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NEW MEXICO OIL CONSERVATION COMMISSION

Form C-122
Revised 12-1-55

MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Pool Bumont Formation Queen County Lea
Initial _____ Annual _____ Special X Date of Test 4-15/4-19-63
Company Tidewater Oil Company Lease State "H" Well No. 2
Unit K Sec. 32 Twp. 19 Rge. 37 Purchaser El Paso Natural Gas Co.
Casing 7" Wt. _____ I.D. _____ Set at 3801 Perf. _____ To _____
Tubing 2" Wt. _____ I.D. _____ Set at 3382' Perf. _____ To _____
Gas Pay: From 3384 To 3535 L 3382 xG .667 -GL 2256 Bar.Press. 13.2
Producing Thru: Casing _____ Tubing X Type Well Single
Single-Bradenhead-G. G. or G.O. Dual
Date of Completion: Oct. 5, 1956 Packer 3050 Reservoir Temp. _____

OBSERVED DATA

Tested Through (Pressure) (Orifice) (Meter) Type Taps _____

No.	Flow Data					Tubing Data		Casing Data		Duration of Flow Hr.
	(<u>Pressure</u>) (Line) Size	(<u>Orifice</u>) (Orifice) Size	Press. psig	Diff. h _w	Temp. °F.	Press. psig	Temp. °F.	Press. psig	Temp. °F.	
SI						<u>804</u>		<u>Packer</u>		<u>72</u>
1.	<u>4</u>	<u>1.25</u>	<u>563</u>	<u>5.29</u>	<u>79</u>	<u>714</u>				<u>24</u>
2.	<u>4</u>	<u>1.25</u>	<u>616</u>	<u>6.23</u>	<u>80</u>	<u>691</u>				<u>24</u>
3.	<u>4</u>	<u>1.25</u>	<u>607</u>	<u>7.29</u>	<u>74</u>	<u>651</u>				<u>24</u>
4.	<u>4</u>	<u>1.25</u>	<u>646</u>	<u>7.29</u>	<u>74</u>	<u>640</u>				<u>24</u>
5.										

FLOW CALCULATIONS

No.	Coefficient (24-Hour)	$\sqrt{h_{wpf}}$	Pressure psia	Flow Temp. Factor F _t	Gravity Factor F _g	Compress. Factor F _{pv}	Rate of Flow Q-MCFPD @ 15.025 psia
1.	<u>9.643</u>	<u>55.20</u>		<u>.9822</u>	<u>.9484</u>	<u>1.056</u>	<u>523.6</u>
2.	<u>9.643</u>	<u>62.71</u>		<u>.9813</u>	<u>.9484</u>	<u>1.056</u>	<u>594.3</u>
3.	<u>9.643</u>	<u>67.24</u>		<u>.9868</u>	<u>.9484</u>	<u>1.061</u>	<u>643.8</u>
4.	<u>9.648</u>	<u>67.73</u>		<u>.9868</u>	<u>.9484</u>	<u>1.061</u>	<u>648.3</u>
5.							

PRESSURE CALCULATIONS

Gas Liquid Hydrocarbon Ratio _____ cf/bbl.
Gravity of Liquid Hydrocarbons _____ deg.
F_c 9.936 (1-e^{-s}) 0.144
Specific Gravity Separator Gas .467
Specific Gravity Flowing Fluid _____
P_c 817.2 P_c² 667.8

No.	P _w P _t (psia)	P _t ²	F _c Q	(F _c Q) ²	(F _c Q) ² (1-e ^{-s})	P _w ²	P _c ² -P _w ²	Cal. P _w	P _w P _c
1.	<u>727.2</u>	<u>528.8</u>	<u>5.202</u>	<u>27.06</u>	<u>3.897</u>	<u>528.7</u>	<u>135.1</u>	<u>729.9</u>	<u>8932</u>
2.	<u>704.2</u>	<u>495.9</u>	<u>5.905</u>	<u>34.87</u>	<u>5.021</u>	<u>500.9</u>	<u>166.9</u>	<u>707.7</u>	<u>8660</u>
3.	<u>664.2</u>	<u>441.2</u>	<u>6.397</u>	<u>40.92</u>	<u>5.892</u>	<u>447.1</u>	<u>220.7</u>	<u>668.7</u>	<u>8183</u>
4.	<u>653.2</u>	<u>426.7</u>	<u>6.443</u>	<u>41.51</u>	<u>5.977</u>	<u>432.7</u>	<u>235.1</u>	<u>657.8</u>	<u>8049</u>
5.									

Absolute Potential: 1,170 MCFPD; n .500
COMPANY Tidewater Oil Company
ADDRESS Box 547, Hobbs, N. Mex.
AGENT and TITLE C. L. Wade, Area Superintendent C. L. Wade
WITNESSED R. A. Mikel
COMPANY El Paso Natural Gas Co.

REMARKS

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INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

NOMENCLATURE

Q = Actual rate of flow at end of flow period at W. H. working pressure (P_w).
MCF/da. @ 15.025 psia and 60° F.

P_c = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater.
psia

P_w = Static wellhead working pressure as determined at the end of flow period.
(Casing if flowing thru tubing, tubing if flowing thru casing.) psia

P_t = Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia

P_f = Meter pressure, psia.

h_w = Differential meter pressure, inches water.

F_g = Gravity correction factor.

F_t = Flowing temperature correction factor.

F_{pv} = Supercompressability factor.

n = Slope of back pressure curve.

Note: If P_w cannot be taken because of manner of completion or condition of well, then P_w must be calculated by adding the pressure drop due to friction within the flow string to P_t .