

HOBBS OCD

13-507

Form 3160-3
(March 2012)

JUN 18 2013

AMENDED

RECEIVED

UNITED STATES
DEPARTMENT OF THE INTERIOR
BUREAU OF LAND MANAGEMENT

OCD Hobbs

FORM APPROVED
OMB No. 1004-0137
Expires October 31, 2014

APPLICATION FOR PERMIT TO DRILL OR REENTER

1a. Type of work: <input checked="" type="checkbox"/> DRILL <input type="checkbox"/> REENTER		5. Lease Serial No. NM LC 060329
1b. Type of Well: <input checked="" type="checkbox"/> Oil Well <input type="checkbox"/> Gas Well <input type="checkbox"/> Other <input checked="" type="checkbox"/> Single Zone <input type="checkbox"/> Multiple Zone		6. If Indian, Allottee or Tribe Name N/A
2. Name of Operator ConocoPhillips Company		7. If Unit or CA Agreement, Name and No. N/A
3a. Address P.O. Box 51810 Midland, Texas 79710-1810		8. Lease Name and Well No. Emerald Federal #9 <38742>
3b. Phone No. (include area code) 432-688-6913		9. API Well No. 30-025-41231
4. Location of Well (Report location clearly and in accordance with any State requirements.) At surface 420' FSL and 1340' FEL; UL O, Sec. 17, T17S, R32E At proposed prod. zone 366' FSL and 964' FEL; UL P, Sec. 17, T17S, R32E		10. Field and Pool, or Exploratory Maljamar; Yeso West <44500>
14. Distance in miles and direction from nearest town or post office* Approximately 3 miles south of Maljamar, New Mexico		11. Sec., T. R. M. or Blk. and Survey or Area Sec. 17, T17S, R32E
15. Distance from proposed* location to nearest property or lease line, ft. (Also to nearest drig. unit line, if any)	16. No. of acres in lease 323.76	17. Spacing Unit dedicated to this well 40
18. Distance from proposed location* to nearest well, drilling, completed, applied for, on this lease, ft.	19. Proposed Depth 7044' MD/7026'TVD	20. BLM/BIA Bond No. on file ES 0085
21. Elevations (Show whether DF, KDB, RT, GL, etc.) 4032' GL	22. Approximate date work will start* 08/23/2013	23. Estimated duration 10 days

24. Attachments

The following, completed in accordance with the requirements of Onshore Oil and Gas Order No.1, must be attached to this form:

- | | |
|--|---|
| 1. Well plat certified by a registered surveyor. | 4. Bond to cover the operations unless covered by an existing bond on file (see Item 20 above). |
| 2. A Drilling Plan. | 5. Operator certification |
| 3. A Surface Use Plan (if the location is on National Forest System Lands, the SUPO must be filed with the appropriate Forest Service Office). | 6. Such other site specific information and/or plans as may be required by the BLM. |

25. Signature <i>Susan B. Maunder</i>	Name (Printed/Typed) Susan B. Maunder	Date 4/26/13
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Title

Senior Regulatory Specialist

Approved by (Signature) <i>/s/George MacDonell</i>	Name (Printed/Typed) <i>/s/George MacDonell</i>	Date JUN 13 2013
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Title

for FIELD MANAGER

Office

CARLSBAD FIELD OFFICE

Application approval does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon.

Conditions of approval, if any, are attached.

APPROVAL FOR TWO YEARS

Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

(Continued on page 2)

*(Instructions on page 2)

Roswell Controlled Water Basin

Approval Subject to General Requirements
& Special Stipulations AttachedSEE ATTACHED FOR
CONDITIONS OF APPROVAL*Jim*

Drilling Plan
ConocoPhillips Company
Maljamar; Yeso, west

Emerald Federal #9

Lea County, New Mexico

1. Estimated tops of geological markers and estimated depths to water, oil, or gas formations:

The ranges of depths for the formation tops, thicknesses, and planned Total Depths for all the wells to be drilled under this Master Drilling Plan are presented in the table below.

The datum for these depths is RKB (which is 13' above Ground Level).

Formations	Top Depth FT TVD	Top Depths FT MD	Contents
Quaternary	Surface	Surface	Fresh Water
Rustler	791	791	Anhydrite
Salado (top of salt)	972	972	Salt
Tansill (base of salt)	1980	1980	Gas, Oil and Water
Yates	2116	2116	Gas, Oil and Water
Seven Rivers	2451	2451	Gas, Oil and Water
Queen	3082	3085	Gas, Oil and Water
Grayburg	3493	3497	Gas, Oil and Water
San Andres	3875	3881	Gas, Oil and Water
Glorieta	5364	5375	Gas, Oil and Water
Paddock	5438	5450	Gas, Oil and Water
Blinberry	5780	5793	Gas, Oil and Water
Tubb	6826	6843	Gas, Oil and Water
Deepest estimated perforation	6826	6843	Deepest estimated perf. is ~ Top of Tubb
Total Depth (maximum)	7026	7044	200' below deepest estimated perforation

All of the water bearing formations identified above will be protected by setting of the 8-5/8" surface casing 25' – 70' into the Rustler formation and circulating of cement from casing shoe to surface in accordance with the provisions of Onshore Oil and Gas Order No. 2 and New Mexico Oil Conservation Division Title 19.

The targeted oil and gas bearing formations identified above will be protected by setting of the 5-1/2" production casing 10' off bottom of TD and circulating of cement from casing shoe to surface in accordance with the provisions of Onshore Oil and Gas Order No. 2 and New Mexico Oil Conservation Division Title 19.

2. Proposed casing program

Type	Hole Size (in)	Interval MD RKB (ft)		OD (inches)	Wt (lb/ft)	Gr	Conn	MIY (psi)	Col (psi)	Jt Str (klbs)	Safety Factors Calculated per ConocoPhillips Corporate Criteria		
		From	To								Burst DF	Collapse DF	Jt Str DF (Tension) Dry/Buoyant
Cond	20	0	40' - 85' (30' - 75' BGL)	16	0.5" wall	B	Line Pipe	N/A	N/A	N/A	NA	NA	NA
Alt. Cond	20	0	40' - 85' (30' - 75' BGL)	13-3/8	48#	H-40	PE	1730	740	N/A	NA	NA	NA
Surf	12-1/4	0	816' - 861'	8-5/8	24#	J-55	STC	2950	1370	244	1.57	5.39	3.59
Prod	7-7/8	0	6989' - 7034'	5-1/2	17#	L-80	LTC	7740	6290	338	2.12	2.46	1.98

The casing will be suitable for H₂S Service. All casing will be new.

The surface and production casing will be set approximately 10' off bottom and we will drill the hole with a 45' range uncertainty for casing set depth to fit the casing string so that the cementing head is positioned at the floor for the cement job.

The production casing will be set 155' to 200' below the deepest estimated perforation to provide rathole for the pumping completion and for the logs to get deep enough to log the interval of interest.

Casing Safety Factors - BLM Criteria:

Type	Depth	W t	MIY	Col	Jt Str	Drill Fluid	Burs t	Collaps e	Tensile-Dry	Tens-Bouy
Surface Casing	861	24	2950	137 0	24400 0	8.5	7.75	3.60	11.8	13.6
Production Casing	7034	17	7740	629 0	33800 0	10	2.12	1.72	2.83	3.34

Casing Safety Factors - Additional ConocoPhillips Criteria:

ConocoPhillips casing design policy establishes Corporate Minimum Design Factors (see table below) and requires that service life load cases be considered and provided for in the casing design.

ConocoPhillips Corporate Criteria for Minimum Design Factors

	Burst	Collapse	Axial
Casing Design Factors	1.15	1.05	1.4

Type	Depth	Wt	MIY	Col	Jt Str	Pipe Yield MW	Burst Col	Ten
Conductor	86	65	35000	-	-	432966	-	-
Surface Casing (8-5/8" 24# J-55 STC)	861	24	2950	1370	244000	381000	8.5	1.57
Production Casing (5-1/2" 17# L-80 LTC)	7034	17	7740	6290	338000	397000	10	2.12

Safety Factors - ConocoPhillips Criteria

The maximum internal (burst) load on the Surface Casing occurs when the surface casing is tested to 1500 psi (as per BLM Onshore Order 2 - III. Requirements).

The maximum internal (burst) load on the Production Casing occurs during the fracture stimulation where the maximum allowable working pressure

(MAWP) is the pressure that would fit ConocoPhillips Corporate Criteria for Minimum Factors.

$$\begin{aligned} \text{Surface Casing Test Pressure} &= 1500 \text{ psi} \\ \text{Surface Rated Working Pressure (ROPE)} &= 3000 \text{ psi} \\ \text{Field SW} &= 10 \text{ ppg} \end{aligned}$$

$$\begin{aligned} \text{Predicted Pore Pressure at TD (PPTD)} &= 8.55 \text{ ppg} \\ \text{Predicted Frac Gradient at Shoe (CSFG)} &= 19.23 \text{ ppg} \end{aligned}$$

Surface Casing Burst Safety Factor = API Burst Rating / Maximum Predicted Surface Pressure (MPSP) 'OR' Maximum Allowable Surface Pressure (MASP)

Production Casing MAWP for the Fracture Stimulation = API Burst Rating / Corporate Minimum Burst Design Factor

Surface Casing Burst Safety Factor:

$$\begin{aligned} \text{Case \#1, MPSP (MWHyd next section)} &= 861 \times 0.052 \times 10 = 448 \\ \text{Case \#2, MPSP (Field SW @ Bullheadcsg + 200 psi)} &= 861 \times 0.052 \times 19.23 = 613 \\ \text{Case \#3, MPSP (Kick Vol @ next section TD)} &= 7034 \times 0.052 \times 8.55 = 617.3 \\ \text{Case \#4, MPSP (PPTD - GG)} &= 7034 \times 0.052 \times 8.55 = 703.4 \\ \text{Case \#3 \& \#4 Limited to MPSP (CSFG + 0.2 ppg)} &= 861 \times 0.052 \times (19.23 + 0.2) = 870 \\ \text{MASP (MWHyd + Test Pressure)} &= 861 \times 0.052 \times 8.5 + 1500 = 1881 \\ \text{Burst Safety Factor (Max. MPSP or MASP)} &= 2950 / 1881 = 1.57 \end{aligned}$$

Production Casing Burst Safety Factor:

$$\begin{aligned} \text{Case \#1, MPSP (MWHyd TD)} &= 7034 \times 0.052 \times 10 = 3657.68 \\ \text{Case \#4, MPSP (PPTD - GG)} &= 7034 \times 0.052 \times 8.55 = 703.4 \\ \text{Burst Safety Factor (Max. MPSP)} &= 7740 / 3658 = 2.12 \\ \text{MAWP for the Fracture Stimulation (Corporate Criteria)} &= 7740 / 1.15 = 6730 \end{aligned}$$

Collapse Safety Factors - ConocoPhillips Criteria

The maximum collapse load on the Surface Casing occurs when the pressure is released after bumping the plug on the surface casing cement

job. The maximum collapse load on the production casing occurs with the well is pumped off on production. We plan to cement the production

casing to surface, and therefore the external pressure profile on the production casing should be equal to the pore pressure of the horizons on the

outside of the casing which we estimate to be 8.5 ppg gradient.

Surface Casing Collapse Safety Factor = API Collapse Rating / Cement Displacement during Cementing to Surface

Production Casing Collapse Safety Factor = API Collapse Rating / Maximum Predicted Surface Pressure 'OR' Cement Displacement during Cementing to Surface

$$\text{Cement Displacement Fluid (FW)} = 8.34 \text{ ppg}$$

Surface Casing Collapse Safety Factor:

$$\begin{aligned} \text{Maximum Diff Lift Pressure} &= [(561 \times 0.052 \times 13.6) + (300 \times 0.052 \times 14.8)] - 373 = 254 \\ \text{Collapse Safety Factor} &= 1370 / 254 = 5.39 \end{aligned}$$

Production Casing Collapse Safety Factor:

$$\begin{aligned} \text{Maximum Diff Lift Pressure} &= [(1634 \times 0.052 \times 11.8) + (5400 \times 0.052 \times 16.4)] - 3051 = 2557 \\ \text{Case \#4, MPSP (PPTD-GG)} &= 7034 \times 0.052 \times 8.6 = 703.4 \\ \text{Collapse Safety Factor} &= 6290 / 2557 = 2.46 \end{aligned}$$

Tensile Strength Safety Factors - ConocoPhillips Criteria

The maximum axial (tension) load occurs if casing were to get stuck and pulled on to try to get it unstuck.

Maximum Allowable Axial Load for Pipe Yield = API Pipe Yield Strength Rating / Corporate Minimum Axial Design Factor

Maximum Allowable Axial Load for Joint = API Joint Strength Rating / Corporate Minimum Axial Design Factor

Maximum Allowable Hook Load (Limited to 75% of Rig Max Load) = Maximum Allowable Axial Load

Maximum Allowable Overpull Margin = Maximum Allowable Hook Load - Bouyant Wt of the String

Tensile Safety Factor = API Pipe Yield 'OR' API Joint Strength 'OR' Rig Max Load Rating / (Bouyant Wt of String + Minimum Overpull Required)

$$\begin{aligned} \text{Rig Max Load (300,000 lbs) x 75\%} &= 225000 \text{ lbs} \\ \text{Minimum Overpull Required} &= 50000 \text{ lbs} \end{aligned}$$

Surface Casing Tensile Strength Safety Factor:

$$\begin{aligned} \text{Air Wt} &= 20664 \\ \text{Bouyant Wt} &= 20664 \times 0.870 = 17982 \\ \text{Max. Allowable Axial Load (Pipe Yield)} &= 381000 / 1.40 = 272143 \\ \text{Max. Allowable Axial Load (Joint)} &= 244000 / 1.40 = 174286 \\ \text{Max. Allowable Hook Load (Limited to 75\% of Rig Max Load)} &= 174286 \\ \text{Max. Allowable Overpull Margin} &= 174286 - (20664 \times 0.870) = 156303 \\ \text{Tensile Safety Factor} &= 244000 / (17982 + 50000) = 3.59 \end{aligned}$$

Production Casing Tensile Strength Safety Factor:

$$\begin{aligned} \text{Air Wt} &= 119578 \\ \text{Bouyant Wt} &= 119578 \times 0.847 = 101322 \\ \text{Max. Allowable Axial Load (Pipe Yield)} &= 397000 / 1.40 = 283571 \\ \text{Max. Allowable Axial Load (Joint)} &= 338000 / 1.40 = 241429 \\ \text{Max. Allowable Hook Load (Limited to 75\% of Rig Max Load)} &= 225000 \\ \text{Max. Allowable Overpull Margin} &= 225000 - (119578 \times 0.847) = 123678 \\ \text{Tensile Safety Factor} &= 300000 / (101322 + 50000) = 1.98 \end{aligned}$$

Compression Strength Safety Factors - ConocoPhillips Criteria

The maximum axial (compression) load for the well is where the surface casing is landed on the conductor

with a support of a plate or landing ring. The surface casing is also calculated to bear 60% of the load

but not limited. Any other axial loads such as a snubbing unit or other would need to be added to the load.

Compression Safety Factor = API Axial Joint Strength Rating 'OR' API Axial Pipe Yield Rating / Maximum Predicted Load

$$\text{Wellhead Load} = 3000 \text{ lbs}$$

Compression Safety Factor

$$\begin{aligned} \text{Surf Casing Wt (Bouyant)} &= (20664 \times 0.870) = 17982 \\ \text{Prod Casing Wt (Bouyant)} &= (119578 \times 0.847) = 101322 \\ \text{Tubing Wt (Air Wt)} &= 7034 \times 6.5 = 45721 \\ \text{Tubing Fluid Wt} &= 7034 \times 0.052 \times 6.55 \times 0.7854 \times 2.441^2 = 11212 \\ \text{Load on Conductor} &= 3000 + 17982 + 101322 + 45721 + 11212 = 179237 \\ \text{Conductor Compression Safety Factor} &= 432966 / 179237 = 2.42 \\ \text{Load on Surface Casing} &= 179237 \times 60\% = 107542 \\ \text{Surface Casing Compression Safety Factor} &= 244000 / 107542 = 2.27 \end{aligned}$$

16" or 13-3/8" Conductor:

Cement to surface with rathole mix, ready mix or Class C Neat cement.
(Note: The gravel used in the cement is not to exceed 3/8" diameter)
TOC at surface.

8-5/8" Surface Casing Cementing Program:

The intention for the cementing program for the Surface Casing is to:

- Place the Tail Slurry from the casing shoe to 300' above the casing shoe,
- Bring the Lead Slurry to surface.

Spacer: 20 bbls Fresh Water

Slurry		Intervals Ft MD		Weight ppg	Sx	Vol Cuft	Additives	Yield ft ³ /sx
Lead	Class C	Surface	516' – 561'	13.6	300	510	+ 2% Extender + 2% CaCl ₂ + 0.125 lb/sx Lost Circulation Control Agent + 0.2% Defoamer Excess = 200% based on gauge hole volume	1.70
Tail	Class C	516' – 561'	816' – 861'	14.8	200	268	1% CaCl ₂ Excess = 100% based on gauge hole volume	1.34

Displacement: Fresh Water.

Note: In accordance with the Pecos District Conditions of Approval, we will Wait on Cement (WOC) for a period of not less than 18 hrs after placement or until at least 500 psi compressive strength has been reached in both the Lead Slurry and Tail Slurry cements on the Surface Casing, whichever is greater.

5-1/2" Production Casing Cementing Program – Single Stage Cementing Option:

The intention for the cementing program for the Production Casing – Single Stage Cementing Option is to:

- Place the Tail Slurry from the casing shoe to above the top of the Paddock,
- Bring the Lead Slurry to surface.

Spacer: 20 bbls Fresh Water

Slurry		Intervals Ft MD		Weight ppg	Sx	Vol Cuft	Additives	Yield ft ³ /sx
Lead	50:50 Poz/C	Surface	5200'	11.8	700	1820	10% Bentonite 8 lbs/sx Salt 0.4% Fluid loss additive 0.125% LCM if needed Excess = 115 % or more if needed based on gauge hole volume	2.6
Tail	Class H	5200'	6989' – 7034'	16.4	400	428	0.2% Fluid loss additive 0.3% Dispersant 0.15% Retarder 0.2% Antifoam Excess = 45% or more if needed based on gauge hole volume	1.07

Displacement: Fresh Water with approximately 250 ppm gluteraldehyde biocide.

Proposal for Option to Adjust Production Casing Cement Volumes:

The production casing cement volumes for the proposed single stage and two-stage option presented above are estimates based on gauge hole. We will adjust these volumes based on the caliper log data for each well and our trends for amount of cement returns to surface. Also, if no caliper log is available for any particular well, we would propose an option to possibly increase the production casing cement volume to account for any uncertainty in regard to the hole volume.

4. Pressure Control Equipment:

A 11" 3M system will be installed, used, maintained, and tested accordingly as described in Onshore Oil and Gas Order No. 2.

Our BOP equipment will be:

- Rotating Head
- Annular BOP, 11" 3M
- Blind Ram, 11" 3M
- Pipe Ram, 11" 3M

After nipping up, and every 30 days thereafter or whenever any seal subject to test pressure is broken followed by related repairs, blowout preventors will be pressure tested. BOP will be inspected and operated at least daily to insure good working order. All pressure and operating tests will be done by an independent service company and recorded on the daily drilling reports. BOP will be tested using a test plug to isolate BOP stack from casing. BOP test will include a low pressure test from 250 to 300 psi for a minimum of 10 minutes or until requirements of test are met, whichever is longer. Ram type preventers and associated equipment will be tested to the approved stack working pressure of 3000 psi isolated by test plug. Annular type preventers will be tested to 50 percent of rated working pressure, and therefore will be tested to 1500 psi. Pressure will be held for at least 10 minutes or until provisions of test are met, whichever is longer. Valve on casing head below test plug will be open during testing of BOP stack. BOP will comply with all provisions of Onshore Oil and Gas Order No. 2 as specified. **See Attached BOPE Schematic.** A variance is respectfully requested to allow for the use of flexible hose. The variance request is included as a separate enclosure with attachments.

5. Proposed Mud System:

The mud systems that are proposed for use are as follows:

DEPTH	TYPE	Density ppg	FV sec/qt	API Fluid Loss cc/30 min	pH	Vol bbl
0 – Surface Casing Point	Fresh Water or Fresh Water Native Mud in Steel Pits	8.5 – 9.0	28 – 40	N.C.	N.C.	150 – 300
Surface Casing Point to TD	Brine (Saturated NaCl ₂) in Steel Pits	10	29	N.C.	10 – 11	300 – 1000
Conversion to Mud at TD	Brine Based Mud (NaCl ₂) in Steel Pits	10	33 – 40	5 – 10	10 – 11	0 – 1000

Drilling mud containing H₂S shall be degassed in accordance with API RP-49, item 5.14. H₂S Monitoring Alarm installed at the possum belly could be set as low as 5 to 10 ppm and go into high alarm. The gases shall be piped into the flare system. Gas detection equipment and pit level flow monitoring equipment will be on location. A percentage flow paddle installed in the flow line measures relative amount of mud flowing in non-pressurized return line. There are 4 mud probes in the system. One probe is installed in each of the individual tanks to measure the volume of the drilling fluid in individual mud and trip tanks at the well site. The mud probe data is collected by the Pit Volume Totalizer (PVT) system and the information is available real-time via display in the dog house and the company representative's office on location. ConocoPhillips Company will maintain sufficient mud and weighting material on location if hole conditions warrant.

Proposal for Option to Not Mud Up at TD:

FW, Brine, and Mud volume presented above are estimates based on gauge 12-1/4" or 7-7/8" holes. We will adjust these volume based on hole conditions. We do not plan to keep any weighting material at the wellsite. Also, we propose an option to not mud up leaving only brine in the hole if we have good hole stability.

In the event that the well is flowing from a waterflow, then we would discharge excess drilling fluids from the steel mud pits through a fas-line into steel frac tanks at an offset location for containment. Depending on the rate of waterflow, excess fluids will be hauled to an approved disposal facility, or if in suitable condition, may be reused on the next well.

No reserve pit will be built.

6. Logging, Coring, and Testing Program: *See COA*

- a. No drill stem tests will be done
- b. Remote gas monitoring planned for the production hole section (optional).
- c. No whole cores are planned
- d. The open hole electrical logging program is planned to be as follows:
 - Total Depth to 2500': Spectral GR, Gamma Ray, Resistivity, Density, and BHC Sonic
 - Total Depth to surface Casing Shoe: Caliper
 - Total Depth to surface, Gamma Ray and Neutron
 - Total Depth to 2500'; Dielectric Scanner (optional)
 - Formation pressure data (XPT) on electric line if needed (optional)
 - Rotary Sidewall Cores on electric line if needed (optional)
 - FMI (Formation Micromager) if needed (optional)

7. Abnormal Pressures and Temperatures:

- No abnormal pressures are expected to be encountered.
- Loss of circulation is a possibility in the horizons below the Top of Grayburg. We expect that normal Loss of Circulation Material will be successful in healing any such loss of circulation events.
 - The bottom hole pressure is expected to be 8.55 ppg gradient.
 - The expected Bottom Hole Temperature is 115 degrees F.
- The estimated H₂S concentrations and ROE calculations for the gas in the zones to be penetrated are presented in the table below for the various producing horizons in this area:

FORMATION / ZONE	H2S (PPM)	Gas Rate (MCFD)	ROE 100 PPM	ROE 500 PPM
Grayburg / San Andres (from MCA)	14000	38	59	27
Yeso Group	400	433	34	15

ConocoPhillips will comply with the provisions of Oil and Gas Order # 6

8. Anticipated starting date and duration of operations:

Well pad and road constructions will begin as soon as all agency approvals are obtained. Anticipated date to drill this well is mid 2013 after receiving approval of the APD.

Attachments:

- Attachment # 1.....BOP and Choke Manifold Schematic – 3M System
- Attachment # 2.....Diagram of Choke Manifold Equipment

Contact Information:

Proposed 16 April 2013 by:
James Chen
Drilling Engineer, ConocoPhillips Company
Phone (832) 486-2184
Cell (832) 768-1647

ConocoPhillips MCBU

Buckeye

Emerald Federal

Emerald Federal 9

Original Hole

Plan: Actual Plan

Standard Planning Report - Geographic

22 April, 2013

ConocoPhillips

Planning Report - Geographic

Database:	EDM Central Planning	Local Co-ordinate Reference:	Well Emerald Federal 9
Company:	ConocoPhillips MCBU	TVD Reference:	RKB @ 4045.0usft (PD 822)
Project:	Buckeye	MD Reference:	RKB @ 4045.0usft (PD 822)
Site:	Emerald Federal	North Reference:	Grid
Well:	Emerald Federal 9	Survey Calculation Method:	Minimum Curvature
Wellbore:	Original Hole		
Design:	Actual Plan		

Project	Buckeye, Lea County, NM		
Map System:	US State Plane 1927 (Exact solution)	System Datum:	Mean Sea Level
Geo Datum:	NAD 1927 (NADCON CONUS)		
Map Zone:	New Mexico East 3001		Using geodetic scale factor

Site	Emerald Federal, New Mexico, Southeast		
Site Position:	Northing:	666,142.95 usft	Latitude: 32° 49' 48.382 N
From: Lat/Long	Easting:	668,872.52 usft	Longitude: 103° 47' 0.841 W
Position Uncertainty:	3.5 usft	Slot Radius: 8"	Grid Convergence: 0.30 °

Well	Emerald Federal 9, Deviated Well		
Well Position	+N/-S	0.0 usft	Northing: 665,535.91 usft
	+E/-W	0.0 usft	Easting: 668,775.09 usft
Position Uncertainty	3.5 usft	Wellhead Elevation:	Ground Level: 4,032.0 usft

Wellbore	Original Hole		
Magnetics	Model Name	Sample Date	Declination
	BGGM2012	4/22/2013	7.60
			Dip Angle 60.61
			Field Strength 48,746 (nT)

Design	Actual Plan		
Audit Notes:			
Version:	1	Phase: PLAN	Tie On Depth: 0.0
Vertical Section:	Depth From (TVD)	+N/-S	+E/-W
	(usft)	(usft)	(usft)
	0.0	0.0	0.0
			Direction 103.57
			(°)

Plan Sections										
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)	TFO (°)	Target
0.0	0.00	0.00	0.0	0.0	0.0	0.00	0.00	0.00	0.00	
2,116.0	0.00	0.00	2,116.0	0.0	0.0	0.00	0.00	0.00	0.00	
2,425.6	4.64	103.57	2,425.2	-2.9	12.2	1.50	1.50	0.00	103.57	
5,448.3	4.64	103.57	5,438.0	-60.4	250.1	0.00	0.00	0.00	0.00	Emerald Federal 9 (T)
7,041.5	4.64	103.57	7,026.0	-90.6	375.5	0.00	0.00	0.00	0.00	

ConocoPhillips

Planning Report - Geographic

Database:	EDM Central Planning	Local Co-ordinate Reference:	Well Emerald Federal 9
Company:	ConocoPhillips MCBU	TVD Reference:	RKB @ 4045.0usft (PD 822)
Project:	Buckeye	MD Reference:	RKB @ 4045.0usft (PD 822)
Site:	Emerald Federal	North Reference:	Grid
Well:	Emerald Federal 9	Survey Calculation Method:	Minimum Curvature
Wellbore:	Original Hole		
Design:	Actual Plan		

Planned Survey										
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Map Northing (usft)	Map Easting (usft)	Latitude	Longitude	
0.0	0.00	0.00	0.0	0.0	0.0	665,535.91	668,775.09	32° 49' 42.380 N	103° 47' 2.020 W	
75.0	0.00	0.00	75.0	0.0	0.0	665,535.91	668,775.09	32° 49' 42.380 N	103° 47' 2.020 W	
Conductor										
100.0	0.00	0.00	100.0	0.0	0.0	665,535.91	668,775.09	32° 49' 42.380 N	103° 47' 2.020 W	
200.0	0.00	0.00	200.0	0.0	0.0	665,535.91	668,775.09	32° 49' 42.380 N	103° 47' 2.020 W	
300.0	0.00	0.00	300.0	0.0	0.0	665,535.91	668,775.09	32° 49' 42.380 N	103° 47' 2.020 W	
400.0	0.00	0.00	400.0	0.0	0.0	665,535.91	668,775.09	32° 49' 42.380 N	103° 47' 2.020 W	
500.0	0.00	0.00	500.0	0.0	0.0	665,535.91	668,775.09	32° 49' 42.380 N	103° 47' 2.020 W	
600.0	0.00	0.00	600.0	0.0	0.0	665,535.91	668,775.09	32° 49' 42.380 N	103° 47' 2.020 W	
700.0	0.00	0.00	700.0	0.0	0.0	665,535.91	668,775.09	32° 49' 42.380 N	103° 47' 2.020 W	
791.0	0.00	0.00	791.0	0.0	0.0	665,535.91	668,775.09	32° 49' 42.380 N	103° 47' 2.020 W	
Rustler										
800.0	0.00	0.00	800.0	0.0	0.0	665,535.91	668,775.09	32° 49' 42.380 N	103° 47' 2.020 W	
816.0	0.00	0.00	816.0	0.0	0.0	665,535.91	668,775.09	32° 49' 42.380 N	103° 47' 2.020 W	
Surface										
900.0	0.00	0.00	900.0	0.0	0.0	665,535.91	668,775.09	32° 49' 42.380 N	103° 47' 2.020 W	
972.0	0.00	0.00	972.0	0.0	0.0	665,535.91	668,775.09	32° 49' 42.380 N	103° 47' 2.020 W	
Salado										
1,000.0	0.00	0.00	1,000.0	0.0	0.0	665,535.91	668,775.09	32° 49' 42.380 N	103° 47' 2.020 W	
1,100.0	0.00	0.00	1,100.0	0.0	0.0	665,535.91	668,775.09	32° 49' 42.380 N	103° 47' 2.020 W	
1,200.0	0.00	0.00	1,200.0	0.0	0.0	665,535.91	668,775.09	32° 49' 42.380 N	103° 47' 2.020 W	
1,300.0	0.00	0.00	1,300.0	0.0	0.0	665,535.91	668,775.09	32° 49' 42.380 N	103° 47' 2.020 W	
1,400.0	0.00	0.00	1,400.0	0.0	0.0	665,535.91	668,775.09	32° 49' 42.380 N	103° 47' 2.020 W	
1,500.0	0.00	0.00	1,500.0	0.0	0.0	665,535.91	668,775.09	32° 49' 42.380 N	103° 47' 2.020 W	
1,600.0	0.00	0.00	1,600.0	0.0	0.0	665,535.91	668,775.09	32° 49' 42.380 N	103° 47' 2.020 W	
1,700.0	0.00	0.00	1,700.0	0.0	0.0	665,535.91	668,775.09	32° 49' 42.380 N	103° 47' 2.020 W	
1,800.0	0.00	0.00	1,800.0	0.0	0.0	665,535.91	668,775.09	32° 49' 42.380 N	103° 47' 2.020 W	
1,900.0	0.00	0.00	1,900.0	0.0	0.0	665,535.91	668,775.09	32° 49' 42.380 N	103° 47' 2.020 W	
1,980.0	0.00	0.00	1,980.0	0.0	0.0	665,535.91	668,775.09	32° 49' 42.380 N	103° 47' 2.020 W	
Tansill										
2,000.0	0.00	0.00	2,000.0	0.0	0.0	665,535.91	668,775.09	32° 49' 42.380 N	103° 47' 2.020 W	
2,100.0	0.00	0.00	2,100.0	0.0	0.0	665,535.91	668,775.09	32° 49' 42.380 N	103° 47' 2.020 W	
2,116.0	0.00	0.00	2,116.0	0.0	0.0	665,535.91	668,775.09	32° 49' 42.380 N	103° 47' 2.020 W	
Yates										
2,200.0	1.26	103.57	2,200.0	-0.2	0.9	665,535.69	668,775.98	32° 49' 42.378 N	103° 47' 2.009 W	
2,300.0	2.76	103.57	2,299.9	-1.0	4.3	665,534.87	668,779.39	32° 49' 42.370 N	103° 47' 1.970 W	
2,400.0	4.26	103.57	2,399.7	-2.5	10.3	665,533.44	668,785.34	32° 49' 42.355 N	103° 47' 1.900 W	
2,425.6	4.64	103.57	2,425.2	-2.9	12.2	665,532.97	668,787.27	32° 49' 42.350 N	103° 47' 1.877 W	
2,451.4	4.64	103.57	2,451.0	-3.4	14.2	665,532.48	668,789.31	32° 49' 42.345 N	103° 47' 1.854 W	
Seven Rivers										
2,500.0	4.64	103.57	2,499.4	-4.4	18.0	665,531.56	668,793.13	32° 49' 42.336 N	103° 47' 1.809 W	
2,600.0	4.64	103.57	2,599.1	-6.3	25.9	665,529.66	668,801.00	32° 49' 42.317 N	103° 47' 1.717 W	
2,700.0	4.64	103.57	2,698.8	-8.2	33.8	665,527.76	668,808.87	32° 49' 42.298 N	103° 47' 1.625 W	
2,800.0	4.64	103.57	2,798.4	-10.1	41.7	665,525.86	668,816.74	32° 49' 42.278 N	103° 47' 1.532 W	
2,900.0	4.64	103.57	2,898.1	-12.0	49.5	665,523.96	668,824.61	32° 49' 42.259 N	103° 47' 1.440 W	
3,000.0	4.64	103.57	2,997.8	-13.9	57.4	665,522.06	668,832.48	32° 49' 42.240 N	103° 47' 1.348 W	
3,084.5	4.64	103.57	3,082.0	-15.5	64.0	665,520.45	668,839.13	32° 49' 42.224 N	103° 47' 1.270 W	
Queen										
3,100.0	4.64	103.57	3,097.4	-15.8	65.3	665,520.16	668,840.35	32° 49' 42.221 N	103° 47' 1.256 W	
3,200.0	4.64	103.57	3,197.1	-17.7	73.1	665,518.26	668,848.22	32° 49' 42.202 N	103° 47' 1.164 W	
3,300.0	4.64	103.57	3,296.8	-19.6	81.0	665,516.36	668,856.09	32° 49' 42.182 N	103° 47' 1.072 W	
3,400.0	4.64	103.57	3,396.5	-21.5	88.9	665,514.46	668,863.96	32° 49' 42.163 N	103° 47' 0.980 W	

ConocoPhillips

Planning Report - Geographic

Database:	EDM Central Planning	Local Co-ordinate Reference:	Well Emerald Federal 9
Company:	ConocoPhillips MCBU	TVD Reference:	RKB @ 4045.0usft (PD 822)
Project:	Buckeye	MD Reference:	RKB @ 4045.0usft (PD 822)
Site:	Emerald Federal	North Reference:	Grid
Well:	Emerald Federal 9	Survey Calculation Method:	Minimum Curvature
Wellbore:	Original Hole		
Design:	Actual Plan		

Planned Survey										
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Map Northing (usft)	Map Easting (usft)	Latitude	Longitude	
3,496.9	4.64	103.57	3,493.0	-23.3	96.5	665,512.62	668,871.58	32° 49' 42.145 N	103° 47' 0.891 W	
Grayburg										
3,500.0	4.64	103.57	3,496.1	-23.4	96.7	665,512.56	668,871.83	32° 49' 42.144 N	103° 47' 0.888 W	
3,600.0	4.64	103.57	3,595.8	-25.2	104.6	665,510.66	668,879.70	32° 49' 42.125 N	103° 47' 0.796 W	
3,700.0	4.64	103.57	3,695.5	-27.1	112.5	665,508.76	668,887.57	32° 49' 42.106 N	103° 47' 0.703 W	
3,800.0	4.64	103.57	3,795.1	-29.0	120.4	665,506.86	668,895.44	32° 49' 42.086 N	103° 47' 0.611 W	
3,880.1	4.64	103.57	3,875.0	-30.6	126.7	665,505.34	668,901.74	32° 49' 42.071 N	103° 47' 0.538 W	
San Andres										
3,900.0	4.64	103.57	3,894.8	-30.9	128.2	665,504.96	668,903.31	32° 49' 42.067 N	103° 47' 0.519 W	
4,000.0	4.64	103.57	3,994.5	-32.8	136.1	665,503.07	668,911.18	32° 49' 42.048 N	103° 47' 0.427 W	
4,100.0	4.64	103.57	4,094.2	-34.7	144.0	665,501.17	668,919.05	32° 49' 42.029 N	103° 47' 0.335 W	
4,200.0	4.64	103.57	4,193.8	-36.6	151.8	665,499.27	668,926.92	32° 49' 42.010 N	103° 47' 0.243 W	
4,300.0	4.64	103.57	4,293.5	-38.5	159.7	665,497.37	668,934.78	32° 49' 41.990 N	103° 47' 0.151 W	
4,400.0	4.64	103.57	4,393.2	-40.4	167.6	665,495.47	668,942.65	32° 49' 41.971 N	103° 47' 0.059 W	
4,500.0	4.64	103.57	4,492.9	-42.3	175.4	665,493.57	668,950.52	32° 49' 41.952 N	103° 46' 59.967 W	
4,600.0	4.64	103.57	4,592.5	-44.2	183.3	665,491.67	668,958.39	32° 49' 41.933 N	103° 46' 59.874 W	
4,700.0	4.64	103.57	4,692.2	-46.1	191.2	665,489.77	668,966.26	32° 49' 41.914 N	103° 46' 59.782 W	
4,800.0	4.64	103.57	4,791.9	-48.0	199.1	665,487.87	668,974.13	32° 49' 41.894 N	103° 46' 59.690 W	
4,900.0	4.64	103.57	4,891.5	-49.9	206.9	665,485.97	668,982.00	32° 49' 41.875 N	103° 46' 59.598 W	
5,000.0	4.64	103.57	4,991.2	-51.8	214.8	665,484.07	668,989.87	32° 49' 41.856 N	103° 46' 59.506 W	
5,100.0	4.64	103.57	5,090.9	-53.7	222.7	665,482.17	668,997.74	32° 49' 41.837 N	103° 46' 59.414 W	
5,200.0	4.64	103.57	5,190.6	-55.6	230.5	665,480.27	669,005.61	32° 49' 41.818 N	103° 46' 59.322 W	
5,300.0	4.64	103.57	5,290.2	-57.5	238.4	665,478.37	669,013.48	32° 49' 41.798 N	103° 46' 59.230 W	
5,374.0	4.64	103.57	5,364.0	-58.9	244.2	665,476.97	669,019.31	32° 49' 41.784 N	103° 46' 59.162 W	
Glorieta										
5,400.0	4.64	103.57	5,389.9	-59.4	246.3	665,476.47	669,021.35	32° 49' 41.779 N	103° 46' 59.138 W	
5,448.3	4.64	103.57	5,438.0	-60.4	250.1	665,475.56	669,025.15	32° 49' 41.770 N	103° 46' 59.093 W	
Paddock										
5,500.0	4.64	103.57	5,489.6	-61.3	254.1	665,474.57	669,029.22	32° 49' 41.760 N	103° 46' 59.045 W	
5,600.0	4.64	103.57	5,589.2	-63.2	262.0	665,472.68	669,037.09	32° 49' 41.741 N	103° 46' 58.953 W	
5,700.0	4.64	103.57	5,688.9	-65.1	269.9	665,470.78	669,044.96	32° 49' 41.722 N	103° 46' 58.861 W	
5,791.4	4.64	103.57	5,780.0	-66.9	277.1	665,469.04	669,052.15	32° 49' 41.704 N	103° 46' 58.777 W	
Blinebry										
5,800.0	4.64	103.57	5,788.6	-67.0	277.8	665,468.86	669,052.83	32° 49' 41.702 N	103° 46' 58.769 W	
5,900.0	4.64	103.57	5,888.3	-68.9	285.6	665,466.98	669,060.70	32° 49' 41.683 N	103° 46' 58.677 W	
6,000.0	4.64	103.57	5,987.9	-70.8	293.5	665,465.08	669,068.57	32° 49' 41.664 N	103° 46' 58.585 W	
6,100.0	4.64	103.57	6,087.6	-72.7	301.4	665,463.18	669,076.44	32° 49' 41.645 N	103° 46' 58.493 W	
6,200.0	4.64	103.57	6,187.3	-74.6	309.2	665,461.28	669,084.31	32° 49' 41.626 N	103° 46' 58.401 W	
6,300.0	4.64	103.57	6,286.9	-76.5	317.1	665,459.38	669,092.18	32° 49' 41.606 N	103° 46' 58.309 W	
6,400.0	4.64	103.57	6,386.6	-78.4	325.0	665,457.48	669,100.05	32° 49' 41.587 N	103° 46' 58.217 W	
6,500.0	4.64	103.57	6,486.3	-80.3	332.9	665,455.58	669,107.92	32° 49' 41.568 N	103° 46' 58.124 W	
6,600.0	4.64	103.57	6,586.0	-82.2	340.7	665,453.68	669,115.79	32° 49' 41.549 N	103° 46' 58.032 W	
6,700.0	4.64	103.57	6,685.6	-84.1	348.6	665,451.78	669,123.66	32° 49' 41.530 N	103° 46' 57.940 W	
6,800.0	4.64	103.57	6,785.3	-86.0	356.5	665,449.88	669,131.53	32° 49' 41.510 N	103° 46' 57.848 W	
6,840.8	4.64	103.57	6,826.0	-86.8	359.7	665,449.11	669,134.74	32° 49' 41.503 N	103° 46' 57.810 W	
Tubb										
6,900.0	4.64	103.57	6,885.0	-87.9	364.3	665,447.98	669,139.40	32° 49' 41.491 N	103° 46' 57.756 W	
7,000.0	4.64	103.57	6,984.6	-89.8	372.2	665,446.08	669,147.27	32° 49' 41.472 N	103° 46' 57.664 W	
7,034.0	4.64	103.57	7,018.5	-90.5	374.9	665,445.44	669,149.94	32° 49' 41.465 N	103° 46' 57.633 W	
Production										
7,041.5	4.64	103.57	7,026.0	-90.6	375.5	665,445.30	669,150.53	32° 49' 41.464 N	103° 46' 57.626 W	
TD										

ConocoPhillips

Planning Report - Geographic

Database:	EDM Central Planning	Local Co-ordinate Reference:	Well Emerald Federal 9
Company:	ConocoPhillips MCBU	TVD Reference:	RKB @ 4045.0usft (PD 822)
Project:	Buckeye	MD Reference:	RKB @ 4045.0usft (PD 822)
Site:	Emerald Federal	North Reference:	Grid
Well:	Emerald Federal 9	Survey Calculation Method:	Minimum Curvature
Wellbore:	Original Hole		
Design:	Actual Plan		

Design Targets

Target Name	- hit/miss target	Shape	Dip Angle (°)	Dip Dir. (°)	TVD (usft)	+N/-S (usft)	+E/-W (usft)	Northing (usft)	Easting (usft)	Latitude	Longitude
Emerald Federal 9 (Top			0.00	0.01	5,438.0	-126.5	355.7	665,409.41	669,130.72	32° 49' 41.110 N	103° 46' 57.860 W
- plan misses target center by 124.2usft at 5457.8usft MD (5447.5 TVD, -60.5 N, 250.8 E)											
- Circle (radius 150.0)											

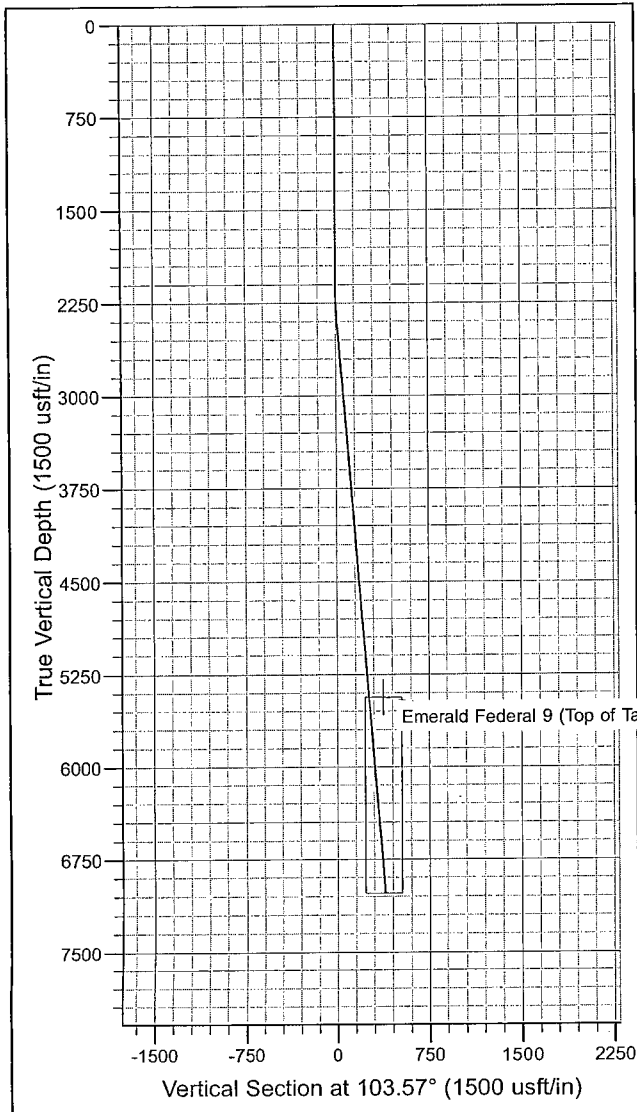
Casing Points

Measured Depth (usft)	Vertical Depth (usft)	Name	Casing Diameter (")	Hole Diameter (")
75.0	75.0	Conductor	16	20
816.0	816.0	Surface	8-5/8	12-1/4
7,034.0	7,018.5	Production	5-1/2	7-7/8

Formations

Measured Depth (usft)	Vertical Depth (usft)	Name	Lithology	Dip (°)	Dip Direction (°)
791.0	791.0	Rustler		0.00	
972.0	972.0	Salado		0.00	
1,980.0	1,980.0	Tansill		0.00	
2,116.0	2,116.0	Yates		0.00	
2,451.4	2,451.0	Seven Rivers		0.00	
3,084.5	3,082.0	Queen		0.00	
3,496.9	3,493.0	Grayburg		0.00	
3,880.1	3,875.0	San Andres		0.00	
5,374.0	5,364.0	Glorieta		0.00	
5,448.3	5,438.0	Paddock		0.00	
5,791.4	5,780.0	Blinebry		0.00	
6,840.8	6,826.0	Tubb		0.00	
7,041.5	7,026.0	TD		0.00	

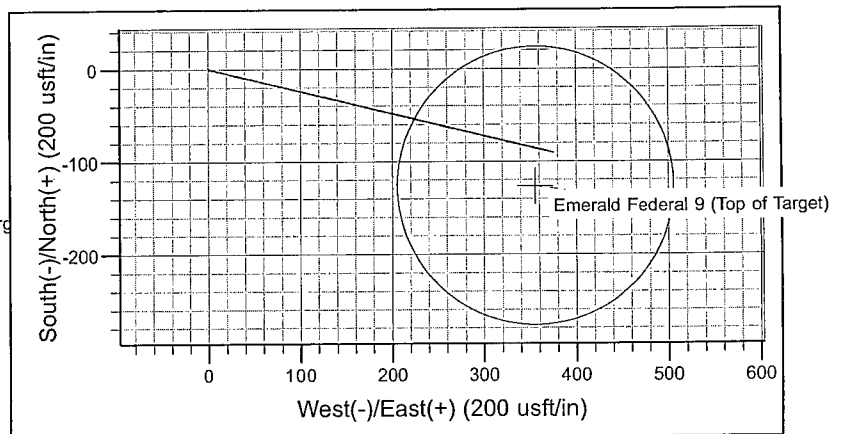
Proposed Directional Well Plan



Project: Buckeye
 Site: Emerald Federal
 Well: Emerald Federal 9
 Wellbore: Original Hole
 Design: Actual Plan

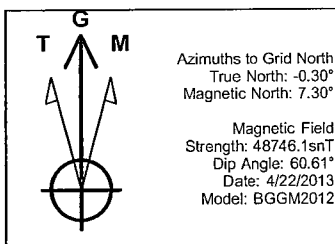
WELL DETAILS: Emerald Federal 9					
Ground Level: 4032.0					
+N/-S	+E/-W	Northing	Easting	Latitude	Longitude
0.0	0.0	665535.91	668775.08	32° 49' 42.380 N	103° 47' 2.020 W

SECTION DETAILS										
Sec	MD	Inc	Azi	TVD	+N/-S	+E/-W	Dleg	TFace	Vsect	Target
1	0.0	0.00	0.00	0.0	0.0	0.0	0.00	0.00	0.0	
2	2116.0	0.00	0.00	2116.0	0.0	0.0	0.00	0.00	0.0	
3	32425.6	4.64	103.57	2425.2	-2.9	12.2	1.50	103.57	12.5	
4	45448.3	4.64	103.57	5438.0	-60.4	250.1	0.00	0.00	257.3	Emerald Federal 9 (Top of Target)
5	7041.5	4.64	103.57	7026.0	-90.6	375.5	0.00	0.00	386.2	



CASING DETAILS				
TVD	MD	Name	Size	
75.0	75.0	Conductor	16	
816.0	816.0	Surface	8-5/8	
7018.57	7034.0	Production	5-1/2	

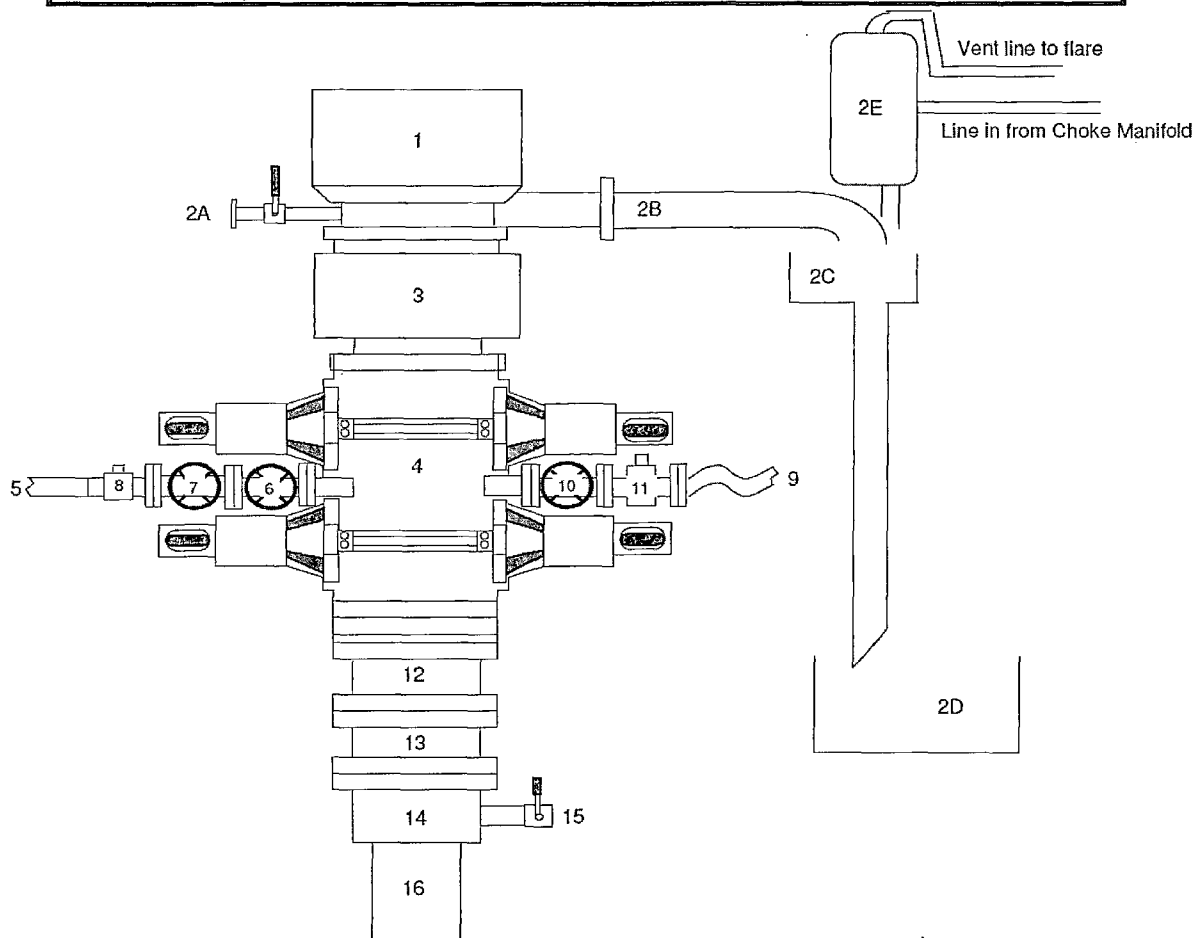
FORMATION TOP DETAILS		
TVDPath	MDPath	Formation
791.0	791.0	Rustler
972.0	972.0	Salado
1980.0	1980.0	Tansill
2116.0	2116.0	Yates
2451.0	2451.4	Seven Rivers
3082.0	3084.5	Queen
3493.0	3496.9	Grayburg
3875.0	3880.1	San Andres
5364.0	5374.0	Glorieta
5438.0	5448.3	Paddock
5780.0	5791.4	Blinberry
6826.0	6840.8	Tubb
7026.0	7041.5	TD



Attachment # 1

BLOWOUT PREVENTER ARRANGEMENT

3M System per Onshore Oil and Gas Order No. 2 utilizing 3M and 5M Rated Equipment



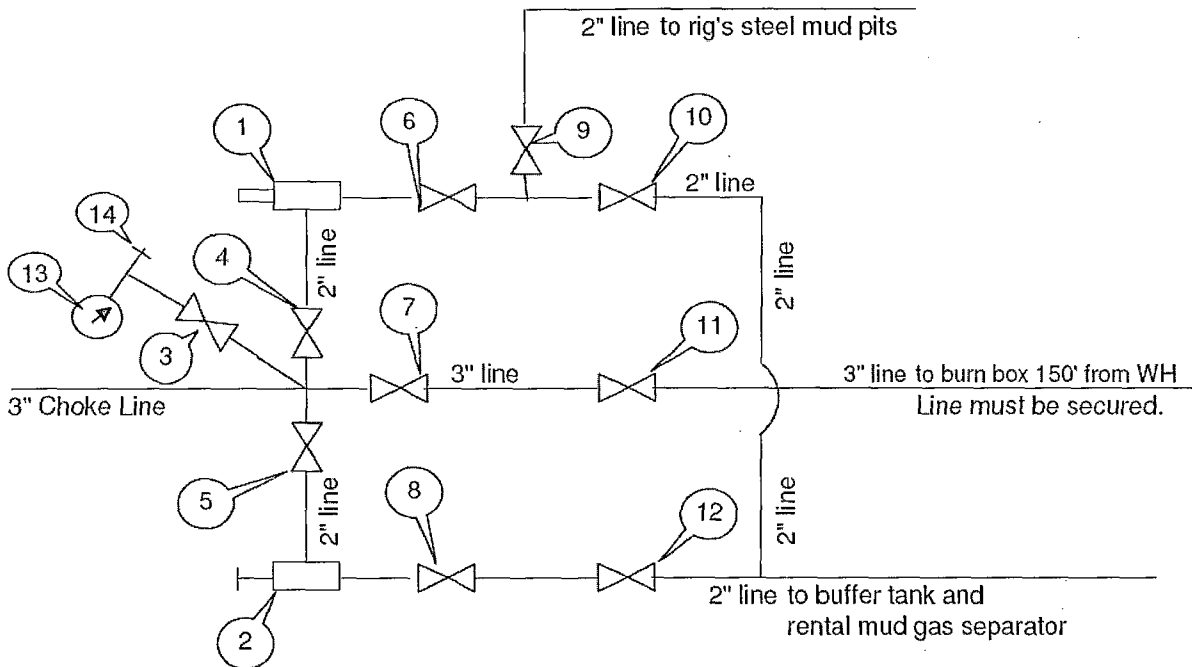
Item	Description
1	Rotating Head, 11"
2A	Fill up Line and Valve
2B	Flow Line (10")
2C	Shale Shakers and Solids Settling Tank
2D	Cuttings Bins for Zero Discharge
2E	Rental Mud Gas Separator with vent line to flare and return line to mud system
3	Annular BOP (11", 3M)
4	Double Ram (11", 3M, equipped with Blind Rams and Pipe Rams)
5	Kill Line (2" flexible hose, 3000 psi WP)
6	Kill Line Valve, Inner (3-1/8", 3000 psi WP)
7	Kill Line Valve, Outer (3-1/8", 3000 psi WP)
8	Kill Line Check Valve (2-1/16", 3000 psi WP)
9	Choke Line (5M Stainless Steel Coflex Line, 3-1/8" 3M API Type 6B, 3000 psi WP)
10	Choke Line Valve, Inner (3-1/8", 3000 psi WP)
11	Choke Line Valve, Outer, (Hydraulically operated, 3-1/8", 3000 psi WP)
12	Adapter Flange (11" 5M to 11" 3M)
13	Spacer Spool (11", 5M)
14	Casing Head (11" 5M)
15	Ball Valve and Threaded Nipple on Casing Head Outlet, 2" 5M
16	Surface Casing

Submitted by: James Chen, Drilling Engineer, Mid-Continent Business Unit, ConocoPhillips Company, 25-Sep-2012

Attachment # 2

CHOKE MANIFOLD ARRANGEMENT

3M System per Onshore Oil and Gas Order No. 2 utilizing 3M and 5M Equipment



All Tees must be targeted

Item	Description
1	Remote Controlled Hydraulically Operated Adjustable Choke, 2-1/16", 3M
2	Manual Adjustable Choke, 2-1/16", 3M
3	Gate Valve, 2-1/16" 5M
4	Gate Valve, 2-1/16" 5M
5	Gate Valve, 2-1/16" 5M
6	Gate Valve, 2-1/16" 5M
7	Gate Valve, 3-1/8" 3M
8	Gate Valve, 2-1/16" 5M
9	Gate Valve, 2-1/16" 5M
10	Gate Valve, 2-1/16" 5M
11	Gate Valve, 3-1/8" 3M
12	Gate Valve, 2-1/16" 5M
13	Pressure Gauge
14	2" hammer union tie-in point for BOP Tester

We will test each valve to 3000 psi from the upstream side.

Drawn by:

Steven O. Moore

Chief Drilling Engineer, Mid-Continent Business Unit, ConocoPhillips Company

Date: 25-Sept-2012

Request for Variance

ConocoPhillips Company

Lease Number: NM LC 060329

Well: Emerald Federal #9

Location: Sec. 17, T17S, R32E

Date: 02-24-13

Request:

ConocoPhillips Company respectfully requests a variance to install a flexible choke line instead of a straight choke line prescribed in the Onshore Order No. 2, III.A.2.b Minimum standards and enforcement provisions for choke manifold equipment. This request is made under the provision of Onshore Order No. 2, IV Variances from Minimum Standard. The rig to be used to drill this well is equipped with a flexible choke line if the requested variance is approved and determined that the proposed alternative meets the objectives of the applicable minimum standards.

Justifications:

The applicability of the flexible choke line will reduce the number of target tees required to make up from the choke valve to the choke manifold. This configuration will facilitate ease of rig up and BOPE Testing.

Attachments:

- Attachment # 1 Specification from Manufacturer
- Attachment # 2 Mill & Test Certification from Manufacturer

Contact Information:

Program prepared by:

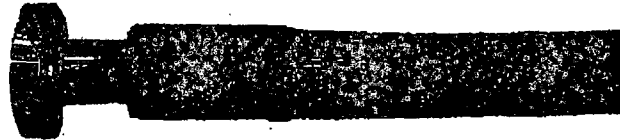
James Chen

Drilling Engineer, ConocoPhillips Company

Phone (832) 486-2184

Cell (832) 768-1647

Date: 24 February 2013



Reliance Eliminator Choke & Kill

This hose can be used as a choke hose which connects the BOP stack to the bleed-off manifold or a kill hose which connects the mud stand pipe to the BOP kill valve.

The Reliance Eliminator Choke & Kill hose contains a specially bonded compounded cover that replaces rubber covered Asbestos, Fibreglass and other fire retardant materials which are prone to damage. This high cut and gouge resistant cover overcomes costly repairs and downtime associated with older designs.

The Reliance Eliminator Choke & Kill hose has been verified by an independent engineer to meet and exceed EUB Directive 36 (700°C for 5 minutes).

Nom. ID		Nom OD		Weight		Min Bend Radius		Max WP	
in.	mm.	in.	mm.	lb/ft	kg/m	in.	mm.	psi	Mpa
3	76.2	5.11	129.79	14.5	21.46	48	1219.2	5000	34.47
3-1/2	88.9	5.79	147.06	20.14	29.80	54	1371.6	5000	34.47

Fittings

RC4X5055
RC3X5055
RC4X5575

Flanges

R35 - 3-1/8 5000# API Type 6B
R31 - 3-1/8 3000# API Type 6B

Hammer Unions

All Union Configurations

Other

LP Threaded Connection
Graylock
Custom Ends



Industrial Products USA, Ltd.

2030 E. 8th Street, Suite B • Greeley, CO 80631

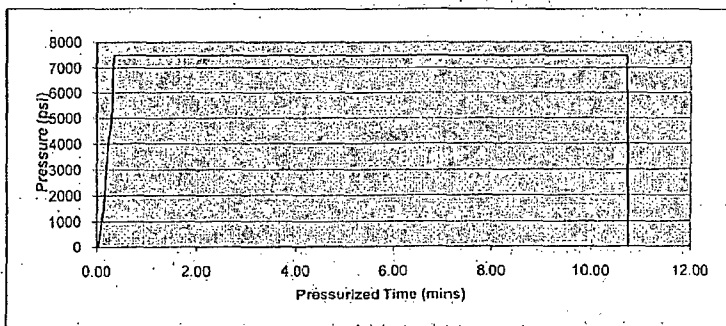
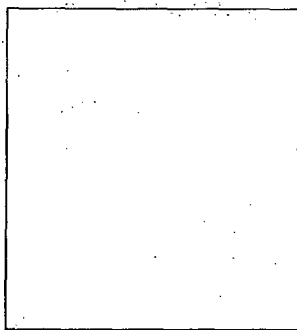
Ph: (970) 346-3751 • Fax: (970) 353-3168 • Toll Free: (866) 771-9739

TEST CERTIFICATE

Customer: PRECISION DRILLING
P.O. #: RIG 822
Invoice #: 27792
Material: 3 1/2" FIREGUARD
Description: 3 1/2" X 10'
Coupling 1: 3 1/2" FLANGE R31
" Serial:
" Quality:
Coupling 2: 3 1/2" FLOATING R31
" Serial:
" Quality:
Working Pressure: 3000
Test Pressure: 7500
Duration (mins): 10

Cert No.: 27792

Date: 9/21/2012



Conducted By: FLORES M.
Test Technician

☒ Acceptable
☐ Not Acceptable

Closed Loop System Design, Operating and Maintenance, and Closure Plan

ConocoPhillips Company

Well: Emerald Federal #9

Location: Sec. 17, T17S, R32E

Date: 02-22-13

ConocoPhillips proposes the following plan for design, operating and maintenance, and closure of our proposed closed loop system for the above named well:

1. We propose to use a closed loop system with steel pits, haul-off bins, and frac tanks for containing all cuttings, solids, mud, water, brine, and liquids. We will not dig a pit, nor will we use a drying pad, nor will we build an earth pit above ground level, nor will we dispose of or bury any waste on location.

All drilling waste and all drilling fluids (fresh water, brine, mud, cuttings, drill solids, cement returns, and any other liquid or solid that may be involved) will be contained on location in the rig's steel pits or in haul-off bins or in frac tanks as needed. The intent is as follows:

- We propose to use the rigs's steel pits for containing and maintaining the drilling fluids.
- We propose to remove cuttings and drilled solids from the mud by using solids control equipment and to contain such cuttings and drilled solids on location in haul-off bins.
- We propose that any excess water that may need to be stored on location will be stored in tanks.

The closed loop system components will be inspected daily by each tour and any needed repairs will be made immediately. Any leak in the system will be repaired immediately, and any spilled liquids and/or solids will be cleaned immediately, and the area where any such spill occurred will be remediated immediately.

2. Cuttings and solids will be removed from location in haul-off bins by an authorized contractor and disposed of at an authorized facility. For this well, we propose the following disposal facility:

Controlled Recovery Inc./ Operator: R-360 Permian Basin, LLC
4507 West Carlsbad Hwy, Hobbs, NM 88240,
P.O. Box 388; Hobbs, New Mexico 88241
Toll Free Phone: 877.505.4274, Local Phone Number: 432.638.4076

The physical address for the plant where the disposal facility is located is Highway 62/180 at mile marker 66 (33 miles West of Hobbs, NM and 32 miles East of Carlsbad, NM).

The Permit Number for R-360 is NM-1-006/R-9166

A photograph showing the type of haul-off bins that will be used is attached.

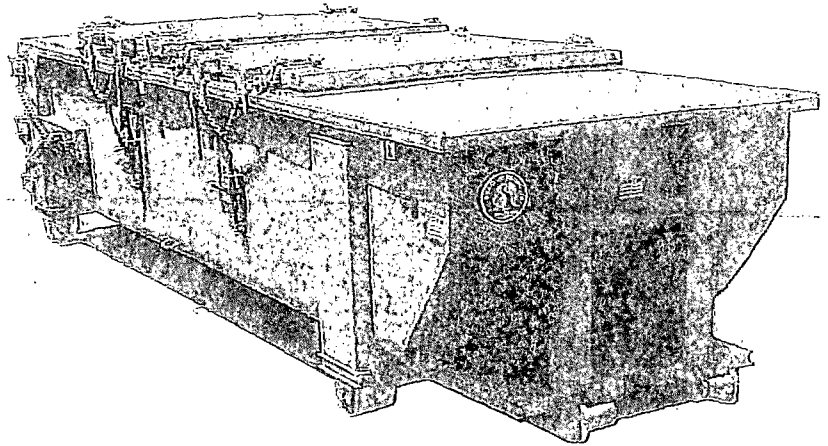
3. Mud will be transported by vacuum truck and disposed of at Controlled Recovery Inc at the facility described above.
4. Fresh Water and Brine will be hauled off by vacuum truck and disposed of at an authorized salt water disposal well. We propose the following for disposal of fresh water and brine as needed:
 - Nabors Well Services Company, 3221 NW County Rd; Hobbs, NM 88240, PO 5208 Hobbs, NM, 88241, Permit SWD 092. (Well Location: **Section 3, T19S R37E**)
 - Basic Energy Services, P.O. Box 1869; Eunice, NM 88231 Phone Number: 575.394.2545, Facility located at Hwy 18, Mile Marker 19; Eunice, NM.

James Chen
Drilling Engineer
Office: 832.486.2184
Cell: 832.678.1647

SPECIFICATIONS

Heavy Duty Split Metal Rolling Lid

FLOOR: 3/16" PL one piece
 CROSS MEMBER: 3 x 4.1 channel 16" on center
 WALLS: 3/16" PL solid welded with tubing top / inside liner hooks
 DOOR: 3/16" PL with tubing frame
 FRONT: 3/16" PL slant formed
 PICK UP: Standard cable with 2" x 6" x 1/4" rails, gusset at each crossmember
 WHEELS: 10 DIA x 9 long with grease fittings
 DOOR LATCH: 3 independent ratchet binders with chains, vertical second latch
 GASKETS: Extruded rubber seal with metal retainers
 WELDS: All welds continuous except sub-structure crossmembers
 FINISH: Coated inside and out with direct to metal, rust inhibiting acrylic enamel color coat
 HYDROTESTING: Full capacity static test
 DIMENSIONS: 22'-11" long (21'-8" inside), 99" wide (88" inside), see drawing for height
 OPTIONS: Steel grit blast and special paint, Ampliroll, Heil and Dino pickup
 ROOF: 3/16" PL roof panels with tubing and channel support frame
 LIDS: (2) 68" x 90" metal rolling lids spring loaded, self raising
 ROLLERS: 4" V-groove rollers with delrin bearings and grease fittings
 OPENING: (2) 60" x 82" openings with 8" divider centered on container
 LATCH: (2) independent ratchet binders with chains per lid
 GASKETS: Extruded rubber seal with metal retainers



CONT.	A	B
20 YD	41	53
25 YD	53	65
30 YD	65	77

