#### 1. Geologic Formations

| TVD of target | 12,836' | Pilot hole depth              | N/A |
|---------------|---------|-------------------------------|-----|
| MD at TD:     | 22,999' | Deepest expected fresh water: |     |

### Basin

| Formation                | Depth (TVD) from<br>KB | Water/Mineral<br>Bearing/ Target Zone? | Hazards* |  |
|--------------------------|------------------------|--|----------|--|
| Rustler                  | 726                    | Barren                                 |          |  |
| Top of Salt              | 1091                   | Barren                                 |          |  |
| Base of Salt             | 5041                   | Barren                                 |          |  |
| Delaware                 | 5291                   | Hydrocarbon                            |          |  |
| Lower Brushy Canyon      | 9386                   | Hydrocarbon                            |          |  |
| 1st BSPG Lime            | 9566                   | Hydrocarbon                            |          |  |
| 1st BSPG Sand            | 10496                  | Hydrocarbon                            |          |  |
| 2nd BSPG Lime            | 10716                  | Hydrocarbon                            |          |  |
| 2nd BSPG Sand            | 11066                  | Hydrocarbon                            |          |  |
| 3rd BSPG Lime            | 11531                  | Hydrocarbon                            |          |  |
| 3rd BSPG Sand            | 12131                  | Hydrocarbon                            |          |  |
| Wolfcamp                 | 12571                  | Hydrocarbon                            |          |  |
| Wolfcamp "A"             | 12776                  | Hydrocarbon                            |          |  |
| Wolfcamp "A" Target Base | 12851                  | Hydrocarbon                            |          |  |
| Wolfcamp "B" Shale       | 13786                  | Hydrocarbon                            |          |  |
|                          |                        |  |          |  |

<sup>\*</sup>H2S, water flows, loss of circulation, abnormal pressures, etc.

#### 2. Casing Program

| Hole Size | Casing Interval |         | Csg.    | Weight  | Grade      | Conn     | SF       | SF Burst | SF      |
|-----------|-----------------|---------|---------|---------|------------|----------|----------|----------|---------|
|           | From            | To      | Size    | (lbs)   |            |          | Collapse |          | Tension |
| 17.5"     | 0               | 775'    | 13.375" | 54.5    | J-55       | BTC      | 3.74     | 3.46     | 2.11    |
| 12.25"    | 0               | 11,600' | 9.625"  | 40      | P-110      | BTC      | 1.25     | 1.59     | 2.58    |
| 8.75"     | 0               | 22,999' | 5.5"    | 17      | P-110      | BTC      | 1.27     | 1.26     | 1.83    |
|           | •               |         |         | BLM Min | imum Safet | y Factor | 1.125    | 1.00     | 1.6 Dry |
|           |                 |         |         |         |            |          |          |          | 1.8 Wet |

All casing strings will be tested in accordance with Onshore Oil and Gas Order #2 III.B.1.h

Must have table for contingency casing

|  | YorN                 |
|--|----------------------|
| Is casing new? If used, attach certification as required in Onshore Order #1   | Y                    |
| Does casing meet API specifications? If no, attach casing specification sheet.   | Y                    |
| Is premium or uncommon casing planned? If yes attach casing specification sheet.   | N                    |
| Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria). | Y                    |
| Will the intermediate pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?                | Y                    |
| Is well located within Capitan Reef?   | l N                  |
| If yes, does production casing cement tie back a minimum of 50' above the Reef?  | 11                   |
| Is well within the designated 4 string boundary.   | +                    |
| is well within the designated 4 string boundary.   | E PERSONAL PROPERTY. |
| Is well located in SOPA but not in R-111-P?  | N                    |
| If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back  |                      |
| 500' into previous casing?   |                      |
|  |                      |
| Is well located in R-111-P and SOPA?   | N                    |
| If yes, are the first three strings cemented to surface?   |                      |
| Is 2 <sup>nd</sup> string set 100' to 600' below the base of salt?   |                      |
| Is well located in high Cave/Karst?  | N                    |
| If yes, are there two strings cemented to surface?   |                      |
| (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?   |                      |
|  | N                    |
| Is well located in critical Cave/Karst?  | IN                   |
| If yes, are there three strings cemented to surface?   |                      |

#### 3. Cementing Program

| Casing             | # Sks | Wt.<br>lb/<br>gal | H₂0<br>gal/sk | Yld<br>ft3/<br>sack | 500#<br>Comp.<br>Strength<br>(hours) | Slurry Description   |
|--------------------|-------|-------------------|---------------|---------------------|--------------------------------------|--|
| 13-3/8"<br>Surface | 605   | 14.8              | 6.32          | 1.33                | 6                                    | Tail: Class C Cement + 0.125 lbs/sack Poly-E-Flake   |
|                    | 1630  | 11.9              | 19.82         | 2.31                | 45                                   | Lead: NeoCem®  |
| 9-5/8"<br>Inter.   | 590   | 14.8              | 5.31          | 1.33                | 25                                   | Tail: (50:50) Class H Cement: Poz (Fly Ash) + 0.5%<br>bwoc HALAD-344 + 0.4% bwoc CFR-3 + 0.2% BWOC<br>HR-601 + 2% bwoc Bentonite |
|                    | 750   | 11.9              | 19.82         | 2.31                | 45                                   | 1st Stage Lead: NeoCem®  |
| 9-5/8"<br>Interme  | 790   | 14.8              | 5.31          | 1.33                | 25                                   | Tail: (50:50) Class H Cement: Poz (Fly Ash) + 0.5%<br>bwoc HALAD-344 + 0.4% bwoc CFR-3 + 0.2% BWOC<br>HR-601 + 2% bwoc Bentonite |
| diate              |       |                   |               |                     | D\                                   | / Tool = 5000ft  |
| Two                | 460   | 11.9              | 19.82         | 2.3                 | 45                                   | 2 <sup>nd</sup> Stage Lead: NeoCem®  |
| Stage              | 200   | 14.8              | 6.32          | 1.33                | 6                                    | 2 <sup>nd</sup> Stage Tail: Class C Cement + 0.125 lbs/sack Poly-E-<br>Flake   |
|                    | 135   | 11.9              | 19.82         | 2.3                 | 45                                   | 2 <sup>nd</sup> Stage Lead: NeoCem®  |
| 5-1/2"<br>Prod     | 2485  | 14.5              | 5.31          | 1.2                 | 25                                   | Tail: (50:50) Class H Cement: Poz (Fly Ash) + 0.5%<br>bwoc HALAD-344 + 0.4% bwoc CFR-3 + 0.2% BWOC<br>HR-601 + 2% bwoc Bentonite |

If a DV tool is used, depth(s) will be adjusted based on hole conditions and cement volumes will be adjusted proportionally. DV tool will be set a minimum of 50 feet below previous casing and a minimum of 200 feet above current shoe. Lab reports with the 500 psi compressive strength time for the cement will be onsite for review.

| Casing String                          | TOC  | % Excess |
|--|--|----------|
| 13-3/8" Surface                        | 0'   | 100%     |
| 9-5/8" Intermediate                    | 0'   | 50%      |
| 9-5/8" Intermediate – Two Stage Option | 1 <sup>st</sup> Stage = 5000' / 2 <sup>nd</sup> Stage = 0' | 50%      |
| 5-1/2" Production Casing               | 10,600′  | 25%      |

#### 4. Pressure Control Equipment

N A variance is requested for the use of a diverter on the surface casing. See attached for schematic.

| BOP installed<br>and tested<br>before drilling<br>which hole? | Size?   | Min.<br>Required<br>WP | T          | ype       | 1        | Tested to:              |      |      |            |
|---|---------|------------------------|------------|-----------|----------|-------------------------|------|------|------------|
|   |         |                        | Anı        | nular     | X        | 50% of working pressure |      |      |            |
|   |         |                        | Bline      | d Ram     |          |                         |      |      |            |
| 12-1/4"   | 13-5/8" | 5M                     | Pipe       | Ram       |          | 5M                      |      |      |            |
|   |         |                        | Doub       | le Ram    | X        | SIVI                    |      |      |            |
|   |         |                        | Other*     |           |          |                         |      |      |            |
|   |         |                        | Anı        | nular     | X        | 50% testing pressure    |      |      |            |
|   |         |                        | 13-5/8" 5M | Bline     | d Ram    |                         |      |      |            |
| 8-3/4"  | 13-5/8" | 12 5/9"                |            | 3-5/8" 5M | Pipe Ram |                         |      |      |            |
| 0-3/4   |         | SIVI                   |            |           | 3171     | SIVI                    | JIVI | SIVI | Double Ram |
|   |         |                        | Other<br>* |           |          |                         |      |      |            |
|   |         |                        | Anı        | nular     |          | 50% testing pressure    |      |      |            |
|   |         |                        | Blind Ram  |           |          |                         |      |      |            |
|   |         |                        | Pipe Ram   |           |          |                         |      |      |            |
|   |         |                        | Double Ram |           |          |                         |      |      |            |
|   |         |                        | Other      |           |          |                         |      |      |            |
|   |         |                        | *          |           |          |                         |      |      |            |

<sup>\*</sup>Specify if additional ram is utilized.

BOP/BOPE will be tested by an independent service company to 250 psi low and the high pressure indicated above per Onshore Order 2 requirements. The System may be upgraded to a higher pressure but still tested to the working pressure listed in the table above. If the system is upgraded all the components installed will be functional and tested.

Pipe rams will be operationally checked each 24 hour period. Blind rams will be operationally checked on each trip out of the hole. These checks will be noted on the daily tour sheets. Other accessories to the BOP equipment will include a Kelly cock and floor safety valve (inside BOP) and choke lines and choke manifold. See attached schematics.

Y Formation integrity test will be performed per Onshore Order #2.
On Exploratory wells or on that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Will be tested in accordance with Onshore Oil and Gas Order #2 III.B.1.i.

- A variance is requested for the use of a flexible choke line from the BOP to Choke Y Manifold. See attached for specs and hydrostatic test chart.
  - Y Are anchors required by manufacturer?
- Y A multibowl wellhead may be used. The BOP will be tested per Onshore Order #2 after installation on the surface casing which will cover testing requirements for a maximum of 30 days. If any seal subject to test pressure is broken the system must be tested.

Devon proposes using a multi-bowl wellhead assembly. This assembly will only be tested when installed on the surface casing. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be 5000 (5M) psi.

- Wellhead will be installed by wellhead representatives.
- If the welding is performed by a third party, the wellhead representative will
  monitor the temperature to verify that it does not exceed the maximum
  temperature of the seal.
- Wellhead representative will install the test plug for the initial BOP test.
- Wellhead company will install a solid steel body pack-off to completely isolate
  the lower head after cementing intermediate casing. After installation of the packoff, the pack-off and the lower flange will be tested to 5M, as shown on the
  attached schematic. Everything above the pack-off will not have been altered
  whatsoever from the initial nipple up. Therefore the BOP components will not be
  retested at that time.
- If the cement does not circulate and one inch operations would have been possible
  with a standard wellhead, the well head will be cut and top out operations will be
  conducted.
- Devon will pressure test all seals above and below the mandrel (but still above the casing) to full working pressure rating.
- Devon will test the casing to 0.22 psi/ft or 1500 psi, whichever is greater, as per Onshore Order #2.

After running the 13-3/8" surface casing, a 13-5/8" BOP/BOPE system with a minimum rating of 5M will be installed on the wellhead system and will undergo a 250 psi low pressure test followed by a 5,000 psi high pressure test. The 5,000 psi high and 250 psi low test will cover testing requirements a maximum of 30 days, as per Onshore Order #2. If the well is not complete within 30 days of this BOP test, another full BOP test will be conducted, as per Onshore Order #2.

After running the 9-5/8' intermediate casing with a mandrel hanger, the 13-5/8" BOP/BOPE system with a minimum rating of 5M will already be installed on the wellhead.

The pipe rams will be operated and checked each 24 hour period and each time the drill pipe is out of the hole. These tests will be logged in the daily driller's log. A 2" kill line and 3" choke line will be incorporated into the drilling spool below the ram BOP. In addition to the rams and annular preventer, additional BOP accessories include a kelly cock, floor safety valve, choke lines, and choke manifold rated at 5,000 psi WP.

Devon's proposed wellhead manufactures will be FMC Technologies, Cactus Wellhead, or Cameron.

Devon requests a variance to use a flexible line with flanged ends between the BOP and the choke manifold (choke line). The line will be kept as straight as possible with minimal turns.

See attached schematic.

5. Mud Program

| Depth   |         | Type          | Weight (ppg) | Viscosity | Water Loss |  |
|---------|---------|---------------|--------------|-----------|------------|--|
| From    | To      |               |              |           |            |  |
| 0       | 775'    | FW Gel        | 8.4-8.5      | 28-34     | N/C        |  |
| 775'    | 11,600' | Oil Based Mud | 8.4-9.0      | 40-50     | 10-15      |  |
| 11,600' | 22,967  | Oil Based Mud | 10.5-11.0    | 40-50     | 10-15      |  |

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times.

| What will be used to monitor the loss or gain | PVT/Pason/Visual Monitoring |
|---|-----------------------------|
| of fluid?                                     |                             |

#### 6. Logging and Testing Procedures

| Logg | ring, Coring and Testing.  |
|------|--|
| X    | Will run GR/CNL fromTD to surface (horizontal well – vertical portion of hole). Stated |
|      | logs run will be in the Completion Report and submitted to the BLM.                    |
|      | Quad Combo is planned on being taken from intermediate shoe to TD                      |
|      | Drill stem test? If yes, explain   |
|      | Coring? If yes, explain  |

| Add | itional logs planned | Interval                |
|-----|----------------------|-------------------------|
|     | Resistivity          | Int. shoe to KOP        |
|     | Density              | Int. shoe to KOP        |
| X   | CBL                  | Production casing       |
| X   | Mud log              | Intermediate shoe to TD |
|     | PEX                  |                         |

#### 7. Drilling Conditions

| Condition                  | Specify what type and where? |
|----------------------------|------------------------------|
| BH Pressure at deepest TVD | 7317 psi                     |
| Abnormal Temperature       | No                           |

Mitigation measure for abnormal conditions. Describe. Lost circulation material/sweeps/mud scavengers.

Hydrogen Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the operator will comply with the provisions of Onshore Oil and Gas Order #6. If Hydrogen Sulfide is encountered, measured values and formations will be provided to the BLM.

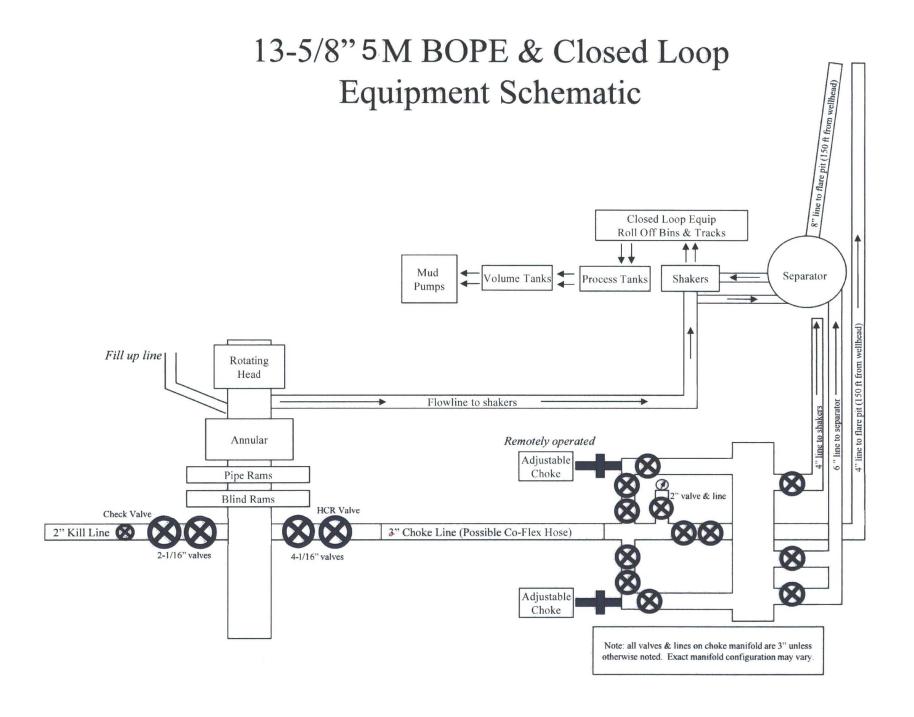
| N | H2S is present    |
|---|-------------------|
| Y | H2S Plan attached |

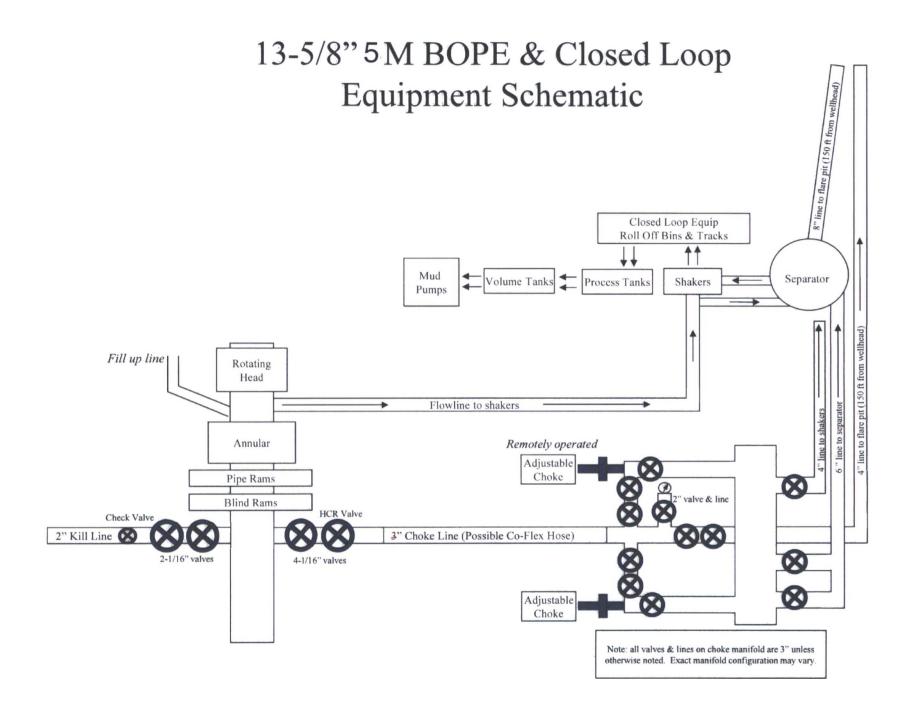
#### 8. Other facets of operation

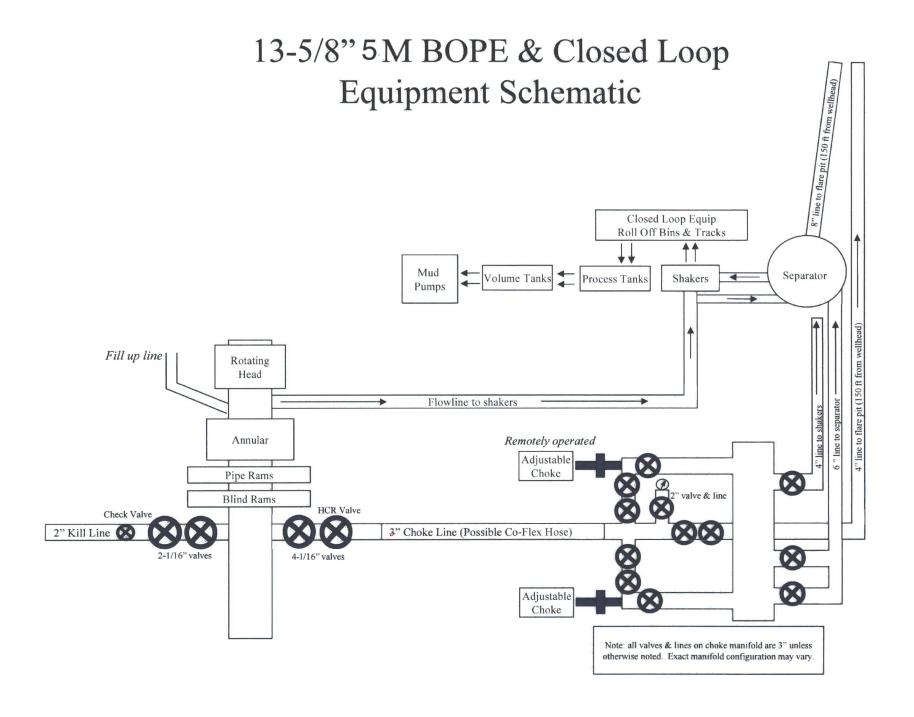
Is this a walking operation? No. Will be pre-setting casing? No.

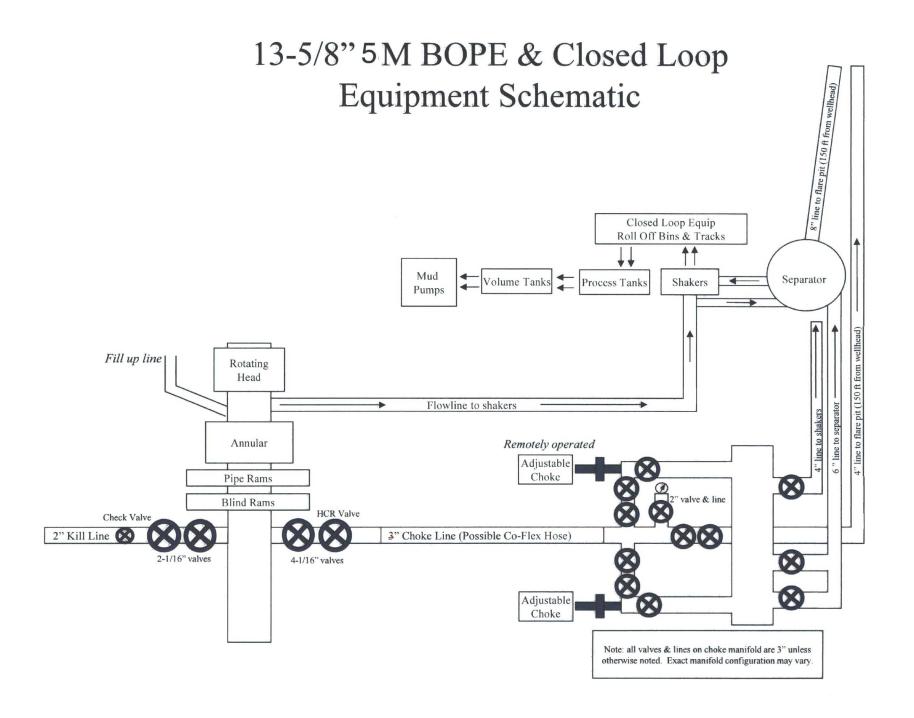
Attachments

\_x\_ Directional Plan \_\_ Other, describe









Casing Assumptions and Load Cases

Surface

All casing design assumptions were ran in Stress Check to determine safety factor which meet or exceed both Devon Energy and BLM minimum requirements. All casing strings will be filled while running in hole in order to not exceed collapse rating of the pipe.

| Surface Casing Burst Design |                         |   |  |
|-----------------------------|-------------------------|---|--|
| Load Case                   | External Pressure       | Internal Pressure                                     |  |
| Pressure Test               | Formation Pore Pressure | Max mud weight of next hole-<br>section plus Test psi |  |
| Drill Ahead                 | Formation Pore Pressure | Max mud weight of next hole section                   |  |
| Displace to Gas             | Formation Pore Pressure | Dry gas from next casing point                        |  |

| Surface Casing Collapse Design                |                               |                 |  |  |
|---|-------------------------------|-----------------|--|--|
| Load Case External Pressure Internal Pressure |                               |                 |  |  |
| Full Evacuation                               | Water gradient in cement, mud | None            |  |  |
|   | above TOC                     |                 |  |  |
| Cementing                                     | Wet cement weight             | Water (8.33ppg) |  |  |

| Surface Casing Tension Design |         |  |  |  |
|-------------------------------|---------|--|--|--|
| Load Case Assumptions         |         |  |  |  |
| Overpull                      | 100kips |  |  |  |
| Runing in hole                | 3 ft/s  |  |  |  |
| Service Loads                 | N/A     |  |  |  |

Casing Assumptions and Load Cases

Intermediate

All casing design assumptions were ran in Stress Check to determine safety factor which meet or exceed both Devon Energy and BLM minimum requirements. All casing strings will be filled while running in hole in order to not exceed collapse rating of the pipe.

| Intermediate Casing Burst Design |                         |   |  |  |
|----------------------------------|-------------------------|---|--|--|
| Load Case                        | External Pressure       | Internal Pressure                                     |  |  |
| Pressure Test                    | Formation Pore Pressure | Max mud weight of next hole-<br>section plus Test psi |  |  |
| Drill Ahead                      | Formation Pore Pressure | Max mud weight of next hole section                   |  |  |
| Fracture @ Shoe                  | Formation Pore Pressure | Dry gas   |  |  |

| Intermediate Casing Collapse Design           |                               |                 |  |  |
|---|-------------------------------|-----------------|--|--|
| Load Case External Pressure Internal Pressure |                               |                 |  |  |
| Full Evacuation                               | Water gradient in cement, mud | None            |  |  |
|   | above TOC                     |                 |  |  |
| Cementing                                     | Wet cement weight             | Water (8.33ppg) |  |  |

| Intermediate Casing Tension Design |             |  |  |  |
|------------------------------------|-------------|--|--|--|
| Load Case                          | Assumptions |  |  |  |
| Overpull                           | 100kips     |  |  |  |
| Runing in hole                     | 2 ft/s      |  |  |  |
| Service Loads                      | N/A         |  |  |  |

Production

All casing design assumptions were ran in Stress Check to determine safety factor which meet or exceed both Devon Energy and BLM minimum requirements. All casing strings will be filled while running in hole in order to not exceed collapse rating of the pipe.

| Production Casing Burst Design |                         |   |  |
|--------------------------------|-------------------------|---|--|
| Load Case                      | External Pressure       | Internal Pressure                                     |  |
| Pressure Test                  | Formation Pore Pressure | Fluid in hole (water or produced water) + test psi    |  |
| Tubing Leak                    | Formation Pore Pressure | Packer @ KOP, leak below surface 8.6 ppg packer fluid |  |
| Stimulation                    | Formation Pore Pressure | Max frac pressure with heaviest frac fluid            |  |

| Production Casing Collapse Design             |  |                 |  |  |
|---|--|-----------------|--|--|
| Load Case External Pressure Internal Pressure |  |                 |  |  |
| Full Evacuation                               | Water gradient in cement, mud above TOC. | None            |  |  |
| Cementing                                     | Wet cement weight                        | Water (8.33ppg) |  |  |

| Production Casing Tension Design |             |  |  |
|----------------------------------|-------------|--|--|
| Load Case                        | Assumptions |  |  |
| Overpull                         | 100kips     |  |  |
| Runing in hole                   | 2 ft/s      |  |  |
| Service Loads                    | N/A         |  |  |



#### Fluid Technology

ContiTech Beattie Corp. Website: www.contitechbeattie.com

Monday, June 14, 2010

RE:

Drilling & Production Hoses Lifting & Safety Equipment

To Helmerich & Payne,

A Continental Contilect hose assembly can perform as intended and suitable for the application regardless of whether the hose is secured or unsecured in its configuration. As a manufacturer of High Pressure Hose Assemblies for use in Drilling & Production, we do offer the corresponding lifting and safety equipment, this has the added benefit of easing the lifting and handling of each hose assembly whilst affording hose longevity by ensuring correct handling methods and procedures as well as securing the hose in the unlikely event of a failure; but in no way does the lifting and safety equipment affect the performance of the hoses providing the hoses have been handled and installed correctly it is good practice to use lifting & safety equipment but not mandatory

Should you have any questions or require any additional information/clarifications then please do not hesitate to contact us.

ContiTech Beattie is part of the Continental AG Corporation and can offer the full support resources associated with a global organization.

Best regards,

Robin Hodgson Sales Manager ContiTech Beattie Corp

ContiTech Beattle Corp, 11535 Brittmoore Park Drive, Houston, TX 77041 Phone: +1 (832) 327-0141 Fax: +1 (832) 327-0148 www.contitechbeattle.com



# R16 212



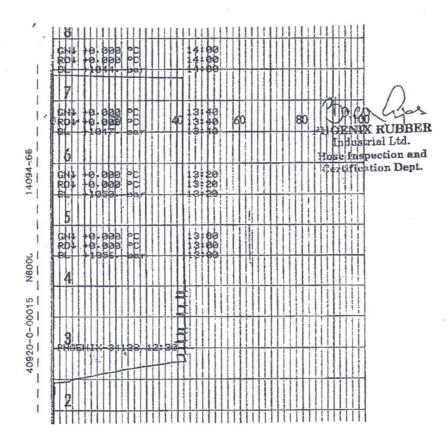
#### **QUALITY DOCUMENT**

## PHOENIX RUBBER INDUSTRIAL LTD.

PHOENIK RUBBER Q.C

\*,6728 Szeged, Budapesti út 10. Hungary \* H--6701 Szeged, P. O. Box 152 hone: (3662) 566-737 \* Fax: (3662) 566-738 SALES & MARKETING: H-1092 Budapest, Ráday u. 42-44. Hungary • H-1440 Budapest, P. O. Box 26 Phone: (361) 456-4200 · Fax: (361) 217-2972, 456-4273 · www.taurusemerge.hu

| QUAL<br>INSPECTION   | ITY CONTR    |              | ATE       | CERT.      | Nº:          | 552         |                     |
|--|--------------|--------------|-----------|------------|--------------|-------------|---------------------|
| PURCHASER:   | Phoenix Beat | tie Co.      |           | P.O. N°    | . 1519       | FA-871      |                     |
| PHOENIX RUBBER order No.   | 170466       | HOSE TYPE:   | 3" ID     | Ch         | oke and Kill | Hose        |                     |
| HOSE SERIAL Nº   | 34128        | NOMINAL / AC | TUAL LENG | тн:        | 11,43 m      |             |                     |
| W.P. 68,96 MPa 10  | 0000 psi     | T.P. 103,4   | MPa 15    | 000 psi    | Duration:    | 60          | min.                |
| Pressure test with water at ambient temperature  ↑ 10 mm = 10 Min.  → 10 mm = 25 MPa |              | achment. (1  | page)     |            |              |             | the stage is a con- |
|  |              | COUPLI       | NGS       |            |              |             | .=1                 |
| Туре   |              | Serial Nº    |           | Quality    |              | Heat N°     |                     |
| 3" coupling with   | 72           | 719          |           | AISI 4130  | )            | C7626       |                     |
| 4 1/16" Flange end   |              |              |           | AISI 4130  |              | 47357       |                     |
|  |              |              |           |            |              |             |                     |
| All metal parts are flawless WE CERTIFY THAT THE ABOVE PRESSURE TESTED AS ABOVE      |              |              |           | ture rate: |              | OF THE ORDE | R AND               |
| Date: 29. April. 2002.   | Inspector    |              | Quality C | CHO!       | ENIX RUB     | i.          | w T                 |



VERIFIED TRUE CO. PHOENIX RUBBER Q.C. A multibowl wellhead may be used. The BOP will be tested per Onshore Order #2 after installation on the surface casing which will cover testing requirements for a maximum of 30 days. If any seal subject to test pressure is broken the system must be tested.

Devon proposes using a multi-bowl wellhead assembly. This assembly will only be tested when installed on the surface casing. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be 3000 (3M) psi.

- Wellhead will be installed by wellhead representatives.
- If the welding is performed by a third party, the wellhead representative will monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
- Wellhead representative will install the test plug for the initial BOP test.
- Wellhead company will install a solid steel body pack-off to completely isolate the lower head after cementing intermediate casing. After installation of the pack-off, the pack-off and the lower flange will be tested to 3M, as shown on the attached schematic. Everything above the pack-off will not have been altered whatsoever from the initial nipple up. Therefore the BOP components will not be retested at that time.
- If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head will be cut and top out operations will be conducted.
- Devon will pressure test all seals above and below the mandrel (but still above the casing) to full working pressure rating.
- Devon will test the casing to 0.22 psi/ft or 1500 psi, whichever is greater, as per Onshore Order #2.

After running the 13-3/8" surface casing, a 13-5/8" BOP/BOPE system with a minimum rating of 3M will be installed on the wellhead system and will undergo a 250 psi low pressure test followed by a 3,000 psi high pressure test. The 3,000 psi high and 250 psi low test will cover testing requirements a maximum of 30 days, as per Onshore Order #2. If the well is not complete within 30 days of this BOP test, another full BOP test will be conducted, as per Onshore Order #2.

After running the 9-5/8' intermediate casing with a mandrel hanger, the 13-5/8" BOP/BOPE system with a minimum rating of 3M will already be installed on the wellhead.

The pipe rams will be operated and checked each 24 hour period and each time the drill pipe is out of the hole. These tests will be logged in the daily driller's log. A 2" kill line and 3" choke line will be incorporated into the drilling spool below the ram BOP. In addition to the rams and annular preventer, additional BOP accessories include a kelly cock, floor safety valve, choke lines, and choke manifold rated at 3,000 psi WP.

Devon's proposed wellhead manufactures will be FMC Technologies, Cactus Wellhead, or Cameron.

