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See Rule 401 & Rule 1122

State of New Mexico
Energy, Minerals and Natural Resources Department

Form C-122
Revised 4-1-91

OIL CONSERVATION DIVISION

P.O. Box 2088
Santa Fe, New Mexico 87504-2088

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator PHILLIPS PETROLEUM COMPANY						Lease or Unit Name RANGER					
Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 5/19/92		Well No. 17			
Completion Date 5/16/92		Total Depth 14100'		Plug Back TD 12925'		Elevation 4150' GL		Unit Ltr. - Sec. - TWP - Rge. M 26 3E 12 34			
Csg. Size 9 5/8"		Wt. 53.5#		Set At 13800'		Perforations: From: 12813 To: 12905'		County LEA			
Tbg. Size 2 7/8"		Wt. 6.5		Set At 12675		Perforations: From: To:		Pool West Ranger Lake (Dev.)			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single						Packer Set At 12675		Formation DEV.			
Producing Thru TBG		Reservoir Temp. °F 60		Mean Annual Temp. °F 60		Baro. Press - P 13.2		Connection			
L 12675	H 12675	Gg .699	% CO ₂ 2.24	% N ₂ 3.36	% H ₂ S	Prover		Meter Run 4.026		Taps FLG	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							2815		PKR		17 HRS
1.	4	X	2.000	450	20.00	71	2667		PKR		30 MIN
2.	4	X	2.000	450	30.00	72	2730		PKR		30 MIN
3.	4	X	2.000	450	38.00	69	2722		PKR		30 MIN
4.	4	X	2.000	450	52.00	59	2683		PKR		1 HR
5.											

RATE OF FLOW CALCULATIONS							
NO.	COEFFICIENT (24 HOUR)		Pressure P _m	Flow Temp. Factor Ft	Gravity Factor Fg	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	19.81	96.25	463.2	.9896	1.196	1.047	2363
2.	19.81	117.88	463.2	.9887	1.196	1.047	2891
3.	19.81	132.67	463.2	.9915	1.196	1.047	3263
4.	19.81	155.20	463.2	1.001	1.196	1.054	3880
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	5.57	Mcf/bbl.
1.	.68	531	1.41	.913	A.P. L Gravity of Liquid Hydrocarbons	70.0 @ 60°	Deg.
2.	.68	532	1.41	.913	Specific Gravity Separator Gas	.699	XXXXXXXXXX
3.	.68	529	1.40	.913	Specific Gravity Flowing Fluid	XXXXXX	
4.	.68	519	1.38	.901	Critical Pressure * 672	P.S.I.A.	656 P.S.I.A.
5.					Critical Temperature * 376	R	508 R

P _c 2828.2 P _c ² 7998.7		1) $\frac{P_c^2}{P_c^2 - P_w^2} = 18.044$		2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^a = 9.576$	
NO.	P _c ²	P _w	P _w ²	P _c ² - P _w ²	
1.	2703.3	7307.8	690.9		
2.	2775.0	7700.6	298.1		
3.	2774.5	7697.9	300.8		
4.	2748.7	7555.4	443.3		
5.					

Absolute Open Flow 37,154 Mcfd @ 15.025		Angle of Slope θ 52		Slope, n .781	
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Remarks: WELL MADE 60.9 BBLs API GR CONDENSATE DURING TEST	
* = CORRECTED TO 2.24% CO ₂ AND 3.36% N ₂ .	

Approved By Division	Conducted By: JOHN WEST ENGINEERING	Calculated By: BM	Checked By: BM
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