## NEW MEXICO OIL COMBERVATION COMESSION

MULTI-POINT BACK PRESS THE TEST FOR THE WELLS Rev

F'o:	rm C-122	
evised	12-1-55	

ool	Buncar	<u> </u>		Formation Justa				County Lea			
Initial Annual Annual					Special			Date of	Test_	24-56	
mpa	ny The T	exas Com	pany		Leas <b>dta</b>	te of N	. M. "J	<mark> ■</mark> _Wel	ll No		
it	<b>7</b> S	Sec. 24	Twp . 19	<b>-\$</b> _Rg	e. <u>36-E</u>	Purch	naser Per	mien Be	nin Pip	e Line Co.	
.sin	5 1/2 W	t. 14	_I.D <b>5</b>	<b>.012</b> Se	t at <b>35</b>	<b>65</b> Per	rf		To		
bin	8 2 3/4 W	t. 4.70	_I.D <u>1</u>	<b>.995</b> Se	t at <b>35</b>	<b>73</b> Per	rf	64	To	67	
s Pa	ay: From_	3565 To	3400	L_35(	<b>4</b> x	G <b>670</b>		88	Bar.Pres	ss. 13.2	
odu	ing Thru:	Casing		Tu	bing		_Type We	ell <b>Sin</b>	<u>clo</u>		
te	of Complet	ion:	-9-54	Packe	r	Sing	gle-Brade Reservo	enhead-G. oir Temp.	G. or G	.O. Dual	
					OBSERV						
_	i Through	_		(Meter)				Type Tap	s Pi	•	
		Flow				Tubing	Data	Casing I	)ata		
	(Preser) (Line)	1/~	<b>\ I</b>	1 5	Temp.	Press.	Temp.	Press.	Temp.	Duration of Flow	
	Size	Size	psi	g h <sub>w</sub>				psig		Hr.	
	<u> </u>	2.90	456.	7 33.2	71	1005.2 740.0		1005.7 852.0		72 1/2 23 3/4	
	<u> </u>	2.00	455.	3 32.2	<b>70</b> 73	723.8		832.7 906.6		23 3/4	
	<u> </u>	2.00	442.	3 2.9	40	944.5		951.3		24 1/4	
					FLOW CAL	CULATIONS	3	<u> </u>	<del></del>		
	Coeffici	efficient		Pressure Flow Te		Temp.			ess. Rate of Flow		
(24-Ho				psia	F-	t	Fg	Fpv		@ 15.025 psia	
	29.92 29.92	12	2.60	149.9 148.5	.989		.9463	1.0	3	3,647	
	29.92	3	9.64	455.5	.947		9463	1.0	12	2.035	
				PR	ESSURE C	ALCU ATI	DNS				
as Liquid Hydrocarbon Ratio					cf/bbl. deg.			Specific Gravity Separator Gas Specific Gravity Flowing Fluid			
			(1-e <sup>-s</sup> )				Pc_1	018.9	_P <sub>c</sub> 1	036.2	
7 1	· w	<del></del> -		T	<del>- T</del>	<del></del>			<del></del>	·	
•	t (psia)	Pt <sup>2</sup>	F <sub>c</sub> ⊋	(F <sub>c</sub> Q) <sup>2</sup>	(F	$\begin{pmatrix} c^{Q} \end{pmatrix}^2 = \begin{pmatrix} c^{Q} - s \end{pmatrix}$	$P_w^2$	$P_c^2 - P_w^2$	Cal P,		
	65.2						748.6	249.6		.85	
Ħ	19.8						715.5 846.0	192.2		- 83	
E	164.5						930.3	107.9	<u> </u>	.95	
solı MPAN	ite Potent	ial:	11,010	COMPANY	MCFPD;	n1.0	(Limit	(d)			
DRES		TOT	1270.	KIDLAND R. DIST					Sak	,	
		. I. I		e. Bist	# 4 1 T T L & A	.73. 10E-2 (1)E			1 1 16		

This is a retest. Due to peer point alignment and slope (n) in excess of 1.00, the slope (n) was drawn through the high rate of flow with a slope of 1.00 in accordance with the instructions in the Manual.

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

- Q  $\equiv$  Actual rate of flow at end of flow period at W. H. working pressure (P<sub>W</sub>). MCF/da. @ 15.025 psia and 60° F.
- $P_{c}$ 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- PwI Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- Pf Meter pressure, psia.
- hw Differential meter pressure, inches water.
- FgI Gravity correction factor.
- $F_t \subseteq$  Flowing temperature correction factor.
- Fnv Supercompressability factor.
- n I Slope of back pressure curve.

Note: If  $P_W$  cannot be taken because of manner of completion or condition of well, then  $P_W$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_t$ .