NEW MEXICO OIL CONSERVATION COMMISSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special		Test Date: 12-23-2[illegible]-6[illegible]	
Company: AMERICAN TRADING & PROD. CORP	Connection: LLANO, INC.		
Pool: SOUTHEAST LEA (WOLFCAMP)	Formation: WOLFCAMP		Unit: L
Completion Date: 12-29-63	Total Depth: 14,043'	Plug Back TD: 14250'	Elevation: 3709 RKB
Farm or Lease Name: LEA UNIT			

Csg. Size	Wt.	d	Set At	Perforations:	Well No.
SEE REMARKS				From 11,413' To 11,422'	2

Tbg. Size	Wt.	d	Set At	Perforations:	Unit	Sec.	Twp.	Rge.
2-3/8"	4.70	1.995"	11,325	From 11413' To 11422'	L	25	20S	35E

Type Well – Single – Bradenhead – G.G. or G.O. Multiple	Packer Set At	County
G.G. - (2 STRINGS 2-3/8" TUBING)	11325' & 12720'	LEA

Producing Thru	Reservoir Temp. °F	Mean Annual Temp. °F	Baro. Press. – P_a	State
2-3/8" TUBING	155 @ 11250'	60°	13.2	NEW MEXICO

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
11,250'	11,250'	0.670	--	--	--	--	2.000	FLANGE

NO.	FLOW DATA: Prover Line Size X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	TUBING DATA: Press. p.s.i.g.	Temp. °F	CASING DATA: Press. p.s.i.g.	Temp. °F	Duration of Flow
SI	2.000 x 1.250				1731		PACKER		S.I. 11[illegible] HRS.
1.	DITTO	540	0.5	87	1702		"		3 HRS
2.	"	500	3.0	89	1317		"		3 HRS
3.	"	520	5.0	90	1277		"		3 HRS
4.	"	520	7.0	87	1072		"		3 HRS
5.									

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	3.120 MCF	16.63	553.2	.9750	1.217	1.053	169
2.	3.120 "	39.25	513.2	.9732	1.217	1.047	355
3.	3.120 "	51.63	533.2	.9723	1.217	1.049	528
4.	3.120 "	61.09	533.2	.9750	1.217	1.051	619
5.							

NO.	P_t	Temp. °R	T_r	Z
1.	0.83	547	1.43	.908
2.	0.77	549	1.44	.912
3.	0.80	550	1.44	.908
4.	0.80	547	1.43	.906
5.				

Gas Liquid Hydrocarbon Ratio 145,153 Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons 55.0 Deg.
Specific Gravity Separator Gas 0.670 XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX
Critical Pressure 669 P.S.I.A. P.S.I.A.
Critical Temperature 352 R R

P_c 2013 P_c^2 4052.2

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1	2356.8	1951	3806.4	245.8
2	1734.5	1812	3283.3	768.9
3	1630.7	1648	2715.9	1336.3
4	1164.2	1487	2211.2	1841.0
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$ _____ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n =$ _____

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n =$ _____

Absolute Open Flow 1090 Mcfd @ 15.025 | Angle of Slope θ 56.5° | Slope, n 0.661

Remarks: 7-5/8" - 33.7# - 6.875" I.D. SET 11500'; 5½" LINER(20# 4.778") SET FROM 11340' - 14565'

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	Harry E. Legendre	Harry E. Legendre	
	HARRY E. LEGENDRE	HARRY E. LEGENDRE	