HOBBS OCD		-			TS-13-	
Form 3160-3 (August 2007) NOV 2 0 2013) UNITED STATES BUREAU OF LAND MAN.			bs	OMB No Expires J 5. Lease Serial No. NM LC 029405B 6. If Indian, Allotee	APPROVE o. 1004-013 uly 31, 201	17 10
APPLICATION FOR PERMIT TO I la. Type of work: ✓ DRILL REENTE		L OR RECNIER		N/A 7. If Unit or CA Agree	ement, N	ame and No.
1b. Type of Well: Oil Well Gas Well Other	- [Single Zone Multipl	le Zone	N/A 8. Lease Name and Ruby Federal 33 9. API Well No. 38 -624-		\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\
3a. Address P.O. Box 51810 Midland, TX 79710-1810		one No. (include area code) 888-6913		10. Field and Pool, or Maljamar; Yeso We	Explorato	44500
4. Location of Well (Report location clearly and in accordance with any At surface UL G, Sec.18, T17S, R32E; 1725' FNL & 1675 At proposed prod. zone UL G, Sec.18, T17S, R32E; 2211' F	5' FEL			11. Sec., T. R. M. or B Sec.18, T17S, R32		rvey or Area
14. Distance in miles and direction from nearest town or post office* Approximately 3 miles south of Maljamar, New Mexico				12. County or Parish Lea County		13. State NM
15 Distance from proposed* About 338' location to nearest property or lease line, ft. (Also to nearest drig. unit line, if any)	16. No 1601	o. of acres in lease 9 6	17. Spacing 40 acres	g Unit dedicated to this v	well	
18. Distance from proposed location* to nearest well, drilling, completed, applied for, on this lease, ft.	693	9' TVD/6978'MD	ES0085	BIA Bond No. on file		
21. Elevations (Show whether DF, KDB, RT, GL, etc.) 3970' GL		pproximate date work will star 1/2014	t*	23. Estimated duratio 9 days	n	
	24.	Attachments				
 The following, completed in accordance with the requirements of Onshor Well plat certified by a registered surveyor. A Drilling Plan. A Surface Use Plan (if the location is on National Forest System SUPO must be filed with the appropriate Forest Service Office). 	Lands, t	4. Bond to cover the Item 20 above). 5. Operator certificate Such other site such other	e operation	is form: ns unless covered by an prination and/or plans as		,
25. Signature Susan S. Munder Title		Name (Printed/Typed) Susan B. Maunder			Date 8	2 13
Senior Regulatory Specialist						
Approved by (Signature)		Name (Printed/Typed)			NO'	V 15 2013
Title /S/ STEPHEN J. CAFFEY		Office CARLSE	BAD FIEL	D OFFICE		
Application approval does not warrant or certify that the applicant hold conduct operations thereon. Conditions of approval, if any, are attached.	s legal c	or equitable title to those right		ject lease which would on APPROVAL FO		•
Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a ct States any false, fictitious or fraudulent statements or representations as t	ime for o any m	any person knowingly and watter within its jurisdiction.	rillfully to n	nake to any department of	or agency	of the United

(Continued on page 2)

*(Instructions on page 2)
Roswell Controlled Water Basin

SEE ATTACHED FOR CONDITIONS OF APPROVAL

Approval Subject to General Requirements & Special Stipulations Attached



Drilling Plan ConocoPhillips Company Maljamar; Grayburg-San Andres, Yeso (west)

Ruby Federal #33

Lea County, New Mexico

1. Estimated tops of geological markers and estimated depths to water, oil, or gas formations:

The datum for these depths is RKB (which is 13' above Ground Level).

Formations	Top Depth FT TVD	Top Depths FT MD	Contents
Quaternary	Surface	Surface	Fresh Water
Rustler	715	715	Anhydrite
Salado (top of salt)	887	887	Salt
Tansill (base of salt)	1882	1882	Gas, Oil and Water
Yates	2082	2082	Gas, Oil and Water
Seven Rivers	2372	2373	Gas, Oil and Water
Queen	3015	3025	Gas, Oil and Water
Grayburg	3451	3468	Gas, Oil and Water
San Andres	3805	3827	Gas, Oil and Water
Glorieta	5275	5314	Gas, Oil and Water
Paddock	_ 5351	5390	Gas, Oil and Water
Blinebry	5730	5769	Gas, Oil and Water
Tubb	6739	6778	Gas, Oil and Water
Deepest estimated perforation	6739	6778	Deepest estimated perf. is ~ Top of Tubb
Total Depth (maximum)	6939	6978	200' below deepest estimated perforation

All of the water bearing formations identified above will be protected by setting of the <u>8-5/8</u> surface casing <u>25' – 70' into the Rustler formation</u> and circulating of cement from casing shoe to surface in accordance with the provisions of Onshore Oil and Gas Order No. 2 and New Mexico Oil Conservation Division Title 19.

The targeted oil and gas bearing formations identified above will be protected by setting of the ____5-1/2" production casing ____10' off bottom of TD ___ and circulating of cement from casing shoe to surface in accordance with the provisions of Onshore Oil and Gas Order No. 2 and New Mexico Oil Conservation Division Title 19.

Ruby Federal #33 (Date: 8/8/2013) Page 1 of 9

2. Proposed casing program:

Type	Hole Size	, M	Interval D RKB (ft)	OD	Wt	Gr	Conn	MIY	Col	Jt Str	l	Safety Fac lated per Co Corporate C	nocoPhillips
rype	(in)	From	То	(inches)	(lb/ft)	Gi	Com	(psi)	(psi)	(klbs)	Burst DF	Collapse DF	Jt Str DF (Tension) Dry/Buoyant
Cond	20	0	40' – 85' (30' – 75' BGL)	16	0.5" wall	В	Line Pipe	N/A	N/A	N/A	NA	NA	NA .
Alt. Cond	20	0	40' – 85' (30' – 75' BGL)	13-3/8	48#	H-40	PE	1730	740	N/A	NA	NA	NA
Surf	12-1/4	0	740' – <u>785'</u>	8-5/8	24#	J-55	STC	2950	1370	244	1.60	3.93	3.67
Prod	7-7/8	0	6923' – 6968'	5-1/2	17#	L-80	LTC	7740	6290	338	2.14	2.52	2.00

The casing will be suitable for H₂S Service. All casing will be new.

The surface and production casing will be set approximately 10' off bottom and we will drill the hole with a 45' range uncertainty for casing set depth to fit the casing string so that the cementing head is positioned at the floor for the cement job.

The production casing will be set 155' to 200' below the deepest estimated perforation to provide rathole for the pumping completion and for the logs to get deep enough to log the interval of interest.

Casing Safety Factors - BLM Criteria:

Type	Depth	Wt	MIY	Col	Jt Str	Drill Fluid	Burst	Collapse	Tensile-Dry	Tens-Bouy
Surface Casing	785	24	2950	1370	244000	8.5	8.50	3.95	13.0	14.9
Production Casing	6977	17	7740	6290	338000	10	2.14	1.74	2.85	3.37

Casing Safety Factors – Additional ConocoPhillips Criteria:

ConocoPhillips casing design policy establishes Corporate Minimum Design Factors (see table below) and requires that service life load cases be considered and provided for in the casing design.

ConocoPhillips Corporate Criteria for Minimum Design Factors

	Control Timps Corporate on	tona for full inflam Boolgit Lasters		
	Burst	Collapse	Axial	
Casing Design Factors	1.15	1.05	1.4	

Ruby Federal #33 (Date: 8/8/2013) Page 2 of 9

Pipe Yield MW Type Conductor Wit Depth MIY Col Jt Str Burst Col Ten 85 432966 Surface Casing (8-5/8" 24# J-55 STC) 1370 244000 381000 Production Casing (5-1/2" 17# L-80 LTC) 6968 6290 397000 338000 Burst - ConocoPhillips Required Load Cases The maximum internal (burst) load on the Surface Casing occurs when the surface casing is tested to 1500 psi (as per BLM Onahore Order 2 - IL Requirements). The maximum internal (burst) load on the Production Casing occurs during the fracture stimulation where the maximum allowable working pressure (MANVP) is the pressure that would fit ConocoPhttipa Corporate Criteria for Minimum Factors. Surface Casing Test Pressure = 1500 psi Predicted Pore Pressure at TD (PPTD) = Surface Rated Working Pressure (BOPE) = 3000 psi Predicted Frac Gradient at Shoe (CSFG) = 19.23 ppg 10 ppg Field SW = Surface Casing Burst Safety Factor = API Burst Rating / Maximum Predicted Surface Pressure (MPSP) 'OR' Maximum Allowable Surface Pressure (MASP) Production Casing MAWP for the Fracture Stimulation = API Burst Rating / Corporate Minimum Burst Design Factor Surface Casing Burst Safety Factor: Case #1. MPSP (MWhyd next section) = 785 0.052 10 408 Case #2. MPSP (Field SW @ Bullhead_{CSFS} + 200 psi) = 785 0.052 19.23 408 200 577 Case #3. MPSP (Kick Vol @ next section TD) =

Case #4. MPSP (PPTD - GG) = 6968 0.052 x 8 55 6183 347 2177 6968 0.052 8.55 2401 696.8 Case #3 & #4 Limited to MPSP (CSFG + 0.2 ppg) = 0.052 19.23 MASP (MWhyd + Test Pressure) = 785 0.052 8.5 1500 1847 Burst Safety Factor (Max. MPSP or MASP) = 2950 1847 1.60 **Production Casing Burst Safety Factor:** Case #1. MPSP (MWhyd TD) = 6968 0.052 10 3623.36 Case #4. MPSP (PPTD - GG) = 6968 0.052 8 55 696.8 2401 Burst Safety Factor (Max. MPSP) = 7740 2.14 3623 MAWP for the Fracture Stimulation (Corporate Criteria) = 1.15 Collapse ~ ConocoPhillips Required Load Cases The maximum collapse load on the Surface Casing occurs when cementing to surface, 1/3 evacuation to the next casing setting depth, or deepest depth of exposure (full evacuation). The maximum collapse load on the Production Casing occurs when cementing to surface, or 1/3 evacuation to the deepest depth of exposure; and therefore, the external pressure profile for the evacuation cases should be equal to the pore pressure of the horizons on the outside of the casing which we assumed to be PPTD. Surface Casing Collapse Safety Factor = API Collapse Rating / Full Evacuation 'OR' Cement Displacement during Cementing to Surface Production Casing Collapse Safety Factor = API Collapse Rating / Maximum Predicted Surface Pressure 'OR' Cement Displacement during Cementing to Surface 8.34 ppg 13.6 ppg 14.6 ppg Cement Displacement Fluid (FVV) = Top of Cement = Cement to Surface 11.8 ppg Surface Cement Lead = Prod Cement Lead = 16.4 ppg Surface Cement Tail = Prod Cement Tail = Top of Surface Tel Cement = 300 n Top of Prod Tail Cement = 5200 Surface Casing Collapse Safety Factor: Full Evacuation Diff Pressure = 0.052 785 8.55 349 Cementing Diff Lift Pressure = 0.052 300 0.052 340] = 233 1370 3.93 Collapse Safety Factor = Production Casing Collapse Safety Factor: 1/3 Evacuation Diff Pressure = 6968 0.052 8.34)] = 2091 3022] Cementing Diff Lift Pressure = 1766 0.052 11.8 5200 0.052 6290 2498 2.52 Collapse Safety Factor = 1 Tensial Strength - ConocoPhillips Required Load Cases The maximum axial (tension) load occurs if casing were to get stuck and pulled on to try to get it unstuck. Maximum Allowable Axial Load for Pipa Yield = API Pipe Yield Strength Rating / Corporate Minimum Axial Design Factor Maximum Allowable Axial Load for Joint = API Joint Strength Rating / Corporate Minimum Axial Design Factor Maximum Allowable Hook Load (Limited to 75% of Rig Max Load) = Maximum Allowable Axial Load Maximum Allowable Overpull Margin = Maximum Allowable Hook Load - Bouyant Wt of the String Tensial Safety Factor = API Pipe Yield 'O'R. API Joint Strength 'OR' Rig Max Load Rating / (Bouyant Wit of String + Minimum Overpuit Required)

... Rig Max Load (300,000 lbs) x 75% = ... 225000 lbs

Minimum Overpuit Required = 50000 lbs Surface Casing Tensial Strength Safety Factor: Air Wt = 18840 18840 Bouyant Wt = 0.870 16395 Max. Allowable Axial Load (Pipe Yield) = 381000 1.40 272143 Max. Allowable Axial Load (Joint) = 244000 174286 1.40 Max. Allowable Hook Load (Limited to 75% of Rig Max Load) = 174286 Max. Allowable Overpull Margin = 174286 18840 157891 0.870 Tensial Safety Factor = 244000 16395 50000 3.67 Production Casing Tensial Strength Safety Factor: Air Wt = 118456 Bouyant Wt = 118456 0.847 100371 Max. Allowable Axial Load (Pipe Yield) = 397000 283571 1.40 Max. Allowable Axial Load (Joint) = 338000 1.40 Max. Allowable Hook Load (Limited to 75% of Rig Max Load) = 225000 Max. Allowable Overpull Margin = 118456 0.847 124629 225000 Tensial Safety Factor = 100371 Compression Strength - ConocoPhillips Required Load Cases The maximum axial (compression) load for the well is where the surface casing is landed on the conductor with a support of a plate or landing ring. The surface casing is also calculated to bear 60% of the load but not limited. Any other axial loads such as a snubbing unit or other would need to be added to the load, Compression Safety Factor = API Axial Joint Strength Rating 'OR' API Axial Pipe Yield Rating / Maximum Predicted Load 3000 bs *Conductor & Surface Compression Safety Factor Surf Casing Wt (Bouyant) = 18840 0.870 16395 х Prod Casing Wt (Bouyant) = 118456 0.847 100371 Tubing Wt (Air Wt) = 6968 6.5 0.052 Tubing Fluid Wt = 6968 0.7854 2.441 42 = 11107 Load on Conductor = 3000 45292 176165 Conductor Compression Safety Factor = 432966 Coad on Surface Casing Compression Safety Factor = Ruby Federal #33 176165 60% 105699 244000 105699 (Date: 8/8/2013) Page 3 of 9

3. Proposed cementing program:

16" or 13-3/8" Conductor:

Cement to surface with rathole mix, ready mix or Class C Neat cement. (Note: The gravel used in the cement is not to exceed 3/8" diameter) TOC at surface.

8-5/8" Surface Casing Cementing Program:

The intention for the cementing program for the Surface Casing is to:

- Place the Tail Slurry from the casing shoe to 300' above the casing shoe,
- Bring the Lead Slurry to surface.

Spacer: 20 bbls Fresh Water

	Slurry	Inter Ft I		Weight ppg	Sx	Vol Cuft	Additives	Yield ft³/sx
Lead	Class C	Surface	440' – 485'	13.6	300	510	2% Extender 2% CaCl ₂ 0.125 lb/sx LCM if needed 0.2% Defoamer Excess =75% based on gauge hole volume	1.70
Tail	Class C	440' – 485'	740' – 785'	14.8	200	268	1% CaCl2 Excess = 100% based on gauge hole volume	1.34

Displacement: Fresh Water.

Note: In accordance with the Pecos District Conditions of Approval, we will Wait on Cement (WOC) for a period of not less than 18 hrs after placement or until at least 500 psi compressive strength has been reached in both the Lead Slurry and Tail Slurry cements on the Surface Casing, whichever is greater.

5-1/2" Production Casing & Cementing Program:

The intention for the cementing program for the Production Casing is to:

- Place the Tail Slurry from the casing shoe to a point approximately 200' above the top of the Paddock,
- Bring the Lead Slurry to surface.

Spacer: 20 bbls Fresh Water

	Slurry	1 '	rvals MD	Weight ppg	Sx	Vol Cuft	Additives	Yield ft³/sx
Lead	50:50 Poz/C	Surface	5200'	11.8	700	1820	10% Bentonite 5% Salt 0.2%-0.4% Fluid loss additive 0.125 lb/sx LCM if needed Excess = 220% or more if needed based on gauge hole volume	2.6
Tail	Class H	5200'	6923' – 6968'	16.4	400	428	0.2% Fluid loss additive 0.3% Dispersant 0.15% Retarder 0.2% Antifoam Excess = 100% or more if needed based on gauge hole volume	1.07

Displacement: Fresh Water with approximately 250 ppm gluteraldehyde biocide.

Ruby Federal #33 (Date: 8/8/2013) Page 4 of 9

5-1/2" Production Casing & Cementing Program - TXI/LW Cementing Option for Grayburg-San Andres:

ConocoPhillips Company respectfully requests the options to our cementing program. This option will only be implemented in the cementing operation of wells requesting for co-mingling after approval and authorization by all agencies have been obtained. The intention for the alternative option to the cementing program for the Production Casing is to:

- Accommodate the additional frac'ing and stimulation of the Grayburg-San Andres by placement of the Tail Slurry from the casing shoe to the top of the Grayburg-San Andres formation,
- Bring the Lead Slurry to surface.

Spacer: 20 bbls Fresh Water

. .

	Slurry		rvals MD	Weight ppg	Sx	Vol Cuft	Additives	Yield ft³/sx
Lead	50:50 Poz/C	Surface	3000,	11.8	500	1300	10% Bentonite 8 lbs/sx Salt 0.2%-0.4% Fluid loss additive 0.125 lb/sx LCM if needed Excess = 200% or more if needed based on gauge hole volume	2.6
Tail	TXI/LW	3000'	6923' – 6968'	13.2	800	1120	0.5% Fluid loss additive 0.10% Retarder 0.2% Antifoam 0.125 lb/sx LCM if needed Excess = 150% or more if needed based on gauge hole volume	1.40

Displacement: Fresh Water with approximately 250 ppm gluteraldehyde biocide.

Proposal for Option to Adjust Production Casing Cement Volumes:

The production casing cement volume presented above are estimates based on gauge 7-7/8" hole. We will adjust these volumes based on the caliper log data for each well and our trends for amount of cement returns to surface. Also, if no caliper log is available for any particular well, we would propose an option to possibly increase the production casing cement volume to account for any uncertainty in regard to the hole volume.

Ruby Federal #33 (Date: 8/8/2013) Page 5 of 9

4. Pressure Control Equipment:

A <u>11" 3M</u> system will be installed, used, maintained, and tested accordingly as described in Onshore Oil and Gas Order No. 2.

Our BOP equipment will be:

- Rotating Head
- o Annular BOP, 11" 3M
- o Blind Ram, 11" 3M
- o Pipe Ram, 11" 3M

After nippling up, and every 30 days thereafter or whenever any seal subject to test pressure is broken followed by related repairs, blowout preventors will be pressure tested. BOP will be inspected and operated at least daily to insure good working order. All pressure and operating tests will be done by an independent service company and recorded on the daily drilling reports. BOP will be tested using a test plug to isolate BOP stack from casing. BOP test will include a low pressure test from 250 to 300 psi for a minimum of 10 minutes or until requirements of test are met, whichever is longer. Ram type preventers and associated equipment will be tested to the approved stack working pressure of 3000 psi isolated by test plug. Annular type preventers will be tested to 50 percent of rated working pressure, and therefore will be tested to 1500 psi. Pressure will be held for at least 10 minutes or until provisions of test are met, whichever is longer. Valve on casing head below test plug will be open during testing of BOP stack. BOP will comply with all provisions of Onshore Oil and Gas Order No. 2 as specified. See Attached BOPE Schematic. A variance is respectfully requested to allow for the use of flexible hose. The variance request is included as a separate enclosure with attachments.

5. Proposed Mud System:

The mud systems that are proposed for use are as follows:

DEPTH	TYPE	Density ppg	FV sec/qt	API Fluid Loss cc/30 min	рН	Vol bbl
0 – Surface Casing Point	Fresh Water or Fresh Water Native Mud in Steel Pits	8.5 – 9.0	28 – 40	N.C.	N.C.	120 – 160
Surface Casing Point to TD	Brine (Saturated NaCl ₂) in Steel Pits	10	29	N.C.	10 – 11	500 – 1000
Conversion to Mud at TD	Brine Based Mud (NaCl ₂) in Steel Pits	10	33 – 40	5 – 10	10 – 11	0 – 750

Gas detection equipment and pit level flow monitoring equipment will be on location. A flow paddle will be installed in the flow line to monitor relative amount of mud flowing in the non-pressurized return line. Mud probes will be installed in the individual tanks to monitor pit volumes of the drilling fluid with a pit volume totalizer. Gas detecting equipment and H2S monitor alarm will be installed in the mud return system and will be monitored. A mud gas separator will be installed and operable before drilling out from the Surface Casing. The gases shall be piped into the flare system. Drilling mud containing H2S shall be degassed in accordance with API RP-49, item 5.14.

In the event that the well is flowing from a waterflow, then we would discharge excess drilling fluids from the steel mud pits through a fas-line into steel frac tanks at an offset location for containment. Depending on the rate of waterflow, excess fluids will be hauled to an approved disposal facility, or if in suitable condition, may be reused on the next well.

No reserve pit will be built.

Proposal for Option to Not Mud Up at TD:

FW, Brine, and Mud volume presented above are estimates based on gauge 12-1/4" or 7-7/8" holes. We will adjust these volume based on hole conditions. We do not plan to keep any weighting material at the wellsite. Also, we propose an option to not mud up leaving only brine in the hole if we have good hole stability.

Ruby Federal #33 (Date: 8/8/2013) Page 6 of 9

6. Logging, Coring, and Testing Program:

- a. No drill stem tests will be done
- b. Remote gas monitoring planned for the production hole section (optional).
- c. No whole cores are planned
- d. The open hole electrical logging program is planned to be as follows:
 - Total Depth to 2500': Resistivity, Density, and Gamma Ray
 - Total Depth to surface Casing Shoe: Caliper
 - Total Depth to surface, Gamma Ray and Neutron
 - Formation pressure data (XPT) on electric line if needed (optional)
 - Rotary Sidewall Cores on electric line if needed (optional)
 - BHC or Dipole Sonic if needed (optional)
 - Spectral Gamma Ray if needed (optional)

7. Abnormal Pressures and Temperatures:

- No abnormal pressures are expected to be encountered.
- Loss of circulation is a possibility in the horizons below the Top of Grayburg. We expect that normal Loss of Circulation Material will be successful in healing any such loss of circulation events.
 - o The bottom hole pressure is expected to be 8.55 ppg gradient.
 - o The expected Bottom Hole Temperature is 115 degrees F.
- The estimated H₂S concentrations and ROE calculations for the gas in the zones to be penetrated are presented in the table below for the various producing horizons in this area:

FORMATION / ZONE	H2S (PPM)	Gas Rate (MCFD)	ROE 100 PPM	ROE 500 PPM
Grayburg / San Andres (from MCA)	14000	38	59	27
Yeso Group	400	433	34	15

ConocoPhillips will comply with the provisions of Oil and Gas Order # 6, Hydrogen Sulfide Operations. Also, ConocoPhillips will provide an H2S Contingency Plan (please see copy attached) and will keep this plan updated and posted at the wellsite during the drilling operation.

8. Anticipated starting date and duration of operations:

Well pad and road constructions will begin as soon as all agency approvals are obtained. Anticipated date to drill this well as early as 2014 after receiving approval of the APD.

Attachments:

- Attachment # 1 BOP and Choke Manifold Schematic 3M System
- Attachment # 2 Diagram of Choke Manifold Equipment

Contact Information:

Proposed 8 August 2013 by: James Chen Drilling Engineer, ConocoPhillips Company Phone (832) 486-2184 Cell (832) 768-1647

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ConocoPhillips MCBU

Buckeye Ruby Federal Ruby Federal 33

Original Hole

Plan: S-Shape Plan

Standard Planning Report - Geographic

05 August, 2013

Planning Report - Geographic

EDM Central Planning Well Ruby Federal 33 Database: ocal Co-ordinate Reference: ConocoPhillips MCBU TVD Reference: Company: RKB @ 3983.0usft (PD 822) Buckeye RKB @ 3983.0usft (PD 822) Project: MD Reference: Ruby Federal Site: North Reference: Grid Survey Calculation Method: Minimum Curvature Ruby Federal 33 Well: Original Hole Wellbore: Design: S-Shape Plan

Project Buckeye, Lea County, NM

Map System: US State Plane 1927 (Exact solution)

Geo Datum: NAD 1927 (NADCON CONUS)

Map Zone: New Mexico East 3001

Svstem Datum:

Mean Sea Level

Using geodetic scale factor

Ruby Federal, New Mexico, Southeast Site Northing: 666,097.48 usft 32° 49' 48.040 N Latitude: Site Position 666,763.63 usft 103° 47' 25.559 W From: Lat/Long Easting: Longitude: Position Uncertainty: 3.5 usft Slot Radius: 0.29

Ruby Federal 33, Deviated Well Well 0.0 usft Northing: 668,652.10 usft 32° 50' 13.500 N Well Position +N/-S Latitude: 103° 48' 7.950 W +E/-W 0.0 usft Easting: 663,133.60 usft Longitude: Position Uncertainty 0.0 usft Wellhead Elevation: Ground Level: 3,970.0 usft

 Wellbore
 Original Hole

 Magnetics
 Model Name
 Sample Date
 Declination (°)
 Dip Angle (nT)

 BGGM2012
 8/5/2013
 7.58
 60.60
 48,714

Design · S-Shape Plan Audit Notes: Version: Phase: **PROTOTYPE** Tie On Depth: +N/-S +E/-W Vertical Section: Depth From (TVD) Direction (usft) (usft) (usft) (°) 0.0 0.0 0.0 176.10

Measured			Vertical			Dogleg	Build	Turn		
Depth (usft)	Inclination (°)	Azimuth (°)	Depth (usft)	+N/-S (usft)	+E/-W (usft)	Rate (°/100usft)	Rate (°/100usft)	Rate (°/100usft)	TFO (°)	Target
0.0	0.00	0.00	0.0	0.0	0.0	0.00	0.00	0.00	0.00	
1,882.0	0.00	0.00	1,882.0	0.0	0.0	0.00	0.00	0.00	0.00	
2,538.8	9.85	176,10	2,535.6	-56.2	3.8	1.50	1.50	0.00	176.10	
4,733.0	9.85	176.10	4,697.4	-430.8	29.3	0.00	0.00	0.00	0.00	
5,389.8	0.00	0.00	5,351.0	-487.0	33.2	1.50	-1.50	0.00	180.00	Ruby Federal 33 (F
6,977.8	0.00	0.00	6,939.0	-487.0	33.2	0.00	0.00	0.00	0.00	

Planning Report - Geographic

терия и деятельного было до доборовать в принце EDM Central Planning Database: Local Co-ordinate Reference: Well Ruby Federal 33 Company: ConocoPhillips MCBU TVD Reference: RKB @ 3983.0usft (PD 822) Buckeye MD Reference: Project: RKB @ 3983 Ousft (PD 822) Ruby Federal Site: Grid Ruby Federal 33 Well: Survey Calculation Method: Minimum Curvature Wellbore: Original Hole S-Shape Plan

leasure	d .	· .	Vertical	•		Map	Мар	$\mathcal{L}_{\mathcal{L}}}}}}}}}}$	
Depth	Inclination	Azimuth	Depth	+N/-S	+E/-W	Northing	Easting		
(usft)	(°)	(°)	(usft)	(usft)	(usft)	(usft)	(usft)	Latitude	Longitude
(0.00	0.00	0.0	0.0	0.0	668,652.10	663,133.60	32° 50' 13.500 N	103° 48' 7
79	0.00	0.00	79.0	0.0	0.0	668,652.10	663,133.60	32° 50' 13.500 N	103° 48' 7
Cond	uctor		•			,			
100	0.00	0.00	100.0	0.0	0.0	668,652.10	663,133.60	32° 50' 13.500 N	103° 48' 7
200	0.00	0.00	200.0	0.0	0.0	668,652.10	663,133.60	32° 50' 13.500 N	103° 48' 7
300		0.00	300.0	0.0	0.0	668,652.10	663,133.60	32° 50′ 13.500 N	103° 48' 7
400		0.00	400.0	0.0	0.0	668,652.10	663,133.60	32° 50' 13.500 N	103° 48' 7
500		0.00	500.0	0.0	0.0	668,652.10	663,133.60	32° 50′ 13.500 N	103° 48' 7
600		0.00	600.0	0.0	0.0	668,652.10	663,133.60	32° 50′ 13.500 N	103° 48' 7
700		0.00	700.0	0.0	0.0	668,652.10	663,133.60	32° 50' 13.500 N	103° 48' 7
715	0.00	0.00	715.0	0.0	0.0	668,652.10	663,133.60	32° 50′ 13.500 N	103° 48' 7.
Rustle									
785	5.0 0.00	0.00	785.0	0.0	0.0	668,652.10	663,133.60	32° 50′ 13.500 N	103° 48' 7.
Surfa	ce				•		,		
800	0.00	0.00	800.0	0.0	0.0	668,652.10	663,133.60	32° 50' 13.500 N	103° 48' 7.
887	0.00	0.00	887.0	0.0	0.0	668,652.10	663,133.60	32° 50′ 13.500 N	103° 48' 7.
Salad	0								
900	0.00	0.00	900.0	0.0	0.0	668,652.10	663,133.60	32° 50' 13.500 N	103° 48' 7.
1,000	0.00	0.00	1,000.0	0.0	0.0	668,652.10	663,133.60	32° 50′ 13.500 N	103° 48' 7.
1,100	0.00	0.00	1,100.0	0.0	0.0	668,652.10	663,133.60	32° 50′ 13.500 N	103° 48' 7.
1,200	0.00	0.00	1,200.0	0.0	0.0	668,652.10	663,133.60	32° 50′ 13.500 N	103° 48' 7.
1,300	0.00	0.00	1,300.0	0.0	0.0	668,652.10	663,133.60	32° 50′ 13.500 N	103° 48' 7.
1,400	0.00	0.00	1,400.0	0.0	0.0	668,652.10	663,133.60	32° 50′ 13.500 N	103° 48' 7.
1,500	0.00	0.00	1,500.0	0.0	0.0	668,652.10	663,133.60	32° 50′ 13.500 N	103° 48' 7.
1,600	0.00	0.00	1,600.0	0.0	0.0	668,652.10	663,133.60	32° 50' 13.500 N	103° 48' 7.
1,700	0.00	0.00	1,700.0	0.0	0.0	668,652.10	663,133.60	32° 50′ 13.500 N	103° 48' 7.
1,800	0.00	0.00	1,800.0	0.0	0.0	668,652.10	663,133.60	32° 50' 13.500 N	103° 48' 7.
1,882	0.00	0.00	1,882.0	0.0	0.0	668,652.10	663,133.60	32° 50′ 13.500 N	103° 48' 7.
Tansi	ij						and the second section and the second section is the second section of the second section sect		
1,900	0.0 0.27	176.10	1,900.0	0.0	0.0	668,652.05	663,133.61	32° 50' 13.500 N	103° 48' 7.
2,000	1.0 1.77	176.10	2,000.0	-1.8	0.1	668,650.28	663,133.73	32° 50' 13.482 N	103° 48' 7.
2,082	2.1 3.00	176.10	2,082.0	-5.2	0.4	668,646.87	663,133.96	32° 50' 13.448 N	103° 48' 7.
Yates									
2,100	0.0 3.27	176.10	2,099.9	-6.2	0.4	668,645.89	663,134.02	32° 50′ 13.439 N	103° 48' 7.
2,200	0.0 4.77	176.10	2,199.6	-13.2	0.9	668,638.90	663,134.50	32° 50′ 13.369 N	103° 48' 7.
2,300	0.0 6.27	176.10	2,299.2	-22.8	1.6	668,629.30	663,135.15	32° 50' 13.274 N	103° 48' 7.
2,373	.4 7.37	176.10	2,372.0	-31.5	2.1	668,620.61	663,135.75	32° 50' 13.188 N	103° 48' 7.
Seven	Rivers					•			
2,400	.0 7.77	176.10	2,398.4	-35.0	2.4	668,617.11	663,135,99	32° 50' 13.154 N	103° 48' 7.
2,500	.0 9.27	176.10	2,497.3	-49.8	3.4	668,602.33	663,136.99	32° 50' 13.007 N	103° 48' 7.
2,538		176.10	2,535.6	-56.2	3.8	668,595.90	663,137.43	32° 50′ 12.944 N	103° 48' 7.
2,600	9.85	176.10	2,595.9	-66.6	4.5	668,585.45	663,138.14	32° 50′ 12.840 N	103° 48' 7.
2,700		176.10	2,694.4	-83.7	5.7	668,568.38	663,139.30	32° 50' 12.671 N	103° 48' 7.
2,800		176.10	2,792.9	-100.8	6.9	668,551.31	663,140.47	32° 50′ 12.502 N	103° 48' 7.
2,900	.0 9.85	176.10	2,891.4	-117.9	8.0	668,534.24	663,141.63	32° 50′ 12.333 N	103° 48' 7.
3,000	.0 9.85	176.10	2,990.0	-134.9	9.2	668,517.17	663,142.79	32° 50′ 12.164 N	103° 48' 7.
3,025	.4 9.85	176.10	3,015.0	-139.3	9.5	668,512.84	663,143.09	32° 50′ 12.122 N	103° 48' 7.
Queer)								,
3,100	.0 9.85	176.10	3,088.5	-152.0	10.4	668,500.10	663,143.95	32° 50′ 11.996 N	103° 48' 7.
3,200	.0 9.85	176.10	3,187.0	-169.1	11.5	668,483.03	663,145.12	32° 50' 11.827 N	103° 48′ 7.
3,300	.0 9.85	176.10	3,285.5	-186.1	12.7	668,465.96	663,146.28	32° 50' 11.658 N	103° 48' 7.8
3,400	.0 9.85	176.10	3,384.1	-203.2	13.8	668,448.89	663,147.44	32° 50' 11,489 N	103° 48' 7.8

Design:

Planning Report - Geographic

Database: Company:

EDM Central Planning

ConocoPhillips MCBU

Project: Site:

Buckeye

Ruby Federal Well: Ruby Federal 33 Original Hole Wellbore: S-Shape Plan Design:

¹ Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

to describe the management of the companies of the contract of Well Ruby Federal 33

RKB @ 3983.0usft (PD 822) RKB @ 3983.0usft (PD 822)

Grid

Minimum Curvature

Planned	Survey

Vieasured : Depth (usft)	Inclination	Azimuth	Vertical Depth (usft)	+N/-S	+E/-W	Map Northing	Map Easting	:	
(usit)	(°)	(°)	(usit)	(usft)	(usft)	(usft)	(usft)	Latitude	Longitude
3,467.9	9.85	176.10	3,451.0	-214.8	14.6	668,437.30	663,148.23	32° 50' 11.374 N	103° 48' 7.79
Grayburg									
3,500.0	9.85	176.10	3,482.6	-220.3	15.0	668,431.82	663,148.60	32° 50′ 11.320 N	103° 48′ 7.78
3,600.0	9.85	176.10	3,581.1	-237.4	16.2	668,414.75	663,149.77	32° 50′ 11.151 N	103° 48' 7.7
3,700.0	9.85	176.10	3,679.6	-254.4	17.3	668,397.68	663,150.93	32° 50′ 10.982 N	103° 48' 7.76
3,800.0	9.85	176.10	3,778.2	-271.5	18.5	668,380.61	663,152.09	32° 50' 10.813 N	103° 48' 7.7
3,827.2	9.85	176.10	3,805.0	-276.2	18.8	668,375.96	663,152.41	32° 50′ 10.767 N	103° 48' 7.74
San Andre	es								
3,900.0	9.85	176.10	3,876.7	-288.6	19.7	668,363.54	663,153.25	32° 50' 10.644 N	103° 48' 7.7
4,000.0	9.85	176.10	3,975.2	-305.6	20.8	668,346.47	663,154.42	32° 50′ 10.475 N	103° 48′ 7.72
4,100.0	9.85	176.10	4,073.7	-322.7	22.0	668,329.40	663,155.58	32° 50' 10.306 N	103° 48′ 7.7′
4,200.0	9.85	176.10	4,172.3	-339.8	23.1	668,312.33	663,156.74	32° 50' 10.137 N	103° 48' 7.69
4,300.0	9.85	176.10	4,270.8	'-356.9	24.3	668,295.26	663,157.90	32° 50' 9.968 N	103° 48' 7.68
4,400.0	9.85	176.10	4,369.3	-373.9	25.5	668,278.19	663,159.07	32° 50' 9.799 N	103° 48' 7.67
4,500.0	9.85	176.10	4,467.8	-391.0	26.6	668,261.12	663,160.23	32° 50' 9.630 N	103° 48' 7.66
4,600.0	9.85	176.10	4,566.4	-408.1	27.8	668,244.05	663,161.39	32° 50' 9.461 N	103° 48' 7.64
4,700.0	9.85	176.10	4,664.9	-425.1	29.0	668,226.98	663,162.56	32° 50' 9.292 N	103° 48' 7.60
4,733.0	9.85	176,10	4,697.4	-430.8	29.3	668,221.35	663,162.94	32° 50' 9.236 N	103° 48' 7.63
4,800.0	8.85	176.10	4,763.5	-441.6	30.1	668,210.49	663,163.68	32° 50' 9.129 N	103° 48' 7.62
4,900.0	7.35	176.10	4,862.5	-455.7	31.0	668,196.44	663,164.64	32° 50' 8.990 N	103° 48' 7.61
5,000.0	5.85	176.10	4,961.9	-467.1	31.8	668,184.98	663,165,42	32° 50' 8.876 N	103° 48' 7.60
5,100.0	4.35	176.10	5,061.5	-476.0	32,4	668,176.11	663,166.02	32° 50' 8.789 N	103° 48' 7.59
5,200.0	2.85	176.10	5,161.3	-482.3	32.8	668,169.85	663,166.45	32° 50' 8.727 N	103° 48' 7.59
5,300.0	1.35	176.10	5,261.2	-485.9	33.1	668,166.20	663,166.69	32° 50' 8.690 N	103° 48' 7.59
5,313.8	1.14	176.10	5,275.0	-486.2	33.1	668,165.90	663,166.72	32° 50' 8.687 N	103° 48' 7.59
Glorieta			0,270.0	,,,,,	• • • • • • • • • • • • • • • • • • • •	000,100.00	000,100.72	02 00 0.001 11	100 40 1.00
5,389.8	0.00	0.00	5,351.0	-487.0	33.2	668,165.15	662 466 77	20% £01 0 C00 N	1029 1017 50
	0.00	0.00	3,331.0	-407.0	33.2	000,100,10	663,166.77	32° 50' 8.680 N	103° 48' 7.59
Paddock	0.00		5 004 0	407.0		200 105 15			
5,400.0	0.00	- 0.00	5,361.2	-487.0	33.2	668,165.15	663,166.77	32° 50' 8.680 N	103° 48' 7.59
5,500.0	0.00	0.00	5,461.2	-487.0	33.2	668,165.15	663,166.77	32° 50' 8.680 N	103° 48' 7.59
5,600.0	0.00	0.00	5,561.2	-487.0	33.2	668,165.15	663,166.77	32° 50′ 8.680 N	103° 48' 7.59
5,700.0	0.00	0.00	5,661.2	-487.0	33.2	668,165.15	663,166.77	32° 50′ 8.680 N	103° 48' 7.59
5,768.8	0.00	0.00	5,730.0	-487.0	33.2	668,165.15	663,166.77	32° 50′ 8.680 N	103° 48' 7.59
Blinebry									
5,800.0	0.00	0.00	5,761.2	-487.0	33.2	668,165.15	663,166.77	32° 50' 8.680 N	103° 48' 7.59
5,900.0	0.00	0.00	5,861.2	-487.0	33.2	668,165.15	663,166.77	32° 50' 8.680 N	103° 48' 7.59
6,000.0	0.00	0.00	5,961.2	-487.0	33.2	668,165.15	663,166.77	32° 50' 8.680 N	103° 48' 7.59
6,100.0	0.00	0.00	6,061.2	-487.0	33.2	668,165.15	663,166.77	32° 50' 8.680 N	103° 48' 7.59
6,200.0	0.00	0.00	6,161.2	-487.0	33.2	668,165.15	663,166.77	32° 50' 8.680 N	103° 48' 7.59
6,300.0	0.00	0.00	6,261.2	-487.0	33.2	668,165.15	663,166.77	32° 50′ 8.680 N	103° 48' 7.59
6,400.0	0.00	0.00	6,361.2	-487.0	33.2	668,165.15	663,166.77	32° 50′ 8,680 N	103° 48' 7.59
6,500.0	0.00	0.00	6,461.2	-487.0	33.2	668,165.15	663,166.77	32° 50′ 8.680 N	103° 48' 7.59
6,600.0	0.00	0.00	6,561.2	-487.0	33.2	668,165.15	663,166.77	32° 50' 8.680 N	103° 48' 7.59
6,700.0	0.00	0.00	6,661.2	-487.0	33.2	668,165.15	663,166.77	32° 50' 8.680 N	103° 48' 7.59
6,777.8	0.00	0.00	6,739.0	-487.0	33.2	668,165.15	663,166.77	32° 50′ 8.680 N	103° 48' 7.59
Tubb						•			
6,800.0	0.00	0.00	6,761.2	-487.0	33.2	668,165.15	663,166.77	32° 50' 8.680 N	103° 48' 7.59
6,900.0	0.00	0.00	6,861.2	-487.0	33.2	668,165.15	663,166.77	32° 50' 8.680 N	103° 48' 7.59
6,968.0	0.00	0.00	6,929.2	-487.0	33.2	668,165.15	663,166.77	32° 50' 8.680 N	103° 48' 7.59
Production 6,977.8		0.00	6,939.0	-487.0	33.2	668,165.15			
0,377.0	0.00	0.00	0,333.0	-40/.U	აა.∠	000,100.10	663,166.77	32° 50′ 8.680 N	103° 48' 7.59

Planning Report - Geographic

Database: Company:	EDM Central ConocoPhillip	- U			Local Co-or	dinate Reference:		Well Ruby Federal 33 RKB @ 3983.0usft (PD 822)			
Project:	Buckeye				MD Reference:			RKB @ 3983.0usft (PD 822)			
Site:	Ruby Federal				North Refer		Grid	. ,			
Well:	Ruby Federal	33			Survey Calo	ulation Method:	Minimum C				
Wellbore:	Original Hole				ginal Hole						
Design:	S-Shape Plan	l Anni anno atau - ta	and and the	_							
Design Targets				•••					*		
Target Name - hit/miss target - Shape	Dip Angle (°)	Dip Dir.	TVD (usft)	+N/-S (usft)	+E/-W (usft)	Northing (usft)	Easting (usft)	Latitude	Longitude		
Ruby Federal 33 (Pla - plan hits target - Circle (radius 0.	center	. 0.00	5,351.0	-487.0	33.2	668,165.15	663,166.77	32° 50' 8.680 N	103° 48' 7.590 V		

Casing Points				· ,			
	Measured Depth (usft)	Vertical Depth (usft)		Name	Casing Diameter (")	Hole Diameter (")	
	79.0	79.0	Conductor	And the second of the second o	16	20	****
	785.0	785.0	Surface		8-5/8	12-1/4	
	6,968.0	6,929.2	Production		5-1/2	7-7/8	

43.6

668,060.99

663,177.22

32° 50' 7.649 N

103° 48' 7.474 W

ormations		•	e e			
	Measured Depth (usft)	Vertical Depth (usft)	Name	Litt	Dip nology (°)	Dip Direction (°)
	715.0	714.0	Rustler		0.00	
	887.0	886.0	Salado		0.00	
	1,882.0	1,881.0	Tansill		0.00	
	2,082.1	2,081.0	Yates		0.00	
	2,373.4	2,371.0	Seven Rivers		0.00	
	3,025.4	3,014.0	Queen		. 0,00	
	3,467.9	3,450.0	Grayburg		0.00	
	3,827.2	3,804.0	San Andres		0.00	
	5,313.8	5,274.0	Glorieta		0.00	
	5,389.8	5,350.0	Paddock		0.00	
	5,768.8	5,729.0	Blinebry	•	0.00	
	6,777.8	6,738.0	Tubb		0.00	
	6,977.8	6,938.0	TD		0.00	

Ruby Federal 33 (Target

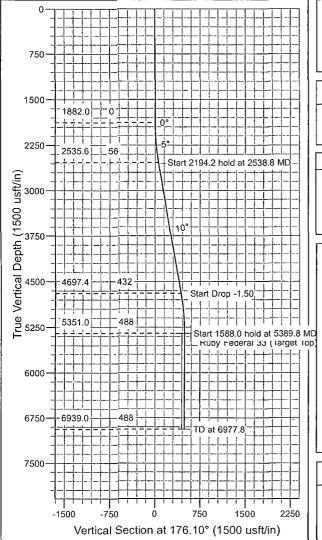
0.00

0.00 5,351.0 -591.1

- plan misses target center by 104.7usft at 5389.8usft MD (5351.0 TVD, -487.0 N, 33.2 E)
- Circle (radius 150.0)



Proposed Directional Well Plan

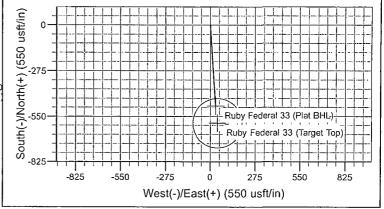


Project: Buckeye Site: Ruby Federal Well: Ruby Federal 33 Wellbore: Original Hole Design: S-Shape Plan

> WELL DETAILS: Ruby Federal 33 Ground Level: 3970.0

			COTION DETAIL O			_
0.0	0.0	668652.09			103° 48' 7.950 W	
+N/-S	+F/-\M	Northing	Easting	Latittude	Longitude	

L		SECTION DETAILS											
	Sec	MD	Inc	Azi	TVD	+N/-S	+E/-W	Dlea	TFace	VSect	Target		
1	1	0.0	0.00	0.00	0.0	0.0	0.0	0.00	0.00	0.0	_		
Т	2 188	32.0	0.00	0.00	1882.0	0.0	0.0	0.00	0.00	0.0			
1	3 25	38.8	9.85	176.10	2535.6	-56.2	3.8	1.50	176.10	56.3			
Т	4 47	33.0	9.85	176.10	4697.4	-430.8	29.3	0.00	0.00	431.8			
Т	5 53	89.8	0.00	0.00	5351.0	-487.0	33.2	1.50	180.00	488.1	Ruby Federal 33 (Plat BHL)		
l	6 69	77.8	0.00	0.00	6939.0	- 487.0	33.2	0.00	0.00	488.1	, ,		

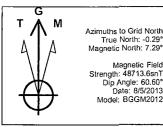


	CASING	DETAILS	
VD	MD	Name	Size
9.0	79.0	Conductor	16

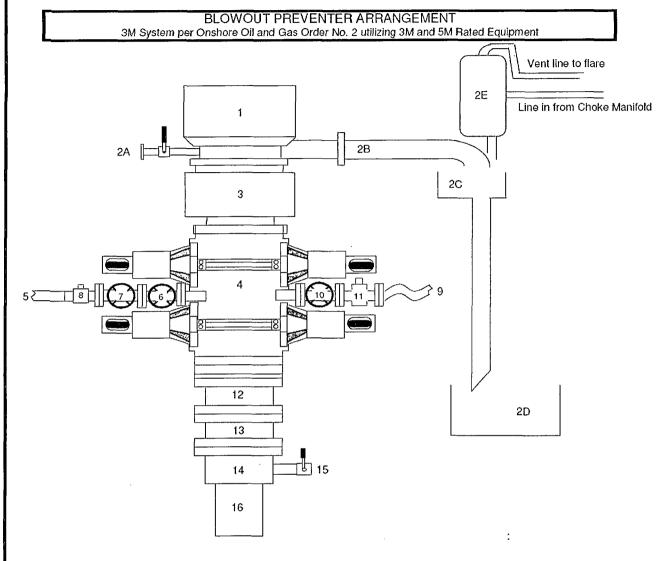
TVD 79.0 785.0	MD 79.0 785.0	Name Conductor Surface	16 8-5/8
6929.2	6968.0	Production	5-1/2

TVDPath	MDPath	Formation
714.0	715.0	Rustler
886.0	887.0	Salado
1881.0	1882.0	Tansill
2081.0	2082.1	Yates
2371.0	2373.4	Seven Rivers
3014.0	3025.4	Queen
3450.0	3467.9	Grayburg
3804.0	3827.2	San Andres
5274.0	5313.8	Glorieta
5350.0	5389.8	Paddock
5729.0	5768.8	Blinebry
6738.0	6777.8	Tubb
6938.0	6977.8	TD

FORMATION TOP DETAILS



Attachment # 1



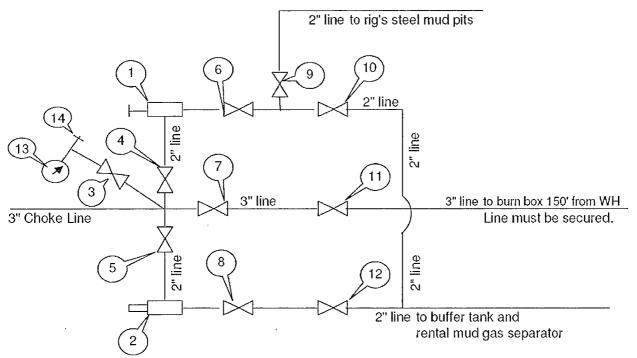
ltom	Description
Item	Description Retains the editors and the second sec
1	Rotating Head, 11"
2A	Fill up Line and Valve
2B	Flow Line (10")
2C	Shale Shakers and Solids Settling Tank
2D	Cuttings Bins for Zero Discharge
2E	Rental Mud Gas Separator with vent line to flare and return line to mud system
3	Annular BOP (11", 3M)
4	Double Ram (11", 3M, equipped with Blind Rams and Pipe Rams)
5	Kill Line (2" flexible hose, 3000 psi WP)
6	Kill Line Valve, Inner (3-1/8", 3000 psi WP)
7	Kill Line Valve, Outer (3-1/8", 3000 psi WP)
8	Kill Line Check Valve (2-1/16", 3000 psi WP
9	Choke Line (5M Stainless Steel Coflex Line, 3-1/8" 3M API Type 6B, 3000 psi WP)
10	Choke Line Valve, Inner (3-1/8", 3000 psi WP)
11	Choke Line Valve, Outer, (Hydraulically operated, 3-1/8", 3000 psi WP)
12	Adapter Flange (11" 5M to 11" 3M)
13	Spacer Spool (11", 5M)
14	Casing Head (11" 5M)
15	Ball Valve and Threaded Nipple on Casing Head Outlet, 2" 5M

Submitted by: James Chen, Drilling Engineer, Mid-Continent Business Unit, ConocoPhillips Company, 25-Sep-2012

Surface Casing

CHOKE MANIFOLD ARRANGEMENT

3M System per Onshore Oil and Gas Order No. 2 utilizing 3M and 5M Equipment



All Tees must be targeted

Item Description

- 1 Manual Adjustable Choke, 2-1/16", 3M
- 2 Remote Controlled Hydraulically Operated Adjustable Choke, 2-1/16", 3M
- 3 Gate Valve, 2-1/16" 5M
- 4 Gate Valve, 2-1/16" 5M
- 5 Gate Valve, 2-1/16" 5M
- 6 Gate Valve, 2-1/16" 5M
- 7 Gate Valve, 3-1/8" 3M
- 8 Gate Valve, 2-1/16" 5M
- 9 Gate Valve, 2-1/16" 5M
- 10 Gate Valve, 2-1/16" 5M
- 11 Gate Valve, 3-1/8" 3M
- 12 < Gate Valve, 2-1/16" 5M
- 13 Pressure Gauge
- 14 2" hammer union tie-in point for BOP Tester

We will test each valve to 3000 psi from the upstream side.

Submitted by:

James Chen

Drilling Engineer, Mid-Continent Business Unit, ConocoPhillips Company

Date: 21-March-2013

Ruby Federal #33 (Date: 8/8/2013) Page 9 of 9

Request for Variance

ConocoPhillips Company

Lease Number: NM LC 029405B

Well: Ruby Federal #33

Location: Sec. 18, T17S, R32E

Date: 6/14/2013

Request:

ConocoPhillips Company respectfully requests a variance to install a flexible choke line instead of a straight choke line prescribed in the Onshore Order No. 2, III.A.2.b Minimum standards and enforcement provisions for choke manifold equipment. This request is made under the provision of Onshore Order No. 2, IV Variances from Minimum Standard. The rig to be used to drill this well is equipped with a flexible choke line if the requested variance is approved and determined that the proposed alternative meets the objectives of the applicable minimum standards.

Justifications:

The applicability of the flexible choke line will reduce the number of target tees required to make up from the choke valve to the choke manifold. This configuration will facilitate ease of rig up and BOPE Testing.

Attachments:

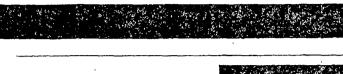
- Attachment # 1 Specification from Manufacturer
- Attachment # 2 Mill & Test Certification from Manufacturer

Contact Information:

Program prepared by: James Chen Drilling Engineer, ConocoPhillips Company Phone (832) 486-2184 Cell (832) 768-1647

Date: 26 September 2012











Reliance Eliminator Choke & Kill

This hose can be used as a choke hose which connects the BOP stack to the bleed-off manifold or a kill hose which connects the mud stand pipe to the BOP kill valve.

The Reliance Eliminator Choke & Kill hose contains a specially bonded compounded cover that replaces rubber covered Asbestos, Fibreglass and other fire retardant materials which are prone to damage. This high cut and gouge resistant cover overcomes costly repairs and downtime associated with older designs.

The Reliance Eliminator Choke & Kill hose has been verified by an independent engineer to meet and exceed EUB Directive 36 (700°C for 5 minutes).

Nom. ID		Nor	Nom OD Weight		Min Be	nd Radius	Max WP		
· in.	mm.	in.	mm	lb/ft	kg/m	in.	mm.	psi	Mpa
3	76.2	5.11	129.79	14.5	21.46	48	1219.2	5000	34.47
3-1/2	88.9	5.79	147.06	20.14	29.80	54	1371.6	5000	34.47



Fittings	Flanges	Hammer Unions	Other
RC4X5055 RC3X5055	R35 - 3-1/8 5000# API Type 6B R31 - 3-1/8 3000# API Type 6B	All Union Configurations	LP Threaded Connectio Graylock
RC4X5575	• .		Custom Ends

