H0838 0 11170 000 Form C-122

Revised 12-1-55

MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS
Formation Seven Rivers-Once County 7:53

| | Rumont | | | | | | 3= | _County_ | | | |
|--------------|---|--|---------------------------|--------------------------------------|--|--------------------|---|-------------------------------------|------------|------------------------|--------------|
| nitia | al | Ann | ual | <u>x</u> | Spec | ial | | _Date of | Test | 9-12 | -56 |
| ompaı | ny | ities Serv | 011 | CoI | ease | State | "AO" | We] | ll No | _1_ | |
| nit | G _Se | ec. 2 T | wp. 21 | SRge | - 36E | Purch | naser | Permian | Basin | <u>Pipeli</u> | по Солр |
| asinį | g 53" W1 | t. 14.0# | I.D. 5.0 | 1 2 # Set | at | 440' Per | ·f | | To | • | |
| ubin: | g 2-3/8" W1 | 4.7£ | I.D. 1.9 | 95" Set | , at 3 | 643 _{Per} | ·f. | | То | | |
| | ay: From | | | | | | | | | | |
| | | | | | | | | | - | | |
| ouu | cing Thru: | Oabing_ | | | ······································ | Sing | le-Brade | nhead-G. | G. or | G.O. D | ual |
| co2 | of Completi - 0.85%, 1 i Through | N ₂ - 1.11% | | | OBSERV | | | Type Tag | | | |
| | | | | | 1 | Tubing | Do+ o | | | | |
| | (Prover) | Flow (Choke) | | Diff. | Temp. | Press. | | Casing I | | - | Duration |
| ۰. | (Line) Size | (Orifice) Size | | h | $\circ_{\mathtt{F}_{ullet}}$ | psig | o _F . | psig |) Jp | | of Flow |
| | Size | prze | psig | h _w | • 1 | herg | r • | | + | | |
| | <u>L</u> M | 1.50× | 471.5 | 4.8 | 93 | | | 890.7 715.0 | 93 | 7 | 2 |
| \bot | 411 | 1.50* | 402.9 | 15.0 | 68_ | | | 610.9 | 68 | | |
| T | <u></u> | 1.50* | | 39.2 | 69 | | | 545.7 | 69_ | + 2 | |
| +- | 4" | 1.50 | 403.4 | 47.1 | 70 | | | 516.7 | 70 | + 2 | 4 |
| | (24-Hour 15.26 15.26 15.26 | r) $\sqrt{h_1}$ | 24 4 27 4 | psia 84.7 96.1 95.7 76.6 | Ft 0.9497 0.9924 0.9915 0.9905 | | 0.9498 1. | | 0/8 0/8 | | 025 psia |
| | | | | | | ALCULATIO | | | | L | Cas |
| vity | quid Hydrod y of Liquid | i Hydrocarl | oons | Gas | cf/bbl. deg. | | Speci | fic Gravi | ity Flo | wing F | luid |
| vity | y of Liquid | l Hydrocari | io nons (1-e-s) | (F _c Q) ² | deg. | -0) ² | Speci | fic Gravi | ity Flo | sl7.0 | luid |
| vity | Pw (psia) | l Hydrocari | oons(1_e_=s | _ _ | deg. | | Speci ^P c—— | P _c -P _w | ity Flo | wing F 817.0 | luid |
| vity | Pw (psia) | l Hydrocari | oons(1_e_=s | _ _ | deg. | -0) ² | Speci ^P c—— | fic Gravi | ity Flo | sl7.0 | luid |
| vity | Pw (psia) | l Hydrocari | oons(1_e_=s | _ _ | deg. | -0) ² | P _c | P _c -P _w | ity Flo | sl7.0 | luid |
| vity | Pw (psia) | l Hydrocari | oons(1_e_=s | _ _ | deg. | -0) ² | Speci P _c P _w 2 | P _c -P _w | ity Flo | sl7.0 | luid |
| DSOLUDINES | Pw Pt (psia) 728.2 558.9 529.9 ute Potent | Pt in the state of | oons_(1-e ^{-s}) | (F _c Q) ² | deg. (F (1MCFPD; | -0) ² | P _w 2 530.3 312.4 280.8 | P _c -P _w 286. | ity Flo | sl7.0 | luid |

being a retest, an average slope at 1.0 was drawn through the high data point.

INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

NOMENCLATURE

- Q I Actual rate of flow at end of flow period at W. H. working pressure ($P_{\rm w}$). MCF/da. @ 15.025 psia and 600 F.
- P_c 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- PwT Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- Pf Meter pressure, psia.
- hw Differential meter pressure, inches water.
- Fg Gravity correction factor.
- Ft Flowing temperature correction factor.
- F_{nv} Supercompressability factor.
- n _ Slope of back pressure curve.

Note: If $P_{\mathbf{W}}$ cannot be taken because of manner of completion or condition of well, then $P_{\mathbf{W}}$ must be calculated by adding the pressure drop due to friction within the flow string to $P_{\mathbf{t}}$.