

NE EXICO OIL CONSERVATION COMMS
MULTIPOINT AND ONE POINT BACK PRESSURE TEST, OR GAS WELL

Form C-122
Revised 9-1-63

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 1-8-86		CONFIDENTIAL	
Company Nearburg Producing Co.		Location To Air			
Pool Und. S.E. Lea		Formation Morrow		Unit	
Completion Date 1-4-86		Total Depth 13,968'		Plug Back TD 13,557'	
				Elevation 3680 G.L.	
Casing Size 5 1/2"		Set At 13,968'		Perforations: From 13,478 to 13,482	
Thg. Size 2 7/8"		Set At 12,743'		Perforations: From Open-Ended	
Type Well - Single - Brodenhead - G.G. or G.O. Multiple Single		Packer Set At 12,743'		Well No. 1	
Producing Thru Tubing		Reservoir Temp. °F 128° @ 13,478		Mean Annual Temp. °F 60°	
				Baro. Press. - P _a 13.2	
L 13,478'		H 13,478'		G _a .6280	
		% CO ₂ .474		% N ₂ .309	
		% H ₂ S		Prover	
				Meter Run	
				Taps Flange	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							2630		PKR	CHOKE	24 Hrs.
1.	4.026	X	1.250	510	5"	84°	2270	75°		4/64	60 Min.
2.	4.026	X	1.250	510	8	90	1880	74		6/64	90
3.	4.026	X	1.250	520	14	92	1290	74		9/64	60
4.	4.026	X	1.250	520	25	85	930	74		14/64	45
5.	4.026	X	1.250	520	38	82	750	74		23/64	30 Min.

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	6.031	51.146	523.2	.9777	1.262	1.041	396.2
2	6.031	64.696	523.2	.9723	1.262	1.041	498.4
3	6.031	86.399	533.2	.9706	1.262	1.042	665.1
4	6.031	115.456	533.2	.9768	1.262	1.042	894.4
5	6.031	142.343	533.2	.9795	1.262	1.042	1105.8

NO.	R	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1	.777	544	1.495	.922	51.2 @ 60°		.6280	X X X X X X X X	673	364
2	.777	550	1.511	.922						
3	.792	552	1.516	.921						
4	.792	545	1.497	.921						
5	.792	542	1.489	.921						

P _c 4401	P _c ² 19368.8	$(1) \frac{P_c^2}{R_c^2 - R_w^2} = 19368.8$		$(2) \left[\frac{R_c^2}{R_c^2 - R_w^2} \right]^n = 2.364$	
NO.	P _i ²	P _w	R _w ²	R _c ² - R _w ²	
1		4176	17438.9	1929.9	
2		4000	16000	3368.8	
3		3658	13381	5987.8	
4		3401	11566.8	7802	
5		3343	11175.7	8193.1	

Absolute Open Flow		2614.2		Mcfd @ 15.025		Angle of Slope @ 45°		Slope, n 1.000	
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Remarks: Calculated from known BHP using Kuster Gauge 5321 Well also made 20.1 Bbls. of condensate. 51.2 @ 60° during test.

Approved By Commission:	Conducted By: W.S.	Calculated By: J.D.	Checked By: J.D.
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