonite + 5% BWOW Sodium Chloride + 0.125 Ibs/sack Poly-E-Flake				
9-5/8"	220	14.8	6.32	1.33	6	Class C Cement + 0.125 lbs/sack Poly-E-Flake				
Intermediate Two Stage				<u> </u>	DV Too	l = 1400ft				
Option	170	12.9	9.81	1.85	15	(65:35) Class C Cement: Poz (Fly Ash): 6% BWOC Bentonite + 5% BWOW Sodium Chloride + 0.125 Ibs/sack Poly-E-Flake				
	140	14.8	6.32	1.33	6	Class C Cement + 0.125 lbs/sack Poly-E-Flake				

Devon Energy, Thistle Unit 34H

7 x 5-1/2"	220	10.4	16.9	3.17	16	Tuned Light * + 0.125 lb/sk Pol-E-Flake
Production Casing	1290	14.5	5.31	1.2	25	(50:50) Class H Cement: Poz (Fly Ash) + 0.5% bwoc HALAD-344 + 0.4% bwoc CFR-3 + 0.2% bwoc HR-601 + 2% bwoc Bentonite
	220	11.9	12.89	2.26	n/a	(50:50) Class H Cement: Poz (Fly Ash) + 10% BWOC Bentonite + 1 lb/sk of Kol-Seal + 0.3% BWOC HR-601 + 0.5lb/sk D-Air 5000
5-1/2" Production	330	12.5	10.86	1.96	30	(65:35) Class H Cement: Poz (Fly Ash) + 6% BWOC Bentonite + 0.25% BWOC HR-601 + 0.125 lbs/sack Poly- E-Flake
Casing	1290	14.5	5.31	1.2	25	(50:50) Class H Cement: Poz (Fly Ash) + 0.5% bwoc HALAD-344 + 0.4% bwoc CFR-3 + 0.2% bwoc HR-601 + 2% bwoc Bentonite

DV tool depth(s) will be adjusted based on hole conditions and cement volumes will be adjusted proportionally. DV tool will be set a minimum of 50 feet below previous casing and a minimum of 200 feet above current shoe. Lab reports with the 500 psi compressive strength time for the cement will be onsite for review.

Casing String	TOC	% Excess
13-3/8" Surface	0'	100%
13-3/8" Surface Two Stage	Stage #1 = 300' / Stage #2 = 0'	100%
9-5/8" Intermediate	0'	75%
9-5/8" Intermediate Two Stage	Stage#1 = 1400' / Stage #2 = 0'	75%
7 x 5-1/2" Production	4600′	25%
5-1/2" Production	4600'	25%

4. Pressure Control Equipment

N A variance is requested for the use of a diverter on the surface casing.

BOP installed and tested before drilling which hole?	Size?	Min. Required WP	T	уре		Tested to:
				nular	x	50% of working pressure
			Blind	l Ram		
12-1/4"	13-5/8"	3M		Ram		3M
			Doub	le Ram	x	5.01
			Other*			
	13-5/8"	3М	Annular		x	50% testing pressure
			Blind Ram			
8-3/4"			Pipe Ram			
			Double Ram		x	3M
			Other *			
			Anı	nular		
			Blind Ram			
			Pipe Ram			
			Double Ram			
			Other			
			*			

*Specify if additional ram is utilized.

BOP/BOPE will be tested by an independent service company to 250 psi low and the high pressure indicated above per Onshore Order 2 requirements. The System may be upgraded to a higher pressure but still tested to the working pressure listed in the table above. If the system is upgraded all the components installed will be functional and tested.

Pipe rams will be operationally checked each 24 hour period. Blind rams will be operationally checked on each trip out of the hole. These checks will be noted on the daily tour sheets. Other accessories to the BOP equipment will include a Kelly cock and floor safety valve (inside BOP) and choke lines and choke manifold.

Y	Formation integrity test will be performed per Onshore Order #2. On Exploratory wells or on that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Will be tested in accordance with Onshore Oil and Gas Order #2 III.B.1.i.
Y	A variance is requested for the use of a flexible choke line from the BOP to Choke Manifold. See attached for specs and hydrostatic test chart.

Devon Energy, Thistle Unit 34H

	Y Are anchors required by manufacturer?						
Y	A multibowl wellhead is being used. The BOP will be tested per Onshore Order #2 after						
1	installation on the surface casing which will cover testing requirements for a maximum of 30 days. If any seal subject to test pressure is broken the system must be tested.						
	 Devon proposes using a multi-bowl wellhead assembly (FMC Uni-head). This assembly will only be tested when installed on the surface casing. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be 3000 (3M) psi. Wellhead will be installed by FMC's representatives. If the welding is performed by a third party, the FMC's representative will monitor the temperature to verify that it does not exceed the maximum temperature of the seal. 						
	 FMC representative will install the test plug for the initial BOP test. FMC will install a solid steel body pack-off to completely isolate the lower head after cementing intermediate casing. After installation of the pack-off, the pack-off and the lower flange will be tested to 3M, as shown on the attached schematic. Everything above the pack-off will not have been altered whatsoever from the initial nipple up. Therefore the BOP components will not be retested at that time. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head will be cut and top out operations will be conducted. Devon will pressure test all scals above and below the mandrel (but still above the casing) to full working pressure rating. Devon will test the casing to 0.22 psi/ft or 1500 psi, whichever is greater, as per Onshore Order #2. 						
	After running the 13-3/8" surface casing, a 13-5/8" BOP/BOPE system with a minimum rating of 3M will be installed on the FMC Uni-head wellhead system and will undergo a 250 psi low pressure test followed by a 3,000 psi high pressure test. The 3,000 psi high and 250 psi low test will cover testing requirements a maximum of 30 days, as per Onshore Order #2. If the well is not complete within 30 days of this BOP test, another full BOP test will be conducted, as per Onshore Order #2. After running the 9-5/8' intermediate casing with a mandrel hanger, the 13-5/8" BOP/BOPE system with a minimum rating of 3M will already be installed on the FMC Uni-head.						
	The pipe rams will be operated and checked each 24 hour period and each time the drill pipe is out of the hole. These tests will be logged in the daily driller's log. A 2" kill line and 3" choke line will be incorporated into the drilling spool below the ram BOP. In addition to the rams and annular preventer, additional BOP accessories include a kelly cock, floor safety valve, choke lines, and choke manifold rated at 3,000 psi WP.						
	Devon requests a variance to use a flexible line with flanged ends between the BOP and the choke manifold (choke line). The line will be kept as straight as possible with minimal turns						

		 -			
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					1
					1

5. Mud Program

	Depth	Туре	Weight (ppg)	Viscosity	Water Loss
From	To				
0	1,350'	FW Gel	8.6-8.8	28-34	N/C
1,350'	5,100'	Saturated Brine	10.0-10.2	28-34	N/C
5,100'	13,363'	Cut Brine	8.5-9.3	28-34	N/C

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times.

What will be used to monitor the loss or gain	PVT/Pason/Visual Monitoring
of fluid?	

6. Logging and Testing Procedures

Log	ging, Coring and Testing.
x	Will run GR/CNL fromTD to surface (horizontal well - vertical portion of hole). Stated
	logs run will be in the Completion Report and submitted to the BLM.
-	No Logs are planned based on well control or offset log information.
	Drill stem test? If yes, explain
	Coring? If yes, explain

Add	litional logs planne	d Interval
	Resistivity	Int. shoe to KOP
	Density	Int. shoe to KOP
X	CBL	Production casing
X	Mud log	Intermediate shoe to TD
	PEX	

Devon Energy, Thistle Unit 34H

7. Drilling Conditions

Condition	Specify what type and where?
BH Pressure at deepest TVD	3930 psi
Abnormal Temperature	No

Mitigation measure for abnormal conditions. Describe. Lost circulation material/sweeps/mud scavengers.

Hydrogen Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the operator will comply with the provisions of Onshore Oil and Gas Order #6. If Hydrogen Sulfide is encountered, measured values and formations will be provided to the BLM.

N	H2S is present
Y	H2S Plan attached

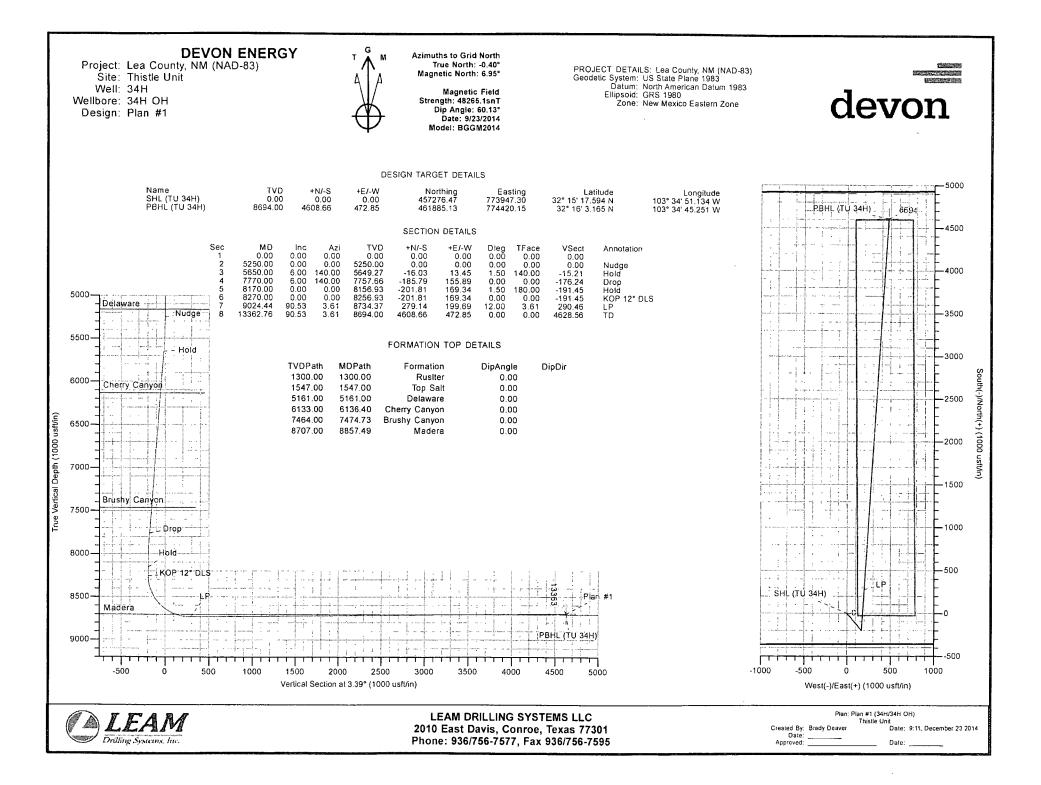
8. Other facets of operation

Is this a walking operation? No. Will be pre-setting casing? No.

Attachments

<u>x</u> Directional Plan Other, describe

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DEVON ENERGY

Lea County, NM (NAD-83) Thistle Unit 34H

34H OH

Plan: Plan #1

Standard Planning Report

23 December, 2014



	AM	r	LEAM	Drilling Systems	LLC		1020 1710-1710 1710-1710 1710-1710
	stems, Inc.			Planning Report			devon
Database: Company:	يني ها مريد ايري ها مريد الحرومي	0.1 Single User D NERGY		Local Co-ordinate R	1 S	Well 34H H&P 394: 3665' GL + 25' F	RKB @
Proječť:	Lea Count	ty, NM (NAD-83)		MD Reference:		3690.00usft (Original Well H&P 394: 3665' GL + 25' F 3690.00usft (Original Well	RKB @
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Design:	Plan #1					a dana mananan disebut disebut yang ang mang ming ming	er efter a 1911 en efter a straditueren aus er
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Vudit Notes: Version: Vertical Section; Measured Depth (usft) 0.00 5,250.00	Plan #1	EGM2014 Depth F (((((((((((((((((((9/23/2014 Phase: rom (TVD) isft) .00 	C(1) 7.35 PLAN +N/-S (usft) 0.00 ↓E/-W (usft) Dogleg (?/100usft) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00	Tie On Depth: +E/-W (usft) 0.00 Build Rate) (7/100usft) 00 0.00 00 0.00	0.00 Direction (?) 3.39 Turn Prate (?) (?) 0.00 0.4 0.00 0.4	(mT) 48,265
Audit Notes: Version: Vertical Section; Measured Depth (usft) 0.00 5,250.00 5,650.00	Plan #1	EGM2014 Depth F (((() () () () () () () () () () ()	9/23/2014 Phase: rom (TVD) isft) .00 .00 .00 .00 .00 .00 .00 .0	F(1) 7.35 PLAN +N/-S (usft) 0.00 4E/-W (usft) (?/100usft) 0.00 0.00 0.00 0.00 13.45 1.	Tie On Depth: +E/-W (usft) 0.00 Build Pate , (*/100usft) 00 0.00 00 0.00 50 1.50	0.00 Direction (?) 3.39 Turn (?/100ust) (?) 0.00 0.4 0.00 0.4 0.00 140.4	(m) 48,265
Audit Notes: Version: Vertical Section; Measured Depth (usft) 0.00 5,250.00 5,650.00 7,770.00	Plan #1 Plan #1 Az 0.00 0.00 6.00 6.00	EGM2014 Depth F (((() () () () () () () () () () ()	9/23/2014 Phase: rom (TVD) isft) .00 .00 .00 .00 .00 .00 .00 .0	F(1) 7.35 PLAN +N/-S (usft) 0.00 E/W E/W (//100usft) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.13.45 1. 155.89 0.	Tie On Depth: +E/-W (usft) 0.00 Build FRate) (*/100usft) 00 0.00 00 0.00 50 1.50 00 0.00	0.00 Direction (?) 3.39 Turn (?)100ust) (?) 0.00 0.4 0.00 0.4 0.00 140.4 0.00 0.4	(m) 48,265
Audit Notes: Audit Notes: /ertical Section; /ertical Section; Measured Depth (usft) 0.00 5,250.00 5,650.00 7,770.00 8,170.00	Plan #1 Plan #1 Plan #1	EGM2014 Depth F ((((((() () () () () () ()	9/23/2014 Phase: rom (ITVD) isft) .00 .00 .00 .00 .00 .00 .00 .0	2-(1) 7.35 PLAN +N/-S (usft) 0.00 +E/-W (usft) (?/100usft 0.00 0. 0.00 0. 0.00 0. 13.45 1. 155.89 0. 169.34 1.	Tie On Depth: +E/-W (usft) 0.00 Build Rates) (*/100usft) 00 0.00 00 0.00 00 0.00 50 1.50 00 0.00 50 1.50	0.00 Direction (?) 3.39 Turn (?) 0.00 0.1 0.00 0.1 0.00 0.1 0.00 140.1 0.00 140.1 0.00 0.1	(m) <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u></u>
Design Audit Notes: /ersion: /ertical Section; /ertical Section; /	Plan #1 Plan #1 Plan #1	EGM2014 Depth F (() () () () () () () () () () () () (9/23/2014 Phase: rom (TVD) isft) .00 .00 .00 .00 .00 .00 .00 .0	7.35 7.35 PLAN +N/-S (usft) 0.00 +E/-W (usft) (?/100usft (?/100usft 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	Tie On Depth: +E/-W (usft) 0.00 Build Rates) (*/100usft) 00 0.00 00 0.00 00 0.00 50 1.50 00 0.00 50 1.50 00 0.00	0.00 0.00 Direction (?) 3.39 Turn Turn (?) 0.00	(m) <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>5</u>
Design Audit Notes: Version: Vertical Section; Plan Sections Measured Dopth (usft) Incli (usft) 0.00 5,250.00 5,650.00 7,770.00 8,170.00	Plan #1 Plan #1 Plan #1	EGM2014 Depth F (() () () () () () () () () () () () ()	9/23/2014 Phase: rom (ITVD) isft) .00 .00 .00 .00 .00 .00 .00 .0	7.35 7.35 PLAN +N/-S (usft) 0.00 +E/-W (usft) (?/100usft (?/100usft 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	Tie On Depth: +E/-W (usft) 0.00 Build Rates) (*/100usft) 00 0.00 00 0.00 00 0.00 50 1.50 00 0.00 50 1.50 00 0.00	0.00 0.00 Direction (?) 3.39 Turn Turn (?) 0.00	(nT) <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>48,265</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u> <u>50</u>

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Planning Report



Database: EDM 5000.1 Single User Db	Local Co-ordinate Reference: Well 34H
Company: DEVON ENERGY	TVD Reference: H&P 394: 3665' GL + 25' RKB @
Project: Lea County, NM (NAD-83)	3690.00usft (Original Well Elev) MDReference: H&P 394: 3665' GL + 25' RKB @
Site:	3690.00usft (Original Well Elev)
Well:	Survey Calculation Method: Minimum Curvature
Wellbore: 34H OH	
Design	

ned Survey	an tha ann								
Measured			Vertical			Vertical	Dögleg	Build	Turn
Depth	Inclination	Azimuth	Depth	+N/-S	+E/-W	Section	Rate	Rate	Rate
(usft)	(*)	(°)	(usft)	(usft)	(usft)	(usft)	(°/100usft)	(°/100usft)	(°/100usft)
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
SHL (TU 34									
100.00	0.00	0.00	100.00	0.00	0.00	0.00	0.00	0.00	0.00
200.00	0.00	0.00	200.00	0.00	0.00	0.00	0.00	0.00	0.00
300.00 400.00	0.00 0.00	0.00 0.00	300.00 400.00	0.00 0.00	0.00 0.00	0,00 0.00	0.00 0.00	0.00 0.00	0.00 0.00
500.00 600.00	0.00 0.00	0.00 0.00	500.00 600.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00
700.00	0.00	0.00	700.00	0.00	0.00	0.00	0.00	0.00	0.00
800.00	0.00	0.00	800.00	0.00	0.00	0.00	0.00	0.00	0.00
900.00	0.00	0.00	900.00	0.00	0.00	0.00	0.00	0.00	0.00
1,000.00	0.00	0.00	1,000.00	0.00	0.00	0.00	0.00	0.00	0.00
1,100.00	0.00	0.00	1,100.00	0.00	0.00	0.00	0.00	0.00	0.00
1,200.00	0.00	0.00	1,200.00	0.00	0.00	0.00	0.00	0.00	0.00
1,300.00	0.00	0.00	1,300.00	0.00	0.00	0.00	0.00	0.00	0.00
Rusiter									
1,400.00	0.00	0.00	1,400.00	0.00	0.00	0.00	0.00	0.00	0.00
1,500.00	0.00	0.00	1,500.00	0.00	0.00	0.00	0.00	0.00	0.00
1,547.00	0.00	0.00	1,547.00	0.00	0.00	0.00	0.00	0.00	0.00
Top Salt									
1,600.00	0.00	0.00	1,600.00	0.00	0.00	0.00	0.00	0.00	0.00
1,700.00	0.00	0.00	1,700.00	0.00	0.00	0.00	0.00	0.00	0.00
1,800.00	0.00	0.00	1,800.00	0.00	. 0.00	0.00	0.00	0.00	0.00
1,900.00	0.00	0.00	1,900.00	0.00	0.00	0.00	0.00	0.00	0.00
2,000.00	0.00	0.00	2,000.00	0.00	0.00	0.00	0.00	0.00	0.00
2,100.00	0.00	0.00	2,100.00	0.00	0.00	0.00	0.00	0.00	0.00
2,200.00 2,300.00	0.00 0.00	0.00 0.00	2,200.00 2,300.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00
2,400.00	0.00	0.00	2,400.00	0.00	0.00	0.00	0.00	0.00	0.00
2,500.00 2,600.00	0.00 0.00	0.00 0.00	2,500.00 2,600.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00
2,700.00	0.00	0.00	2,700.00	0.00	0.00	0.00	0.00	0.00	0.00
2,800.00	0.00	0.00	2,800.00	0.00	0.00	0.00	0.00	0.00	0.00
2,900.00	0.00	0.00	2,900.00	0.00	0.00	0.00	0.00	0.00	0.00
3,000.00	0.00	0.00	3,000.00	0.00	0.00	0.00	0.00	0.00	0.00
3,100.00	0.00	0.00	3,100.00	0.00	0.00	0.00	0.00	0.00	0.00
3,200.00	0.00	0.00	3,200.00	0.00	0.00	0.00	0.00	0.00	0.00
3,300.00	0.00	0.00	3,300.00	0.00	0.00	0.00	0.00	0.00	0.00
3,400.00	0.00	0.00	3,400.00	0.00	0.00	0.00	0.00	0.00	0.00
3,500.00	0.00	0.00	3,500.00	0.00	0.00	0.00	0.00	0.00	0.00
3,600.00	0.00	0.00	3,600.00	0.00	0.00	0.00	0.00	0.00	0.00
3,700.00	0.00	0.00	3,700.00	0.00	0.00	0.00	0.00	0.00	0.00
3,800.00	0.00	0.00	3,800.00	0.00	0.00	0.00	0.00	0.00	0.00
3,900.00	0.00	0.00	3,900.00	0.00	0.00	0.00	0.00	0.00	0.00
4,000.00	0.00	0.00	4,000.00	0.00	0.00	0.00	0.00	0.00	0.00
4,100.00	0.00	0.00	4,100.00	0.00	0.00	0.00	0.00	0.00 0.00	0.00 0.00
4,200.00 4,300.00	0.00 0.00	0.00 0.00	4,200.00 4,300.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00	0.00
4,400.00	0.00	0.00	4,400.00	0.00	0.00	0.00	0.00	0.00	0.00
4,500.00 4,600.00	0.00	0.00	4,500.00 4,600.00	0.00	0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00
4 000 00	0.00	0.00	4,000.00	0.00	0.00	0.00	0.00	0.00	0.00

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COMPASS 5000.1 Build 74



Planning Report



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Database: EDM 5000.1 Single User Db	Local Co-ordinate Reference:	
Company:	TVD Reference: H&P 394: 3665' GL + 25' RKB @	
	3690.00usft (Original Well Elev)	
Project: Lea County, NM (NAD-83)	MD Reference: H&P 394: 3665' GL + 25' RKB @	
	3690.00usft (Original Well Elev)	
Site:	North Reference: Grid	
Well: 34H	Survey Calculation Method: Minimum Curvature	
Wellbore: 34H OH		
Design: Plan #1		
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Planned Survey	r suise anna an Stàiseanna an S	e i ^{for} t Handleren (* 1977) 1977 - Sander (* 1977)	. A Partitud I An and an an	Carl Andrews		a an	nin <u>- Stan</u> in	en e	
Measured			Vertical			Vertical	Dogleg	Build	Turn
Depth	Inclination	Azimuth	Depth	+N/-S	+E/-W	Section	Rate	Rate	Rate
(usft)	(°)	NATION AND AND AND AND AND AND AND AND AND AN	(usft)	(usft)	S.A. 1. 1. 1. 1. 1.	(usft)	(°/100usft)		(°/100usft)
4,800.00	***\۵۰۵ 0.00	0.00	4,800.00	0.00	1448-000 000 0000 0.00	0.00	0.00	0.00	0.00
					0.00				
4,900.00	0.00	0.00	4,900.00	0.00	0.00	0.00	0.00	0.00	0.00
5,000.00	0.00	0.00	5,000.00	0.00	0.00	0.00	0.00	0.00	0.00
5,100.00 5,161.00	0.00 0.00	0.00 0.00	5,100.00 5,161.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00
Delaware	0.00	0.00	5,101.00	0.00	0.00	0.00	0.00	0.00	0.00
5,200.00	0.00	0.00	5,200.00	0.00	0.00	0.00	0.00	0.00	0.00
5,250.00	0.00	0.00	5,250.00	0.00	0.00	0.00	0.00	0.00	0.00
Nudge	0.75	140.00	E 200.00	0.05		0.24	1.50	1.50	0.00
5,300.00 5,400.00	0.75 2.25	140.00 140.00	5,300.00 5,399.96	-0.25 -2.26	0.21 1.89	-0.24 -2.14	1.50 1.50	1.50 1.50	0.00 0.00
5,500.00	3.75	140.00	5,499.82	-2.26	5.26	-2.14	1.50	1.50	0.00
5,600.00	5.25	140.00	5,599.51	-12.28	10.30	-11.64	1.50	1.50	0.00
5,650.00	6.00	140.00	5,649.27	-16.03	13.45	-15.21	1.50	1.50	0.00
Hold 5,700.00	6.00	140.00	5,699.00	-20.03	16.81	-19.00	0.00	0.00	0.00
5,800.00	6.00	140.00	5,798.45	-20.03	23,53	-19.00	0.00	0.00	0.00
5,900.00	6.00	140.00	5,897.90	-36.05	30.25	-34.20	0.00	0.00	0.00
6,000.00	6.00	140.00	5,997.35	-44.06	36.97	-41.79	0.00	0.00	0.00
6,100.00	6.00	140.00	6,096.80	-52.06	43,69	-49.39	0.00	0.00	0.00
6,136.40	6.00	140.00	6,133.00	-52.08	45.69	-49.39 -52.15	0.00	0.00	0.00
Cherry Cany		140.00	0,100.00	-34.30	40.15	-52.15	0.00	0.00	0.00
6,200.00	6.00	140.00	6,196.26	-60.07	50,40	-56.98	0.00	0.00	0.00
6,300.00	6.00	140.00	6,295.71	-68.08	57.12	-64.58	0.00	0.00	0.00
6,400.00	6.00	140.00	6,395.16	-76.08	63.84	-72.18	0.00	0.00	0.00
6,500.00	6.00	140.00	6,494.61	-84.09	70,56	-79.77	0.00	0.00	0.00
6,600.00	6.00	140.00	6,594.07	-92.10	77.28	-87.37	0.00	0.00	0.00
6,700.00	6.00	140.00	6,693.52	-100.11	84.00	-94,96	0.00	0.00	0.00
6,800.00	6.00	140.00	6,792.97	-108,11	90.72	-102.56	0.00	0.00	0.00
6,900.00	6.00	140.00	6,892.42	-116.12	97.44	-110.16	0,00	0.00	0.00
7,000.00	6.00	140.00	6,991.87	-124.13	104,16	-117.75	0.00	0.00	0.00
7,100.00	6.00	140.00	7,091.33	-132.14	110.88	-125.35	0.00	0.00	0.00
7,200.00	6.00	140.00	7,190.78	-140.14	117,59	-132.94	0.00	0.00	0.00
7,300.00	6.00	140.00	7,290.23	-148.15	124.31	-140.54	0.00	0.00	0.00
7,400.00	6.00	140.00	7,389.68	-156.16	131.03	-148.14	0.00	0.00	0.00
7,474.73	6.00	140.00	7,464.00	-162.14	136.05	-153.81	0.00	0.00	0.00
Brushy Cany	/on								
7,500.00	6.00	140.00	7,489.13	-164.17	137.75	-155.73	0.00	0.00	0.00
7,600.00	6.00	140.00	7,588.59	-172.17	144.47	-163.33	0.00	0.00	0.00
7,700.00	6.00	140.00	7,688.04	-180.18	151.19	-170.92	0.00	0.00	0.00
7,770.00	6.00	140.00	7,757.66	-185.79	155.89	-176.24	0.00	0.00	0.00
Drop									
7,800.00	5.55	140.00	7,787.50	-188.10	157,83	-178.44	1.50	-1.50	0.00
7,900.00	4.05	140.00	7,887.15	-194.51	163.21	-184.52	1.50	-1.50	0.00
8,000.00	2.55	140.00	7,986.98	-198.92	166.91	-188.70	1.50	-1.50	0.00
8,100.00	1.05	140.00	8,086.93	-201.32	168.93	-190.98	1,50 1,50	-1.50 -1.50	0.00 0.00
8,170.00	0.00	0.00	8,156.93	-201.81	169.34	-191.45	1.50	-1.50	0.00
Hold			1. Sec. 1. Sec		·				
8,200.00	0.00	0.00	8,186.93	-201.81	169.34	-191.45	0.00	0.00	0.00
8,270.00	0.00	0.00	8,256.93	-201.81	169.34	-191.45	0.00	0.00	0.00
KOP 12° DLS	6								

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COMPASS 5000.1 Build 74



Planning Report



Database: EDM 5000.1 Single User Db	1. 感謝的になり、「チーマは勉強性が必要」というに認識。
Company: DEVON ENERGY	Local Co-ordinate Reference: Well 34H
Company. DEVON ENERGY	TVD Reference: H&P 394: 3665' GL + 25' RKB @
	3690.00usft (Original Well Elev)
Project: Lea County, NM (NAD-83)	MD Reference: H&P 394: 3665' GL + 25' RKB @
	3690.00usft (Original Well Elev)
Site:	North Reference: Grid
Well:	Survey Calculation Method: Minimum Curvature
Wellbore: 34H OH	
Design:	
Planned Suprov	

nned Survey	n in an	و عمری در در در بدری در در	n a shearan na	and an state of the	na nanagena	an anna a' maraithean a	an 191 an Arnadar S		u antiko mansaki kuren ing
Measured			Vertical			Vertical	Dogleg	Build	Tum
	ination 🔆 A:		Depth	+N/-S	+E/-W	Section	Rate	Rate	Rate
(usft)	(°)	(°)	(usft)	(usft)	(usft)	(usft)	(°/100usft)	(°/100usft) ('	/100usft)
8,275.00	0.60	3.61	8,261.93	-201.79	169.34	-191.42	12.00	12.00	0.00
8,300.00	3.60	3.61	8,286.91	-200.87	169.40	-190.51	12.00	12.00	0.00
8,325.00	6.60	3.61	8,311.80	-198.66	169.54	-188.28	12.00	12.00	0.00
8,350.00	9.60	3.61	8,336.55	-195,14	169.76	-184.76	12.00	12.00	0.00
8,375.00	12.60	3.61	8,361.08	-190.34	170.07	-179.95	12.00	12.00	0.00
8,400.00	15.60	3.61	8,385.32	-184.26	170.45	-173.86	12.00	12.00	0.00
8,425.00	18.60	3.61	8,409.22	-176.93	170.91	-166.51	12.00	12.00	0.00
8,450.00	21.60	3.61	8,432.69	-168.35	171.45	-157.92	12.00	12.00	0.00
8,475.00	24.60	3.61	8,455.68	-158.56	172.07	-148.11	12.00	12.00	0.00
8,500.00	27.60	3.61	8,478.13	-147.59	172.76	-137.11	12.00	12.00	0.00
8,525.00	30.60	3.61	8,499.97	-135.46	173.53	-124.96	12.00	12.00	0.00
8,550.00	33.60	3.61	8,521.15	-122.20	174.37	-111,67	12.00	12.00	0.00
8,575.00	36.60	3.61	8,541.60	-107.85	175.27	-97.30	12.00	12.00	0.00
8,600.00	39.60	3.61	8,561.27	-92.46	176.24	-81.88	12.00	12.00	0.00
8,625.00	42.60	3.61	8,580.11	-76.06	177.28	-65.44	12.00	12.00	0.00
8,650.00	45.60	3.61	8,598.06	-58.70	178.37	-48.05	12.00	12.00	0.00
8,675.00	48.60	3.61	8,615.08	-40.42	179.53	-29.74	12.00	12.00	0.00
8,700.00	51.60	3.61	8,631.11	-21.28	180.73	-10.56	12.00	12.00	0.00
8,725.00	54.60	3.61	8,646.12	-1.33	181,99	9.43	12.00	12.00	0.00
8,750.00	57.60	3.61	8,660.06	19.37	183.30	30.18	12.00	12.00	0.00
8,775.00	60.60	3.61	8,672.90	40.78	184.65	51.63	12.00	12.00	0.00
8,800.00	63.60	3.61	8,684.60	62.83	186.04	73.72	12.00	12.00	0.00
8,825.00	66.60	3,61	8,695.12	85.46	187.47	96.39	12.00	12.00	0.00
8,850.00	69.60	3.61	8,704.44	108.60	188.93	119.58	12.00	12.00	0.00
8,857.49	70.50	3.61	8,707.00	115.63	189.37	126.62	12.00	12.00	0.00
Madera		0.01	0,101.00	110.00	100.07		12.00	12.00	0.00
8,875.00	72.60	3.61	8,712.54	132.20	190.42	143.23	12.00	12.00	0.00
8,900.00	75.60	3.61	8,719.39	156.20	191.93	167.27	12.00	12.00	0.00
8,925.00	78.60	3.61	8,724.97	180.52	193.46	191.64	12.00	12.00	0.00
8,950.00									
8,975.00	81.60 84.60	3.61 3.61	8,729.27 8,732.27	205.09	195.02	216.26	12.00	12.00	0.00
9,000.00	87.60	3.61	8,733.97	229.86	196.58 198.15	241.08	12.00	12.00	0.00
9,024.44	90.53	3.61	8,734.37	254.75 279.14	199.15	266.02 290.46	12.00 12.00	12.00 12.00	0.00 0.00
LP		0.01	0,104.07	219.17	100.00	230.40	12.00	12.00	0.00
9,100.00	90.53	3.61	8,733.67	354.54	204.44	366.01	0.00	0.00	0.00
9,200.00	90.53	3.61	8,732.74	454.34	210.74	466.00	0.00	0.00	0.00
9,300.00	90.53	3.61	8,731.81	554.14	217.04	566.00	0.00	0.00	0.00
9,400.00	90.53	3.61	8,730.87	653.93	223.33	665.99	0.00	0.00	0.00
9,500.00	90.53	3.61	8,729.94	753.73	229.63	765,99	0.00	0.00	0.00
9,600.00	90.53	3.61	8,729.01	853.53	235.93	865.98	0.00	0.00	0.00
9,700.00	90.53	3.61	8,728.08	953.32	242.22	965.98	0.00	0.00	0.00
9,800.00	90.53	3.61	8,727.15	1,053.12	248.52	1,065.97	0.00	0.00	0.00
9,900.00	90.53	3.61	8,726.22	1,152.92	254.82	1,165.97	0.00	0.00	0.00
10,000.00	90.53	3.61	8,725.29	1,252.72	261.11	1,265.96	0.00	0.00	0.00
10,100.00	90.53	3.61	8,724.36	1,352.51	267.41	1,365.96	0.00	0.00	0.00
10.200.00	90.53	3.61	8,723.43	1,452.31	273.71	1,465.95	0.00	0.00	0.00
10,300.00	90.53	3.61	8,722.50	1,552.11	280.00	1,565.95	0.00	0.00	0.00
10,400.00	90.53	3.61	8,721.57	1,651.90	286.30	1,665.94	0.00	0.00	0.00
10,500.00	90.53	3.61	8,720.64	1,751.70	292.60	1,765.94	0.00	0.00	0.00
10,600.00	90.53	3.61	8,719.71	1,851.50	298.89	1,865.93	0.00	0.00	0.00
10,700.00	90.53	3.61	8,718.78	1,951.30	305.19	1,965.93	0.00	0.00	0.00
10,700.00	90.53	3.61	8,718.78	2,051.09	303.19	1,903.93	0.00	0.00	0.00

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COMPASS 5000.1 Build 74



Planning Report



Local Co-ordinate Reference: . N. A. Marketter and the state of the state 25 EDM 5000.1 Single User Db Database: Well 34H Company: DEVON ENERGY TVD Reference: H&P 394: 3665' GL + 25' RKB @ 3690.00usft (Original Well Elev) Project: Lea County, NM (NAD-83) MD Reference: H&P 394: 3665' GL + 25' RKB @ 3690.00usft (Original Well Elev) North Reference: Site: ू Thistle Unit 1.22 Grid ें 34H Well: Survey Calculation Method: Minimum Curvature Wellbore: 34H OH Design: 💫 Plan #1 · · ·

Measured	and the state of the	A CARLON AND	Vertical	그 같은 것은 것을 수요	• *****	Vertical	Dogleg	Build	Jurn 🔬
	lination	Azimuth	Depth	+N/-S	+E/-W	Section	Rate	Rate	Rate
(usft)	(°)	(°)	(usft)	(usft)	(usft)	(usft)	(°/100usft)	(°/100usft)	(°/100usft)
10,900.00	90.53	3.61	8,716.92	2,150.89	317.78	2,165.92	0.00	0.00	0.00
11,000.00	90.53	3.61	8,715.99	2,250.69	324.08	2,265.91	0.00	0.00	0.00
11,100.00	90.53	3.61	8,715.06	2,350.49	330.37	2,365.91	0.00	0.00	0.00
11,200.00	90.53	3.61	8,714.13	2,450.28	336.67	2,465.90	0.00	0.00	0.00
11,300.00	90.53	3.61	8,713.19	2,550.08	342.97	2,565.90	0.00	0.00	0.00
11,400.00	90.53	3.61	8,712.26	2,649.88	349.26	2,665.89	0.00	0.00	0.00
11,500.00	90.53	3.61	8,711.33	2,749.67	355.56	2,765.89	0.00	0.00	0.00
11,600.00	90.53	3.61	8,710.40	2,849.47	361.86	2,865.88	0.00	0.00	0.00
11,700.00	90.53	3.61	8,709.47	2,949.27	368.15	2,965.88	0.00	0.00	0.00
11,800.00	90.53	3.61	8,708.54	3,049.07	374.45	3,065.87	0.00	0.00	0.00
11,900.00	90.53	3.61	8,707.61	3,148.86	380.75	3,165.87	0.00	0.00	0.00
12,000.00	90.53	3.61	8,706.68	3,248.66	387.04	3,265.86	0.00	0.00	0.00
12,100.00	90.53	3.61	8,705.75	3,348.46	393.34	3,365.86	0.00	0.00	0.00
12,200.00	90.53	3.61	8,704.82	3,448.26	399.64	3,465.85	0.00	0.00	0.00
12,300.00	90.53	3.61	8,703.89	3,548.05	405.93	3,565.85	0.00	0.00	0.00
12,400.00	90.53	3.61	8,702.96	3,647.85	412.23	3,665.84	0.00	0.00	0.00
12,500.00	90.53	3.61	8,702.03	3,747.65	418.53	3,765.84	0.00	0.00	0.00
12,600.00	90.53	3.61	8,701.10	3,847.44	424.82	3,865.83	0.00	0.00	0.00
12,700.00	90.53	3.61	8,700.17	3,947.24	431.12	3,965.83	0.00	0.00	0.00
12,800.00	90.53	3.61	8,699.24	4,047.04	437.42	4,065.82	0.00	0.00	0.00
12,900.00	90.53	3.61	8,698.31	4,146.84	443.71	4,165.82	0.00	0.00	0.00
13,000.00	90.53	3.61	8,697.38	4,246.63	450.01	4,265.81	0.00	0.00	0.00
13,100.00	90.53	3.61	8,696.45	4,346.43	456.31	4,365.81	0.00	0.00	0.00
13,200.00	90.53	3.61	8,695.51	4,446.23	462.60	4,465.80	0.00	0.00	0.00
13,300.00	90.53	3.61	8,694.58	4,546.02	468.90	4,565.80	0.00	0.00	0.00
13,362.76	90.53	3.61	8,694.00	4,608.66	472.85	4,628.56	0.00	0.00	0.00
TD - PBHL (TÙ 34	H)								

Target Name - hit/miss target Dir - Shape	oAngle E (°)	ip Dir. (१)	TVD (usft)	+N/-S (usft)	+E/-W (usft)	Northing (usft)	Easting (usft)	Latitude	Longitude
SHL (TU 34H) - plan hits target center - Point	0.00	0.00	0.00	0.00	0.00	457,276.47	773,947.30	32° 15' 17.594 N	103° 34' 51.134 W
PBHL (TU 34H) - plan hits target center - Point	0.00	0.00	8,694.00	4,608.66	472.85	461,885.13	774,420.15	32° 16' 3.165 N	103° 34' 45.251 W



8,270.00

9,024.44 13,362.76

8,256.93

8,734.37 8,694.00 -201.81

279.14 4,608.66

LEAM Drilling Systems LLC

Planning Report

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Company: DEV(Project: Lea (Local Co-ordinate Reference: TVD Reference: MD Reference: North Reference: Survey Calculation: Method:	Well 34H H&P 394: 3665' GL + 25' RKB @ 3690.00usft (Original Well Elev) H&P 394: 3665' GL + 25' RKB @ 3690.00usft (Original Well Elev) Grid Minimum Curvature		
Formations	en anna an		en no a la companya de la companya El companya de la comp			
Measured Depth (usft)	Vertical Depth (usft)	Nam		Dip Dip Direction (1)		
1,300.00	1,300.00	Rusiter	eLithology	0.00		
1,547.00	1,547.00	Top Salt		0.00		
5,161.00	5,161.00	Delaware		0.00		
6,136.40	6,133.00	Cherry Canyon		0.00		
7,474,73	7,464.00	Brushy Canyon		0.00		
8,857.49	8,707.00	Madera		0.00		
Plan Annotations Measured Depth (usft) 5,250.00 5,650.00 7,770.00 8,170.00	Vertical Depth (usit) 5,250.00 5,649.27 7,757.66 8,155.93	Local Coord +N/-S (usft) 0.00 -16.03 -185.79 -201.81	inates +E/-W (usft) Comment 0.00 Nudge 13.45 Hold 155.89 Drop 169.34 Hold			

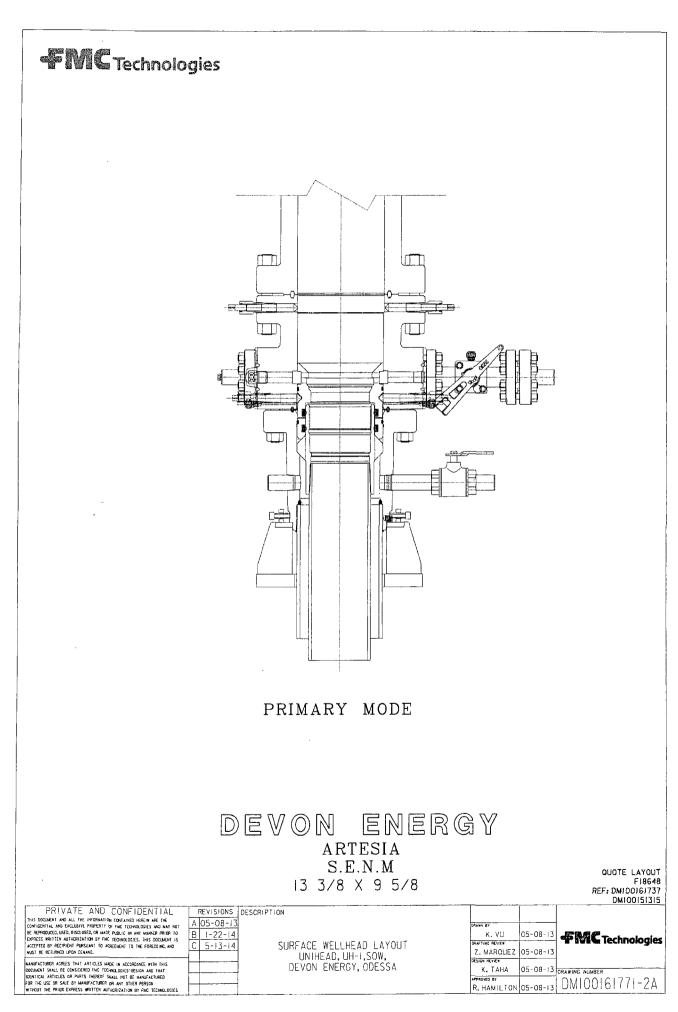
169.34

199.69 472.85

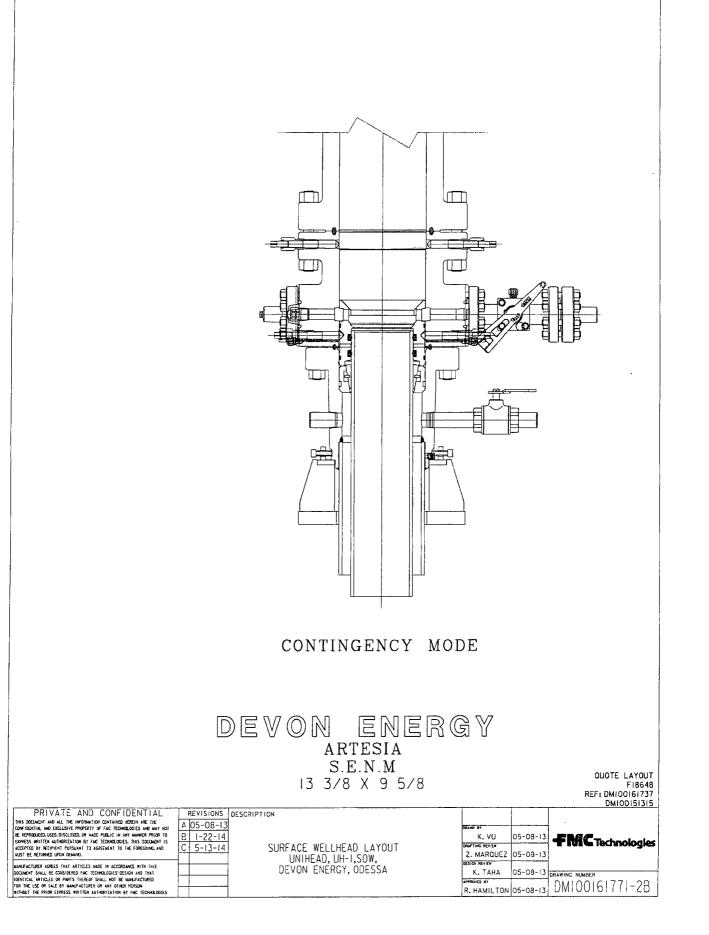
i.

KOP 12° DLS LP

TD

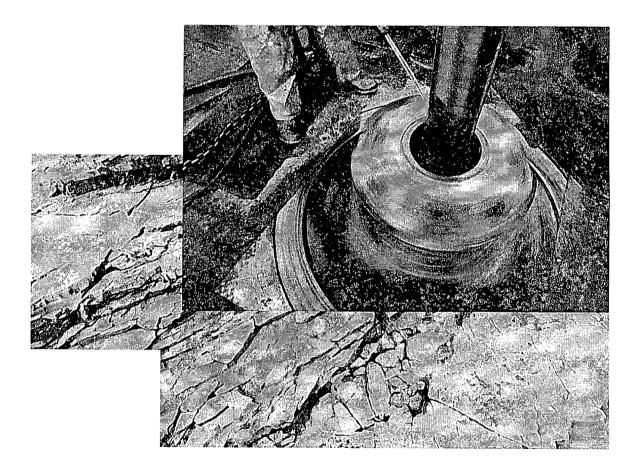


-FMC Technologies



devon

Commitment Runs Deep



Design Plan Operation and Maintenance Plan Closure Plan

SENM - Closed Loop Systems June 2010

I. Design Plan

Devon uses MI SWACO closed loop system (CLS). The MI SWACO CLS is designed to maintain drill solids at or below 5%. The equipment is arranged to progressively remove solids from the largest to the smallest size. Drilling fluids can thus be reused and savings is realized on mud and disposal costs. Dewatering may be required with the centrifuges to insure removal of ultra fine solids.

The drilling location is constructed to allow storm water to flow to a central sump normally the cellar. This insures no contamination leaves the drilling pad in the event of a spill. Storm water is reused in the mud system or stored in a reserve fluid tank farm until it can be reused. All lubricants, oils, or chemicals are removed immediately from the ground to prevent the contamination of storm water. An oil trap is normally installed on the sump if an oil spill occurs during a storm.

A tank farm is utilized to store drilling fluids including fresh water and brine fluids. The tank farm is constructed on a 20 ml plastic lined, bermed pad to prevent the contamination of the drilling site during a spill. Fluids from other sites may be stored in these tanks for processing by the solids control equipment and reused in the mud system. At the end of the well the fluids are transported from the tank farm to an adjoining well or to the next well for the rig.

Prior to installing a closed-loop system on site, the topsoil, if present, will be stripped and stockpiled for use as the final cover or fill at the time of closure.

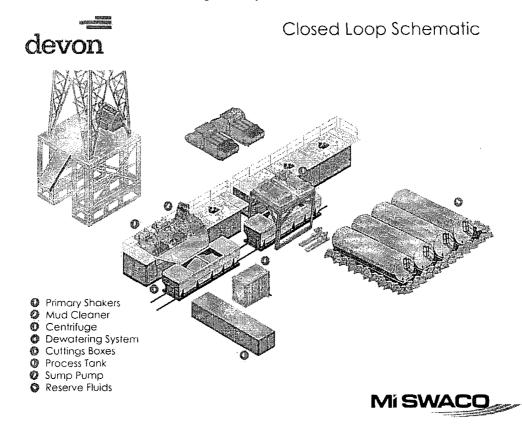
Signs will be posted on the fence surrounding the closed-loop system unless the closed-loop system is located on a site where there is an existing well, that is operated by Devon.

II. Operations and Maintenance Plan

Primary Shakers: The primary shakers make the first removal of drill solids from the drilling mud as it leaves the well bore. The shakers are sized to handle maximum drilling rate at optimal screen size. The shakers normally remove solids down to 74 microns.

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Mud Cleaner: The Mud Cleaner cleans the fluid after it leaves the shakers. A set of hydrocyclones are sized to handle 1.25 to 1.5 times the maximum circulating rate. This ensures all the fluid is being processed to an average cut point of 25 microns. The wet discharged is dewatered on a shaker equipped with ultra fine mesh screens and generally cut at 40 microns.



Centrifuges: The centrifuges can be one or two in number depending on the well geometry or depth of well. The centrifuges are sized to maintain low gravity solids at 5% or below. They may or may not need a dewatering system to enhance the removal rates. The centrifuges can make a cut point of 8-10 microns depending on bowl speed, feed rate, solids loading and other factors.

The centrifuge system is designed to work on the active system and be flexible to process incoming fluids from other locations. This set-up is also dependent on well factors.

Dewatering System: The dewatering system is a chemical mixing and dosing system designed to enhance the solids removal of the centrifuge. Not commonly used in shallow wells. It may contain pH adjustment, coagulant mixing and dosing, and polymer mixing and dosing. Chemical flocculation binds ultra fine solids into a mass that is within the centrifuge operating design. The dewatering system improves the centrifuge cut point to infinity or allows for the return of clear water or brine fluid. This ability allows for the ultimate control of low gravity solids.

Cuttings Boxes: Cuttings boxes are utilized to capture drill solids that are discarded from the solids control equipment. These boxes are set upon a rail system that allows for the removal and replacement of a full box of cuttings with an empty one. They are equipped with a cover that insures no product is spilled into the environment during the transportation phase.

Process Tank: (Optional) The process tank allows for the holding and process of fluids that are being transferred into the mud system. Additionally, during times of lost circulation the process tank may hold active fluids that are removed for additional treatment. It can further be used as a mixing tank during well control conditions.

Sump and Sump Pump: The sump is used to collect storm water and the pump is used to transfer this fluid to the active system or to the tank for to hold in reserve. It can also be used to collect fluids that may escape during spills. The location contains drainage ditches that allow the location fluids to drain to the sump.

Reserve Fluids (Tank Farm): A series of frac tanks are used to replace the reserve pit. These are steel tanks that are equipped with a manifold system and a transfer pump. These tanks can contain any number of fluids used during the drilling process. These can include fresh water, cut brine, and saturated salt fluid. The fluid can be from the active well or reclaimed fluid from other locations. A 20 ml liner and berm system is employed to ensure the fluids do not migrate to the environment during a spill.

If a leak develops, the appropriate division district office will be notified within 48 hours of the discovery and the leak will be addressed. Spill prevention is accomplished by maintaining pump packing, hoses, and pipe fittings to insure no leaks are occurring. During an upset condition the source of the spill is isolated and repaired as soon as it is discovered. Free liquid is removed by a diaphragm pump and returned to the mud system. Loose topsoil may be used to stabilize the spill and the contaminated soil is excavated and placed in the cuttings boxes. After the well is finished and the rig has moved, the entire location is scrapped and testing will be performed to determine if a release has occurred.

All trash is kept in a wire mesh enclosure and removed to an approved landfill when full. All spent motor oils are kept in separate containers and they are removed and sent to an approved recycling center. Any spilled lubricants, pipe dope, or regulated chemicals are removed from soil and sent to landfills approved for these products.

These operations are monitored by Mi Swaco service technicians. Daily logs are maintained to ensure optimal equipment operation and maintenance. Screen and chemical use is logged to maintain inventory control. Fluid properties are monitored and recorded and drilling mud volumes are accounted for in the mud storage farm. This data is kept for end of well review to insure performance goals are met. Lessons learned are logged and used to help with continuous improvement.

A MI SWACO field supervisor manages from 3-5 wells. They are responsible for training personnel, supervising installations, and inspecting sites for compliance of MI SWACO safety and operational policy.

III. Closure Plan

A maximum 340' X 340' caliche pad is built per well. All of the trucks and steel tanks fit on this pad. All fluid cuttings go to the steel tanks to be hauled by various trucking companies to an agency approved disposal.