

MEXICO OIL CONSERVATION COMMISSION
 MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special				Test Date 9/11/80	
Company The Superior Oil Company			Connection		
Pool			Formation Morrow		Unit West Lynch Deep Unit
Completion Date 9/12/80		Total Depth 13,875'	Plug Back TD 13,771'	Elevation 3,728'	Farm or Lease Name West Lynch Deep Unit
Csg. Size 5-1/2"	Wt. 17#	d 4.892	Set At 13,875'	Perforations: From To	
Thq. Size 2-7/8"	Wt. 6.5	d 2.441	Set At 13,540	Perforations: From 13,724 To 13,740	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 13,540' & 13,135'	County Lea
Producing Thru Tubing		Reservoir Temp. °F 287	Mean Annual Temp. °F 74	Baro. Press. - P _a 13.2	State New Mexico
L 13,732	H 13,732	G _g .678	% CO ₂ 0.68	% N ₂ 0.40	% H ₂ S 0
				Prover	Meter Run 2.900
				Taps Flange	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI	2.900		2.000				4474	74	PKR	-----	SI 72 hr
1.	2.900		2.000	510	21.0	85	1289	79	PKR	-----	6.5
2.	2.900		2.000	500	14.0	82	1922	79	PKR	-----	1.25
3.	2.900		2.000	505	9.0	82	2420	79	PKR	-----	1.0
4.	2.900		2.000	490	4.0	80	3412	79	PKR	-----	1.0
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	28993.85	104.8198	523.2	.9768	.9407	1.048	2927
2	28993.85	84.7632	513.2	.9795	.9407	1.049	2375
3	28993.85	68.2920	518.2	.9795	.9407	1.049	1905
4	28993.85	44.8642	503.2	.9813	.9407	1.049	1260
5							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1	2.80	643	1.39	.713	14.8 Mcf/bbl.	55.2 Deg.	.678	.914	673 P.S.I.A.	381 R
2	3.98	643	1.39	.715					666 P.S.I.A.	460 R
3	4.87	643	1.39	.752						
4	6.54	643	1.39	.867						
5										

P _c 6501 P _c ² 42,263				(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.539$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.539$
NO.	P _i ²	P _w	P _w ²	P _c ² - P _w ²	
1	1696		5779	36484	
2	3745		11096	31167	
3	5920		16080	26183	
4	11732		27458	14805	
5					

Absolute Open Flow 3400 Mcfd @ 15.025 Angle of Slope θ 45.0 Slope, n 1.000

Remarks:

Approved By Commission:	Conducted By: FESCO, Inc.	Calculated By: R. N. Aycok	Checked By: Vonda Flanagan
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