| Form 3160 5 <b>at 0<sup>CD</sup></b>  |   |  |                                |   |   |  |
|---|---|--|--------------------------------|---|---|--|
| (August 2000) - (1) 3 D   | UNITED STATES<br>EPARTMENT OF THE INT   | OCD Hobb   | s                              | FORM<br>OMB N<br>Expires:                 | APPROVED<br>O. 1004-0135<br>July 31, 2010 |  |
| SUNDRY  | ſ   | 5. Lease Serial No.<br>NMNM104685                                    |                                |   |   |  |
| Do norruse the  | nis form for proposals to dri<br>ell. Use form 3160-3 (APD)                   | ŀ  | 6. If Indian, Allottee of      | or Tribe Name                             |   |  |
| SUBMIT IN TR  | IPLICATE - Other instructio   | ns on reverse side.  |                                | 7. If Unit or CA/Agre                     | ement, Name and/or No.                    |  |
| 1. Type of Well   |   |  |                                | 8. Well Name and No.<br>TAYLOR DRAW       | 7 FED 1H                                  |  |
| 2. Name of Operator<br>DEVON ENERGY PRODUC  | Contact: TR<br>TION CO.E <b>R</b> Mail: trina.couch@d                         | INA C COUCH  |                                | 9. API Well No.<br>30-025-41146           | ~   |  |
| 3a. Address<br>DEVON ENERGY PRODUC<br>OKLAHOMA CITY, OK 7310  | TION CO.LP 333 WEST SHE   | D. Phone No. (include area code<br>RIDANS-282E-72903AHOMA            | CITY, OK 78                    | 10. Field and Pool, or<br>102.USK; BONE S | Exploratory<br>PRING                      |  |
| 4. Location of Well (Footage, Sec., 2   | T., R., M., or Survey Description)  | <u> </u>   |                                | 11. County or Parish,                     | and State                                 |  |
| Sec 7 T19S R32E 1650FSL 2   | 200FEL  |  |                                | LEA COUNTY (                              | COUNTY, NM                                |  |
| 12. CHECK APP   | ROPRIATE BOX(ES) TO IN  | NDICATE NATURE OF  | NOTICE, RE                     | PORT, OR OTHE                             | R DATA                                    |  |
| TYPE OF SUBMISSION  |   | ТҮРЕ О   | F ACTION                       |   |   |  |
| Notice of Intent  |   | Deepen   | Productio                      | on (Start/Resume)                         | □ Water Shut-Off                          |  |
| Subsequent Report   | Alter Casing  | Fracture Treat   | Reclamat                       | ion                                       | Well Integrity                            |  |
| Final Abandonment Notice  | Casing Repair   | Plug and Abandon   |                                | rily Abandon                              | Change to Original A                      |  |
|   | Convert to Injection  | Plug Back  | U Water Di                     | sposal                                    | PD  |  |
| belowing competed. Final A<br>determined that the site is ready for the<br>Devon Energy Production Co<br>following:   | inpanton Notices shall be filed of<br>inal inspection.)                       | ests approval to change th   | ne SHL to the                  | have been completed,                      | and the operator has                      |  |
| Current location: SHL: 1650   | FSL & 200 FEL   |  |                                |   |   |  |
| TO  |   |  |                                |   |   |  |
| Proposed location: SHL: 165<br>Surface: OK. HU  | oFSL& 260 FEL<br>approved Costs appl  | es. Indradahal 'o  | 123/B                          |   |   |  |
| Attachments:  | ,   |  |                                |   |   |  |
| Eng, Reylei   | 9/25/13-  | JAM-C  | 0795                           | upden                                     | ted.                                      |  |
| 14. I hereby certify that the foregoing is  | s true and correct.<br>Electronic Submission #2202<br>For DEVON ENERGY        | 241 verified by the BLM We<br>PRODUCTION CO.LP, sen                  | II Information St to the Hobbs | System                                    |   |  |
| Name(Printed/Typed) TRINA C   | COUCH   | Title REGUL  | ATORY ASS                      | DCIATE                                    |   |  |
| Signature (Electronic Submission) Date 09/16/2013   |   |  |                                |   |   |  |
|   | THIS SPACE FOR  | FEDERAL OR STATE   | OFFICE US                      | E   |   |  |
| _Approved By // COdy L  | ayton   | Title_NR   | S                              |   | Date 10/23/13                             |  |
| Conditions of approval, if any, are altached. Approval of this notice does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon. |   |  |                                |   |   |  |
| Title 18 U.S.C. Section 1001 and Title 43<br>States any false, fictitious or fraudulent   | U.S.C. Section 1212, make it a crim<br>statements or representations as to an | e for any person knowingly and<br>ny matter within its jurisdiction. | willfully to make              | e to any department or a                  | agency of the United                      |  |
| ** OPERAT   | TOR-SUBMITTED ** OPEI   | RATOR-SUBMITTED *  | * OPERATO                      | R-SUBMITTED                               | **  |  |
|   |   |  | 001                            | 2.9 2013                                  | Ph P                                      |  |
|   | 1   |  | -                              |   | $(n; L) \perp$                            |  |

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# Additional data for EC transaction #220241 that would not fit on the form

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#### 32. Additional remarks, continued

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Drilling Plan Directional Survey C-102

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District.1 1625 N. French Dr., Hobbs, NM \$8240 Phone: (575) 393-6161 Fax: (575) 393-0720 District II 811 S. First St., Artesia, NM 38210 Phone: (575) 748-1283 Fax: (575) 748-9720 District.III 1000 Rio Brazos Road, Aztec, NM \$7410 Phone: (305) 334-6178 Fax: (505) 334-6170 District.IV 1220 S. St. Francis Dr., Santa Fe, NM \$7505 Phone: (505) 476-3460 Fax: (505) 476-3462

# State of New Mexico Energy, Minerals & Natural Resources Department OIL CONSERVATION DIVISION 1220 South St. Francis Dr. Santa Fe, NM 87505

Form C-102 Revised August 1, 2011 Submit one copy to appropriate District Office

AMENDED REPORT

## WELL LOCATION AND ACREAGE DEDICATION PLAT

| 1.                            | API Numbe                | r                       |                                | <sup>2</sup> Pool Code | 2                 | <sup>3</sup> Pool Name |               |          |         |            |  |
|-------------------------------|--------------------------|-------------------------|--------------------------------|------------------------|-------------------|------------------------|---------------|----------|---------|------------|--|
| <sup>4</sup> Property (       | Code                     |                         |                                |                        | <sup>3</sup> Proj | perty Name             |               | T        | 4 W     | ell Number |  |
|                               |                          |                         |                                | TA                     | YLOR DR           | AW 7 FEDERAL           |               |          |         | 1H         |  |
| <sup>7</sup> OGRID            | No.                      |                         |                                |                        | <sup>8</sup> Ope  | rator Name             |               |          | 9       | Elevation  |  |
| 6137                          | [                        |                         | DEV                            | ON ENEF                | RGY PRO           | DUCTION COMPA          | NY, L.P.      |          | 3       | 3618.2     |  |
|                               |                          |                         |                                |                        | " Surfa           | ice Location           |               |          |         |            |  |
| UL or lot no.                 | Section                  | Township                | Range                          | Lot Idn                | Fect from t       | he North/South line    | Feet from the | East/Wes | st line | County     |  |
| I                             | 7                        | 19 S                    | 32 E                           |                        | 1650              | SOUTH                  | 260           | EAS      | T       | LEA        |  |
|                               |                          | ·                       | " Bo                           | ttoin Hol              | le Locatio        | on If Different From   | n Surface     |          |         |            |  |
| UL or lot no.                 | Section                  | Township                | Range                          | Lot Ida                | Feet from t       | he North/South line    | Feet from the | East/Wes | at line | County     |  |
| 3                             | 7                        | 19 S                    | S 32 E 1980 SOUTH 330 WEST LEA |                        |                   |                        |               |          |         | LEA        |  |
| <sup>12</sup> Dedicated Acres | s <sup>13</sup> Joint of | rin ûli <sup>lu</sup> C | onsolidation                   | Code <sup>13</sup> Or  | der No.           |                        |               |          |         |            |  |

No allowable will be assigned to this completion until all interests have been consolidated or a non-standard unit has been approved by the division.

| ND0'24'49"W                       | N89'53'16"E<br>NW CORNER SEC. 7<br>LAT. = 32.6822969'N<br>LONG. = 103.8143075'W<br>NMSP EAST (FT)<br>N = 612341.34<br>E = 701027.38   | 2673.43 FT<br>N O CORNER SEC. 7<br>LAT. = 32[6822750'N<br>LONG. = 103.8056206'W<br>NMSP EAST (FT)<br>N = 612346.57<br>E = 703700.19  | N89'49'41"E 2643.33 FT<br>NE CORNER SEC. 7<br>LAT. = 32.6822604'N<br>LONG. = 103.7970314'W<br>NMSP EAST (FT)<br>N = 612354.50<br>E = 706342.90<br>N<br>T   | <sup>17</sup> OPERATOR CERTIFICATION<br>I hereby certify that the information contained herein is true and complete<br>to the best of my knowledge and belief, and that this organization either<br>owns a working interest or unleased mineral interest in the land including<br>the proposed bottom hole location or has a right to drill this well at this<br>location pursuant to a contract with an owner of such a mineral or working<br>interest, or to a voluntary pooling agreement or a compulsory pooling<br>order heretofore entered by the division. |
|-----------------------------------|---|--|--|---|
| 2642.09 FT NO0'24'52"W 2640.30 FT | LOT 2<br>W O CORNER SEC. 7<br>LAT. = 32.6750365'N<br>LONG. = 103.8142876'W<br>NMSP EAST (FT)<br>N = 609699.93<br>E = 701046.45<br>LOT J<br>ABOTTOM<br>OF HOLE<br>BO<br>LAT. = 32.667781<br>LONG. = 103.81422<br>NMSP EAST (FT)<br>N = 607060.31<br>E = 701065.55<br>S89'52'32'W | <i>TAYLOR DRAW</i> "7" <i>I</i><br><i>TAYLOR DRAW</i> "7" <i>I</i><br>ELEV. =, 3618.2'<br>LAT. = 32.6722731'N<br>LONG. = 103.797857.<br>NMSP EAST (FT)<br>N = 608719.71<br>E = 706107.12<br><i>TTOM OF HOLE</i>  <br>= 32.6732196'N<br>C. = 103.8132103'W<br>SP EAST (FT)  <br>609040.54<br>701381.15<br>7 S Q CORNER SEC. 7<br>O'N LAT. = 32.6677607'N<br>S75'W LONG. = 103.8055900'W<br>NMSP EAST (FT)<br>N = 607066.11<br>E = 703735.87<br>2670.94 FT | E O CORNER SEC. 7<br>LAT. = 32.6749969 N<br>LONG. = 103.7970173 W<br>FEDERAL #1H N = 609711.95<br>(NAD83)   E = 706360.59<br>(NAD83)   260'<br>  370'<br>  3 | Signature       Date         Printed Name       E-mail Address         I*SURVEYOR CERTIFICATION       I hereby certify that the well-location shown on this plat was plated from India Indus of actual surveys made by the or under Mrs. supervision, and that the same is the and correct to the bear of my belief.         SEPTEMBER 4.20192797       Date of Sprvey         Signature and Seal of Protestional surveys.       Certificate Number:         Fill NON E JARAMILLO, PLS 12797       SURVEY NO. 1382A   |









### Taylor Draw 7 Fed 1H – APD DRILLING PLAN

KKS 1-07-2013

KKS 4-16-13 revised intermediate casing depth to 4,525', casing design factors & cement volume

AAA 9-13-13 revised plat for surface change; request new directional well plans and updated depths; replace 5-1/2" LTC with 5-1/2" BTC; updated casing design factors & cement volumes

Casing Program

Zel (.)

| 6A | <u>Hole</u><br><u>Size</u> | <u>Hole</u><br>Interval<br>960' | <u>OD Csg</u>  | <u>Casing</u><br>Interval | <u>Weight</u> | <u>Collar</u> | <u>Grade</u> |
|----|----------------------------|---------------------------------|----------------|---------------------------|---------------|---------------|--------------|
|    | 17-1/2"                    | 0-1,925                         | 13-3/8"        | 0-1,025                   | 48#           | STC           | H-40         |
|    | 12-1/4"                    | 1,025 - 4,525                   | <b>9-</b> 5/8" | 0-4,525                   | 40#           | LTC           | HCK-55       |
|    | 8-3/4"                     | 4,525 - 13,944                  | 5-1/2"         | 0-13,944                  | 17#           | BTC           | HCP-110      |

Note: only new casing will be utilized

MAXIMUM TVD in lateral: 9315'

Design Factors:

| <u>Casing Size</u>       | Collapse Design Factor | Burst Design Factor | <u>Tension Design Factor</u> |
|--------------------------|------------------------|---------------------|------------------------------|
| 13-3/8", 48#, H-40, ST&C | 1.61                   | 3.61                | 6.54                         |
| 9-5/8", 40#, HCK-55 LT&C | 1.80                   | 1.68                | 3.48                         |
| 5-1/2" 17# HCP-110 BTC   | 1.69                   | 2.41                | 6.34                         |

Mud Program:

SU

| (DA  | Depth 960      | Mud Wt.   | Visc.   | Fluid Loss | Type System |  |
|------|----------------|-----------|---------|------------|-------------|--|
| ( DN | 0-1,025        | 8.4 - 9.0 | 30 - 34 | N/C        | FW          |  |
|      | 1,025 - 4,525  | 9.8-10.0  | 28-32   | N/C        | Brine       |  |
|      | 4,525 - 14,711 | 8.6-9.0   | 28-32   | N/C-12     | FW          |  |

Pressure Control Equipment:

The BOP system used to drill the intermediate hole will consist of a 13-5/8" Double Ram and Annular preventer. The BOP system will be tested as per BLM Onshore Oil and Gas Order No. 2, a 3M system will be installed and tested prior to drilling out the surface casing shoe.

The BOP system used to drill the production hole will consist of a 13-5/8" Double Ram and Annular preventer. The BOP system will be tested as per BLM Onshore Oil and Gas Order No. 2 a 3M system will be installed prior to drilling out the intermediate casing shoe.

The pipe rams will be operated and checked each 24 hour period and each time the drill pipe is out of the hole. These tests will be logged in the daily driller's log. A 2" kill line and 3" choke line will be incorporated into the drilling spool below the ram BOP. In addition to the rams and annular preventer, additional BOP accessories include a kelly cock, floor safety valve, choke lines, and choke manifold rated at 3,000 psi WP.

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PLP

Devon requests a variance to use a flexible line with flanged ends between the BOP and the choke manifold (choke line); if an H&P rig drills this well. Otherwise no flex line is needed. The line will be kept as straight as possible with minimal turns.

# Cementing Program (cement volumes based on at least 100 % excess on Surface, 50% excess on Intermediate 25% excess on Production)

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| 13-3/8" Surface     | Lead: 500 sacks Class C Cement + 2% bwoc Calcium Chloride + 0.125 lbs/sack Poly-E-Flake + 4% bwoc Bentonite + 70.1% Fresh Water, 13.5 ppg  |
|---------------------|--|
|                     | Yield: 1.75 cf/sk  |
|                     | TOC @ surface  |
|                     | Tail: 515 sacks Class C Cement + 2% bwoc Calcium Chloride + 0.125 lbs/sack Poly-E-Flake + 63.1% Fresh Water, 14.8 ppg  |
|                     | Yield: 1.35 cf/sk  |
| 9-5/8" Intermediate | Lead: 900 sacks (65:35) Class C Cement:Poz (Fly Ash): + 5% bwow Sodium Chloride + 0.125<br>lbs/sack Poly-E-Flake + 6% bwoc Bentonite + 70.9% Fresh Water, 12.9 ppg                                 |
|                     | Yield: 1.85 cf/sk  |
|                     | TOC @ surface  |
|                     | 1000 ft.Tail: 360 sacks Class C Cement + 0.125 lbs/sack Poly-E-Flake + 63.5% Water, 14.8 ppg   |
|                     | Yield: 1.33 cf/sk  |
| 5-1/2" Production   | Lead<br>Lead: 446 sacks Tuned Lite Class C Cement: HR-601 + 13.54 Gal/sk Fresh Water, 10.2 ppg   |
|                     | Yield: 2.91 cf/sk  |
|                     | Tail: 1484 sacks (50:50) Class H Cement:Poz (Fly Ash) + 1 lb/sk Sodium Chloride + 0.5% bwoc<br>HALAD-344 + 0.4% bwoc CFR-3 + 0.1% bwoc HR-601 + 2% bwoc Bentonite + 58.8% Fresh<br>Water, 14.5 ppg |
|                     | Yield: 1.22 cf/sk  |
|                     |  |
|                     |  |

TOC @ 4025 ft

#### ACTUAL CEMENT VOLUMES WILL BE ADJUSTED BASED ON FLUID CALIPER AND CALIPER LOG DATA.

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# Devon Energy, Inc.

Lea County (NAD83) Taylor Draw 7 Fed #1H

ОН

Plan: Plan 2

# **Standard Planning Report**

12 September, 2013



# Pathfinder - A Schlumberger Company

Planning Report

| r  |  |   |   |  |   |   | and a state of the second s |  |   |  |
|--|--|---|---|--|---|---|---|--|---|--|
| Database:  | 1 EDM 50   | 000.1 Single U  | Iser Db   |  | Local Co  | ordinate Refer  | ence:   | Well #1H   |   |  |
| Company:   | Devon l  | Energy Inc.   |   |  |   | rence:  |   | Est RKB = 20!  | @ 3636 80usff   |  |
| Project:   | Lea Co   | unty (NAD83)  |   | · · · ·  | MD Refer  | once:   |   | Est RKB = 20'  | @ 3636 8006   |  |
| Site   | Tavlor D   | )raw 7 Fed  |   |  | North Po  | foronço:  | See (18) See 14<br>an troinne See   | Grid   | @ 0000.000.3ii  |  |
| Wall   |  | 9777777   |   |  | Suping  |   |   | Minimum Cun  | atura   |  |
| VVUII.   | #10<br>OU  |   |   |  | Suivey C  | aiculation-meti   | ioa:  | winnmann.curv  | ature   | 4  |
| wellbore:  |  |   |   |  |   | a la francés  |   |  |   | · · · · ·  |
| Design:  | Plan 2   | 60m   |   |  | ×   |   |   |  |   | an and the second of the secon |
| Broingt  |  |   | ela di de anaplacama  | a rational marca lear  | م معديد محمد  | 4 · · · · · · · · · · · · · · · · · · ·   |   |  | وأسون إساحه أحراجها   |  |
| FIOIBEL  | Lea Cou  |   |   |  | <u></u>   |   |   |  |   | <u></u>  |
| Map System:  | US State   | Plane 1983  |   |  | System Da   | tum:  | M   | ean Sea Level  |   |  |
| Geo Datum:   | North Ame  | erican Datum '  | 1983  |  | -   |   |   |  |   |  |
| Map Zone:  | New Mexi   | co Eastern Zo   | ne  |  |   |   |   |  |   |  |
|  |  |   |   |  |   |   |   | • · · ·  |   |  |
| Site   | Taylor Di  | raw 7 Fed   |   | nii aaniinaana a adda  |   | · · · · · · · · · · · · · · · · · · ·   | ne na tiyar inte an ya naar   |  | ه پېرىمىد قىرىدى د بار س  | na an ananana na marina an a   |
| 0.11. D. 11.   |  | 1.2   | North   |  | 609   | 710 71 usft   |   |  |   |  |
| Site Position:   |  |   | North   | iing:  | 000   | ,/ 19./ 1 USIL  | Latitude:   |  |   | 32° 40' 20.183 N   |
| From:  | мар  |   | Easti   | ng:  | 706   | 5,107.12 <b>us</b> π  | Longitude:  |  |   | 103° 47' 52.286 W  |
| Position Uncer   | tainty:  | 0.00  | ) usft Slot F   | Radius:  |   | 13-3/16 "   | Grid Converg  | jence:   |   | 0.29 °   |
| Well   | · #1H  | e an san he .   |   | <u></u>  |   |   |   | · · · ·  | · · · · · · · · · · · · · · · · · · ·   | 1000 1100 10 11 10 10 10 10  |
|  |  |   |   | <u> </u>   |   | 000 740 74  |   |  | <u></u>   | <u></u>  |
| Well Position  | +N/-S  | 0.0   |   | ortning:   |   | 608,719,71  | usπ Lat   | itude:   |   | 32° 40' 20,183 N   |
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| Wellbore<br>Magnetics  | 이번<br>Mod  | el Name   | Sampl   | e Date   | Declina<br>(°)  | ítlon   | Dip 4   | vngle<br>')  | Field:  | Strength<br>nit):  |
| Wellbore<br>Magnetics  | OH<br>Mod  | el Name<br>IGRF2010   | Sampl   | le Date<br>1/3/2013  | Decilina<br>(°)   | ition<br>7.53   | Dip A<br>(1   | <b>Angle</b><br>')<br>60.52  | Field (   | Strength<br>nT):<br>48,705   |
| Wellbore<br>Magnetics<br>Design  | Mod<br>Plan 2  | el Name<br>IGRF2010   | Sampl   | le Date<br>1/3/2013  | Deçilna<br>(°)  | ition<br>7.53   | Dip 4   | ngle<br>)<br>60.52   | Field&  | Strength<br>nT)<br>48,705  |
| Wellbore<br>Magnetics<br>Design<br>Audit Notes:  | OH<br>Mod<br>Plan 2  | el Name<br>IGRF2010   | Sampl   | e Date<br>1/3/2013   | Deçilina<br>(°)   | itlón<br>7.53   | Dip⁄¢<br>(  | ngie<br>)<br>60.52   | Field:  | Strength<br>nT):<br>48,705   |
| Wellbore<br>Magnetics<br>Design<br>Audit Notes:<br>Version:  | OH<br>Mod<br>Plan 2  | el Name<br>IGRF2010   | Sampl   | le Date<br>1/3/2013<br>e: Pl   | Deçilina<br>(?)   | ition<br>7.53<br>Tie  | On Depth:   | (ngile<br>')<br>60.52  | Field:<br>(   | Strength<br>nin):<br>48,705  |
| Wellbore<br>Magnetics<br>Design<br>Audit Notes:<br>Version:<br>Vertical Section  | Plan 2   | el.Name<br>IGRF2010   | Sampi<br>Phas<br>epth From (IT)   | e Date<br>1/3/2013<br>e: Pl<br>VD)   | Declina<br>(°)<br>LAN<br>+N/-S  | itlon<br>7.53<br>Tie<br>+Er   | Dip ⁄4<br>(f  | ngjle<br>)<br>60.52<br>Di  | Fielda<br>(<br>0.00<br>rection  | Strength<br>nTp)<br>48,705   |
| Wellbore<br>Magnetics<br>Design<br>Audit Notes:<br>Version:<br>Vertical Section  | Plan 2   | el.Name<br>IGRF2010   | Sampi<br>Phas<br>epth From (IT<br>(usft)  | e Date<br>1/3/2013<br>e: Pl<br>VD)   | Declina<br>(°)<br>LAN<br>+N/-S<br>(usft)  | itlon<br>7.53<br>Tie<br>+Er<br>(us  | Dip ⁄4<br>(f  | ngile<br>)<br>60.52<br>Di  | Field<br>(<br>0.00<br>rection   | Strength<br>nit)<br>48,705   |
| Wellbore<br>Magnetics<br>Design<br>Audit Notes:<br>Version:<br>Vertical Section  | Plan 2   | el.Name<br>IGRF2010   | Sampi<br>Phas<br>Phas<br>(usit)<br>0.00   | e Date<br>1/3/2013<br>e: Pl<br>VD)   | Decilina<br>(*)<br>(*)<br>LAN<br>+N/-S<br>(usft)<br>0.00  | ition<br>7.53<br>Tie<br>*E/<br>(US<br>0.0   | Dip /4<br>(1)<br>On Depth:  | ngie<br>)<br>60.52<br>Di   | Field<br>(<br>0.00<br>rection<br>( <sup>2</sup> )<br>70.00  | Strength<br>nT):<br>48,705   |
| Wellbore<br>Magnetics<br>Design<br>Audit Notes:<br>Version:<br>Vertical Section  | Plan 2   | el:Name<br>IGRF2010   | Sampl<br>Phas<br>epth From (T)<br>(usft)<br>0.00  | le Date<br>1/3/2013<br>e: Pl<br>VD)  | Decilina<br>(°)<br>LAN<br>+N/-Ş<br>(uşft)<br>0.00   | ition<br>7.53<br>Tie<br>+E/<br>(us<br>0.0   | Dip /4<br>(1<br>On Depth:<br>(-W/<br>(-1)<br>(-1)<br>(-1)<br>(-1)<br>(-1)<br>(-1)<br>(-1)<br>(-1)               | ngle<br>)<br>60.52<br>Di   | Field:<br>(<br>0.00<br>rection<br>(?)<br>70.00  | Strength<br>nit):<br>48,705  |
| Weilbore<br>Magnetics<br>Design<br>Audit Notes:<br>Version:<br>Vertical Section<br>Plan Sections   | OH<br>Mod<br>Plan 2  | el.Name<br>IGRF2010   | Sampl<br>Phas<br>Ppth From (IT)<br>(usft)<br>0.00   | le Date<br>1/3/2013<br>e: Pl<br>VD)  | Deçilina<br>(?)<br>LAN<br>+N/-Ş<br>(usft)<br>0.00   | ition<br>7.53<br>Tie<br>+E/<br>(us<br>0.0   | On Depth:   | ngie<br>)<br>60.52<br>Di   | Field:<br>0.00<br>rection<br>(3)<br>70.00   | Strength<br>nin):<br>48,705  |
| Wellbore<br>Magnetics<br>Design<br>Audit Notes:<br>Version:<br>Vertical Section<br>Plan Sections<br>Measured   | Plan 2   | el:Name<br>IGRF2010   | Sampl<br>Phas<br>epth From (TT<br>(usft)<br>0.00<br>Vertical  | le Date<br>1/3/2013<br>e: Pl<br>VD)  | Decilina<br>(°)<br>LAN<br>+N/-Ş<br>(uşft)<br>0.00   | ition<br>7.53<br>Tie<br>+E/<br>(us<br>0.(   | On Depth:<br>(1)<br>(1)<br>(1)<br>(2)<br>(2)<br>(2)<br>(2)<br>(2)<br>(2)<br>(2)<br>(2)<br>(2)<br>(2             | ngle<br>)<br>60.52<br>Di<br>2  | Field:<br>0.00<br>rection<br>(*)<br>70.00   | Strength<br>nin):<br>48,705  |
| Wellbore<br>Magnetics<br>Design<br>Audit Notes:<br>Version:<br>Vertical Section<br>Plan Sections<br>Measured<br>Depth  | Plan 2   | el:Name<br>IGRF2010<br>De   | Sampl<br>Phas<br>spth From (T)<br>(usft)<br>0.00<br>Vertical<br>Depth   | le Date<br>1/3/2013<br>e: Pl<br>VD)<br>+N/-S   | Decilina<br>(°)<br>(AN<br>+N/-Ş<br>(uşft)<br>0.00<br>+E/-W  | ition<br>7.53<br>Tie<br>+E/<br>(us<br>0.0<br>Dogleg<br>Rate   | On Depth:<br>(1)<br>(2)<br>(2)<br>(2)<br>(2)<br>(2)<br>(2)<br>(2)<br>(2)<br>(2)<br>(2                           | ngle<br>)<br>60.52<br>Di<br>2<br>Turn<br>Rate  | Field:<br>0.00<br>rection:<br>(*)<br>70.00  | Strength<br>nin):<br>48,705  |
| Wellbore<br>Magnetics<br>Design<br>Audit Notes:<br>Version:<br>Vertical Section<br>Plan Sections<br>Measured<br>Depth<br>(usft)  | Plan 2   | el:Name<br>IGRF2010<br>"De<br>Azimuth<br>(*)  | Sampi<br>Phas<br>spth From (IT)<br>(usft)<br>0.00<br>Vertical<br>Depth<br>(usft)  | le Date<br>1/3/2013<br>e: Pl<br>VD)<br>+N/-S<br>(usft)   | Decilina<br>(°)<br>(AN<br>+N/-Ş<br>(usft)<br>0,00<br>+E/-W<br>(usft)  | ition<br>7.53<br>Tie<br>+E/<br>(us<br>0.0<br>Dogleg<br>Rate<br>(*/100usft)  | On Depth:<br>   | ngle<br>)<br>60.52<br>Di<br>2<br>Turn<br>Rate<br>('100usft)  | Field:<br>0.00<br>rection:<br>(*)<br>70.00  | Strength<br>nT)<br>48,705  |
| Weilbore<br>Magnetics<br>Design<br>Audit Notes:<br>Version:<br>Vertical Section<br>Plan Sections<br>Measured<br>Depth<br>(usift)   | Plan 2   | el:Name<br>IGRF2010<br>De<br>Azimuth<br>(?)   | Sampi<br>Phas<br>spth From (T)<br>(usft)<br>0.00<br>Vertical<br>Depth<br>(usft)   | le Date<br>1/3/2013<br>e: Pl<br>VD)<br>+N/-S<br>(usft)   | Decilina<br>(°)<br>LAN<br>+N/-Ş<br>(usft)<br>0.00<br>+E/-W<br>(usft)  | ition<br>7.53<br>Tie<br>+E/<br>(us<br>0.0<br>Dogleg<br>Rate<br>(°/100usft)  | Dip/4<br>(1)<br>On Depth:<br>(-W)<br>(1)<br>D0<br>Build<br>Rate<br>(*/100usft)                                  | ngle<br>)<br>60.52<br>Di<br>2<br>Turn<br>Rate<br>(*/100usft)   | Field<br>(<br>0.00<br>rection<br>(')<br>70.00<br>TFO<br>(')   | Strength<br>nin):<br>48,705  |
| Weilbore<br>Magnetics<br>Design<br>Audit Notes:<br>Version:<br>Vertical Section<br>Plan Sections<br>Measured<br>Depth<br>(usft)<br>0.00  | Plan 2<br>Plan 2   | el:Name<br>IGRF2010<br>"De<br>Azimuth<br>(*)<br>0.00  | Sampi<br>Phas<br>spth From (IT)<br>(usft)<br>0.00<br>Vertical<br>Depth<br>(usft)<br>0.00  | le Date<br>1/3/2013<br>e: Pl<br>VD)<br>+N/-S<br>(usft)<br>0.00   | Decilina<br>(*)<br>(*)<br>LAN<br>+N/-Ş<br>(usft)<br>0,00<br>+E/-W<br>(usft)<br>0,00   | ition<br>7.53<br>Tie<br>+E/<br>(us<br>0.0<br>Dogleg<br>Rate<br>(*/100usft)<br>0.00  | Dip/4<br>(1)<br>On Depth:<br>(-W<br>(ft))<br>DO<br>Build<br>Rate<br>(*/100usft)<br>0.00                         | ngle<br>)<br>60.52<br>Di<br>2<br>Turn<br>Rate<br>(*/100usft)<br>0.00   | Field:<br>0.00<br>rection:<br>(*)<br>70.00<br>TFO<br>(*)<br>0.00  | Strength<br>nTp)<br>48,705<br>Target   |
| Weilbore<br>Magnetics<br>Design<br>Audit Notes:<br>Vertical Section<br>Vertical Section<br>Plan Sections<br>Measured<br>Depth<br>(usft)<br>0.00<br>7,500.00  | OH<br>Mod<br>Plan 2  | el:Name<br>IGRF2010<br>"De<br>Azimuth<br>(*)<br>0.00<br>0.00  | Sampi<br>Phas<br>Phas<br>spth From (IT<br>(usft)<br>0.00<br>Vertical<br>Depth<br>(usft)<br>0.00<br>7,500.00   | e: Pl<br>/D):<br>+N/-S<br>(usft)<br>0.00<br>0.00   | Decilina<br>(°)<br>(AN<br>+N/-S<br>(usft)<br>0.00<br>+E/-W<br>(usft)<br>0.00<br>0.00  | ition<br>7.53<br>Tie<br>+E/<br>(us<br>0.0<br>Dogleg<br>Rate<br>(*/100usft)<br>0.00<br>0.00  | Dip/4<br>(1)<br>On Depth:<br>(  | ngle<br>)<br>60.52<br>Di<br>2<br>Turn<br>Rate<br>(*/100usft)<br>0.00<br>0.00                                   | Field:<br>0.00<br>rection:<br>(*)<br>70.00<br>TFO<br>(*)<br>0.00<br>0.00  | Strength<br>nTp)<br>48,705<br>Target   |
| Wellbore<br>Magnetics<br>Design<br>Audit Notes:<br>Vertical Section<br>Vertical Section<br>Plan Sections<br>Measured<br>Depth<br>(usft)<br>0.00<br>7,500.00<br>8,202.02  | OH<br>Mod<br>Plan 2<br>Plan 2  | IGRF2010<br>  | Sampi<br>Phas<br>Phas<br>epth From (IT)<br>(usft)<br>0.00<br>Vertical<br>Depth<br>(usft)<br>0.00<br>7,500.00<br>8,195.02  | e: Pl<br>√D)<br>↓N/-S<br>(usft)<br>0.00<br>0.00<br>74.02   | Declina<br>(*)<br>(*)<br>LAN<br>+N/-S<br>(usft)<br>0.00<br>+E/-W<br>(usft)<br>0.00<br>0.00<br>0.00<br>42.96   | ition<br>7.53<br>Tie<br>*E/<br>(us<br>0.0<br>Dogleg<br>Rate<br>(*/100usft)<br>0.00<br>0.00<br>2.00  | Dip/4<br>(1)<br>On Depth:<br>   | ngie<br>)<br>60.52<br>Di<br>2<br>Turn<br>Rate<br>(*/100usft)<br>0.00<br>0.00<br>0.00                           | Field:<br>0.00<br>rection:<br>(*)<br>70.00<br>TFO<br>(*)<br>0.00<br>0.00<br>0.00<br>30.13   | Strength<br>nit)<br>48,705<br>Target   |
| Wellbore<br>Magnetics<br>Design<br>Audit Notes:<br>Vertical Section<br>Vertical Section<br>Plan Sections<br>Measured<br>Depth<br>(usft)<br>0.00<br>7,500.00<br>8,202.02<br>8,710.19  | Plan 2<br>Plan 2   | IGRF2010<br>  | Sampi<br>Phas<br>Phas<br>epth From (IT)<br>(usft)<br>0.00<br>Vertical<br>Depth<br>(usft)<br>0.00<br>7,500.00<br>8,195.02<br>8,688.01  | e Date<br>1/3/2013<br>e: Pl<br>√D)<br>↓N/-S<br>(usft)<br>0.00<br>0.00<br>74.02<br>180.65                   | Declina<br>(*)<br>(*)<br>LAN<br>+N/-S<br>(usft)<br>0.00<br>+E/-W<br>(usft)<br>0.00<br>0.00<br>42.96<br>104.85   | ttion<br>7.53<br>Tie<br>+E/<br>(us<br>0.0<br>Dogleg<br>Rate<br>(*/100usft)<br>0.00<br>0.00<br>2.00<br>0.00  | Dip /4<br>(1<br>On Depth:<br>   | ngie<br>)<br>60.52<br>Di<br>2<br>Turn<br>Rate<br>(*/100usft)<br>0.00<br>0.00<br>0.00<br>0.00                   | Field:<br>0.00<br>rection:<br>(*)<br>70.00<br>TFO<br>(*)<br>0.00<br>0.00<br>30.13<br>0.00   | Strength<br>nit)<br>48,705   |
| Wellbore<br>Magnetics<br>Design<br>Audit Notes:<br>Vertical Section<br>Vertical Section<br>Plan Sections<br>Measured<br>Depth<br>(usft)<br>0.00<br>7,500.00<br>8,202.02<br>8,710.19<br>9,697.84                                | ۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹۹۲<br>۲۹<br>۲۹ | El.Name<br>IGRF2010<br>De<br>Azimuth<br>(°)<br>0.00<br>0.00<br>30.13<br>30.13<br>270.00                         | Sampi<br>Phas<br>Phas<br>epth From (IT)<br>(usft)<br>0.00<br>Vertical<br>Depth<br>(usft)<br>0.00<br>7,500.00<br>8,195.02<br>8,688.01<br>9.315.00  | e: Pl<br>√D)<br>•: Pl<br>vD)<br>0.00<br>0.00<br>74.02<br>180.65<br>320.83                                  | Declina<br>(°)<br>(AN<br>+N/-S<br>(usft)<br>0.00<br>+E/-W<br>(usft)<br>0.00<br>0.00<br>42.96<br>104.85<br>-481.53   | ttion<br>7.53<br>Tie<br>+E/<br>(us<br>0.0<br>Dogleg<br>Rate<br>(*/100usft)<br>0.00<br>0.00<br>2.00<br>0.00<br>10.00                                   | Dip /4<br>(1)<br>On Depth:<br>  | Turn<br>Rate<br>(*/100usft)<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00  | Field:<br>0.00<br>rection:<br>(*)<br>70.00<br>TFO<br>(*)<br>0.00<br>0.00<br>0.00<br>30.13<br>0.00<br>-118.90                                      | Strength<br>nit)<br>48,705<br>Target   |
| Wellbore<br>Magnetics<br>Design<br>Audit Notes:<br>Version:<br>Vertical Section<br>Plan Sections<br>Measured<br>Depth<br>(usft)<br>0.00<br>7,500.00<br>8,202.02<br>8,710.19<br>9,697.84<br>10,963.47                           | Plan 2<br>Plan 2<br>Inclination<br>(°)<br>0.00<br>0.00<br>14.04<br>14.04<br>91.81<br>91.81   | El.Name<br>IGRF2010<br>De<br>Azimuth<br>(°)<br>0.00<br>0.00<br>30.13<br>30.13<br>270.00<br>270.00               | Sampl<br>Phas<br>Phas<br>Phas<br>Phas<br>Path From (IT)<br>(usft)<br>0.00<br>Vertical<br>Depth<br>(usft)<br>0.00<br>7,500.00<br>8,195.02<br>8,668.01<br>9,315.00<br>9,275.00                | e: PL<br>VD)<br>0.00<br>0.00<br>74.02<br>180.65<br>320.83<br>320.83  | Decilina<br>(?)<br>LAN<br>+N/-S<br>(usft)<br>0.00<br>+E/-W<br>(usft)<br>0.00<br>0.00<br>42.96<br>104.85<br>-481.53<br>-1746 52                            | ition<br>7.53<br>Tie<br>+E/<br>(us<br>0.0<br>Dogleg<br>Rate<br>(*/100usft)<br>0.00<br>0.00<br>2.00<br>0.00<br>10.00<br>0.00                           | Dip/4<br>(1<br>On Depth:<br>  | Turn<br>Rate<br>(*/100usft)<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.                      | Field:<br>0.00<br>rection<br>(*)<br>70.00<br>TFO<br>(*)<br>0.00<br>0.00<br>30.13<br>0.00<br>-118.99<br>- 200                                      | Strength<br>nTp)<br>48,705<br>Target   |
| Wellbore<br>Magnetics<br>Design<br>Audit Notes:<br>Version:<br>Vertical Section<br>Plan Sections<br>Measured<br>Depth<br>(usft)<br>0.00<br>7,500.00<br>8,202.02<br>8,710.19<br>9,697.84<br>10,963.47<br>10,963.47              | Plan 2<br>Plan 2<br>Plan 2<br>Inclination<br>(*)<br>0.00<br>0.00<br>14.04<br>14.04<br>91.81<br>91.81<br>91.81<br>91.72   | El.Name<br>IGRF2010<br>De<br>Azimuth<br>(?)<br>0.00<br>0.00<br>30.13<br>30.13<br>270.00<br>270.00<br>270.00     | Sampl<br>Phas<br>Phas<br>Phas<br>Phas<br>Phas<br>Phas<br>Phas<br>Phas   | e: PL<br>VD)<br>0.00<br>0.00<br>74.02<br>180.65<br>320.83<br>320.83<br>320.83                              | Decilina<br>(?)<br>LAN<br>+N/-S<br>(usft)<br>0.00<br>+E/-W<br>(usft)<br>0.00<br>0.00<br>42.96<br>104.85<br>-481.53<br>-1,746.53<br>1.766.55               | ition<br>7.53<br>Tie<br>*E/<br>(us<br>0.0<br>0<br>0.00<br>2.00<br>0.00<br>2.00<br>0.00<br>10.00<br>0.00   | Dip/4<br>(1<br>On Depth:<br>  | Turn<br>Rate<br>(*/100usft)<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.                      | Field:<br>0.00<br>rection<br>(*)<br>70.00<br>TFO<br>(*)<br>0.00<br>0.00<br>0.00<br>0.00<br>30.13<br>0.00<br>-118.99<br>0.00                       | Strength<br>nT)<br>48,705<br>Target<br>Target  |
| Wellbore<br>Magnetics<br>Design<br>Audit Notes:<br>Version:<br>Vertical Section<br>Plan Sections<br>Measured<br>Depth<br>(usft)<br>0.00<br>7,500.00<br>8,202.02<br>8,710.19<br>9,697.84<br>10,963.47<br>10,967.52              | Plan 2<br>Plan 2<br>Plan 2<br>Plan 2<br>0.00<br>0.00<br>14.04<br>14.04<br>91.81<br>91.81<br>91.81<br>91.73<br>04.72  | El.Name<br>IGRF2010<br>Azimuth<br>(*)<br>0.00<br>0.00<br>30.13<br>30.13<br>270.00<br>270.00<br>270.00<br>270.00 | Sampl<br>Phas<br>Phas<br>Phas<br>Phas<br>Phas<br>Phas<br>Phas<br>Phas   | e: Pl<br>VD)<br>0.00<br>74.02<br>180.65<br>320.83<br>320.83<br>320.83<br>320.83                            | Decilina<br>(?)<br>LAN<br>+N/-S<br>(usft)<br>0.00<br>+E/-W<br>(usft)<br>0.00<br>0.00<br>42.96<br>104.85<br>-481.53<br>-1,746.53<br>-1,746.53<br>-1,750.58 | tition<br>7.53<br>Tie<br>*E/<br>(us<br>0.0<br>0.00<br><b>Dogleg</b><br>Rate<br>(*/100usft)<br>0.00<br>0.00<br>2.00<br>0.00<br>10.00<br>0.00<br>2.00   | Dip/4<br>(1<br>On Depth:<br>  | Turn<br>Rate<br>(*/100usft)<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.                      | Field<br>0.00<br>rection<br>(*)<br>70.00<br>TFO<br>(*)<br>0.00<br>0.00<br>0.00<br>0.00<br>30.13<br>0.00<br>-118.99<br>0.00<br>180.00              | Strength<br>nT):<br>48,705<br>Target<br>Target<br>Taylor Draw 7 Fed He<br>Taylor Draw Fed Mid  |
| Wellbore<br>Magnetics<br>Design<br>Audit Notes:<br>Version:<br>Vertical Section<br>Plan Sections<br>Measured<br>Depth<br>(usft)<br>0.00<br>7,500.00<br>8,202.02<br>8,710.19<br>9,697.84<br>10,963.47<br>10,967.52<br>13,944.27 | OH<br>Mod<br>Plan 2<br>Plan 2<br>0.00<br>0.00<br>14.04<br>14.04<br>91.81<br>91.81<br>91.73<br>91.73  | El.Name<br>IGRF2010<br>Azimuth<br>(*)<br>0.00<br>0.00<br>30.13<br>30.13<br>270.00<br>270.00<br>270.00<br>270.00 | Sampl<br>Phas<br>Phas<br>Phas<br>Path From (IT<br>(usft)<br>0.00<br>Vertical<br>Depth<br>(usft)<br>0.00<br>7,500.00<br>8,195.02<br>8,688.01<br>9,315.00<br>9,275.00<br>9,274.88<br>9,185.00 | e: Pl<br>VD)<br>→N/-S<br>(usft)<br>0.00<br>0.00<br>74.02<br>180.65<br>320.83<br>320.83<br>320.83<br>320.83 | Decilina<br>(?)<br>LAN<br>+N/-S<br>(usft)<br>0.00<br>+E/-W<br>(usft)<br>0.00<br>0.00<br>42.96<br>104.85<br>-481.53<br>-1,746.53<br>-1,750.58<br>-4,725.97 | tition<br>7.53<br>Tie<br>(us<br>0.0<br>Dogleg<br>Rate<br>(*/100usft)<br>0.00<br>0.00<br>2.00<br>0.00<br>10.00<br>0.00<br>2.00<br>0.00<br>2.00<br>0.00 | Dip/4<br>(1<br>On Depth:<br>  | Turn<br>Rate<br>(*/100usft)<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.                      | Field<br>0.00<br>rection<br>(*)<br>70.00<br>TFO<br>(*)<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>18.99<br>0.00<br>180.00<br>0.00<br>0.00 | Strength<br>nT):<br>48,705<br>Target<br>Target<br>Taylor Draw 7 Fed He<br>Taylor Draw 7 Fed Hid<br>Taylor Draw 7 Fed Mid   |

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# Pathfinder - A Schlumberger Company

Planning Report

| Database:      | EDM 5000,1 Sin                    | igle User Db                             | 2 4 · · · k 2        | Local C  | o-ordinate Ref  | erence:       | Well #1H  | <del>adan Bratzaren 1</del> 71                                    |  |
|----------------|-----------------------------------|--|----------------------|--|---|---------------|---|---|--|
| Compariy:      | Devon Energy, I                   | nc                                       |                      | TVD Re   | ference:  |               | Est RKB = 20'   | @ 3636:80usft   |  |
| Project:       | Lea County (NA                    | D83)                                     |                      | MD Ref   | erence:   |               | Est RKB = 20'   | @ 3636:80usft   |  |
| Sito           | Taylor Draw 7 Fe                  | ed                                       |                      | NorthB   | eference  | \$ 10 C       | Grid  |   |  |
| VALAIL.        | iy eye<br>⊈waa                    |  |                      | Survey   | Calculation M   | thod          | Minimum Curv  | iature  | 1  |
| VVOII.         | анни<br>ОЩ                        |  |                      | Ourvey   |   |               |   |   |  |
| Desion:        | Plan 2                            |  | ala di Sala          | - u  | ્યું છે.<br>આ ગામના ગ<br>આ ગામના ગા |               | 1   |   |  |
|                |                                   | en e |                      |  |   |               | 1/200 - 100 |   | a man a second to be the second s   |
| Planned Survey |                                   |  |                      | ر با محکمه کردیو در است.<br>در این از این از این از این از ا |   |               |   | ور با منظوم به مارینهای و ورد.<br>با های از انداز از مارینهای و ا |  |
| Measured       |                                   |  | Vertical             |  |   | Vertical      | Doglega   | Build   | Turn   |
| Depth          | Inclination                       | Azimuth                                  | Depth                | +N/-S  | +E/-W   | Section       | Rate  | Rate  | Rate   |
| (usft)         | ຳແຫຼນເບເສ<br>ເວັ້າ(ຄ). ເຈົ້າເວັ້າ | (1) ····                                 | (usft)               | (usft)   | (usft)  | (üsft)        | (*/100usft)   | (°/100usft)   | (°/100usft)  |
|                | A                                 |  | 2 A                  |  | r and a start and a   | . 01 V . 4 F- | in the spring there   | a set a set a set a set   | and the second |
| 7,500.00       | 0.00                              | 0.00                                     | 7,500.00             | 0.00   | 0.00  | 0.00          | 0.00  | 0.00  | 0.00   |
| 7,600.00       | 2.00                              | 30.13                                    | 7,599.98             | 1.51   | 0.88  | -0.88         | 2.00  | 2.00  | 0.00   |
| 7,700.00       | 4.00                              | 30,13                                    | 7,099.84             | 0.04   | 3.50  | -3,50         | 2.00  | 2.00  | 0.00   |
| 7,800.00       | 6.00                              | 30.13                                    | 7,799,40             | 74 11  | 13.00   | -7.00         | 2.00  | 2.00  | 0.00   |
| 7,900.00       | 8.00                              | 30.13                                    | 7,030.70             | 24.11  | 10.00   | -10.00        | 2.00  | 2.00  | 0.00   |
| 8,000.00       | 10.00                             | 30.13                                    | 7,997.47             | 37.64  | 21.85   | -21.85        | 2.00  | 2.00  | 0.00   |
| 8,100.00       | 12.00                             | 30.13                                    | 8,095.62             | 54.14  | 31.42   | -31.42        | 2.00  | 2.00  | 0.00   |
| 8,200.00       | 14.00                             | 30.13                                    | 8,193.06             | 73.60  | 42.72   | -42.72        | 2.00  | 2.00  | 0.00   |
| 8,202.02       | 14.04                             | 30,13                                    | 8,195.02             | 74.02  | 42.96   | -42.96        | 2.00  | 2.00  | 0.00   |
| 8,300.00       | 14.04                             | 30.13                                    | 8,290.07             | 94.58  | 54.89   | -54.89        | 0.00  | 0.00  | 0.00   |
| 8,400.00       | 14.04                             | 30.13                                    | 8,387.08             | 115.56   | 67.07   | -67.07        | 0.00  | 0.00  | 0.00   |
| 8,500.00       | 14.04                             | 30.13                                    | 8,484.09             | 136.55   | 79.25   | -79.25        | 0.00  | 0.00  | 0.00   |
| 8,600.00       | 14.04                             | 30.13                                    | 8,581.11             | 157.53   | 91.43   | -91,43        | 0.00  | 0.00  | 0.00   |
| 8,700.00       | 14.04                             | 30,13                                    | 8,678.12             | 178.51   | 103.60  | -103,60       | 0.00  | 0.00  | 0.00   |
| 8,710.19       | 14.04                             | 30.13                                    | 8,688.01             | 180.65   | 104.85  | -104.85       | 0.00  | 0.00  | 0.00   |
| 8 800 00       | 12.42                             | 350.73                                   | 8,775,60             | 199.65   | 108.77  | -108.77       | 10.00   | -1.80   | -43.87   |
| 8,900,00       | 17.13                             | 315,18                                   | 8,872,46             | 220.76   | 96.62   | -96.62        | 10.00   | 4.71  | -35.55   |
| 9,000.00       | 25.09                             | 298.02                                   | 8,965,76             | 241.22   | 67.44   | -67.44        | 10.00   | 7.96  | -17.16   |
| 9,100.00       | 34.10                             | 289,10                                   | 9,052.66             | 260.40   | 22.13   | -22.13        | 10.00   | 9.00  | -8.92  |
| 9,200.00       | 43.50                             | 283.62                                   | 9,130.54             | 277.73   | -37.96  | 37.96         | 10.00   | 9.40  | -5.48  |
| 9 300 00       | 53.08                             | 279 78                                   | 9 197 01             | 292.66   | -110 98   | 110 98        | 10.00   | 9.58  | -3.84  |
| 9,000.00       | 62.00                             | 276 81                                   | 9 250 07             | 304.76   | -194.73   | 194.73        | 10.00   | 9.68  | -2.97  |
| 9 500.00       | 72.49                             | 274.32                                   | 9,288,10             | 313.65   | -286.65   | 286.65        | 10.00   | 9.73  | -2.49  |
| 9,600.00       | 82.25                             | 272.09                                   | 9,309,94             | 319.06   | -383,95   | 383.95        | 10.00   | 9.76  | -2.23  |
| 9,697.84       | 91.81                             | 270.00                                   | 9,315.00             | 320.83   | -481.53   | 481.53        | 10.00   | 9.77  | -2.13  |
| 0,700,00       | 04.84                             | 270.00                                   | 0 214 02             | 220.92   | 492.60  | 493.60        | 0.00  | 0.00  | 0.00   |
| 9,700.00       | 91.01                             | 270.00                                   | 9,314.93             | 320.83   | -403.09   | 403.09        | 0.00  | 0.00  | 0.00   |
| 9,800.00       | 91.01                             | 270.00                                   | 9,311.77             | 320.03   | -583.04   | 683.50        | 0.00  | 0.00  | 0.00   |
| 9,900.00       | 91.01                             | 270.00                                   | 9,305.01             | 320.83   | -783.54   | 783.54        | 0.00  | 0.00  | 0.00   |
| 10,000.00      | 91.81                             | 270.00                                   | 9 302 29             | 320.83   | -883 49   | 883 49        | 0.00  | 0.00  | 0.00   |
| 10,100.00      | 01.01                             | 270.00                                   |                      |  |   |               |   |   |  |
| 10,200.00      | 91.81                             | 270.00                                   | 9,299,13             | 320.83   | -983.44   | 983.44        | 0,00  | 0.00  | 0.00   |
| 10,300.00      | 91.81                             | 270.00                                   | 9,295.97             | 320.83   | -1,083.39   | 1,083.39      | 0.00  | 0.00  | 0.00   |
| 10,400.00      | 91.81                             | 270.00                                   | 9,292.81             | 320.83   | -1,183.34   | 1,183.34      | 0.00  | 0.00  | 0.00   |
| 10,500.00      | 91.81                             | 270.00                                   | 9,289.65             | 320.83   | -1,283.29   | 1,283.29      | 0.00  | 0.00  | 0.00   |
| 10,600.00      | 91.01                             | 270.00                                   | 9,200.49             | 320.03   | -1,303.24   | 1,303.24      | 0.00  | 0.00  | 0.00   |
| 10,700.00      | 91.81                             | 270.00                                   | 9,283.33             | 320.83   | -1,483.19   | 1,483.19      | 0.00  | 0.00  | 0.00   |
| 10,800.00      | 91.81                             | 270.00                                   | 9,280.17             | 320.83   | -1,583.14   | 1,583.14      | 0.00  | 0.00  | 0.00   |
| 10,900.00      | 91.81                             | 270.00                                   | 9,277.01             | 320.83   | -1,683.09   | 1,683.09      | 0.00  | 0.00  | 0.00   |
| 10,963.47      | 91.81                             | 270.00                                   | 9,275.00             | 320.83   | -1,746.53   | 1,746.53      | 0.00  | 0.00  | 0.00   |
| 10,967.52      | 91.73                             | 270.00                                   | 9,274.88             | 320.83   | -1,750.58   | 1,750.58      | 2.00  | -2.00   | 0.00   |
| 11,000.00      | 91.73                             | 270.00                                   | 9,273.89             | 320.83   | -1,783.04   | 1,783.04      | 0.00  | 0.00  | 0.00   |
| 11,100.00      | 91.73                             | 270.00                                   | 9,270.88             | 320.83   | -1,882.99   | 1,882.99      | 0.00  | 0.00  | 0.00   |
| 11,200.00      | 91.73                             | 270.00                                   | 9,267.86             | 320.83   | -1,982.95   | 1,982.95      | 0.00  | 0.00  | 0.00   |
| 11,300.00      | 91,73                             | 270.00                                   | 9,264.84             | 320.83   | -2,082.90   | 2,082.90      | 0.00  | 0.00  | 0.00   |
| 11,400.00      | 91,73                             | 270.00                                   | 9,261.82             | 320.83   | -2,182.86   | 2,182.86      | 0.00  | 0.00  | 0.00   |
| 11 500 00      | 91 73                             | 270 00                                   | 9,258 80             | 320.83   | -2.282 81   | 2,282 81      | 0.00  | 0.00  | 0.00   |
| 11 600.00      | 91.73                             | 270.00                                   | 9,255.78             | 320.83   | -2.382.77   | 2.382.77      | 0.00  | 0.00  | 0.00   |
| 11,700.00      | 91.73                             | 270.00                                   | 9,252.76             | 320.83   | -2,482.72   | 2,482.72      | 0.00  | 0.00  | 0.00   |
| 11,800.00      | 91.73                             | 270.00                                   | 9,249.74             | 320.83   | -2,582.67   | 2,582.67      | 0.00  | 0.00  | 0.00   |
| 11,900.00      | 91.73                             | 270.00                                   | 9,246.72             | 320.83   | -2,682.63   | 2,682.63      | 0.00  | 0.00  | 0.00   |
| 40,000,00      | 04 70                             | 270.00                                   | 0.040.70             | 200.80   | 0 700 50  | 0 780 50      | 0.00  | c   | 0.00   |
| 12,000.00      | 91.73                             | 270.00<br>270.00                         | 9,243.70<br>9,240.69 | 320,83<br>330 ₽3   | -2,/82.58   | 2,/02.58      | 0.00  | 0,00  | 0,00   |
| 12,100.00      | 01.70<br>01.70                    | 270.00                                   | 9,240.00             | 320.03   | -2,002.04   | 2,002.04      | 0.00  | 0.00  | 0,00   |
| 12,200.00      | 91.73                             | 270.00                                   | 9 234 64             | 320.03   | -2,502.45   | 3 082 45      | 0.00  | 0.00  | 0.00   |
| 12,300.00      | 31.13                             | 210.00                                   | 0,207.07             | 020.00   | -0,002.40   | 3,002.43      | 0.00  | 0.00  | 0.00   |

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# Pathfinder - A Schlumberger Company

Planning Report

|  | DM EOOD 1 S                             | ingle Lloor Dh                                | all a start and a start of the | and a second |  | 1.1.1   |   | <del>شن هان باق بارسوس (س</del> ریس)                | status and experience and the and   |
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| Company:                                   | evon Energy                             | , IIIU.                                       | · • •                          |  | Reference:   |   | ESTRKE = 20                                       | 0 @ 3636.60usn                                      |   |
| Project:                                   | ea County (N                            | AD83)   |                                | MD R   | eference:  | $\mathcal{F} = \{ \mathcal{F} \in \mathcal{F} \}$     | 1 Est RKB = 20                                    | )' @ 3636.80usft                                    |   |
| Site:                                      | aylor Draw 7                            | Fed   | the second second              | North  | Réference:   | e   | Grid  |   |   |
| Well: #                                    | 1H                                      |   |                                | Surve  | y Calculation M  | Aethod:   | § Minimum Cur                                     | vature  |   |
| Wellbore:                                  | н<br>H                                  | an a      |                                |  |  |   | 1   | 1   |   |
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| Planned                                    | 1                                       | <u> </u>                                      | 1                              | 131 <u>-144</u> -13  | ra statisk stario Vi   |   | a hand and and a set                              |   | an and a second s |
| , and a start of the start                 |   | مند به مرتشد.<br>الله رياني <sup>مر</sup> قعي |                                | مەرىمە - يىھەر مار مەرىپىد   | ين وي ما <sup>ن</sup> بطور محدد<br>مراجع   | a.  | and the set of the set                            | المريك فأرجع والمحرج والمحرج                        |   |
| Moneyrod                                   |   |   | Vortical                       | Same Carl  | 4 A A  | Vortical  | Docioc  | Build   | -S<br>Turne   |
| Donth                                      | م<br>المعادة الق                        | Aminauth                                      | Denth                          | IN R   | LEIVIE C   | Section   | Poto  | Bato  | Data  |
| (infit)                                    | icination •                             | Azimum  | (jieff)                        | 710-3<br>(110-8)   |  | Section 2   | /º/100060   | 10/100 meft   | (9/100 in #1)   |
| lusity                                     |   |   | Jusit                          | (usit)   | ุ (และเ)   | a tuaity a  | ( / i vusic)                                      | ( inousit)  | Willouaith  |
| 12,400.00                                  | 91.73                                   | 270.00  | 9,231.63                       | 320.83   | -3,182.40  | 3,182.40  | 0.00  | 0.00  | 0.00  |
| 12,500.00                                  | 91.73                                   | 270.00  | 9,228.61                       | 320.83   | -3,282.36  | 3,282.36  | 0.00  | 0,00  | 0.00  |
| 12,600.00                                  | 91.73                                   | 270.00  | 9,225.59                       | 320.83   | -3,382.31  | 3,382.31  | 0.00  | 0.00  | 0.00  |
| 12,700.00                                  | 91.73                                   | 270.00  | 9,222.57                       | 320.83   | -3,482.26  | 3,482.26  | 0.00  | 0.00  | 0.00  |
| 12,800.00                                  | 91.73                                   | 270.00  | 9,219.55                       | 320.83   | -3,582.22  | 3,582.22  | 0.00  | 0.00  | 0.00  |
| 12,900.00                                  | 91.73                                   | 270.00  | 9,216.53                       | 320.83   | -3,682.17  | 3,682.17  | 0.00  | 0.00  | 0.00  |
| 13.000.00                                  | 91.73                                   | 270.00  | 9.213.51                       | 320.83   | -3.782.13  | 3,782,13  | 0.00  | 0.00  | 0.00  |
| 13,100.00                                  | 91.73                                   | 270.00  | 9,210,49                       | 320,83   | -3.882.08  | 3.882.08  | 0.00  | 0.00  | 0.00  |
| 13,200.00                                  | 91.73                                   | 270.00  | 9,207,47                       | 320.83   | -3.982.04  | 3,982.04  | 0.00  | 0.00  | 0.00  |
| 13,300.00                                  | 91,73                                   | 270.00  | 9,204,45                       | 320.83   | -4.081.99  | 4,081,99  | 0.00  | 0.00  | 0.00  |
| 13,400.00                                  | 91.73                                   | 270.00  | 9,201.43                       | 320.83   | -4,181.95  | 4,181,95  | 0.00  | 0.00  | 0.00  |
| 13 500 00                                  | 01 72                                   | 270.00  | 0 109 41                       | 200 82   | 4 284 00   | 4 384 66  | 0.00  | 0.00  |   |
| 13,500.00                                  | 91.73                                   | 270.00  | 9,190.41                       | 320.83   | 4,201.90   | 4,201.90  | 0.00  | 0.00  | 0.00  |
| 13,000,00                                  | 91.73                                   | 270.00  | 9,193,39                       | 320,03   | 4,301.00   | 4,301.03  | 0.00  | 0.00  | 0,00  |
| 13,700.00                                  | 91.73                                   | 270.00  | 0 180 36                       | 320.83   | 4 581 76   | 4,401.01  | 0.00  | 0.00  | 0.00  |
| 13,000.00                                  | 91 73                                   | 270.00  | 9 186 34                       | 320,83   | -4 681 72  | 4,501.70  | 0.00  | 0.00  | 0.00  |
| 10,000,00                                  | 01.70                                   | 270.00  | 5,100.04                       | 520.00   | 4,001.72   | 4,001.72  | 0.00  | 0.00  | 0.00  |
| 13,944.27                                  | 91.73                                   | 270.00  | 9,185.00                       | 320,83   | -4,725.97  | 4,725.97  | 0.00  | 0.00  | 0.00  |
|  | يعبد بيرق تغريبه أبأر                   |   | I - in the Art                 |  | ala da antes en antes e  | altanki Arabia i ana i                                | a alla a jong and a so an a so an an a so an an a | e e a appene i sta altra artale                     | No an about an an anna an an an an an an an an an a   |
| Designingiges                              | بر ای دار سان واهمیرد.<br>ای از در ای ا | may an    | بالموقوقية والمريانية          | an an an again the again the again   | and the second | ىيە ئېرىرىيەر سەمىيىسار بولىد.<br>بېرىمىرىيەر مەمىيەر | a na manana ang kang kang kang kang kang kang     | بالمطالب الجاريب بالمساولوات الإساط                 |   |
| Target Name                                |   |   |                                |  | 1. 4. 50   |   |   |   | 1982 - 1982 - 1983 - 1983 - 1983 - 1983 - 1983 - 1983 - 1983 - 1983 - 1983 - 1983 - 1983 - 1983 - 1983 - 1983 -   |
| hit/miss target                            | Din Angle                               |   | Ē.∕∩. ∔Ň/                      | S. +E/-W   | Northi   | no.   | ting 7  | និងនេះ ដែលមិត អាត្រ<br>ភ្លាំនេះ និ និសិនិតិនិងនេះ ដ |   |
| Shane                                      |   |   | 1001 - 110<br>1001 - 110       |  |  | ig cas  | uny<br>41   |   | ្រូវប្រទេស ដែលស្រី មានដែលទី។<br>ភ្លើម ស្រុក ស្រុក ស្រុក ស្រុក   |
|  |   | 17 1  | uşit) (Us                      | iu) iusiu  | luait  | in the second second                                  | bit)/   | Latitude  | Longitude   |
| Taylor Draw 7 Fed #1H F                    | 0.00                                    | 0.00 9  | 185.00 3                       | 20.83 -4.725   | 5 97 609 (   | 040 54 70   | 1381 15 3   | 32° 40' 23 590 N                                    | 103º 48' 47 557 W   |
| - plan hits target cente                   | r                                       | 0.00 0,                                       | 100.00                         | 20.00 4,720  |  | 0-0.0-  | 1,001.10  | 2 40 20.000 N                                       | 105 40 47.557 44  |
| - Point                                    | •                                       |   |                                |  |  |   |   |   |   |
|  |   |   |                                |  |  |   |   |   |   |
| Taylot Draw Fed Mid Pt                     | 0.00                                    | 0.00 9,                                       | 275.00 3                       | 20.83 -1,746   | 5,53 609,0   | 040.54 70   | 4,360.59 3  | 32° 40' 23.445 N                                    | 103° 48' 12.700 W   |
| <ul> <li>plan hits target cente</li> </ul> | ۲                                       |   |                                |  |  |   |   |   |   |
| - Point                                    |   |   |                                |  |  |   |   |   |   |
| Taylor Draw 7 Fed Heel                     | 0.00                                    | 0.00 9,                                       | 315.00 3                       | 20.83 -481   | .53 609,0  | 040.54 70   | 5,625.59 3  | 32° 40′ 23.382 N                                    | 103° 47' 57.901 W   |
| <ul> <li>plan hits target cente</li> </ul> | r                                       |   |                                |  |  |   |   |   |   |
| - Point                                    |   |   |                                |  |  |   |   |   |   |
|  |   |   |                                |  |  |   |   |   |   |

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# PECOS DISTRICT CONDITIONS OF APPROVAL

| <b>OPERATOR'S NAME:</b> | Devon Energy Production Company, L.P. |
|-------------------------|---------------------------------------|
| LEASE NO.:              | NMNM-104685                           |
| WELL NAME & NO.:        | Taylor Draw 7 Fed 1H                  |
| SURFACE HOLE FOOTAGE:   | 1650' FSL & 0260' FEL                 |
| BOTTOM HOLE FOOTAGE     | 1980' FSL & 0330' FWL                 |
| LOCATION:               | Section 7, T. 19 S., R 32 E., NMPM    |
| COUNTY:                 | Lea County, New Mexico                |
| API:                    | 30-025-41146                          |

### The original COAs still stand with the following drilling modifications:

# I. DRILLING

### A. DRILLING OPERATIONS REQUIREMENTS

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)

# **Lea County**

Call the Hobbs Field Station, 414 West Taylor, Hobbs NM 88240, (575) 393-3612

- 1. A Hydrogen Sulfide (H2S) Drilling Plan shall be activated prior to drilling out the surface shoe. As a result, the Hydrogen Sulfide area must meet Onshore Order 6 requirements, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, provide measured values and formations to the BLM.
- Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval. If the drilling rig is removed without approval an Incident of Non-Compliance will be written and will be a "Major" violation.

- 3. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works is located, this does not include the dog house or stairway area.
- 4. The record of the drilling rate along with the GR/N well log run from TD to surface (horizontal well vertical portion of hole) shall be submitted to the BLM office as well as all other logs run on the borehole 30 days from completion. If available, a digital copy of the logs is to be submitted in addition to the paper copies. The Rustler top and top and bottom of Salt are to be recorded on the Completion Report.

## **B.** CASING

Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.).

Centralizers required on surface casing per Onshore Order 2.III.B.1.f.

Wait on cement (WOC) time prior to drilling out for a primary cement job will be a minimum 18 hours for a water basin, 24 hours in the potash area, or 500 pounds compressive strength, whichever is greater for all casing strings. DURING THIS WOC TIME, NO DRILL PIPE, ETC. SHALL BE RUN IN THE HOLE. Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. IF OPERATOR DOES NOT HAVE THE WELL SPECIFIC CEMENT DETAILS ONSITE PRIOR TO PUMPING THE CEMENT FOR EACH CASING STRING, THE WOC WILL BE 30 HOURS. See individual casing strings for details regarding lead cement slurry requirements.

No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.

Possibility of water and brine flows in the Salado and Delaware Mountain Groups. Possibility of lost circulation in the Rustler, Capitan, and Delaware Mountain Groups.

- 1. The 13-3/8 inch surface casing shall be set at approximately 960 feet (a minimum of 25 feet into the Rustler Anhydrite and above the salt) and cemented to the surface. In this area of the proposed well, a salt zone often appears about 45 feet below the base of the Magenta, avoid this layer. If salt is encountered, set casing at least 25 feet above the salt.
  - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
  - **b.** Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry.
  - c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
  - d. If cement falls back, remedial cementing will be done prior to drilling out that string.

### **Special Capitan Reef requirements:**

If any lost circulation occurs below the Base of the Salt, the operator shall do the following:

- Switch to fresh water mud to protect the Capitan Reef and use fresh water mud until setting the intermediate casing. The appropriate BLM office is to be notified for a PET to witness the switch to fresh water.
- Daily drilling reports from the Base of the Salt to the setting of the intermediate casing are to be submitted to the BLM CFO engineering staff via e-mail by 0800 hours each morning. Any lost circulation encountered is to be recorded on these drilling reports. The daily drilling report should show mud volume per shift/tour. Failure to submit these reports will result in an Incidence of Non-Compliance being issued for failure to comply with the Conditions of Approval. If not already planned, the operator shall run a caliper survey for the intermediate well bore and submit to the appropriate BLM office.
- 2. The minimum required fill of cement behind the 9-5/8 inch intermediate casing is:

Cement to surface. If cement does not circulate see B.1.a, c-d above.

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Centralizers required on horizontal leg, must be type for horizontal service and a minimum of one every other joint.

- 3. The minimum required fill of cement behind the 5-1/2 inch production casing is:
  - Cement should tie-back at least 50 feet above the Capitan Reef. Operator shall provide method of verification. Excess calculates to 24% Additional cement may be required.
- 4. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.

# C. PRESSURE CONTROL

- 1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in Onshore Oil and Gas Order No. 2 and API RP 53 Sec. 17.
- 2. Variance approved to use flex line from BOP to choke manifold. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor. If the BLM inspector questions the straightness of the hose, a BLM engineer will be contacted and will review in the field or via picture supplied by inspector to determine if changes are required (operator shall expect delays if this occurs).
- 3. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be **3000 (3M)** psi.
  - a. **For surface casing only:** If the BOP/BOPE is to be tested against casing, the wait on cement (WOC) time for that casing is to be met (see WOC statement at start of casing section). Independent service company required.

- 4. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
  - a. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead when specified), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).
  - b. The tests shall be done by an independent service company utilizing a test plug **not a cup or J-packer**. The operator also has the option of utilizing an independent tester to test without a plug (i.e. against the casing) pursuant to Onshore Order 2 with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for water basin (18 hours) or potash (24 hours) or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).
  - c. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall have a maximum 2 hour clock.
  - d. The results of the test shall be reported to the appropriate BLM office.
  - e. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
  - f. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.

# D. DRILL STEM TEST

If drill stem tests are performed, Onshore Order 2.III.D shall be followed.

## E. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area.

Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

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