NEW MEXICO OIL CONSERVATION COMMSSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special				Test Date: 6-25-77	
Company: UNION TEXAS PETROLEUM CORP.			Connection: Northern Natural Gas Company		
Pool: Eumont (Gas)			Formation: Queen		Unit:
Completion Date: 10-7-76	Total Depth: 5215		Plug Back TD: 3850	Elevation: 3568	Farm or Lease Name: Britt "A"
Csg. Size: 5½" / Wt.: 14.0# / d: 5012' / Set At: 5215'			Perforations: From 3125' To 3290'		Well No.: 6
Tbg. Size: 2 3/8" / Wt.: 4.7# / d: 1.995" / Set At: 3269'			Perforations: From -- To --		Unit: N / Sec.: 6 / Twp.: 20 / Rge.: 37
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single			Packer Set At: None		County: Lea
Producing Thru: Tubing	Reservoir Temp. °F: 90 @ 3207	Mean Annual Temp. °F: 70°	Baro. Press. – P_a: 13.2		State: New Mexico

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
3.207	3207	.672	--	---	--	--	4.0"	Pipe

	FLOW DATA				TUBING DATA		CASING DATA		
NO.	Prover Line Size X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI					495				96.3
1.	4.000 x 2.000	118	.5	72	478	70	0		1.0
2.	4.000 x 2.000	119	1.0	69	463	70	0		1.0
3.	4.000 x 2.000	120	2.0	67	444	70	0		1.0
4.	4.000 x 2.000	121	3.9	65	412	70	0		1.0
5.									

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	69.52	8.10	131.2	.9887	1.2199	1.0129	688
2.	69.52	11.50	132.2	.9915	1.299	1.0134	980
3.	69.52	16.32	133.2	.9933	1.2199	1.0137	1394
4.	69.52	22.88	134.2	.9952	1.2199	1.0140	1958
5.							

NO.	P_t	Temp. °R	T_r	Z
1.	.20	532	1.40	.975
2.	.20	529	1.39	.974
3.	.20	527	1.38	.973
4.	.20	525	1.38	.973
5.				

Gas Liquid Hydrocarbon Ratio: 0 Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons: 0 Deg.
Specific Gravity Separator Gas: .672 — XXXXXXXXX
Specific Gravity Flowing Fluid: XXXXX — .672
Critical Pressure: 669 P.S.I.A. — 669 P.S.I.A.
Critical Temperature: 381 R — 381 R

P_c 507.5 P_c^2 258

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1	241	496	246	11
2	227	487	238	20
3	209	481	232	26
4	181	476	227	31
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 8.3323$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 8.3323$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 16,314$

Absolute Open Flow: 16,314 Mcfd @ 15.025 Angle of Slope θ: 45 Slope, n: 1.000

Remarks:

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	Paul Granger	William Higgins	