### 1. Geologic Formations

TVD of target	10517'	Pilot Hole Depth	N/A
MD at TD:	20667'	Deepest Expected fresh water:	909'

**Delaware Basin** 

Formation	TVD - RKB	<b>Expected</b> Fluids
Rustler	909	Water/Oil/Gas
Salado	1005	
Castile	3292	
Lamar/Delaware	4662	
Bell Canyon*	4677	
Cherry Canyon*	5555	
Brushy Canyon*	6896	Oil/Gas
Bone Spring	8489	Oil/Gas
1st Bone Spring	9662	Oil/Gas
2nd Bone Spring	9934	Oil/Gas

\*H2S, water flows, loss of circulation, abnormal pressures, etc.

### 2. Casing Program

									Buoyant	Buoyant
	Casing Int	erval	Csg. Size	Weight	0	<b>C</b>	SF		Body SF	Joint SF
Hole Size (in)	From (ft)	To (ft)	(in)	(lbs)	Grade	Conn.	Collapse	SF BUIST	Tension	Tension
17.5	0	959	13.375	54.5	J55	BTC	2.19	1.31	2.41	2.59
12.25	0	7500	9.625	47	L80	BTC	1.21	1.43	1.84	1.93
12.25	7500	9903	9.625	47	HP L80	BTC	1.19	1.48	3.54	4.39
8.5	9803	20667	5.5	20	P-110	DQX	1.98	1.20	2.31	2.54

All casing strings will be tested in accordance with Onshore Oil and Gas Order #2 III.B.1.h \*OXY requests the option to set casing shallower yet still below the salts if losses or hole conditions require this. Cement volumes may be adjusted if casing is set shallower and a DV tool will be run in case a contingency second stage is required for cement to reach surface. If cement circulated to surface during first stage we will drop a cancelation cone and not pump the second stage.

	YOTN		
Is casing new? If used, attach certification as required in Onshore Order #1	Y		
Does casing meet API specifications? If no, attach casing specification sheet.			
Is premium or uncommon casing planned? If yes attach casing specification sheet.	Y		
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y		
Will the intermediate pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?			
Is well located within Capitan Reef?	N		
If yes, does production casing cement tie back a minimum of 50' above the Reef?			
Is well within the designated 4 string boundary.			



# **OXY USA Inc** APD ATTACHMENT: SPUDDER RIG DATA

### **OPERATOR NAME / NUMBER:** <u>OXY USA Inc</u>

#### **1. SUMMARY OF REQUEST:**

Oxy USA respectfully requests approval for the following operations for the surface hole in the drill plan:

1. Utilize a spudder rig to pre-set surface casing for time and cost savings.

### 2. Description of Operations

- 1. Spudder rig will move in to drill the surface hole and pre-set surface casing on the well.
  - **a.** After drilling the surface hole section, the spudder rig will run casing and cement following all of the applicable rules and regulations (OnShore Order 2, all COAs and NMOCD regulations).
  - **b.** The spudder rig will utilize fresh water-based mud to drill the surface hole to TD. Solids control will be handled entirely on a closed loop basis. No earth pits will be used.
- 2. The wellhead will be installed and tested as soon as the surface casing is cut off and the WOC time has been reached.
- 3. A blind flange at the same pressure rating as the wellhead will be installed to seal the wellbore. Pressure will be monitored with needle valves installed on two wingvalves.

**a.** A means for intervention will be maintained while the drilling rig is not over the well.

- 4. Spudder rig operations are expected to take 2-3 days per well on the pad.
- 5. The BLM will be contacted and notified 24 hours prior to commencing spudder rig operations.
- 6. Drilling operations will begin with a larger rig and a BOP stack equal to or greater than the pressure rating that was permitted will be nippled up and tested on the wellhead before drilling operations resume on each well.
  - **a.** The larger rig will move back onto the location within 90 days from the point at which the wells are secured and the spudder rig is moved off location.
  - **b.** The BLM will be contacted / notified 24 hours before the larger rig moves back on the pre-set locations.
- 7. Oxy will have supervision on the rig to ensure compliance with all BLM and NMOCD regulations and to oversee operations.
- 8. Once the rig is removed, Oxy will secure the wellhead area by placing a guard rail around the cellar area.

# PERFORMANCE DATA

TMK UP DQX Technical Data Sheet 5.500 in

20.00 lbs/ft

10

P-110

psi lbs lbs psi psi

Tubular Parameters	Stenne of	. '	キャーナイ しょう 切り入りためたい	Tight of
Size	5.500	in	Minimum Yield	110,000
Nominal Weight	20.00	lbs/ft	Minimum Tensile	125,000
Grade	P-110		Yield Load	641,000
PE Weight	19.81	lbs/ft	Tensile Load	729,000
Wall Thickness	0.361	in	Min. Internal Yield Pressure	12,600
Nominal ID	4.778	in	Collapse Pressure	11,100
Drift Diameter	4.653	in	and the second	
Nom. Pipe Body Area	. 5. <b>928</b>	in²		
		•		
Connection Parameters			-	
Connection OD	6.050	in		
Connection ID	4.778	in		
Make-Up Loss	4.122	in		
Critical Section Area	5.828	in²		براند میں جب ا میں میں میں میں میں میں میں میں میں میں
Tension Efficiency	100.0	%		
Compression Efficiency	. 100.0	%		

444

Yield Load In Tension641,000ibsMin. Internal Yield Pressure12,600psiCollapse Pressure11,100psiMake-Up Torques11,0001000

Min. Make-Up Torque	11,600	ft-lbs
Opt. Make-Up Torque	12,900	ft-lbs
Max. Make-Up Torque	14,100	ft-lbs
Yield Torque	20,600	ft-lbs



### Printed on: July-29-2014

#### NOTE

The content of this Technical Data Sheet is for general information only and does not guarantee performance or imply fitness for a particular purpose, which only a competent drilling professional can determine considering the specific installation and operation parameters. Information that is printed or downloaded is no longer controlled by TMK IPSCO and might not be the latest information. Anyone using the information herein does so at their own risk. To verify that you have the latest TMK IPSCO technical information, please contact TMK IPSCO Technicat Sales toll-free at 1-888-258-2000.

IPSCO

St. Anary Straw

Is well located in SOPA but not in R-111-P?	N
If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back	
500' into previous casing?	
Is well located in R-111-P and SOPA?	N
If yes, are the first three strings cemented to surface?	
Is 2 <sup>nd</sup> string set 100' to 600' below the base of salt?	
Is well located in high Cave/Karst?	N
If yes, are there two strings cemented to surface?	
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there three strings commented to surface?	

# 3. Cementing Program

Casing	# Sks	Wt. lb/ gal	Yld ft3/ sack	H20 gal/sk	500# Comp. Strength (hours)	Slurry Description
Surface	768	14.8	1.35	6.53	6:50	Class C Cement, Accelerator
Production	1542	10.2	3.05	15.63	15:07	Pozzolan Cement, Retarder
Casing	239	13.2	1.65	8.45	12:57	Class H Cement, Retarder, Dispersant, Salt
DV/ECP Tool @	4712' (We reque	est the option to a	cancel the seco	nd stage if ceme	nt is circulated to s	surface during the first stage of cement operations)
and Stage	1152	12.9	. 1.85	9.86	12:44	Class C Cement, Accelerator, Retarder
2nd Stage	265 /	14.8	1.33	6.34	6:31	Class C Cement
Production Liner	1758	13.2	1.631	8.37	15:15	Class H Cement, Retarder, Dispersant, Salt

Casing String	Top of Lead (ft)	Bottom of Lead (ft)	Top of Tail (ft)	Bottom of Tail (ft)	% Excess Lead	% Excess Tail
Surface	N/A	N/A	0	959	N/A	50%
Production Casing	0	8903	8903	9903	75%	20%
2nd Stage Prodution Casing	0	4212	4212	4712	75%	125%
Production Liner	N/A	N/A	9803	20667	N/A	15%

# • <u>Cement Top and Liner Overlap</u>

 $\cap$ 

- OXY is requesting permission to have minimum fill of cement behind the 5-1/2" production liner to be 100 ft into previous casing string. The reason for this is so that we can come back and develop shallower benches from the same 9-5/8" mainbore in the future
- Our plan is to use a whipstock for our exit through the mainbore. Based on our lateral target, we are planning a whipstock cased/hole exit so that kick-off point will allow for roughly 10deg/100' doglegs needed for the curve
- Cement will be brought to the top of this liner hanger

### 4. Pressure Control Equipment

BOP installed and tested before drilling which hole?	Size?	Min. Required WP	Туре			Tested to:
			Annula	r	✓ <sup>1</sup>	70% of working pressure
12.25" Production	10.5/02	54	Blind Ram		✓	~ <b>^</b>
	13-5/8"	эм	Pipe Ram			
		Double Ram		✓	250/5000psi	
			Other*			

\*Specify if additional ram is utilized.

BOP/BOPE will be tested by an independent service company to 250 psi low and the high pressure indicated above per Onshore Order 2 requirements. The System may be upgraded to a higher pressure but still tested to the working pressure listed in the table above. If the system is upgraded all the components installed will be functional and tested.

Pipe rams will be operationally checked each 24 hour period. Blind rams will be operationally checked on each trip out of the hole. These checks will be noted on the daily tour sheets. Other accessories to the BOP equipment will include a Kelly cock and floor safety valve (inside BOP) and choke lines and choke manifold. See attached schematics.

Fo	mation integrity test will be performed per Onshore Order #2.
On	Exploratory wells or on that portion of any well approved for a 5M BOPE system or
gre	ater, a pressure integrity test of each casing shoe shall be performed. Will be tested in
acc	ordance with Onshore Oil and Gas Order #2 III.B.1.i.
A Ma	ariance is requested for the use of a flexible choke line from the BOP to Choke nifold. See attached for specs and hydrostatic test chart.
Y	Are anchors required by manufacturer?
A in	nultibowl wellhead is being used. The BOP will be tested per Onshore Order #2 after
ins	allation on the surface casing which will cover testing requirements for a maximum of
30	days. If any seal subject to test pressure is broken the system must be tested. We will
tes	the flange connection of the wellhead with a test port that is directly in the flange. We
are	proposing that we will run the wellhead through the rotary prior to cementing surface
cas	ing as discussed with the BLM on October 8, 2015.

#### Depth Weight (ppg) Viscosity Water Loss Type From (ft) To (ft) 959 Water-Based Mud 8.4-8.6 40-60 N/C 0 959 4712 Brine 9.8-10.0 35-45 N/C 4712 9903 Water-Based Mud 8.8-9.6 38-50 N/C 9903 N/C 20667 Oil-Based Mud 8.8-9.6 35-50

### 5. Mud Program

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times. The following is a general list of products: Barite, Bentonite, Gypsum, Lime, Soda Ash, Caustic Soda, Nut Plug, Cedar Fiber, Cotton Seed Hulls, Drilling Paper, Salt Water Clay, CACL2. OXY will use a closed mud system.

OXY proposes to drill out the 13-3/8" surface casing shoe with a saturated brine system from 959-4712', which is the base of the salt system. At this point we will swap fluid systems to a high viscosity mixed metal hydroxide system or a fully saturated direct emulsion system. We will drill with this system to the production TD @ 9903'.

What will be used to monitor the loss or gain	PVT/MD Totco/Visual Monitoring
of fluid?	

# 6. Logging and Testing Procedures

Logg	ing, Coring and Testing.
Yes	Will run GR from TD to surface (horizontal well – vertical portion of hole). Stated logs
	run will be in the Completion Report and submitted to the BLM.
No	Logs are planned based on well control or offset log information.
No	Drill stem test? If yes, explain
No	Coring? If yes, explain

Addi	tional logs planned	Interval
No	Resistivity	
No	Density	
No	CBL	
Yes	Mud log	Surface Shoe - TD
No	PEX	

# 7. Drilling Conditions

Condition	Specify what type and where?
BH Pressure at deepest TVD	5251 psi
Abnormal Temperature	No
BH Temperature at deepest TVD	165°F

Pump high viscosity sweeps as needed for hole cleaning. The mud system will be monitored visually/manually as well as with an electronic PVT. The necessary mud products for additional weight and fluid loss control will be on location at all times. Appropriately weighted mud will be used to isolate potential gas, oil, and water zones until such time as casing can be cemented into place for zonal isolation.

Hydrogen Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the operator will comply with the provisions of Onshore Oil and Gas Order #6. If Hydrogen Sulfide is encountered, measured values and formations will be provided to the BLM.

NH2S is presentYH2S Plan attached

# 8. Other facets of operation

	Yes/No
Will the well be drilled with a walking/skidding operation? If yes, describe.	Yes
• We plan to drill the two well pad in batch by section: all surface sections,	
intermediate sections and production sections. The wellhead will be	
secured with a night cap whenever the rig is not over the well.	
Will more than one drilling rig be used for drilling operations? If yes, describe.	Yes
• OXY requests the option to contract a Surface Rig to drill, set surface	
casing, and cement for this well. If the timing between rigs is such that	
OXY would not be able to preset surface, the Primary Rig will MIRU and	
drill the well in its entirety per the APD. Please see the attached document	
for information on the spudder rig.	

# Total estimated cuttings volume: 2344.6 bbls.

# 9. Company Personnel

Name	Title	Office Phone	Mobile Phone
Philippe Haffner	Drilling Engineer	713-985-6379	832-767-9047
Diego Tellez	Drilling Engineer Supervisor	713-350-4602	713-303-4932
Simon Benavides	Drilling Superintendent	713-522-8652	281-684-6897
John Willis	Drilling Manager	713-366-5556	713-259-1417

# OXY's Minimum Design Criteria

Burst, Collapse, and Tensile SF are calculated using Landmark's Stress Check (Casing Design) software. A sundry will be requested if any lesser grade or different size casing is substituted.

- **1)** Casing Design Assumptions
  - a) Burst Loads

CSG Test (Surface)

- Internal: Displacement fluid + pressure required to comply with regulatory casing test pressures. This will comply with both Onshore Oil and Gas Order No. 2 and 19.15.16 of the OCD Rules.
- External: Pore pressure in open hole.

CSG Test (Intermediate)

- Internal: Displacement fluid + pressure required to comply with regulatory casing test pressures. This will comply with both Onshore Oil and Gas Order No. 2 and 19.15.16 of the OCD Rules.
- External: Mud Weight to TOC, cement mix water gradient (8.4 ppg) below TOC, and pore pressure in open hole.

CSG Test (Production)

- o Internal:
  - For Drilling: Displacement fluid + pressure required to comply with regulatory casing test pressures. This will comply with both Onshore Oil and Gas Order No. 2 and 19.15.16 of the OCD Rules.
  - For Production: The design pressure test should be the greater of (1) the planned test pressure prior to stimulation down the casing. (2) the regulatory test pressure, and (3) the expected gas lift system pressure. The design test fluid should be the fluid associated with pressure test having the greatest pressure.
- o External:
  - For Drilling: Mud Weight to TOC, cement mix water gradient (8.4 ppg) below TOC, and pore pressure in open hole.
  - For Production: Mud base-fluid density to TOC, cement mix water gradient (8.4 ppg) below TOC, and pore pressure in open hole.

Gas Column (Surface)

- Internal: Assumes a full column of gas in the casing with a Gas/Oil Gradient of 0.1 psi/ft in the absence of better information. It is limited to the controlling pressure based on the fracture pressure at the shoe or the maximum expected pore pressure within the next drilling interval, whichever results in a lower surface pressure.
- External: Fluid gradient below TOC, pore pressure from the TOC to the Intermediate CSG shoe (if applicable), and MW of the drilling mud that was in the hole when the CSG was run from Intermediate CSG shoe to surface.

Bullheading (Surface / Intermediate)

- Internal: The string must be designed to withstand a pressure profile based on the fracture pressure at the casing shoe with a column of water above the shoe plus an additional surface pressure (in psi) of 0.02 X MD of the shoe to account for pumping friction pressure.
- External: Mud weight to TOC, cement mix water gradient (8.4 ppg) below TOC, and pore pressure in open hole.

Gas Kick (Intermediate)

- The string must be designed to at least a gas kick load case unless the rig is unable to detect a kick. For the gas kick load case, the internal pressure profile must be based on a minimum volume of 50 bbl or the minimum kick detection capability of the rig, whichever is greater, and a kick intensity of 2.0 ppg for Class 1, 1.0 ppg of Class 2, and 0.5 ppg for Class 3 and 4 wells.
- Internal: Influx depth of the maximum pore pressure of 0.55 "gas kick gravity" of gas to surface while drilling the next hole section.
- External: Mud weight to the TOC, cement mix water gradient below TOC, and pore pressure in open hole.

Tubing Leak Near Surface While Producing (Production)

- Internal: SITP plus a packer fluid gradient to the shoe or top of packer.
- •. External: Mud base-fluid density to TOC, cement mix water gradient (8.4 ppg) below TOC, and pore pressure in open hole.

Tubing Leak Near Surface While Stimulating (Production)

- Internal: Surface pressure or pressure-relief system pressure, whichever is lower plus packer fluid gradient.
- External: Mud base-fluid density to TOC, cement mix water gradient (8.4 ppg) below TOC, and pore pressure in open hole.

Injection / Stimulation Down Casing (Production)

- o Internal: Surface pressure plus injection fluid gradient.
- External: Mud base-fluid density to TOC, cement mix water gradient (8.4 ppg) below TOC, and pore pressure in open hole.
- **b)** Collapse Loads

Lost Circulation (Surface / Intermediate)

- Internal: Lost circulation at the TD of the next hole section, and the fluid level falls to a depth where the hydrostatic of the mud equals pore pressure at the depth of the lost circulation zone.
- External: MW of the drilling mud that was in the hole when the casing was run.

Cementing (Surface / Intermediate / Production)

- o Internal: Displacement fluid density.
- External: Mud weight from TOC to surface and cement slurry weight from TOC to casing shoe.

Full Evacuation (Production)

- o Internal: Full void pipe.
- o External: MW of drilling mud in the hole when the casing was run.

c) Tension Loads

Running Casing (Surface / Intermediate / Production)

 Axial: Buoyant weight of the string plus the lesser of 100,000 lb or the string weight in air.

Green Cement (Surface / Intermediate / Production)

Axial: Buoyant weight of the string plus cement plug bump pressure load.

# OXY's Minimum Design Criteria

Burst, Collapse, and Tensile SF are calculated using Landmark's Stress Check (Casing Design) software. A sundry will be requested if any lesser grade or different size casing is substituted.

- **1)** Casing Design Assumptions
  - a) Burst Loads

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- Internal: Displacement fluid + pressure required to comply with regulatory casing test pressures. This will comply with both Onshore Oil and Gas Order No. 2 and 19.15.16 of the OCD Rules.
- External: Pore pressure in open hole.

CSG Test (Intermediate)

- Internal: Displacement fluid + pressure required to comply with regulatory casing test pressures. This will comply with both Onshore Oil and Gas Order No. 2 and 19.15.16 of the OCD Rules.
- External: Mud Weight to TOC, cement mix water gradient (8.4 ppg) below TOC, and pore pressure in open hole.

CSG Test (Production)

- o Internal:
  - For Drilling: Displacement fluid + pressure required to comply with regulatory casing test pressures. This will comply with both Onshore Oil and Gas Order No. 2 and 19.15.16 of the OCD Rules.
  - For Production: The design pressure test should be the greater of (1) the planned test pressure prior to stimulation down the casing. (2) the regulatory test pressure, and (3) the expected gas lift system pressure. The design test fluid should be the fluid associated with pressure test having the greatest pressure.
- External:
  - For Drilling: Mud Weight to TOC, cement mix water gradient (8.4 ppg) below TOC, and pore pressure in open hole.
  - For Production: Mud base-fluid density to TOC, cement mix water gradient (8.4 ppg) below TOC, and pore pressure in open hole.

Gas Column (Surface)

- Internal: Assumes a full column of gas in the casing with a Gas/Oil Gradient of 0.1 psi/ft in the absence of better information. It is limited to the controlling pressure based on the fracture pressure at the shoe or the maximum expected pore pressure within the next drilling interval, whichever results in a lower surface pressure.
- External: Fluid gradient below TOC, pore pressure from the TOC to the Intermediate CSG shoe (if applicable), and MW of the drilling mud that was in the hole when the CSG was run from Intermediate CSG shoe to surface.

Bullheading (Surface / Intermediate)

- Internal: The string must be designed to withstand a pressure profile based on the fracture pressure at the casing shoe with a column of water above the shoe plus an additional surface pressure (in psi) of 0.02 X MD of the shoe to account for pumping friction pressure.
- External: Mud weight to TOC, cement mix water gradient (8.4 ppg) below TOC, and pore pressure in open hole.

Gas Kick (Intermediate)

- The string must be designed to at least a gas kick load case unless the rig is unable to detect a kick. For the gas kick load case, the internal pressure profile must be based on a minimum volume of 50 bbl or the minimum kick detection capability of the rig, whichever is greater, and a kick intensity of 2.0 ppg for Class 1, 1.0 ppg of Class 2, and 0.5 ppg for Class 3 and 4 wells.
- Internal: Influx depth of the maximum pore pressure of 0.55 "gas kick gravity" of gas to surface while drilling the next hole section.
- External: Mud weight to the TOC, cement mix water gradient below TOC, and pore pressure in open hole.

Tubing Leak Near Surface While Producing (Production)

- Internal: SITP plus a packer fluid gradient to the shoe or top of packer.
- External: Mud base-fluid density to TOC, cement mix water gradient (8.4 ppg) below TOC, and pore pressure in open hole.

Tubing Leak Near Surface While Stimulating (Production)

- Internal: Surface pressure or pressure-relief system pressure, whichever is lower plus packer fluid gradient.
- External: Mud base-fluid density to TOC, cement mix water gradient (8.4 ppg) below TOC, and pore pressure in open hole.

Injection / Stimulation Down Casing (Production)

- o Internal: Surface pressure plus injection fluid gradient.
- External: Mud base-fluid density to TOC, cement mix water gradient (8.4 ppg) below TOC, and pore pressure in open hole.
- **b)** Collapse Loads

Lost Circulation (Surface / Intermediate)

- Internal: Lost circulation at the TD of the next hole section, and the fluid level falls to a depth where the hydrostatic of the mud equals pore pressure at the depth of the lost circulation zone.
- o External: MW of the drilling mud that was in the hole when the casing was run.

Cementing (Surface / Intermediate / Production)

- o Internal: Displacement fluid density.
- External: Mud weight from TOC to surface and cement slurry weight from TOC to casing shoe.

Full Evacuation (Production)

- o Internal: Full void pipe.
- External: MW of drilling mud in the hole when the casing was run.

c) Tension Loads

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 Axial: Buoyant weight of the string plus the lesser of 100,000 lb or the string weight in air.

Green Cement (Surface / Intermediate / Production)

Axial: Buoyant weight of the string plus cement plug bump pressure load.

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  - a) Burst Loads

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- External: Pore pressure in open hole.

CSG Test (Intermediate)

- Internal: Displacement fluid + pressure required to comply with regulatory casing test pressures. This will comply with both Onshore Oil and Gas Order No. 2 and 19.15.16 of the OCD Rules.
- External: Mud Weight to TOC, cement mix water gradient (8.4 ppg) below TOC, and pore pressure in open hole.

CSG Test (Production)

- o Internal:
  - For Drilling: Displacement fluid + pressure required to comply with regulatory casing test pressures. This will comply with both Onshore Oil and Gas Order No. 2 and 19.15.16 of the OCD Rules.
  - For Production: The design pressure test should be the greater of (1) the planned test pressure prior to stimulation down the casing. (2) the regulatory test pressure, and (3) the expected gas lift system pressure. The design test fluid should be the fluid associated with pressure test having the greatest pressure.
- o **External**:
  - For Drilling: Mud Weight to TOC, cement mix water gradient (8.4 ppg) below TOC, and pore pressure in open hole.
  - For Production: Mud base-fluid density to TOC, cement mix water gradient (8.4 ppg) below TOC, and pore pressure in open hole.

Gas Column (Surface)

- Internal: Assumes a full column of gas in the casing with a Gas/Oil Gradient of 0.1 psi/ft in the absence of better information. It is limited to the controlling pressure based on the fracture pressure at the shoe or the maximum expected pore pressure within the next drilling interval, whichever results in a lower surface pressure.
- External: Fluid gradient below TOC, pore pressure from the TOC to the Intermediate CSG shoe (if applicable), and MW of the drilling mud that was in the hole when the CSG was run from Intermediate CSG shoe to surface.

Bullheading (Surface / Intermediate)

- Internal: The string must be designed to withstand a pressure profile based on the fracture pressure at the casing shoe with a column of water above the shoe plus an additional surface pressure (in psi) of 0.02 X MD of the shoe to account for pumping friction pressure.
- External: Mud weight to TOC, cement mix water gradient (8.4 ppg) below TOC, and pore pressure in open hole.

Gas Kick (Intermediate)

- The string must be designed to at least a gas kick load case unless the rig is unable to detect a kick. For the gas kick load case, the internal pressure profile must be based on a minimum volume of 50 bbl or the minimum kick detection capability of the rig, whichever is greater, and a kick intensity of 2.0 ppg for Class 1, 1.0 ppg of Class 2, and 0.5 ppg for Class 3 and 4 wells.
- Internal: Influx depth of the maximum pore pressure of 0.55 "gas kick gravity" of gas to surface while drilling the next hole section.
- External: Mud weight to the TOC, cement mix water gradient below TOC, and pore pressure in open hole.

Tubing Leak Near Surface While Producing (Production)

- Internal: SITP plus a packer fluid gradient to the shoe or top of packer.
- External: Mud base-fluid density to TOC, cement mix water gradient (8.4 ppg) below TOC, and pore pressure in open hole.

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- Internal: Surface pressure or pressure-relief system pressure, whichever is lower plus packer fluid gradient.
- External: Mud base-fluid density to TOC, cement mix water gradient (8.4 ppg) below TOC, and pore pressure in open hole.

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- o Internal: Surface pressure plus injection fluid gradient.
- External: Mud base-fluid density to TOC, cement mix water gradient (8.4 ppg) below TOC, and pore pressure in open hole.
- **b)** Collapse Loads

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- Internal: Lost circulation at the TD of the next hole section, and the fluid level falls to a depth where the hydrostatic of the mud equals pore pressure at the depth of the lost circulation zone.
- External: MW of the drilling mud that was in the hole when the casing was run.

Cementing (Surface / Intermediate / Production)

- o Internal: Displacement fluid density.
- External: Mud weight from TOC to surface and cement slurry weight from TOC to casing shoe.

Full Evacuation (Production)

- o Internal: Full void pipe.
- External: MW of drilling mud in the hole when the casing was run.

#### c) Tension Loads

Running Casing (Surface / Intermediate / Production)

• Axial: Buoyant weight of the string plus the lesser of 100,000 lb or the string weight in air.

Green Cement (Surface / Intermediate / Production)

• Axial: Buoyant weight of the string plus cement plug bump pressure load.

# OXY's Minimum Design Criteria

Burst, Collapse, and Tensile SF are calculated using Landmark's Stress Check (Casing Design) software. A sundry will be requested if any lesser grade or different size casing is substituted.

- **1)** Casing Design Assumptions
  - a) Burst Loads

CSG Test (Surface)

- Internal: Displacement fluid + pressure required to comply with regulatory casing test pressures. This will comply with both Onshore Oil and Gas Order No. 2 and 19.15.16 of the OCD Rules.
- External: Pore pressure in open hole.
- CSG Test (Intermediate)
- Internal: Displacement fluid + pressure required to comply with regulatory casing test pressures. This will comply with both Onshore Oil and Gas Order No. 2 and 19.15.16 of the OCD Rules.
- External: Mud Weight to TOC, cement mix water gradient (8.4 ppg) below TOC, and pore pressure in open hole.

CSG Test (Production)

- o Internal:
  - For Drilling: Displacement fluid + pressure required to comply with regulatory casing test pressures. This will comply with both Onshore Oil and Gas Order No. 2 and 19.15.16 of the OCD Rules.
  - For Production: The design pressure test should be the greater of (1) the planned test pressure prior to stimulation down the casing. (2) the regulatory test pressure, and (3) the expected gas lift system pressure. The design test fluid should be the fluid associated with pressure test having the greatest pressure.
- o External:
  - For Drilling: Mud Weight to TOC, cement mix water gradient (8.4 ppg) below TOC, and pore pressure in open hole.
  - For Production: Mud base-fluid density to TOC, cement mix water gradient (8.4 ppg) below TOC, and pore pressure in open hole.

Gas Column (Surface)

- Internal: Assumes a full column of gas in the casing with a Gas/Oil Gradient of 0.1 psi/ft in the absence of better information. It is limited to the controlling pressure based on the fracture pressure at the shoe or the maximum expected pore pressure within the next drilling interval, whichever results in a lower surface pressure.
- External: Fluid gradient below TOC, pore pressure from the TOC to the Intermediate CSG shoe (if applicable), and MW of the drilling mud that was in the hole when the CSG was run from Intermediate CSG shoe to surface.

Bullheading (Surface / Intermediate)

- Internal: The string must be designed to withstand a pressure profile based on the fracture pressure at the casing shoe with a column of water above the shoe plus an additional surface pressure (in psi) of 0.02 X MD of the shoe to account for pumping friction pressure.
- External: Mud weight to TOC, cement mix water gradient (8.4 ppg) below TOC, and pore pressure in open hole.

Gas Kick (Intermediate)

- The string must be designed to at least a gas kick load case unless the rig is unable to detect a kick. For the gas kick load case, the internal pressure profile must be based on a minimum volume of 50 bbl or the minimum kick detection capability of the rig, whichever is greater, and a kick intensity of 2.0 ppg for Class 1, 1.0 ppg of Class 2, and 0.5 ppg for Class 3 and 4 wells.
- Internal: Influx depth of the maximum pore pressure of 0.55 "gas kick gravity" of gas to surface while drilling the next hole section.
- External: Mud weight to the TOC, cement mix water gradient below TOC, and pore pressure in open hole.

Tubing Leak Near Surface While Producing (Production)

- o Internal: SITP plus a packer fluid gradient to the shoe or top of packer.
- External: Mud base-fluid density to TOC, cement mix water gradient (8.4 ppg) below TOC, and pore pressure in open hole.

Tubing Leak Near Surface While Stimulating (Production)

- Internal: Surface pressure or pressure-relief system pressure, whichever is lower plus packer fluid gradient.
- External: Mud base-fluid density to TOC, cement mix water gradient (8.4 ppg) below TOC, and pore pressure in open hole.

Injection / Stimulation Down Casing (Production)

- o Internal: Surface pressure plus injection fluid gradient.
- External: Mud base-fluid density to TOC, cement mix water gradient (8.4 ppg) below TOC, and pore pressure in open hole.
- **b)** Collapse Loads

Lost Circulation (Surface / Intermediate)

- Internal: Lost circulation at the TD of the next hole section, and the fluid level falls to a depth where the hydrostatic of the mud equals pore pressure at the depth of the lost circulation zone.
- External: MW of the drilling mud that was in the hole when the casing was run.

Cementing (Surface / Intermediate / Production)

- Internal: Displacement fluid density.
- External: Mud weight from TOC to surface and cement slurry weight from TOC to casing shoe.

Full Evacuation (Production)

- o Internal: Full void pipe.
- External: MW of drilling mud in the hole when the casing was run.

c) Tension Loads

Running Casing (Surface / Intermediate / Production)

 Axial: Buoyant weight of the string plus the lesser of 100,000 lb or the string weight in air.

Green Cement (Surface / Intermediate / Production)

o Axial: Buoyant weight of the string plus cement plug bump pressure load.









# 5M BOP Stack



PIPE

SPOOL

4. 5,000 psi Lower Pipe

 $\Sigma$ 

Ram (13-5/8" ID)

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Fluid Technology

Quality Document

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PURCHASER:	Phoenix I	Beattie C	io.			P.O. Nº:	O	02491	
CONTITECH ORDER Nº:	HOS	E TYPE:	3"	ID	Ch	oke and Ki	ll Hose		
HOSE SERIAL Nº: 52777 NOMINAL / ACTUAL LENGTH: 10,67 m									
W.P. 68,96 MPa	10000	psi T.P.	103,4	MPa	15000	psł	Duration:	60 ~	nin
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**Coflex Hose Certification** 

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# **Coflex Hose Certification**

Form No 100/12

# - PHOENIX Beattie

Phoenix Beattle Corp LISSS Brittmoore Part Drive Houston, TX 77041 Tel: (832) 327-0148 F-sci (832) 327-0148 E-scill sail@phoenixtenttic.com www.phoenixbastle.com

# **Delivery Note**

Customer Order Number	370-369-001	Delivery Note Number	003078	Paga	1
Customer / Invoice Addre HELMERICH & PAYNE INT'L 1437 SOUTH BOULDER TULSA, OK 74119	88 DRILLING CO	Delivery / Address HELMERICH & PAYNE IDC ATTN: JOE STEPHENSON - RI 13609 INDUSTRIAL ROAD HOUSTON, TX 77015	3 370	-	

Customer Acc No	Phoenix Beattie Contract Manager	Phoenix Beattie Reference	Date
H01	JJL	006330	05/23/2008

ltern No	Beattle Part Number / Description	Qty Ordered	Qty Sent	Qty To Foliow
1	HP10CK3A-35-4F1 3° 10K 16C C&K HOSE x 35ft OAL CW 4.1/16° API SPEC FLANGE E/ End 1: 4.1/16° 10Kpsi API Spec 6A Type 68X Flange End 2: 4.1/16° 10Kpsi API Spec 6A Type 68X Flange c/w BX155 Standard ring groove at each end Suitable for H2S Service Working pressure: 10,000psi Test pressure: 15,000psi Standard: API 16C Full specification Armor Guarding: Included Fire Rating: Not Included Temperature rating: -20 Deg C to +100 Deg C	1	1	0
2	SECK3-HPF3 LIFTING & SAFETY EQUIPHENT TO SUIT HP10CK3-35-F1 2 x 160mm ID Safety Clamps 2 x 244mm ID Lifting Collars & element C's 2 x 7ft Stainless Steel wire rope 3/4" OD 4 x 7.75t Shackles	1	1	0
3	SC725-200CS SAFETY CLAMP 200MM 7.25T C/S GALVANISED	1	1	0

Continued...

All goods remain the property of Phoenix Besttie until paid for in full. Any damage or shortage on this delivery must be advised within 5 days. Returns may be subject to a handling charge.

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# **Coflex Hose Certification**

Form No 100/12

Phoenix Beattie Corp LISS & titozore Perk Drive Houston, TX 77041 Tel: (822) 327-0141 Fex: (832) 327-0148 E-ext1 # all Reptoent deattie.com www.piventsDeattie.com

# **Delivery Note**

Customer Order Number	370-369-001	Delivery Note Number	003078	Page	2
Customer / Invoice Addre HELMERICH & PAYNE INT'L 1437 SOUTH BOULDER TULSA, OK 74119	ss DRILLING CO	Delivery / Address Helmerich & Payne IDC Attn: Joe Stephenson - Rig 13609 Industrial Road Houston, Tx 77015	3 370		

Customer Acc'No	Phoenix Beattie Contract Manager	Phoenix Beattle Reference	Date
H01	JJL	006330	05/23/2008

ltem No	Beattle Part Number / Description	Qty Ordered	Oty Sent	Qty To Follow
4	SC725-132CS SAFETY CLAMP 132MM 7.25T C/S GALVANIZED C/W BOLTS	1	1	0
<b>5</b>	ODCERT-HYDRO HYDROSTATIC PRESSURE TEST CERTIFICATE	1	• 1	0
6	OOCERT-LOAD LOAD TEST CERTIFICATES	1	1	O
7	OOFREIGHT INBOUND / OUTBOUND FREIGHT PRE-PAY & ADD TO FINAL INVDICE NOTE: MATERIAL MUST BE ACCOMPANIED BY PAPERWORK INCLUDING THE PURCHASE ORDER, RIG NUMBER TO ENSURE PROPER PAYMENT	1	1	0
	, T	Pa	$\bigwedge$	
	Phoenix Beattle Inspection Signature :	ANALAN	WALCH	· · · · · · · · · · · · · · · · · · ·
	Received in Good Condition : Signature		V	
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All goods remain the property of Phoenix Beattle until paid for in full. Any damage or shortage on this delivery must be advised within 5 days. Returns may be subject to a handling charge.

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# - PHOENIX Beattie

Material Identification Certificate

PA No   006	330 Client HE	LMERICH & PA	YNE INT'L DRILLING	Client	Ref 37	0-369-001			Page	1
Part No	Description	Material Deco	Material Soon	Otu		Patch No.	Test Cart No.		Dee Ma	
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We hereby certify that these goods have been inspected by our Quality Management System, and to the best of our knowledge are found to conform to relevant industry standards within the requirements of the purchase order as issued to Phoenix Beattle Corporation.

**Coflex Hose Certification** 

FH-S

**Coflex Hose Certification** 



Fluid Technology Quality Document FH-6

# CERTIFICATE OF CONFORMITY

Supplier : CONTITECH RUBBER INDUSTRIAL KFT. Equipment : 6 pcs. Choke and Kill Hose with installed couplings Type : 3" x 10,67 m WP: 10000 psi Supplier File Number : 412638 Date of Shipment : April. 2008 Customer : Phoenix Beattle Co. Customer P.o. : 002491 Referenced Standards / Codes / Specifications : API Spec 16 C Serial No.: 52754,52755,52776,52777,52778,52782

# STATEMENT OF CONFORMITY

We hereby certify that the above items/equipment supplied by us are in conformity with the terms, conditions and specifications of the above Purchaser Order and that these items/equipment were fabricated inspected and tested in accordance with the referenced standards, codes and specifications and meet the relevant acceptance criteria and design requirements.

# COUNTRY OF ORIGIN HUNGARY/EU

Signed

Position: Q.C. Manager

\_ontiTech Rubber Industrial Kit. Quality Control Dept. (1)

Date: 04. April. 2008

# PERFORMANCE DATA

# TMK UP DQX **Technical Data Sheet**

# 5.500 in

20.00 lbs/ft

P-110

#### **Tubular Parameters** Size 5.500 Minimum Yield in Minimum Tensile Nominal Weight 20.00 lbs/ft P-110 Yield Load Grade **PE Weight Tensile Load** 19.81 lbs/ft Wall Thickness Min. Internal Yield Pressure 0.361 in Nominal ID 4.778 ïn **Collapse Pressure** Drift Diameter 4.653 in Nom. Pipe Body Area 5.828 in²

Connection Parameters		1
Connection OD	6.050	in `
Connection ID	4.778	in
Make-Up Loss	4.122	in
Critical Section Area	5.828	in²
Tension Efficiency	100.0	%
Compression Efficiency	100.0	: %
Yield Load In Tension	641,000	lbs
Min. Internal Yield Pressure	12,600	psi
Collapse Pressure	- 11,100	psi

#### Make-Up Torques Min. Make-Up Torque 11,600

Opt. Make-Up Torque	12,900	ft-lbs
Max. Make-Up Torque	14,100	ft-lbs
Yield Torque	20,600	ft-lbs

#### 110,000 psi 125,000 psi 641,000 lbs 729,000 lbs 12,600 psi 11,100 psi



Printed on: July-29-2014

#### NOTE:

The content of this Technical Data Sheet is for general information only and does not guarantee performance or imply fitness for a particular purpose, which only a competent drilling professional can determine considering the specific installation and operation parameters. Information that is printed or downloaded is no longer controlled by TMK IPSCO and might not be the latest information. Anyone using the information herein does so at their own risk. To verify that you have the latest TMK IPSCO technical information, please contact TMK IPSCO Technical Sales toil-free at 1-888-258-2000.

ft-lbs



# FAFMSS

U.S. Department of the Interior **BUREAU OF LAND MANAGEMENT** 

# Drilling Plan Data Report 10/31/2017

APD ID: 10400014735

**Operator Name: OXY USA INCORPORATED** 

Well Name: MESA VERDE 18-7 FEDERAL COM

Well Number: 6H

Highlighted data reflects the most recent changes

Show Final Text

Well Type: OIL WELL

Well Work Type: Drill

Submission Date: 06/14/2017

# **Section 1 - Geologic Formations**

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Formation			True Vertical	Measured			Producing
D	Formation Name	Elevation	Dépth	Depth	Lithologies	Mineral Resources	Formation
1	RUSTLER	3570	909	909	SHALE,DOLOMITE ,ANHYDRITE	USEABLE WATER	No
2	SALADO	2565	1005	1005	SHALE,DOLOMITE ,HALITE,ANHYDRI TE	OTHER : SALT	No
3	CASTILE	278	3292	3292	ANHYDRITE	OTHER : salt	No
4	LAMAR	-1092	4662	4662	LIMESTONE,SAND STONE,SILTSTON E	NATURAL GAS,OIL,OTHER : BRINE	No
5	BELL CANYON	-1107	4677	4677	SANDSTONE,SILT STONE	NATURAL GAS,OIL,OTHER : BRINE	No
6	CHERRY CANYON	-1985	5555	5555	SANDSTONE,SILT STONE	NATURAL GAS,OIL,OTHER : BRINE	No
7	BRUSHY CANYON	-3326	6896	6913	LIMESTONE,SAND STONE,SILTSTON E	NATURAL GAS,OIL,OTHER : BRINE	No
8	BONE SPRING	-4919	8489	8531	LIMESTONE,SAND STONE,SILTSTON E	NATURAL GAS,OIL	Yes
9	BONE SPRING 1ST	-6092	9662	9721	LIMESTONE,SAND STONE,SILTSTON E	NATURAL GAS,OIL	Yes
10	BONE SPRING 2ND	-6364	9934	9993	LIMESTONE,SAND STONE,SILTSTON E	NATURAL GAS,OIL	Yes

# **Section 2 - Blowout Prevention**

Pressure Rating (PSI): 5M

Rating Depth: 10517

Equipment: 13-5/8" 5M Annular, Blind Ram, Double Ram

Requesting Variance? YES

Variance request: Request for the use of a flexible choke line from the BOP to Choke Manifold.

Testing Procedure: BOP/BOPE will be tested by an independent service company to 250 psi low and the high pressure indicated above per Onshore Order 2 requirements. The System may be upgraded to a higher pressure but still tested to the

Below is a summary that describes the general operational steps to drill and complete the well.

- Drill 17-1/2" hole x 13-3/8" casing for surface section. Cement to surface.
- Drill 12-1/4" hole x 9-5/8" casing for intermediate section. Cement to surface.
- Drill 8-1/2" hole x 5-1/2" liner for production section. Cement to top of liner, 100' inside 9-5/8" shoe.
- Release drilling rig from location
- Move in workover rig and run a 5-1/2" 20# P110 DQX tie-back frack string and seal assembly (see connection specs below). Tie into liner hanger Polished Bore Receptacle (PBR) with seal assembly.
- Pump hydraulic fracture job.
- Flowback and produce well.

When a decision is made to develop a secondary bench from this wellbore, a workover rig will be moved to location. The workover rig will then retrieve the tie-back frack string and seal assembly before temporarily abandoning the initial lateral.

General well schematic:



5 <sup>1</sup>/<sub>2</sub>" 17# P110 DQX Tie-back string specifications: