

NEW MEXICO OIL CONSERVATION COMMISSION

Form C-122

Revised 12-1-55

ONE HOBBS OFFICE OCC

POINT BACK PRESSURE TEST FOR GAS WELLS

1950 APR 14 AM

Pool Blinebry Formation Blinebry County LeaInitial X Annual _____ Special _____ Date of Test Dec. 19-20, 1957Company Neville G. Penrose, Inc. Lease Hinton Well No. 5Unit P Sec. 12 Twp. 22S Rge. 37E Purchaser Permian Basin Pipeline Co.Casing 5½ Wt. 15.5 I.D. 4.950" Set at 6215' Perf. 5606' To 5642'Tubing 2 3/8 Wt. 4.70 I.D. 1.995" Set at 6210' Perf. 6206' To 6210'(Garrett Sleeve)
Gas Pay: From 5606' To 5642' L 5992' xG 0.700 set 4194' Bar.Press. 13.2Producing Thru: Casing _____ Tubing only Type Well Gas-gas dualDate of Completion: 12-15-57 Packer 6022' Reservoir Temp. _____
Single-Bradenhead-G. G. or G.O. Dual

OBSERVED DATA

4" Meter run
Tested Through (Prover) (Choke) (Meter) Type Taps _____

| Flow Data | | | | | | Tubing Data | | Casing Data | | Duration of Flow Hr. |
|-----------|----------------------------|------------------------------|----------------|-------------------------|--------------|----------------|--------------|----------------|--------------|----------------------------|
| No. | (Prover) (Line) Size | (Choke) (Orifice) Size | Press. psig | Diff. h _w | Temp. °F. | Press. psig | Temp. °F. | Press. psig | Temp. °F. | |
| 1. | 4 | 1.25" | 511.0 | 12.1 | 62 | 1610.5 | 1623.7 | | | 48 hrs. |
| 2. | | | | | | 520.2 | 533.4 | | | 24 hrs |
| 3. | | | | | | | | | | |
| 4. | | | | | | | | | | |
| 5. | | | | | | | | | | |

FLOW CALCULATIONS

| No. | Coefficient (24-Hour) | $\sqrt{h_w P_g}$ | Pressure psia | Flow Temp. Factor F _t | Gravity Factor F _g | Compress. Factor F _{pv} | Rate of Flow Q-MCFPD @ 15.025 psia |
|-----|--------------------------|------------------|------------------|--|-------------------------------------|--|--|
| 1. | 10.24 | 79.64 | | 0.9981 | 0.9258 | 1.068 | 805 |
| 2. | | | | | | | |
| 3. | | | | | | | |
| 4. | | | | | | | |
| 5. | | | | | | | |

PRESSURE CALCULATIONS

Gas Liquid Hydrocarbon Ratio _____ cf/bbl.
Gravity of Liquid Hydrocarbons _____ deg.
F_c _____ (1-e^{-s})
Specific Gravity Separator Gas _____
Specific Gravity Flowing Fluid _____
P_c _____ P_c _____

| No. | P _w P _t (psia) | P _t ² | F _c Q | (F _c Q) ² | (F _c Q) ² (1-e ^{-s}) | P _w ² | P _c ² -P _w ² | Cal. P _w | P _w P _c |
|-----|---|-----------------------------|------------------|---------------------------------|---|-----------------------------|--|------------------------|----------------------------------|
| 1. | 284.5 | 284.5 | 7.998 | 63.97 | 16.06 | 300.6 | 2335.8 | 548.3 | .39 |
| 2. | | | | | | | | | |
| 3. | | | | | | | | | |
| 4. | | | | | | | | | |
| 5. | | | | | | | | | |

Absolute Potential: 898 MCFPD; n 0.90COMPANY Permian Basin Pipeline CompanyADDRESS Hobbs, New MexicoAGENT and TITLE R.L. WestWITNESSED Glenn G. Neill *Glenn G. Neill*COMPANY Neville G. Penrose, Inc.

REMARKS

Well tested through 4" meter run.

Specific gravity was estimated at .700 and the average Blinebry Pool
slope (n) was used in the calculation of potentials.L. A. UTZ
GAS ENGINEER

INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

NOMENCLATURE

Q = Actual rate of flow at end of flow period at W. H. working pressure (P_w).
MCF/da. @ 15.025 psia and 60° F.

P_c = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater.
psia

P_w = Static wellhead working pressure as determined at the end of flow period.
(Casing if flowing thru tubing, tubing if flowing thru casing.) psia

P_t = Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia

P_f = Meter pressure, psia.

h_w = Differential meter pressure, inches water.

F_g = Gravity correction factor.

F_t = Flowing temperature correction factor.

F_{pv} = Supercompressability factor.

n = Slope of back pressure curve.

Note: If P_w cannot be taken because of manner of completion or condition of well, then P_w must be calculated by adding the pressure drop due to friction within the flow string to P_t .