

### 1. FORMATION TOPS

The estimated tops of important geologic markers are as follows:

FORMATION	SUB-SEA TVD	KBTVD	MD
Rustler		800	
Castile		3480	
Lamar		4900	
Bell Canyon		4930	
Cherry Canyon		5970	
Brushy Canyon		7620	
Bone Spring Limestone		9090	
Upr. Avalon		9120	
Top Bone Spring 1		10040	
Top Bone Spring 2		10700	
Top Bone Spring 3		11740	
Wolfcamp		12140	
Wolfcamp A1		12193	
Wolfcamp A2		12,523	
Lateral TD (Wolfcamp A2)		12,523	23000

### 2. ESTIMATED DEPTH OF WATER, OIL, GAS & OTHER MINERAL BEARING FORMATIONS

The estimated depths at which the top and bottom of the anticipated water, oil, gas, or other mineral bearing formations are expected to be encountered are as follows:

Substance	Formation	Depth
Deepest Expected Base of Fresh Water		700
Water	Rustler	800
Water	Bell Canyon	4930
Water	Cherry Canyon	5970
Oil/Gas	Brushy Canyon	7620
Oil/Gas	Bone Spring Limestone	9090
Oil/Gas	Upr. Avalon	9120
Oil/Gas	Top Bone Spring 1	10040
Oil/Gas	Top Bone Spring 2	10700
Oil/Gas	Top Bone Spring 3	11740
Oil/Gas	Wolfcamp	12140
Oil/Gas	Wolfcamp A1	12193
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All shows of fresh water and minerals will be reported and protected.

### 3. BOP EQUIPMENT

Will have a minimum of a 10000 psi rig stack (see proposed schematic) for drill out below surface (Wolfcamp is not exposed until drillout of the intermediate casing). Could possibly utilize the 5000 psi rig stack (see proposed schematic) for drill out below surface casing due to the availability of 10 M annular. (Wolfcamp is not exposed until drillout of the intermediate casing) Stack will be tested as specified in the attached testing requirements. Batch drilling of the surface, intermediate, and production will take place. A full BOP test will be performed unless approval from BLM is received otherwise. Flex choke hose will be used for all wells on the pad (see attached specs) BOP test will be conducted by a third party.

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#### 4. CASING PROGRAM

a. The proposed casing program will be as follows:

Purpose	From	To	Hole Size	Csg Size	Weight	Grade	Thread	Condition
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Intermediate	0'	11,500'	12-1/4"	9-5/8"	43.5#	HCK-L80	LTC	New
Liner	10,850'	12,300'	8-1/2"	7-5/8"	29.7 #	HCP-110	H513	New
Production (Taper String)	0'	12,500'	6-3/4"	5.5"	20#	P-110-ICY	TXP BTC	New
	12,500'	23,000'	6-3/4"	5"	18#	P-110 IC	TSH521	New

b. Casing design subject to revision based on geologic conditions encountered.

c. \*\*\*A "Worst Case" casing design for wells in a particular area is used below to calculate the Casing Safety Factors. If for any reason the casing design for a particular well requires setting casing deeper than the following "worst case" design, then the Casing Safety Factors will be recalculated & sent to the BLM prior to drilling.

d. Chevron will fill casing at a minimum of every 20 jts (840') while running for intermediate and production casing in order to maintain collapse SF.

#### SF Calculations based on the following "Worst Case" casing design:

Surface Casing: 850'  
Intermediate Casing: 11,200' TVD  
Production Casing: 23,000' MD/12,750' TVD (10,300' VS @ 90 deg inc)

Casing String	Min SF Burst	Min SF Collapse	Min SF Tension	Min SF Tri-Axial
Surface	1.36	3.12	3.17	1.70
Intermediate	1.12	1.44	1.93	1.37
Liner	1.69	5.36	2.50	2.09
Production	1.11	1.23	1.97	1.37

Min SF is the smallest of a group of safety factors that include the following considerations:

	Surf	Int	Liner	Prod
<b>Burst Design</b>				
Pressure Test- Surface, Int, Prod Csg P external: Water P internal: Test psi + next section heaviest mud in csg	X	X	X	X
Displace to Gas- Surf Csg P external: Water P internal: Dry Gas from Next Csg Point	X			
Frac at Shoe, Gas to Surf- Int Csg P external: Water P internal: Dry Gas, 16 ppg Frac Gradient		X	X	
Stimulation (Frac) Pressures- Prod Csg P external: Water P internal: Max inj pressure w/ heaviest injected fluid				X
Tubing leak- Prod Csg (packer at KOP) P external: Water P internal: Leak just below surf, 8.7 ppg packer fluid				X
<b>Collapse Design</b>				
Full Evacuation P external: Water gradient in cement, mud above TOC P internal: none	X	X	X	X
Cementing- Surf, Int, Prod Csg P external: Wet cement P internal: water	X	X	X	X
<b>Tension Design</b>				
100k lb overpull	X	X	X	X

5. **CEMENTING PROGRAM**

Slurry	Type	Top	Bottom	Weight	Yield	%Excess	Sacks	Water
Surface				(ppg)	(sx/cu ft)	Open Hole		gal/sk
Tail	Class C	0'	800'	14.8	1.33	50	650	6.57
Intermediate								
Stage 2 Lead	Class C	0'	4570	11.9	2.39	100	1070	13.46
Stage 2 Tail	Class C	4570	4870	14.8	1.33	25	89	6.35
Stage 1 Lead	50:50 Poz Class C	4,870'	10,650'	11.9	2.21	25	1024	12.18
Stage 1 Tail	Class H	10,650'	11,150'	15.6	1.22	25	184	5.37
Liner								
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Tail	Acid Soluble	10,350'	23,000'	15.6	1.2	10	1300	5.05

1. Final cement volumes will be determined by caliper.
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From	To	Type	Weight	F. Vis	Filtrate
0'	800'	Spud Mud	8.3 - 8.7	32 - 34	NC - NC
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A closed system will be utilized consisting of above ground steel tanks. All wastes accumulated during drilling operations will be contained in a portable trash cage and removed from location and deposited in an approved sanitary landfill. Sanitary wastes will be contained in a chemical porta-toilet and then hauled to an approved sanitary landfill.

All fluids and cuttings will be disposed of in accordance with New Mexico Oil Conservation Division rules and regulations.

A mud test shall be performed every 24 hours after mudding up to determine, as applicable: density, viscosity, gel strength, filtration, and pH.

Visual mud monitoring equipment shall be in place to detect volume changes indicating loss or gain of circulating fluid volume. When abnormal pressures are anticipated -- a pit volume totalizer (PVT), stroke counter, and flow sensor will be used to detect volume changes indicating loss or gain of circulating fluid volume.

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- A Directional Survey will be run.

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No abnormal pressures or temperatures are expected. Estimated BHP at production TD is: 9830 psi
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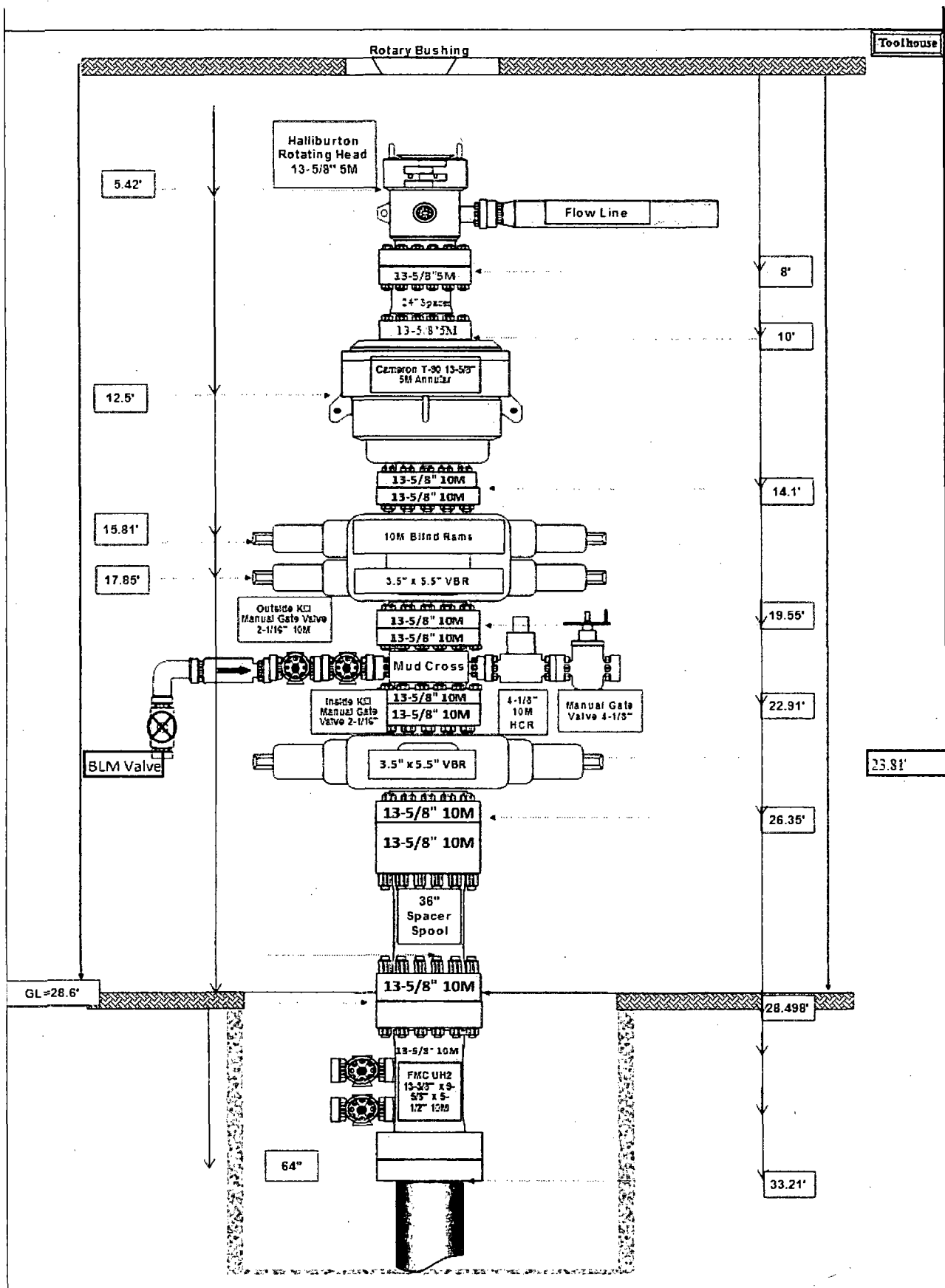


Diagram A

# CHOKE MANIFOLD SCHEMATIC

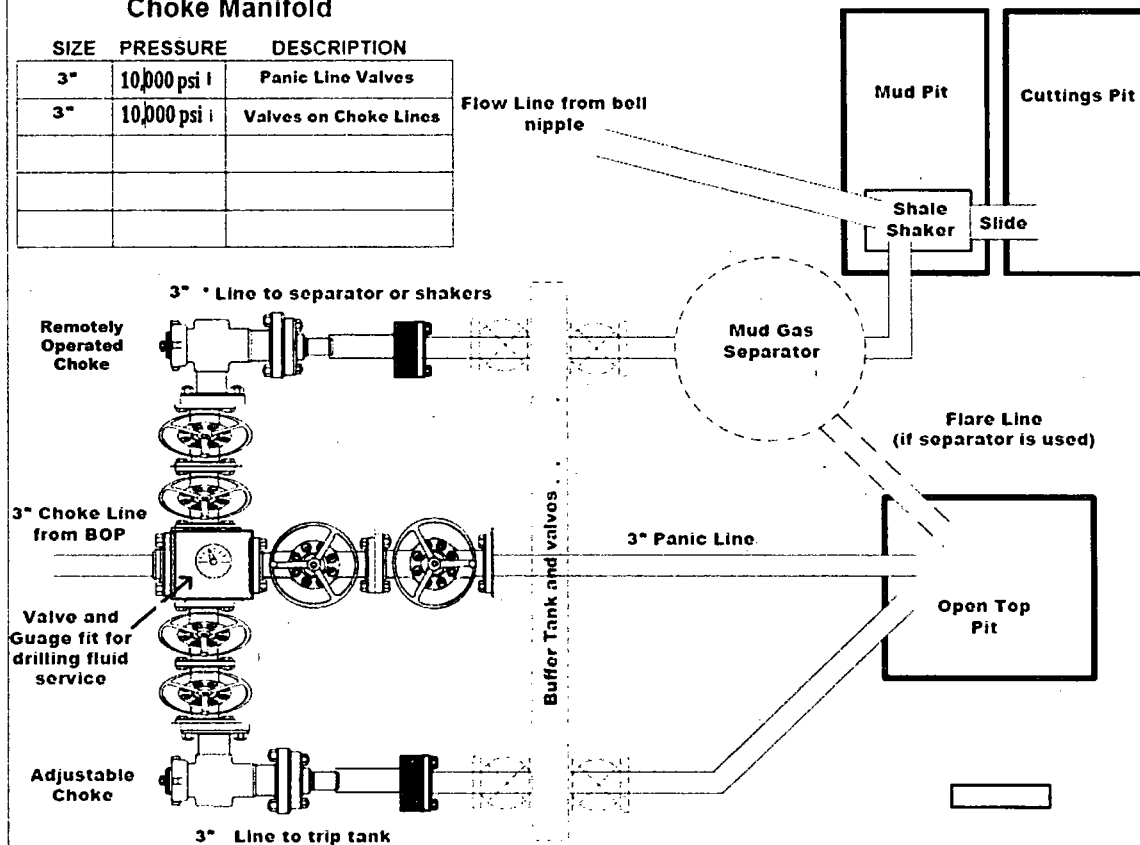
## Minimum Requirements

OPERATION : Wolfcamp A wells

Minimum System  
Pressure Rating : 10,000 psi

### Choke Manifold

SIZE	PRESSURE	DESCRIPTION
3"	10,000 psi	Panic Line Valves
3"	10,000 psi	Valves on Choke Lines



### Installation Checklist

The following item must be verified and checked off prior to pressure testing of BOP equipment.

- ☐ The installed BOP equipment meets at least the minimum requirements (rating, type, size, configuration) as shown on this schematic. Components may be substituted for equivalent equipment rated to higher pressures. Additional components may be put into place as long as they meet or exceed the minimum pressure rating of the system.
- ☐ Adjustable Chokes may be Remotely Operated but will have backup hand pump for hydraulic actuation in case of loss of rig air pressure or power.
- ☐ Flare and Panic lines will terminate a minimum of 150' from the wellhead. These lines will terminate at a location as per approved APD.
- ☐ The choke line, kill line, and choke manifold lines will be straight unless turns use toe blocks or are targeted with running toss, and will be anchored to prevent whip and reduce vibration. This excludes the line between mud gas separator and shale shaker.
- ☐ All valves (except chokes) on choke line, kill line, and choke manifold will be full opening and will allow straight through flow. This excludes any valves between mud gas separator and shale shakers.
- ☐ All manual valves will have hand wheels installed.
- ☐ If used, flare system will have effective method for ignition
- ☐ All connections will be flanged, welded, or clamped (no threaded connections like hammer unions)
- ☐ If buffer tank is used, a valve will be used on all lines at any entry or exit point to or from the buffer tank.

After Installation Checklist is complete, fill out the information below and email to Superintendent and Drilling Engineer

Wellname: \_\_\_\_\_

Representative: \_\_\_\_\_

Date: \_\_\_\_\_

Diagram B

# **10M BLOWOUT PREVENTER SCHEMATIC**

Minimum Requirements

**OPERATION:** Wolfcamp Wells in Salado Draw

**Minimum System Pressure Rating: 10,000 PSI**

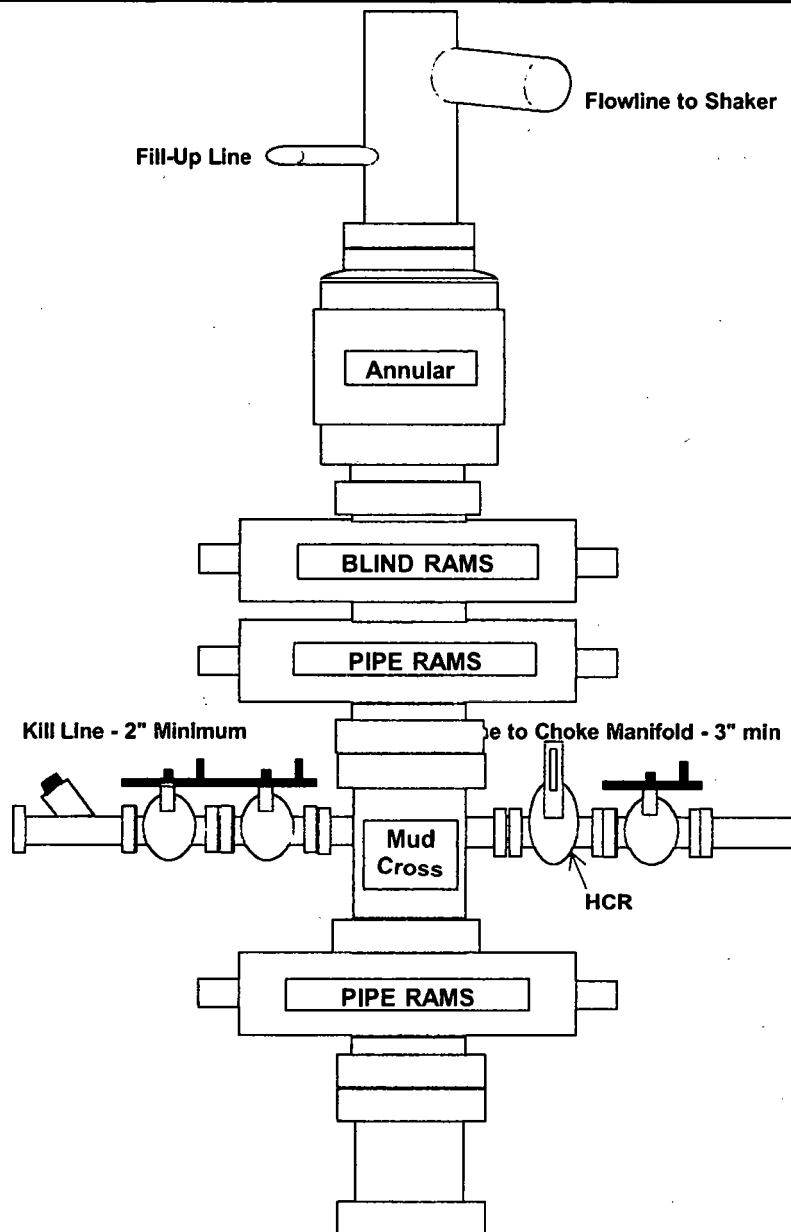


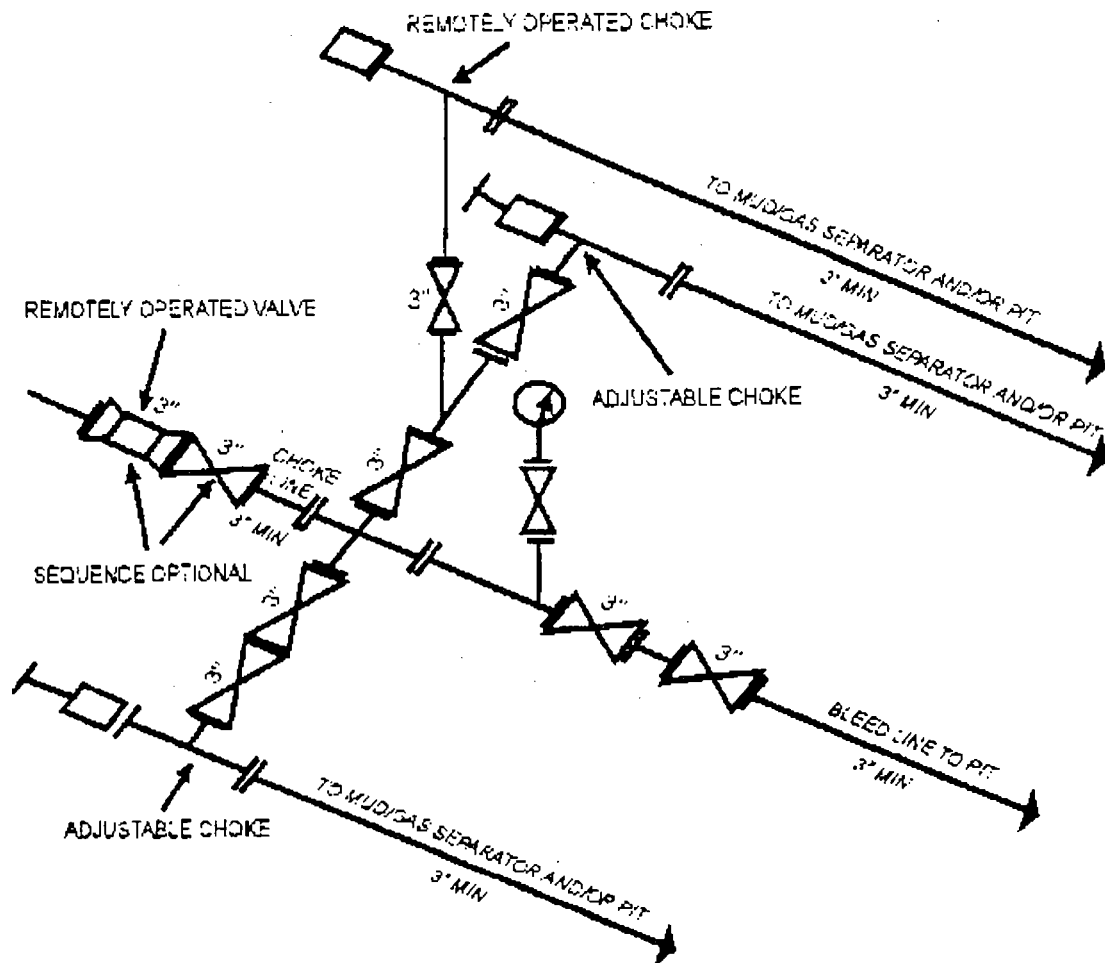
Diagram C

# 10M Choke Manifold SCHEMATIC

Minimum Requirements

**OPERATION:** Production and Open Hole Sections

**Minimum System Pressure Rating: 10,000 PSI**



10M AND 15M CHOKE MANIFOLD EQUIPMENT - CONFIGURATION OF CHOKES MAY VARY

[53 FR 49661, Dec. 9, 1988 and 54 FR 39528, Sept. 27, 1989]

Diagram D



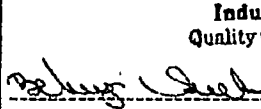
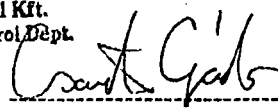


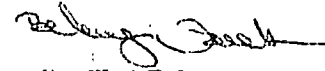
ContiTech

CONTITECH RUBBER  
Industrial Kft.

No: QC-DB- 231/ 2014

Page: 10 / 119

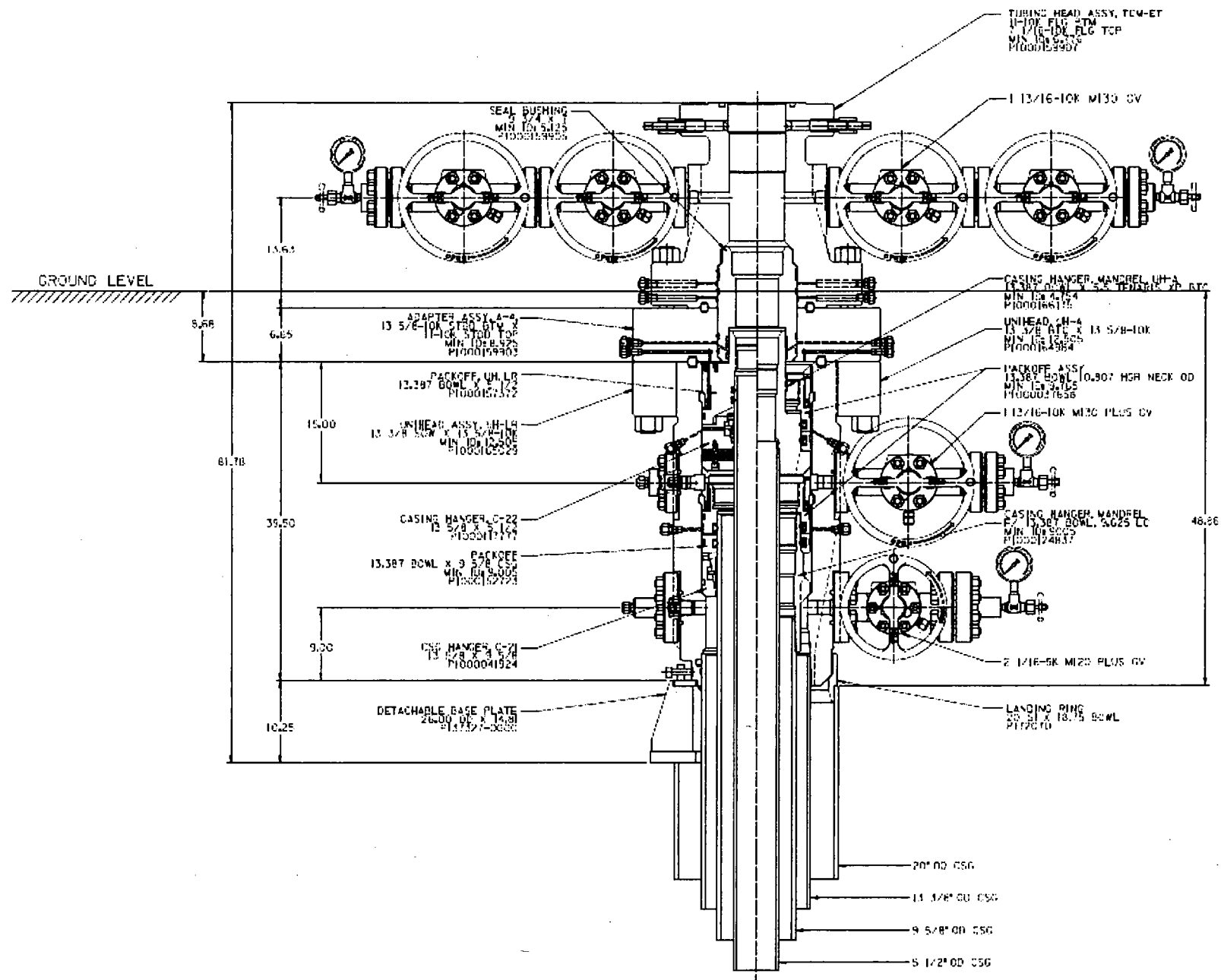
QUALITY CONTROL INSPECTION AND TEST CERTIFICATE				CERT. N°: 594	
PURCHASER: ContiTech Oil & Marine Corp.			P.O. N°: 4500412631		
CONTITECH ORDER N°: 538332		HOSE TYPE: 3" ID Choke & Kill Hose			
HOSE SERIAL N°: 67349		NOMINAL / ACTUAL LENGTH: 13,72 m / 13,85 m			
W.P. 68,9 MPa 10000 psi		T.P. 103,4 MPa 15000 psi		Duration: 60 min.	
Pressure test with water at ambient temperature					
See attachment. ( 1 page )					
↑ 10 mm = 10 Min. → 10 mm = 25 MPa					
COUPLINGS Type		Serial N°		Quality	
3" coupling with 4 1/16" 10K API Swivel Flange end Hub		1435 1436		AISI 4130 AISI 4130 AISI 4130	
				Heat N° A1258U 034939 A1045N	
Not Designed For Well Testing				API Spec 16 C	
Tag No.: 66 – 1198				Temperature rate: "B"	
All metal parts are flawless					
WE CERTIFY THAT THE ABOVE HOSE HAS BEEN MANUFACTURED IN ACCORDANCE WITH THE TERMS OF THE ORDER INSPECTED AND PRESSURE TESTED AS ABOVE WITH SATISFACTORY RESULT.					
STATEMENT OF CONFORMITY: We hereby certify that the above items/equipment supplied by us are in conformity with the terms, conditions and specifications of the above Purchaser Order and that these items/equipment were fabricated inspected and tested in accordance with the referenced standards, codes and specifications and meet the relevant acceptance criteria and design requirements.					
Date:  03. April 2014.		Inspector		Quality Control ContiTech Rubber Industrial Kft. Quality Control Dept. (1)  	



ChemTech Rubber  
Industrial Kit.  
Quality Control Dept.  
(1)

GNr	+19.7	°C	10
RDr	+20.7	°C	10
EL	+1057	bar	10
GNr	+19.7	°C	10
RDr	+20.7	°C	10
EL	+1058	bar	10
GNr	+19.7	°C	10
RDr	+20.7	°C	10
EL	+1058	bar	10
GNr	+19.7	°C	10
RDr	+20.7	°C	10
EL	+1057	bar	10
GNr	+19.7	°C	10
RDr	+20.7	°C	10
EL	+1058	bar	10
GNr	+19.7	°C	10
RDr	+20.7	°C	10
EL	+1058	bar	10

02-09-2019 22:50  
17341 4720



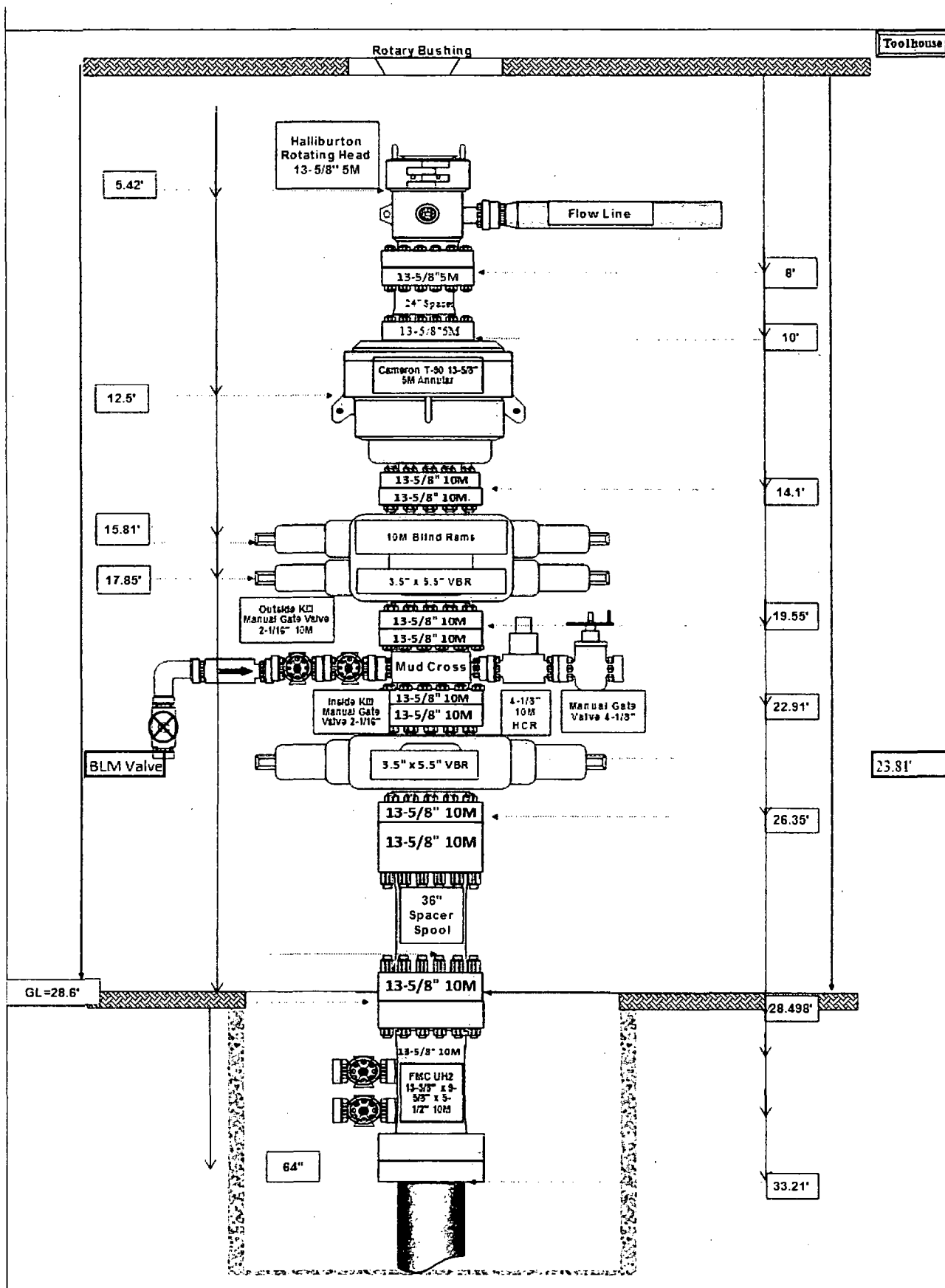


Diagram A

# CHOKE MANIFOLD SCHEMATIC

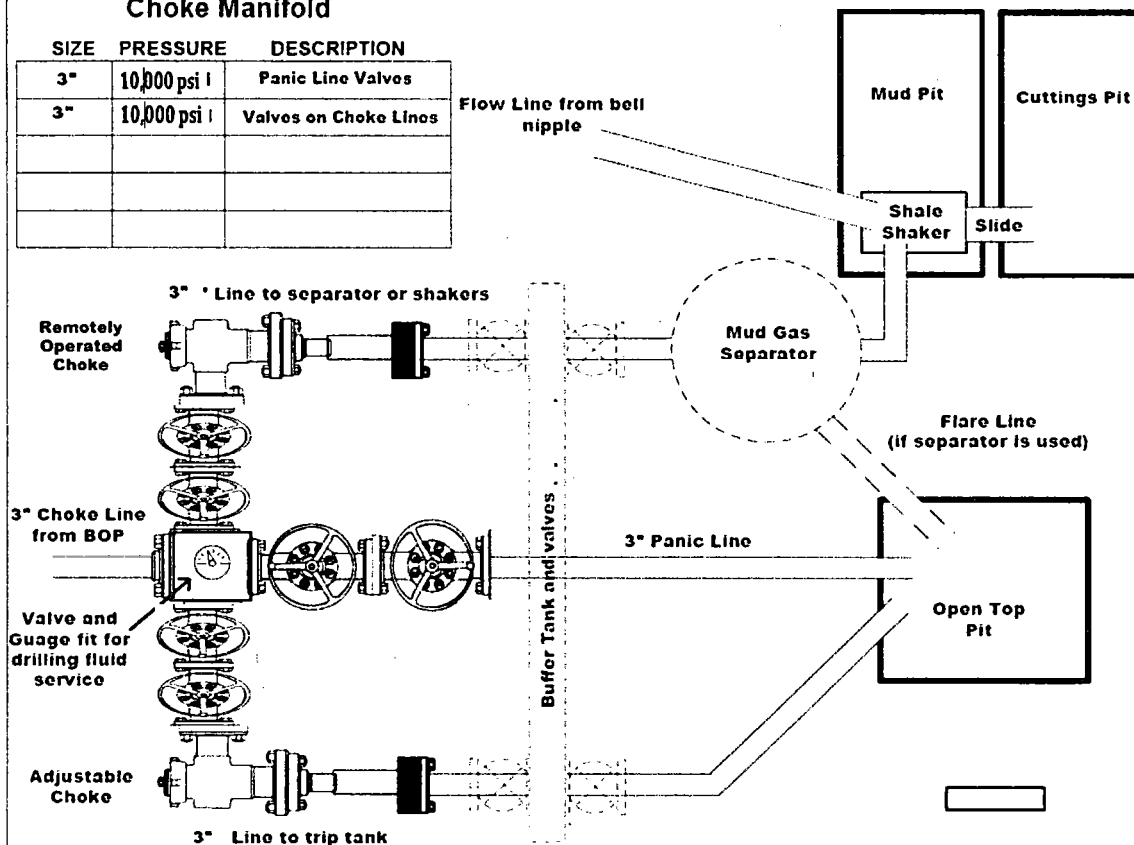
## Minimum Requirements

OPERATION : Wolfcamp A wells

Minimum System  
Pressure Rating : 10,000 psi

## Choke Manifold

SIZE	PRESSURE	DESCRIPTION
3"	10,000 psi	Panic Line Valves
3"	10,000 psi	Valves on Choke Lines



## Installation Checklist

The following item must be verified and checked off prior to pressure testing of BOP equipment.

- ☐ The installed BOP equipment meets at least the minimum requirements (rating, type, size, configuration) as shown on this schematic. Components may be substituted for equivalent equipment rated to higher pressures. Additional components may be put into place as long as they meet or exceed the minimum pressure rating of the system.
- ☐ Adjustable Chokes may be Remotely Operated but will have backup hand pump for hydraulic actuation in case of loss of rig air pressure or power.
- ☐ Flare and Panic lines will terminate a minimum of 150' from the wellhead. These lines will terminate at a location as per approved APD.
- ☐ The choke line, kill line, and choke manifold lines will be straight unless turns use tee blocks or are targeted with running tool, and will be anchored to prevent whip and reduce vibration. This excludes the line between mud gas separator and shale shaker.
- ☐ All valves (except chokes) on choke line, kill line, and choke manifold will be full opening and will allow straight through flow. This excludes any valves between mud gas separator and shale shakers.
- ☐ All manual valves will have hand wheels installed.
- ☐ If used, flare system will have effective method for ignition
- ☐ All connections will be flanged, welded, or clamped (no threaded connections like hammer unions)
- ☐ If buffer tank is used, a valve will be used on all lines at any entry or exit point to or from the buffer tank.

After Installation Checklist is complete, fill out the information below and email to Superintendent and Drilling Engineer

Wellname: \_\_\_\_\_

Representative: \_\_\_\_\_

Date: \_\_\_\_\_

Diagram B

# **10M BLOWOUT PREVENTER SCHEMATIC**

Minimum Requirements

**OPERATION:** Wolfcamp Wells in Salado Draw

**Minimum System Pressure Rating: 10,000 PSI**

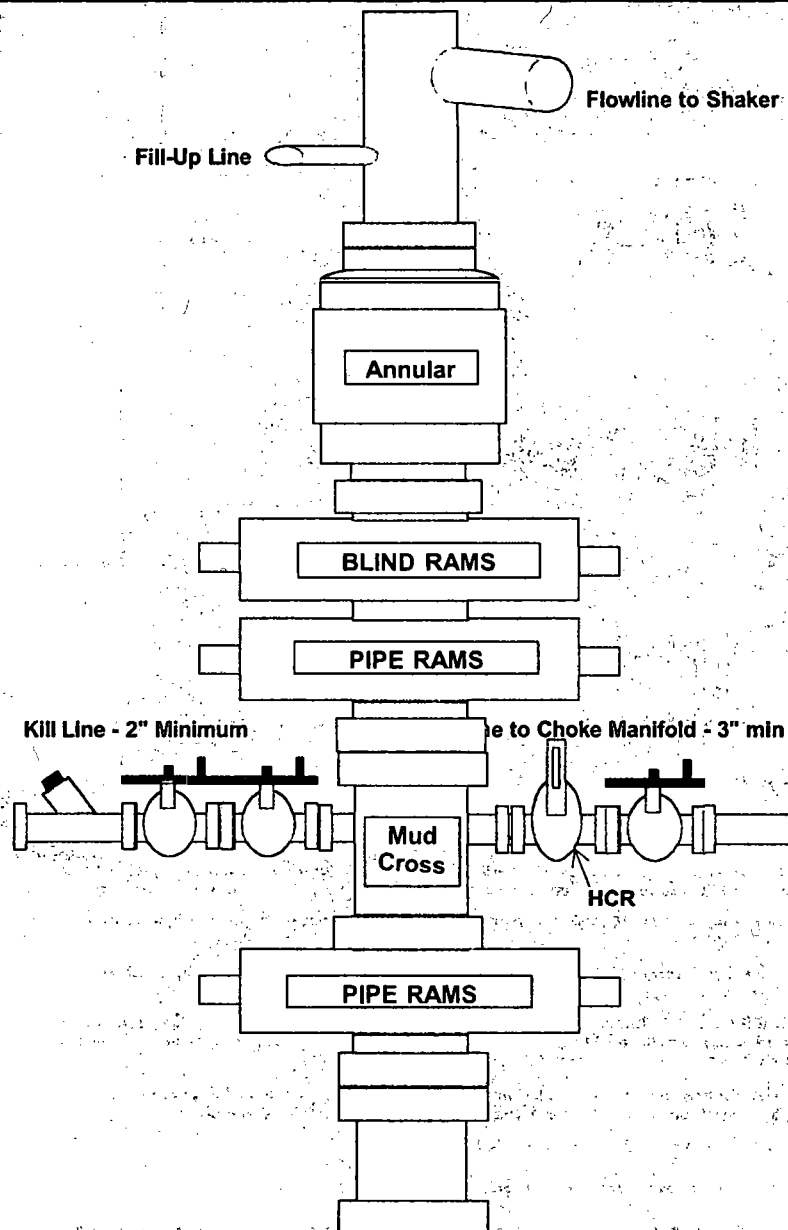


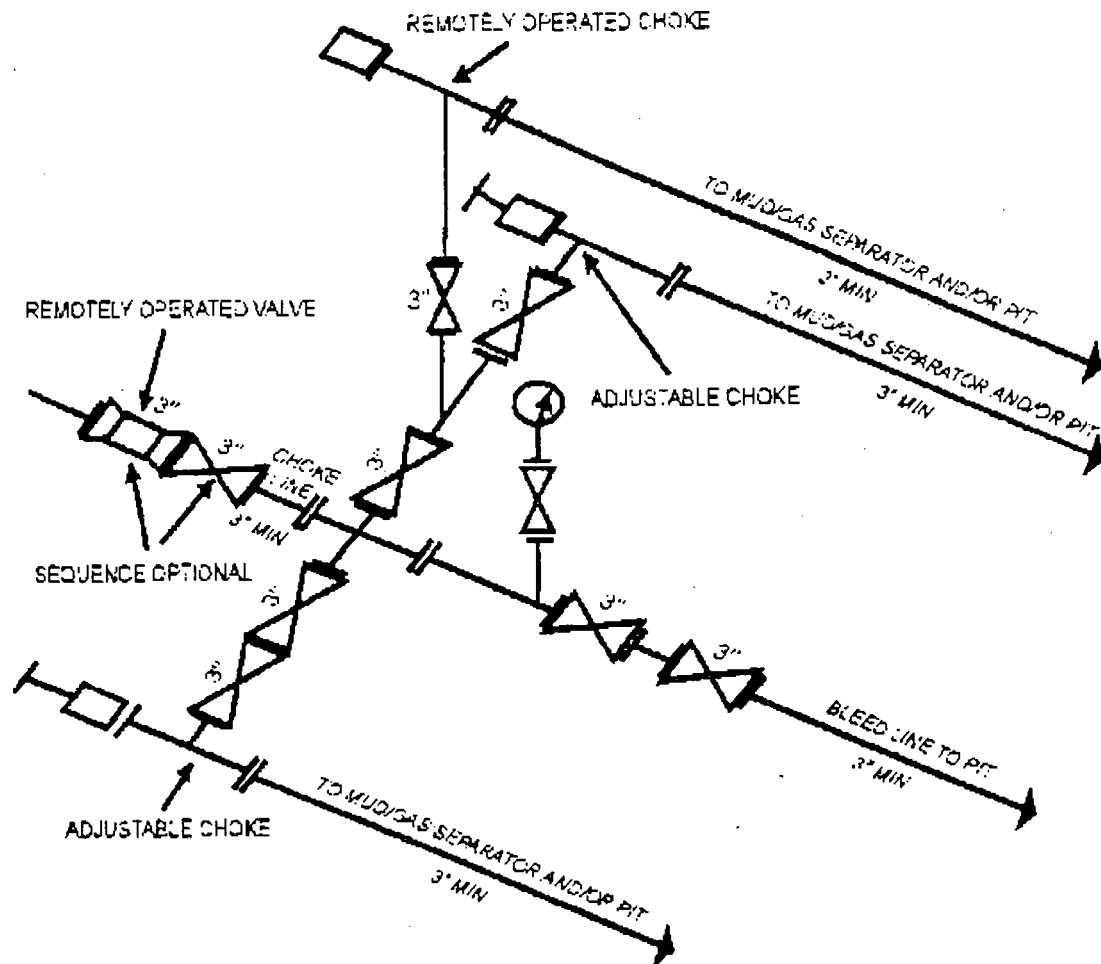
Diagram C

# 10M Choke Manifold SCHEMATIC

Minimum Requirements

**OPERATION:** Production and Open Hole Sections

**Minimum System Pressure Rating: 10,000 PSI**



10M AND 15M CHOKE MANIFOLD EQUIPMENT - CONFIGURATION OF CHOKES MAY VARY

[53 FR 49661, Dec. 9, 1988 and 54 FR 39528, Sept. 27, 1989]

Diagram D

For the latest performance data, always visit our website: [www.tenaris.com](http://www.tenaris.com)

January 18 2016



**Connection:** TenarisXP® BTC  
**Casing/Tubing:** CAS  
**Coupling Option:** REGULAR

**Size:** 5.500 in.  
**Wall:** 0.361 in.  
**Weight:** 20.00 lbs/ft  
**Grade:** P110-ICY  
**Min. Wall Thickness:** 87.5 %

#### PIPE BODY DATA

GEOMETRY			
Nominal OD	5.500 in.	Nominal Weight	20.00 lbs/ft
Nominal ID	4.778 in.	Wall Thickness	0.361 in.
Plain End Weight	19.83 lbs/ft	Standard Drift Diameter	4.653 in.
		Special Drift Diameter	N/A

#### PERFORMANCE

Body Yield Strength	729 x 1000 lbs	Internal Yield	14360 psi
Collapse	12100 psi	SMYS	125000 psi

#### TENARISXP® BTC CONNECTION DATA

GEOMETRY			
Connection OD	6.100 in.	Coupling Length	9.450 in.
Critical Section Area	5.828 sq. in.	Threads per in.	5.00
		Connection ID	4.766 in.
		Make-Up Loss	4.204 in.

#### PERFORMANCE

Tension Efficiency	100 %	Joint Yield Strength	729 x 1000 lbs
Structural Compression Efficiency	100 %	Structural Compression Strength	729 x 1000 lbs
External Pressure Capacity	12100 psi	Internal Pressure Capacity <sup>(1)</sup>	14360 psi
		Structural Bending <sup>(2)</sup>	104 °/100 ft

#### ESTIMATED MAKE-UP TORQUES<sup>(3)</sup>

Minimum	11540 ft-lbs	Optimum	12820 ft-lbs
		Maximum	14100 ft-lbs

#### OPERATIONAL LIMIT TORQUES

Operating Torque	22700 ft-lbs	Yield Torque	25250 ft-lbs
------------------	--------------	--------------	--------------

#### BLANKING DIMENSIONS

##### Blanking Dimensions



- **(1)** Internal Pressure Capacity related to structural resistance only. Internal pressure leak resistance as per section 10.3 API 5C3 / ISO 10400 - 2007.
  - (2)** Structural rating, pure bending to yield (i.e no other loads applied)
  - (3)** Torque values calculated for API Modified thread compounds with Friction Factor=1. For other thread compounds please contact us at [licensees@oilfield.tenaris.com](mailto:licensees@oilfield.tenaris.com). Torque values may be further reviewed.
- For additional information, please contact us at [contact-tenarishydri@tenaris.com](mailto:contact-tenarishydri@tenaris.com)

For the latest performance data, always visit our website: [www.tenaris.com](http://www.tenaris.com)

June 17 2015



**Connection:** Wedge 521™  
**Casing/Tubing:** CAS

**Size:** 5.000 in.  
**Wall:** 0.362 in.  
**Weight:** 18.00 lbs/ft  
**Grade:** P110-IC  
**Min. Wall Thickness:** 87.5 %

#### PIPE BODY DATA

GEOMETRY			
Nominal OD	<b>5.000 in.</b>	Nominal Weight	<b>18.00 lbs/ft</b>
Nominal ID	<b>4.276 in.</b>	Wall Thickness	<b>0.362 in.</b>
Plain End Weight	<b>17.95 lbs/ft</b>	Standard Drift Diameter	<b>4.151 in.</b>
		Special Drift Diameter	<b>N/A</b>
PERFORMANCE			
Body Yield Strength	<b>580 x 1000 lbs</b>	Internal Yield	<b>13940 psi</b>
Collapse	<b>14840 psi</b>	SMYS	<b>110000 psi</b>

#### WEDGE 521™ CONNECTION DATA

GEOMETRY			
Connection OD	<b>5.359 in.</b>	Connection ID	<b>4.226 in.</b>
Critical Section Area	<b>3.891 sq. in.</b>	Make-Up Loss	<b>3.620 in.</b>
		Threads per in.	<b>3.36</b>
PERFORMANCE			
Tension Efficiency	<b>73.8 %</b>	Joint Yield Strength	<b>428 x 1000 lbs</b>
Compression Strength	<b>514 x 1000 lbs</b>	Internal Pressure Capacity	<b>13940 psi</b>
External Pressure Capacity	<b>14840 psi</b>	Compression Efficiency	<b>88.7 %</b>
		Bending	<b>75 °/100 ft</b>
MAKE-UP TORQUES			
Minimum	<b>6100 ft-lbs</b>	Optimum	<b>7300 ft-lbs</b>
		Maximum (±)	<b>10700 ft-lbs</b>
OPERATIONAL LIMIT TORQUES			
Operating Torque	<b>17300 ft-lbs</b>	Yield Torque	<b>26000 ft-lbs</b>
BLANKING DIMENSIONS			

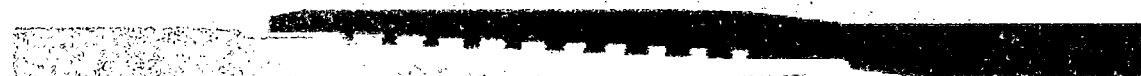
Blanking Dimensions

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\* If you need to use torque values that are higher than the maximum indicated, please contact a local Tenaris technical sales representative.

TH DS-16.0372 23 August 2016  
Rev 00

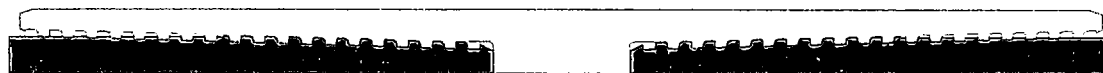
## 5.000" 18.00 lb/ft P110-ICY TenarisHydril Wedge 521®



PIPE BODY DATA					
GEOMETRY					
Nominal OD	5.000 in.	Nominal Weight	18.00 lbs/ft	Standard Drift Diameter	4.151 in.
Nominal ID	4.276 in.	Wall Thickness	0.362 in.	Special Drift Diameter	N/A
Plain End Weight	17.95 lbs/ft				
PERFORMANCE					
Body Yield Strength	659 x 1000 lbs.	Internal Yield <sup>1</sup>	16290 psi	Collapse	14840 psi
CONNECTION DATA					
GEOMETRY					
Box OD (Turned)	5.359 in.	Pin ID (Bored)	4.226 in.	Make-Up Loss	3.62 in.
Critical Section Area	3.891 sq. in.	Threads per in.	3.36		
PERFORMANCE					
Tension Efficiency	73.8 %	Joint Yield Strength	486 x 1000 lbs	Internal Yield <sup>1</sup>	16290 psi
Compression Efficiency	88.7 %	Compression Rating	585 x 1000 lbs	Collapse	14840 psi
Bending	85°/100 ft				
MAKE-UP TORQUES					
Minimum	6100 ft-lbs	Optimum	7300 ft-lbs	Maximum*	10700 ft-lbs
OPERATIONAL LIMIT TORQUES					
Operational	20000 ft-lbs			Yield Torque	30000 ft-lbs

\*If you need to use torque values that are higher than the maximum indicated, please contact a local Tenaris technical sales representative

1. Internal Yield Rating is based on 90% RBW.

**5" 18.00 ppf P110-ICY - TenarisXP® BTC (min wt 90%)  
(USC Units)**


PIPE BODY DATA					
GEOMETRY					
Nominal OD	5.000 in.	Nominal Weight	18.00 lbs/ft	Standard Drift Diameter	4.151 in.
Nominal ID	4.276 in.	Wall Thickness	0.362 in.	Special Drift Diameter	-
Plain End Weight	17.95 lbs/ft				
PERFORMANCE					
Body Yield Strength	659 x 1000 lbs	Internal Yield <sup>(4)</sup>	16290 psi	Collapse	14840 psi
CONNECTION DATA					
Regular OD	5.720 in.	Coupling Length	9.325 in.	Connection ID	4.264 in.
Critical Section Area	5.275 sq. in.	Threads per in.	5	Make-Up Loss	4.141 in.
PERFORMANCE					
Tension Efficiency	100.0 %	Joint Yield Strength	659 x 1000 lbs	Internal Pressure Capacity <sup>(1) (4)</sup>	16290 psi
Structural Compression Efficiency	100.0 %	Structural Compression Rating	659 x 1000 lbs	External Pressure Capacity	14840 psi
Structural Bending <sup>(2)</sup>	115°/100 ft				
MAKE-UP TORQUES <sup>(3)</sup>					
Minimum	11480 ft-lbs	Target	12750 ft-lbs	Maximum	14030 ft-lbs
Operating Torque	15800 ft-lbs	Yield Torque	17700 ft-lbs		

(1) Internal Yield pressure related to structural resistance only. Internal pressure leak resistance as per section 10.3 API 5C3 / ISO 10400 - 2007.

(2) Structural rating, pure bending to yield (i.e no other loads applied)

(3) Torque values calculated for API Modified thread compounds with Friction Factor=1. For other thread compounds please contact us at [licensees@oilfield.tenaris.com](mailto:licensees@oilfield.tenaris.com).

(4) Minimum wall thickness 90% of nominal

### 1. FORMATION TOPS

The estimated tops of important geologic markers are as follows:

FORMATION	SUB-SEA TVD	KBTVD	MD
Rustler		800	
Castile		3480	
Lamar		4900	
Bell Canyon		4930	
Cherry Canyon		5970	
Brushy Canyon		7620	
Bone Spring Limestone		9090	
Upr. Avalon		9120	
Top Bone Spring 1		10040	
Top Bone Spring 2		10700	
Top Bone Spring 3		11740	
Wolfcamp		12140	
Wolfcamp A1		12193	
Wolfcamp A2		12,523	
Lateral TD (Wolfcamp A2)		12,523	23000

### 2. ESTIMATED DEPTH OF WATER, OIL, GAS & OTHER MINERAL BEARING FORMATIONS

The estimated depths at which the top and bottom of the anticipated water, oil, gas, or other mineral bearing formations are expected to be encountered are as follows:

Substance	Formation	Depth
Deepest Expected Base of Fresh Water		700
Water	Rustler	800
Water	Bell Canyon	4930
Water	Cherry Canyon	5970
Oil/Gas	Brushy Canyon	7620
Oil/Gas	Bone Spring Limestone	9090
Oil/Gas	Upr. Avalon	9120
Oil/Gas	Top Bone Spring 1	10040
Oil/Gas	Top Bone Spring 2	10700
Oil/Gas	Top Bone Spring 3	11740
Oil/Gas	Wolfcamp	12140
Oil/Gas	Wolfcamp A1	12193
Oil/Gas	Wolfcamp A2	12,523

All shows of fresh water and minerals will be reported and protected.

### 3. BOP EQUIPMENT

Will have a minimum of a 10000 psi rig stack (see proposed schematic) for drill out below surface (Wolfcamp is not exposed until drillout of the intermediate casing). Could possibly utilize the 5000 psi rig stack (see proposed schematic) for drill out below surface casing due to the availability of 10 M annular. (Wolfcamp is not exposed until drillout of the intermediate casing) Stack will be tested as specified in the attached testing requirements. Batch drilling of the surface, intermediate, and production will take place. A full BOP test will be performed unless approval from BLM is received otherwise. Flex choke hose will be used for all wells on the pad (see attached specs) BOP test will be conducted by a third party.

Chevron requests a variance to use a FMC UH2 Multibowl wellhead, which will be run through the rig floor on surface casing. BOPE will be nipped up and tested after cementing surface casing. Subsequent tests will be performed as needed, not to exceed 30 days. The field report from FMC and BOP test information will be provided in a subsequent report at the end of the well. Please see the attached wellhead schematic. An installation manual has been placed on file with the BLM office and remains unchanged from previous submittal.

#### 4. CASING PROGRAM

a. The proposed casing program will be as follows:

Purpose	From	To	Hole Size	Csg Size	Weight	Grade	Thread	Condition
Surface	0'	800'	17-1/2"	13-3/8"	55 #	J55	STC	New
Intermediate	0'	11,500'	12-1/4"	9-5/8"	43.5#	HCK-L80	LTC	New
Liner	10,850'	12,300'	8-1/2"	7-5/8"	29.7 #	HCP-110	H513	New
Production (Taper String)	0'	12,500'	6-3/4"	5.5"	20#	P-110-ICY	TXP BTC	New
	12,500'	23,000'	6-3/4"	5"	18#	P-110 IC	TSH521	New

b. Casing design subject to revision based on geologic conditions encountered.

c. \*\*\*A "Worst Case" casing design for wells in a particular area is used below to calculate the Casing Safety Factors. If for any reason the casing design for a particular well requires setting casing deeper than the following "worst case" design, then the Casing Safety Factors will be recalculated & sent to the BLM prior to drilling.

d. Chevron will fill casing at a minimum of every 20 jts (840') while running for intermediate and production casing in order to maintain collapse SF.

#### SF Calculations based on the following "Worst Case" casing design:

Surface Casing: 850'  
Intermediate Casing: 11,200' TVD  
Production Casing: 23,000' MD/12,750' TVD (10,300' VS @ 90 deg inc)

Casing String	Min SF Burst	Min SF Collapse	Min SF Tension	Min SF Tri-Axial
Surface	1.36	3.12	3.17	1.70
Intermediate	1.12	1.44	1.93	1.37
Liner	1.69	5.36	2.50	2.09
Production	1.11	1.23	1.97	1.37

Min SF is the smallest of a group of safety factors that include the following considerations:

	Surf	Int	Liner	Prod
<b>Burst Design</b>				
Pressure Test- Surface, Int, Prod Csg P external: Water P internal: Test psi + next section heaviest mud in csg	X	X	X	X
Displace to Gas- Surf Csg P external: Water P internal: Dry Gas from Next Csg Point	X			
Frac at Shoe, Gas to Surf- Int Csg P external: Water P internal: Dry Gas, 16 ppg Frac Gradient		X	X	
Stimulation (Frac) Pressures- Prod Csg P external: Water P internal: Max inj pressure w/ heaviest injected fluid				X
Tubing leak- Prod Csg (packer at KOP) P external: Water P internal: Leak just below surf, 8.7 ppg packer fluid				X
<b>Collapse Design</b>				
Full Evacuation P external: Water gradient in cement, mud above TOC P internal: none	X	X	X	X
Cementing- Surf, Int, Prod Csg P external: Wet cement P internal: water	X	X	X	X
<b>Tension Design</b>				
100k lb overpull	X	X	X	X

5. **CEMENTING PROGRAM**

Slurry	Type	Top	Bottom	Weight	Yield	%Excess	Sacks	Water
Surface				(ppg)	(sx/cu ft)	Open Hole		gal/sk
Tail	Class C	0'	800'	14.8	1.33	50	650	6.57
Intermediate								
Stage 2 Lead	Class C	0'	4570	11.9	2.39	100	1070	13.46
Stage 2 Tail	Class C	4570	4870	14.8	1.33	25	89	6.35
Stage 1 Lead	50:50 Poz Class C	4,870'	10,650'	11.9	2.21	25	1024	12.18
Stage 1 Tail	Class H	10,650'	11,150'	15.6	1.22	25	184	5.37
Liner								
Tail	Class H	10,850'	12,300'	15.6	1.22	17	123	5.34
Production								
Tail	Acid Soluble	10,350'	23,000'	15.6	1.2	10	1300	5.05

1. Final cement volumes will be determined by caliper.
2. Surface casing shall have at least one centralizer installed on each of the bottom three joints starting with the shoe joint.
3. Production casing will have one horizontal type centralizer on every joint for the first 1000' from TD, then every other joint to EOB, and then every third joint to KOP. Bowspring type centralizers will be run from KOP to intermediate casing.



## 6. MUD PROGRAM

From	To	Type	Weight	F. Vis	Filtrate
0'	800'	Spud Mud	8.3 - 8.7	32 - 34	NC - NC
800'	11,150'	Oil Based Mud	8.7-9.2	28 - 30	25-30
11,150'	12,300'	Oil Based Mud	9.5-13.5	70 - 75	25 - 30
12,300'	23,000'	Oil Based Mud	12.0-15.0	70 - 75	25 - 30

A closed system will be utilized consisting of above ground steel tanks. All wastes accumulated during drilling operations will be contained in a portable trash cage and removed from location and deposited in an approved sanitary landfill. Sanitary wastes will be contained in a chemical porta-toilet and then hauled to an approved sanitary landfill.

All fluids and cuttings will be disposed of in accordance with New Mexico Oil Conservation Division rules and regulations.

A mud test shall be performed every 24 hours after mudding up to determine, as applicable: density, viscosity, gel strength, filtration, and pH.

Visual mud monitoring equipment shall be in place to detect volume changes indicating loss or gain of circulating fluid volume. When abnormal pressures are anticipated -- a pit volume totalizer (PVT), stroke counter, and flow sensor will be used to detect volume changes indicating loss or gain of circulating fluid volume.

A weighting agent and lost circulating material (LCM) will be onsite to mitigate pressure or lost circulation as hole conditions dictate.

## 7. TESTING, LOGGING, AND CORING

The anticipated type and amount of testing, logging, and coring are as follows:

- Drill stem tests are not planned.
- The logging program will be as follows:

TYPE	Logs	Interval	Timing	Vendor
Mudlogs	2 man mudlog	Int Csg to TD	Drillout of Int Csg	TBD
LWD	MWD Gamma	Int. and Prod. Hole	While Drilling	TBD

- Conventional whole core samples are not planned.
- A Directional Survey will be run.

## 8. ABNORMAL PRESSURES AND HYDROGEN SULFIDE

- No abnormal pressures or temperatures are expected. Estimated BHP at intermediate TD is: 5750 psi  
No abnormal pressures or temperatures are expected. Estimated BHP at production TD is: 9830 psi
- Hydrogen sulfide gas is not anticipated. An H2S Contingency plan is attached with this APD in the event that H2S is encountered

**Casing and Tubing Performance Data****PIPE BODY DATA****GEOMETRY**

Outside Diameter	9.625 in	Wall Thickness	0.435 in	API Drift Diameter	8.599 in
Nominal Weight	43.50 lbs/ft	Nominal ID	8.755 in	Alternative Drift Diameter	8.625 in
Plain End Weight	42.73 lbs/ft	Nominal cross section	12.559 in		

**PERFORMANCE**

Steel Grade	L80	Minimum Yield	80,000 psi	Minimum Ultimate	95,000 psi
Tension Yield	1,005,000 in	Internal Pressure Yield	6,330 psi	Collapse Pressure	3,810 psi
Available Seamless	Yes	Available Welded	No		

**CONNECTION DATA****TYPE: LTC****GEOMETRY**

Coupling Reg OD	10.625 in	Threads per in	8	Thread turns make up	3.5
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**PERFORMANCE**

Steel Grade	L80	Coupling Min Yield	80,000 psi	Coupling Min Ultimate	95,000 psi
Joint Strength	813,000 lbs			Internal Pressure Resistance	6,330 psi

**Operator Name:** CHEVRON USA INCORPORATED

**Well Name:** SD EA 18 19 FED COM P15

**Well Number:** 19H

**Disturbance type:** EXISTING ACCESS ROAD

**Describe:**

**Surface Owner:** BUREAU OF LAND MANAGEMENT

**Other surface owner description:**

**BIA Local Office:**

**BOR Local Office:**

**COE Local Office:**

**DOD Local Office:**

**NPS Local Office:**

**State Local Office:**

**Military Local Office:**

**USFWS Local Office:**

**Other Local Office:**

**USFS Region:**

**USFS Forest/Grassland:**

**USFS Ranger District:**

**Disturbance type:** WELL PAD

**Describe:**

**Surface Owner:** OTHER

**Other surface owner description:** A E & J ROYALTIES, LLC

**BIA Local Office:**

**BOR Local Office:**

**COE Local Office:**

**DOD Local Office:**

**NPS Local Office:**

**State Local Office:**

**Military Local Office:**

**USFWS Local Office:**

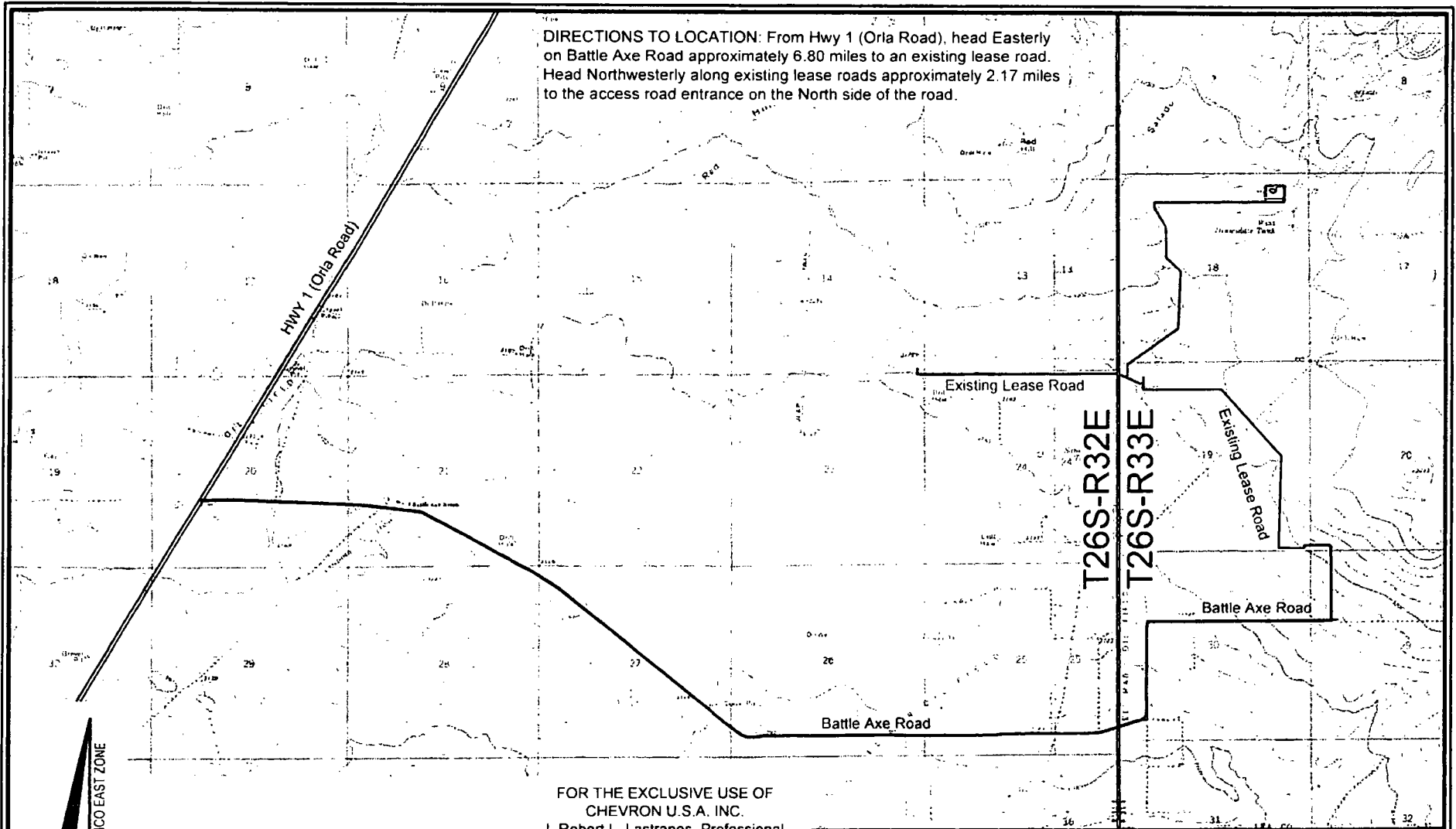
**Other Local Office:**

**USFS Region:**

**USFS Forest/Grassland:**

**USFS Ranger District:**

DIRECTIONS TO LOCATION: From Hwy 1 (Orla Road), head Easterly on Battle Axe Road approximately 6.80 miles to an existing lease road. Head Northwesterly along existing lease roads approximately 2.17 miles to the access road entrance on the North side of the road.



NAD 27 NEW MEXICO EAST ZONE

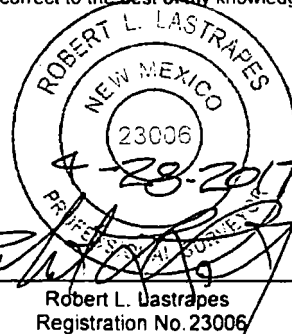
#### LEGEND

- Proposed Well
- Proposed Access Road
- Proposed Drillsite
- Existing Road
- Township/Range Line

Scale: 1" = 4,000'

4,000' 0 2,000' 4,000'

FOR THE EXCLUSIVE USE OF  
CHEVRON U.S.A. INC.  
I, Robert L. Lastrapes, Professional  
Surveyor, do hereby state this plat is true  
and correct to the best of my knowledge.



#### ROAD PLAT

**CHEVRON U.S.A. INC.**

SD EA 18 19 FED COM P15 NO. 16H WELL  
LOCATED 455' FNL & 980' FEL  
SECTION 18, T26S-R33E  
LEA COUNTY, NEW MEXICO

DRAWN BY: BOR	REVISIONS		
PROJ. MGR.: VHV	No. 2	DATE: 04/24/2017	REVISED BY: BOR
DATE: 03/22/2017	No. 3	DATE: 04/28/2017	REVISED BY: BOR
FILENAME: T:\2017\2175527\DWG\SD EA 18 19 Fed Com P15 16H_Road Plat.dwg			



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