

NEW XICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special					Test Date 3/11-12/68						
Company American Trading & Production Corp.					Connection None						
Pool Wildcat					Formation Wolfcamp						
Completion Date 3/12/68			Total Depth 14,644		Plug Back TD 14,644		Elevation 3679 GL		Farm or Lease Name New Mexico #26th State Southeast Lea Unit		
Csg. Size 7	Wt. 32	d 6.094	Set At 12,090	Perforations: From 11,400 To 11,470					Well No. 1		
Tbg. Size 2 3/8	Wt. 4.7	d 1.995	Set At 11,342	Perforations: From open ended To					Unit J		
Type Well - Single - Bradenhead - G.G. or G.O. Multiple GO Dual					Packer Set At 11,336			County Lea			
Producing Thru Tubing		Reservoir Temp. °F 140° 12,000		Mean Annual Temp. °F 60°		Baro. Press. - P _a 13.2		State New Mexico			
L 11342	H 11342	G _g .665	% CO ₂ 0.2	% N ₂ 1.38	% H ₂ S 0	Prover	Meter Run X	Taps Flange			
FLOW DATA					TUBING DATA			CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							4385		Choke		24
1.	4.026	X	2.00	705	4.0	84	4292		9/64		2
2.	4.026	X	2.00	660	11.8	84	4163		13/64		2
3.	4.026	X	2.00	930	19.5	85	3853		17/64		3
4.	4.026	X	2.00	900	43.0	88	3400		20/64		2
5.											
RATE OF FLOW CALCULATIONS											
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd				
1	19.81	53.60	718.2	.9777	1.226	1.066	1357				
2	19.81	89.13	673.2	.9777	1.226	1.062	2248				
3	19.81	135.6	943.2	.9768	1.226	1.088	3500				
4	19.81	198.2	913.2	.9741	1.226	1.082	5074				
5											
NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio 4.112 Mcf/bbl.						
1	1.07	544	1.44	.880	A.P.I. Gravity of Liquid Hydrocarbons 55.5 Deg.						
2	1.01	544	1.44	.886	Specific Gravity Separator Gas .665 X X X X X X X X						
3	1.41	545	1.44	.845	Specific Gravity Flowing Fluid X X X X X						
4	1.36	548	1.45	.854	Critical Pressure 670 P.S.I.A. P.S.I.A.						
5					Critical Temperature 378 R R						
P _c 6788.2* P _c ² 46079.7					(1) $\frac{P_c^2}{P_c^2 - R_w^2} = \underline{5.780}$ (2) $\left[\frac{P_c^2}{P_c^2 - R_w^2} \right]^n = \underline{3.066}$						
NO.	P _i ²	P _w ²	P _w ²	P _c ² - P _w ²	AOF = Q $\left[\frac{P_c^2}{P_c^2 - R_w^2} \right]^n = \underline{15,557}$						
1		6714.2	45080	1000							
2		6634.2	44013	2067							
3		6450.2	41605	4475							
4		6173.2	38108	7972							
5											
Absolute Open Flow 15,557 Mcfd @ 15.025					Angle of Slope θ 57°			Slope, n .639			
Remarks: *From BHP bomb set at 11,300											
Approved By Commission:			Conducted By: <i>A. L. Smith</i>			Calculated By: <i>Wonna Keller</i>			Checked By:		