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appropriate district office
See Rule 401 & Rule 1122

State of New Mexico
Energy, Minerals and Natural Resources Department

Form C-122
Revised 4-1-91

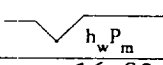
OIL CONSERVATION DIVISION

P.O. Box 2088
Santa Fe, New Mexico 87504-2088

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator Meridian Oil Inc.				Lease or Unit Name Shell State			
Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 10-11-91		Well No. 9	
Completion Date 8-8-91		Total Depth 3700		Plug Back TD 3644		Elevation 3534.2' GR	
Csg. Size 4 1/2		Wt. 11.6		Set At 3700		Perforations: From: 3377' To: 3598'	
Tbg. Size 2 3/8		Wt. 4.7		Set At 3341		Perforations: From: To:	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At None		Formation Queen	
Producing Thru tubing		Reservoir Temp. °F 60		Mean Annual Temp. °F 60		Baro. Press - P _a 13.2	
L 3341		H 3341		Gg .847		% CO ₂ 4.65	
				% N ₂ 1.86		% H ₂ S	
				Prover		Meter Run 2.067	
						Taps flange	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							40		150		72 hrs.
1.	2	X	1.500	34	6.00	60	34		-		24 hrs.
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	COEFFICIENT (24 HOUR)		Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg.	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	12.76		16.83	47.2	1.000	1.087	1.006
2.							235
3.							
4.							
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio DRY GAS Mcf/bbl.		
1.	.06	520	1.21	.988	A.P. I. Gravity of Liquid Hydrocarbons DRY Deg.		
2.					Specific Gravity Separator Gas .847 XXXXXXXXXXXX		
3.					Specific Gravity Flowing Fluid N/A XXXXXX		
4.					Critical Pressure *680 P.S.I.A. P.S.I.A.		
5.					Critical Temperature *428 R R		

P_c 163.2		P_c^2 26.6				
NO.	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$	1) $\frac{P_c^2}{P_c^2 - P_w^2} = \underline{1.494}$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \underline{1.494}$
1.		94.1	8.9	17.8		
2.						
3.						
4.						
5.						

AOF = Q	$\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \underline{.351}$
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$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = .351$$

Absolute Open Flow 351 Mcfd @ 15.025	Angle of Slope Θ 45	Slope, n 1.000
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Remarks: ***=corrected to 4.65% CO₂ & 1.86% N₂**

NO FLUID PRODUCED DURING TEST

Approved By Division	Conducted By: Pro Well Testers	Calculated By: BM	Checked By: BM
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RECEIVED

OCT 24 1991

HOBBS OFFICE