NEW ..EXICO OIL CONSERVATION COMMSSI..I

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special				Test Date: 1-28-82	
Company: AMOCO PRODUCTION COMPANY			Connection: LLANO PIPE LINE		
Pool: WILDCAT			Formation: UND. MORROW		Unit:
Completion Date: 1-8-82	Total Depth: 14623.		Plug Back TD: 14593.	Elevation: 3268.	Farm or Lease Name: STATE IT
Csg. Size: 4.500 / Wt.: 15.1 / d: 3.707	Set At: 14623.		Perforations: From 14418. To 14450.		Well No.: 1
Tbg. Size: 2.875 / Wt.: 6.5 / d: 2.441	Set At: 14165.		Perforations: From 0. To 0.		Unit: F / Sec.: 16 / Twp.: 26 / Rge.: 33
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: SINGLE			Packer Set At: 11613.		County: LEA
Producing Thru: TUBING	Reservoir Temp. °F: 184 @ 14434.	Mean Annual Temp. °F: 60.0	Baro. Press. – P_a: 13.2		State: NEW MEXICO

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
14434.	14434.	0.635	0.59	0.97	0.	0.	4.0	FLANGE

	FLOW DATA				TUBING DATA		CASING DATA		
NO.	Prover Line Size X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI					8390.	69.			46.0
1.	4.03 x 1.500	380.	5.0	36.	7210.	64.	0.	0.	0.7
2.	4.03 x 1.500	385.	10.0	34.	6100.	68.	0.	0.	0.7
3.	4.03 x 1.500	390.	18.0	30.	5325.	70.	0.	0.	0.7
4.	4.03 x 1.500	390.	29.0	23.	4250.	71.	0.	0.	0.7
5.									

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	10.84	44.34	393.2	1.0239	1.2549	1.0452	646.
2.	10.84	63.10	398.2	1.0260	1.2549	1.0465	922.
3.	10.84	85.19	403.2	1.0302	1.2549	1.0484	1252.
4.	10.84	108.13	403.2	1.0376	1.2549	1.0506	1604.
5.							

NO.	P_r	Temp. °R	T_r	Z
1.	0.59	496.	1.36	0.915
2.	0.59	494.	1.35	0.913
3.	0.60	490.	1.34	0.910
4.	0.60	483.	1.32	0.906
5.				

Gas Liquid Hydrocarbon Ratio 0. Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons 0. Deg.
Specific Gravity Separator Gas 0.635 XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX 0.635
Critical Pressure 672. P.S.I.A. 672. P.S.I.A.
Critical Temperature 366. R 366. R

P_c 8410.4 P_c^2 70734

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1	52175.	7224.	52183.	18551.
2	37371.	6108.	37305.	33429.
3	28496.	5330.	28409.	42325.
4	18175.	4253.	18089.	52645.
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.6799$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.6437$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 2058$

Absolute Open Flow 2058 Mcfd @ 15.025 Angle of Slope θ 46.2 Slope, n .958

Remarks: Point No. 3 used to extrapolate AOF.

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
		Barbara Hemmeline	Larry Sheppard