

UNITED STATES
DEPARTMENT OF THE INTERIOR
BUREAU OF LAND MANAGEMENT

OCD HOBBS

Lease Serial No.
OMB No. 1004-0137
Expires October 31, 2014

NMLC 080258

APPLICATION FOR PERMIT TO DRILL OR REENTER

JUN 16 2014

1a. Type of work: <input checked="" type="checkbox"/> DRILL <input type="checkbox"/> REENTER		7. If Unit or CA Agreement, Name and No. N/A	
1b. Type of Well: <input checked="" type="checkbox"/> Oil Well <input type="checkbox"/> Gas Well <input type="checkbox"/> Other <input type="checkbox"/> Single Zone <input checked="" type="checkbox"/> Multiple Zone		8. Lease Name and Well No. Garnet Federal 5	
2. Name of Operator ConocoPhillips Company (217817)		9. API Well No. 30-025- 41924	
3a. Address 600 N. Dairy Ashford Rd, Office P10 4-4054 Houston, TX 77079		3b. Phone No. (include area code) (281)206-5281	
10. Field and Pool, or Exploratory Maljamar; Yeso West (44500)		11. Sec., T. R. M. or Blk. and Survey or Area Sec. 15, 17S, 32E	
4. Location of Well (Report location clearly and in accordance with any State requirements.)* At surface 869' FSL and 1084' FEL; UL P, Sec. 15, 17S, 32E At proposed prod. zone 340' FSL and 1041' FEL; UL P, Sec. 15, 17S, 32E		12. County or Parish Lea County	
13. State NM		14. Distance in miles and direction from nearest town or post office* Approximately 3 miles south east of Maljamar, New Mexico	
15. Distance from proposed* location to nearest property or lease line, ft. (Also to nearest drig. unit line, if any) 279'		16. No. of acres in lease 80.00	
17. Spacing Unit dedicated to this well 40.00		18. Distance from proposed location* to nearest well, drilling, completed, applied for, on this lease, ft. 130'	
19. Proposed Depth 7066' TVD/7112' MD		20. BLM/BIA Bond No. on file ES 0085	
21. Elevations (Show whether DF, KDB, RT, GL, etc.) 4027'		22. Approximate date work will start* 10/01/2013	
23. Estimated duration 7 days		24. Attachments	

The following, completed in accordance with the requirements of Onshore Oil and Gas Order No.1, must be attached to this form:

- | | |
|--|---|
| 1. Well plat certified by a registered surveyor. | 4. Bond to cover the operations unless covered by an existing bond on file (see Item 20 above). |
| 2. A Drilling Plan. | 5. Operator certification |
| 3. A Surface Use Plan (if the location is on National Forest System Lands, the SUPO must be filed with the appropriate Forest Service Office). | 6. Such other site specific information and/or plans as may be required by the BLM. |

25. Signature <i>Susan B. Maunders</i>	Name (Printed/Typed) Susan B. Maunders	Date 12/11/13
Title Senior Regulatory Specialist		
Approved by (Signature) <i>Steve Caffey</i>	Name (Printed/Typed)	Date JUN 13 2014
Title FIELD MANAGER		
Office CARLSBAD FIELD OFFICE		

Application approval does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon.
Conditions of approval, if any, are attached.

APPROVAL FOR TWO YEARS

Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

(Continued on page 2)

*(Instructions on page 2)

ROSWELL CONTROLLED WATER BASIN

K2
06/16/14

CANNOT PRODUCE UNTIL NSL IS APPROVED

CANNOT PRODUCE UNTIL NSL IS APPROVED

Approval Subject to General Requirements
& Special Stipulations AttachedSEE ATTACHED FOR
CONDITIONS OF APPROVAL

JUN 17 2014

Operator Certification

HOBBS OCD

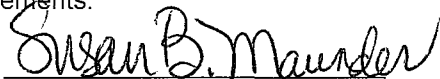
JUN 16 2014

CONOCOPHILLIPS COMPANY

CERTIFICATION:

RECEIVED

I hereby certify that I, or persons under my direct supervision, have inspected the proposed drill site and access route proposed herein; that I am familiar with the conditions which currently exist; that I have full knowledge of State and Federal laws applicable to this operation; that the statements made in this APD package are, to the best of my knowledge, true and correct; and that the work associated with the operations proposed herein will be performed in conformity with this APD package and the terms and conditions under which it is approved. I also certify that I, or the company I represent, am responsible for the operations conducted under this application with bond coverage provided by Nationwide Bond ES0085. These statements are subject to the provisions of 18 U.S.C. 1001 for the filing of false statements.



Susan B. Maunder
Senior Regulatory Specialist

Date: 12/11/13

Drilling Plan
ConocoPhillips Company
Maljamar; Grayburg-San Andres, Yeso (west)

Garnet Federal #5

Lea County, New Mexico

1. Estimated tops of geological markers and estimated depths to water, oil, or gas formations:

The datum for these depths is RKB (which is 13' above Ground Level).

Formations	Top Depth FT TVD	Top Depths FT MD	Contents
Quaternary	Surface	Surface	Fresh Water
Rustler	866	866	Anhydrite
Salado (top of salt)	1038	1038	Salt
Tansill (base of salt)	2047	2047	Gas, Oil and Water
Yates	2187	2187	Gas, Oil and Water
Seven Rivers	2543	2544	Gas, Oil and Water
Queen	3149	3160	Gas, Oil and Water
Grayburg	3554	3573	Gas, Oil and Water
San Andres	3991	4018	Gas, Oil and Water
Glorieta	5421	5467	Gas, Oil and Water
Paddock	5511	5557	Gas, Oil and Water
Blaine	5803	5849	Gas, Oil and Water
Tubb	6866	6912	Gas, Oil and Water
Deepest estimated perforation	6866	6912	Deepest estimated perf. is ~ Top of Tubb
Total Depth (maximum)	7066	7112	200' below deepest estimated perforation

All of the water bearing formations identified above will be protected by setting of the 8-5/8" surface casing 25' – 70' into the Rustler formation and circulating of cement from casing shoe to surface in accordance with the provisions of Onshore Oil and Gas Order No. 2 and New Mexico Oil Conservation Division Title 19.

The targeted oil and gas bearing formations identified above will be protected by setting of the 5-1/2" production casing 10' off bottom of TD and circulating of cement from casing shoe to surface in accordance with the provisions of Onshore Oil and Gas Order No. 2 and New Mexico Oil Conservation Division Title 19.

2. Proposed casing program:

Type	Hole Size	Interval MD RKB (ft)		OD	Wt	Gr	Conn	MIY	Col	Jt Str	Safety Factors Calculated per ConocoPhillips Corporate Criteria		
		From	To								Burst DF	Collapse DF	Jt Str DF (Tension) Dry/Buoyant
Cond	20	0	40' - 85' (30' - 75' BGL)	16	0.5" wall	B	Line Pipe	N/A	N/A	N/A	NA	NA	NA
Alt. Cond	20	0	40' - 85' (30' - 75' BGL)	13-3/8	48#	H-40	PE	1730	740	N/A	NA	NA	NA
Surf	12-1/4	0	891' - 936'	8-5/8	24#	J-55	STC	2950	1370	244	1.53	3.23	3.49
Prod	7-7/8	0	7057' - 7102'	5-1/2	17#	L-80	LTC	7740	6290	338	2.10	2.49	1.97

The casing will be suitable for H₂S Service. All casing will be new.

The surface and production casing will be set approximately 10' off bottom and we will drill the hole with a 45' range uncertainty for casing set depth to fit the casing string so that the cementing head is positioned at the floor for the cement job.

The production casing will be set 155' to 200' below the deepest estimated perforation to provide rathole for the pumping completion and for the logs to get deep enough to log the interval of interest.

Casing Safety Factors - BLM Criteria:

Type	Depth	Wt	MIY	Col	Jt Str	Drill Fluid	Burst	Collapse	Tensile-Dry	Tens-Bouy
Surface Casing	936	24	2950	1370	244000	8.5	6.99	3.25	10.6	12.2
Production Casing	7102	17	7740	6290	338000	10	2.10	1.70	2.80	3.31

Casing Safety Factors - Additional ConocoPhillips Criteria:

ConocoPhillips casing design policy establishes Corporate Minimum Design Factors (see table below) and requires that service life load cases be considered and provided for in the casing design.

ConocoPhillips Corporate Criteria for Minimum Design Factors

	Burst	Collapse	Axial
Casing Design Factors	1.15	1.05	1.4

Type	Depth	Wt	MIY	Col	Jt Str	Pipe Yield MW	Burst	Col	Ten
Conductor	85	65	35000	-	-	432966	-	-	-
Surface Casing (8-5/8" 24# J-55 STC)	936	24	2950	1370	244000	381000	8.5	1.54	3.29
Production Casing (5-1/2" 17# L-80 LTC)	7102	17	7740	6290	338000	397000	10	2.10	2.49

Burst - ConocoPhillips Required Load Cases

The maximum internal (burst) load on the Surface Casing occurs when the surface casing is tested to 1500 psi (as per BLM Onshore Order 2 - II. Requirements).

The maximum internal (burst) load on the Production Casing occurs during the fracture stimulation where the maximum allowable working pressure

(MAWP) is the pressure that would fit ConocoPhillips Corporate Criteria for Minimum Factors.

Surface Casing Test Pressure =	1500 psi	Predicted Pore Pressure at TD (PPTD) =	8.55 ppg
Surface Rated Working Pressure (ROPE) =	3000 psi	Predicted Frac Gradient at Shoe (CSFG) =	19.23 ppg
Field SW =	10 ppg		

Surface Casing Burst Safety Factor = API Burst Rating / Maximum Predicted Surface Pressure (MPSP) OR Maximum Allowable Surface Pressure (MASP)

Production Casing MAWP for the Fracture Stimulation = API Burst Rating / Corporate Minimum Burst Design Factor

Surface Casing Burst Safety Factor:

Case #1. MPSP (MWhyd next section) =	936	x	0.052	x	10	=	487			
Case #2. MPSP (Field SW @ Bullhead+200 psi) =	936	x	0.052	x	19.23	=	487	+	200	= 649
Case #3. MPSP (Kick Vol @ next section TD) =	7102	x	0.052	x	8.55	=	616.6	-	414	= 2127
Case #4. MPSP (PPTD - GG) =	7102	x	0.052	x	8.55	=	710.2	=		2447
Case #3 & #4 Limited to MPSP (CSFG + 0.2 ppg) =	936	x	0.052	x	19.23	+	0.2	=		946
MASP (MWhyd + Test Pressure) =	936	x	0.052	x	8.5	+	1500	=		1914
Burst Safety Factor (Max. MPSP or MASP) =	2950	/	1914	=	1.54					

Production Casing Burst Safety Factor:

Case #1. MPSP (MWhyd TD) =	7102	x	0.052	x	10	=	3693.04			
Case #4. MPSP (PPTD - GG) =	7102	x	0.052	x	8.55	=	710.2	=		2447
Burst Safety Factor (Max. MPSP) =	7740	/	3693	=	2.10					
MAWP for the Fracture Stimulation (Corporate Criteria) =	7740	/	1.15	=	6730					

Collapse - ConocoPhillips Required Load Cases

The maximum collapse load on the Surface Casing occurs when cementing to surface, 1/3 evacuation to the next casing setting depth, or deepest depth of exposure (full evacuation).

The maximum collapse load on the Production Casing occurs when cementing to surface, or 1/3 evacuation to the deepest depth of exposure; and

therefore, the external pressure profile for the evacuation cases should be equal to the pore pressure of the horizons on the outside of the casing which we assumed to be PPTD.

Surface Casing Collapse Safety Factor = API Collapse Rating / Full Evacuation OR Cement Displacement during Cementing to Surface

Production Casing Collapse Safety Factor = API Collapse Rating / Maximum Predicted Surface Pressure OR Cement Displacement during Cementing to Surface

Cement Displacement Fluid (FW) =	8.34 ppg	Top of Cement =	Cement to Surface
Surface Cement Lead =	13.6 ppg	Prod Cement Lead =	11.8 ppg
Surface Cement Tail =	14.8 ppg	Prod Cement Tail =	16.4 ppg
Top of Surface Tail Cement =	300 ft	Top of Prod Tail Cement =	5200 ft

Surface Casing Collapse Safety Factor:

Full Evacuation Diff Pressure =	936	x	0.052	x	8.55	=	416			
Cementing Diff Lift Pressure =	[(636	x	0.052	x	13.6)+ (300	x	0.052	x	14.8) - 406] = 275
Collapse Safety Factor =	1370	/	416	=	3.29					

Production Casing Collapse Safety Factor:

1/3 Evacuation Diff Pressure =	[(7102	x	0.052	x	8.55)- (7102	/	3	x	0.052	x	8.34] =	2131
Cementing Diff Lift Pressure =	[(1902	x	0.052	x	11.8)+ (5200	x	0.052	x	16.4)- 3080] =	2522	
Collapse Safety Factor =	6290	/	2522	=	2.49								

Tensile Strength - ConocoPhillips Required Load Cases

The maximum axial (tension) load occurs if casing were to get stuck and pulled on to try to get it unstuck.

Maximum Allowable Axial Load for Pipe Yield = API Pipe Yield Strength Rating / Corporate Minimum Axial Design Factor

Maximum Allowable Axial Load for Joint = API Joint Strength Rating / Corporate Minimum Axial Design Factor

Maximum Allowable Hook Load (Limited to 75% of Rig Max Load) = Maximum Allowable Axial Load

Maximum Allowable Overpull Margin = Maximum Allowable Hook Load - Bouyant Wt of the String

Tensile Safety Factor = API Pipe Yield OR API Joint Strength OR Rig Max Load Rating / (Bouyant Wt of String + Minimum Overpull Required)

Rig Max Load (300,000 lbs) x 75% =	225000 lbs
Minimum Overpull Required =	50000 lbs

Surface Casing Tensile Strength Safety Factor:

Air Wt =	22464									
Bouyant Wt =	22464	x	0.870	=	19549					
Max. Allowable Axial Load (Pipe Yield) =	381000	/	1.40	=	272143					
Max. Allowable Axial Load (Joint) =	244000	/	1.40	=	174286					
Max. Allowable Hook Load (Limited to 75% of Rig Max Load) =	174286									
Max. Allowable Overpull Margin =	174286	- (22464	x	0.870) =	154737				
Tensile Safety Factor =	244000	/ (19549	+	50000) =	3.51				

Production Casing Tensile Strength Safety Factor:

Air Wt =	120734									
Bouyant Wt =	120734	x	0.847	=	102301					
Max. Allowable Axial Load (Pipe Yield) =	397000	/	1.40	=	283571					
Max. Allowable Axial Load (Joint) =	338000	/	1.40	=	241429					
Max. Allowable Hook Load (Limited to 75% of Rig Max Load) =	225000									
Max. Allowable Overpull Margin =	225000	- (120734	x	0.847) =	122699				
Tensile Safety Factor =	300000	/ (102301	+	50000) =	1.97				

Compression Strength - ConocoPhillips Required Load Cases

The maximum axial (compression) load for the well is where the surface casing is landed on the conductor

with a support of a plate or landing ring. The surface casing is also calculated to bear 60% of the load

but not limited. Any other axial loads such as a snubbing unit or other would need to be added to the load.

Compression Safety Factor = API Axial Joint Strength Rating OR API Axial Pipe Yield Rating / Maximum Predicted Load

Wellhead Load =	3000 lbs
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Conductor & Surface Compression Safety Factor

Surf Casing Wt (Bouyant) =	(22464	x	0.870) =	19549					
Prod Casing Wt (Bouyant) =	(120734	x	0.847) =	102301					
Tubing Wt (Air Wt) =	7102	x	6.5	=	46163					
Tubing Fluid Wt =	7102	x	0.052	x	6.55	x	0.7854	x	2.441	*2 = 11320
Load on Conductor =	3000	+	19549	+	102301	+	46163	+	11320	= 182333
Conductor Compression Safety Factor =	432966	/	182333	=	2.37					
Load on Surface Casing =	182333	x	60%	=	109400					
Surface Casing Compression Safety Factor =	244000	/	109400	=	2.23					

3. Proposed cementing program:

16" or 13-3/8" Conductor:

Cement to surface with rathole mix, ready mix or Class C Neat cement.
(Note: The gravel used in the cement is not to exceed 3/8" diameter)
TOC at surface.

8-5/8" Surface Casing Cementing Program:

The intention for the cementing program for the Surface Casing is to:

- Place the Tail Slurry from the casing shoe to 300' above the casing shoe,
- Bring the Lead Slurry to surface.

Spacer: 20 bbls Fresh Water

Slurry		Intervals Ft MD		Weight ppg	Sx	Vol Cuft	Additives	Yield ft ³ /sx
Lead	Class C	Surface	591' – 636'	13.6	300	510	2% Extender 2% CaCl ₂ 0.125 lb/sx LCM if needed 0.2% Defoamer Excess = 75% based on gauge hole volume	1.70
Tail	Class C	591' – 636'	891' – 936'	14.8	200	268	1% CaCl ₂ Excess = 100% based on gauge hole volume	1.34

Displacement: Fresh Water.

Note: In accordance with the Pecos District Conditions of Approval, we will Wait on Cement (WOC) for a period of not less than 18 hrs after placement or until at least 500 psi compressive strength has been reached in both the Lead Slurry and Tail Slurry cements on the Surface Casing, whichever is greater.

5-1/2" Production Casing & Cementing Program:

The intention for the cementing program for the Production Casing is to:

- Place the Tail Slurry from the casing shoe to a point approximately 200' above the top of the Paddock,
- Bring the Lead Slurry to surface.

Spacer: 20 bbls Fresh Water

Slurry		Intervals Ft MD		Weight ppg	Sx	Vol Cuft	Additives	Yield ft ³ /sx
Lead	50:50 Poz/C	Surface	5200'	11.8	700	1820	10% Bentonite 5% Salt 0.2%-0.4% Fluid loss additive 0.125 lb/sx LCM if needed Excess = 220% or more if needed based on gauge hole volume	2.6
Tail	Class H	5200'	7057' – 7102'	16.4	400	428	0.2% Fluid loss additive 0.3% Dispersant 0.15% Retarder 0.2% Antifoam Excess = 100% or more if needed based on gauge hole volume	1.07

Displacement: Fresh Water with approximately 250 ppm glutaraldehyde biocide.

5-1/2" Production Casing & Cementing Program – TXI/LW Cementing Option for Grayburg-San Andres:

ConocoPhillips Company respectfully requests the options to our cementing program. This option will only be implemented in the cementing operation of wells requesting for co-mingling after approval and authorization by all agencies have been obtained. The intention for the alternative option to the cementing program for the Production Casing is to:

- Accommodate the additional frac'ing and stimulation of the Grayburg-San Andres by placement of the Tail Slurry from the casing shoe to the top of the Grayburg-San Andres formation,
- Bring the Lead Slurry to surface.

Spacer: 20 bbls Fresh Water

Slurry		Intervals Ft MD		Weight ppg	Sx	Vol Cuft	Additives	Yield ft ³ /sx
Lead	50:50 Poz/C	Surface	3000'	11.8	500	1300	10% Bentonite 8 lbs/sx Salt 0.2%-0.4% Fluid loss additive 0.125 lb/sx LCM if needed Excess = 200% or more if needed based on gauge hole volume	2.6
Tail	TXI/LW	3000'	7057' – 7102'	13.2	800	1120	0.5% Fluid loss additive 0.10% Retarder 0.2% Antifoam 0.125 lb/sx LCM if needed Excess = 150% or more if needed based on gauge hole volume	1.40

Displacement: Fresh Water with approximately 250 ppm gluteraldehyde biocide.

Proposal for Option to Adjust Production Casing Cement Volumes:

The production casing cement volume presented above are estimates based on gauge 7-7/8" hole. We will adjust these volumes based on the caliper log data for each well and our trends for amount of cement returns to surface. Also, if no caliper log is available for any particular well, we would propose an option to possibly increase the production casing cement volume to account for any uncertainty in regard to the hole volume.

4. Pressure Control Equipment:

A 11" 3M system will be installed, used, maintained, and tested accordingly as described in Onshore Oil and Gas Order No. 2.

Our BOP equipment will be:

- Rotating Head
- Annular BOP, 11" 3M
- Blind Ram, 11" 3M
- Pipe Ram, 11" 3M

After nipping up, and every 30 days thereafter or whenever any seal subject to test pressure is broken followed by related repairs, blowout preventors will be pressure tested. BOP will be inspected and operated at least daily to insure good working order. All pressure and operating tests will be done by an independent service company and recorded on the daily drilling reports. BOP will be tested using a test plug to isolate BOP stack from casing. BOP test will include a low pressure test from 250 to 300 psi for a minimum of 10 minutes or until requirements of test are met, whichever is longer. Ram type preventers and associated equipment will be tested to the approved stack working pressure of 3000 psi isolated by test plug. Annular type preventers will be tested to 50 percent of rated working pressure, and therefore will be tested to 1500 psi. Pressure will be held for at least 10 minutes or until provisions of test are met, whichever is longer. Valve on casing head below test plug will be open during testing of BOP stack. BOP will comply with all provisions of Onshore Oil and Gas Order No. 2 as specified. **See Attached BOPE Schematic.** A variance is respectfully requested to allow for the use of flexible hose. The variance request is included as a separate enclosure with attachments.

5. Proposed Mud System:

The mud systems that are proposed for use are as follows:

DEPTH	TYPE	Density ppg	FV sec/qt	API Fluid Loss cc/30 min	pH	Vol bbl
0 – Surface Casing Point	Fresh Water or Fresh Water Native Mud in Steel Pits	8.5 – 9.0	28 – 40	N.C.	N.C.	120 – 160
Surface Casing Point to TD	Brine (Saturated NaCl ₂) in Steel Pits	10	29	N.C.	10 – 11	500 – 1000
Conversion to Mud at TD	Brine Based Mud (NaCl ₂) in Steel Pits	10	33 – 40	5 – 10	10 – 11	0 – 750

Gas detection equipment and pit level flow monitoring equipment will be on location. A flow paddle will be installed in the flow line to monitor relative amount of mud flowing in the non-pressurized return line. Mud probes will be installed in the individual tanks to monitor pit volumes of the drilling fluid with a pit volume totalizer. Gas detecting equipment and H₂S monitor alarm will be installed in the mud return system and will be monitored. A mud gas separator will be installed and operable before drilling out from the Surface Casing. The gases shall be piped into the flare system. Drilling mud containing H₂S shall be degassed in accordance with API RP-49, item 5.14.

In the event that the well is flowing from a waterflow, then we would discharge excess drilling fluids from the steel mud pits through a fas-line into steel frac tanks at an offset location for containment. Depending on the rate of waterflow, excess fluids will be hauled to an approved disposal facility, or if in suitable condition, may be reused on the next well.

No reserve pit will be built.

Proposal for Option to Not Mud Up at TD:

FW, Brine, and Mud volume presented above are estimates based on gauge 12-1/4" or 7-7/8" holes. We will adjust these volume based on hole conditions. We do not plan to keep any weighting material at the wellsite. Also, we propose an option to not mud up leaving only brine in the hole if we have good hole stability.

6. Logging, Coring, and Testing Program:

- a. No drill stem tests will be done
- b. Remote gas monitoring planned for the production hole section (optional).
- c. No whole cores are planned
- d. The open hole electrical logging program is planned to be as follows:
 - Total Depth to 2500': Resistivity, Density, and Gamma Ray
 - Total Depth to surface Casing Shoe: Caliper
 - Total Depth to surface, Gamma Ray and Neutron
 - Formation pressure data (XPT) on electric line if needed (optional)
 - Rotary Sidewall Cores on electric line if needed (optional)
 - BHC or Dipole Sonic if needed (optional)
 - Spectral Gamma Ray if needed (optional)

7. Abnormal Pressures and Temperatures:

- No abnormal pressures are expected to be encountered.
- Loss of circulation is a possibility in the horizons below the Top of Grayburg. We expect that normal Loss of Circulation Material will be successful in healing any such loss of circulation events.
 - The bottom hole pressure is expected to be 8.55 ppg gradient.
 - The expected Bottom Hole Temperature is 115 degrees F.
- The estimated H₂S concentrations and ROE calculations for the gas in the zones to be penetrated are presented in the table below for the various producing horizons in this area:

FORMATION / ZONE	H2S (PPM)	Gas Rate (MCFD)	ROE 100 PPM	ROE 500 PPM
Grayburg / San Andres (from MCA)	14000	38	59	27
Yeso Group	860	160	29	13

ConocoPhillips will comply with the provisions of Oil and Gas Order # 6, Hydrogen Sulfide Operations. Also, ConocoPhillips will provide an H₂S Contingency Plan (please see copy attached) and will keep this plan updated and posted at the wellsite during the drilling operation.

8. Anticipated starting date and duration of operations:

Well pad and road constructions will begin as soon as all agency approvals are obtained. Anticipated date to drill this well as early as 2014 after receiving approval of the APD.

Attachments:

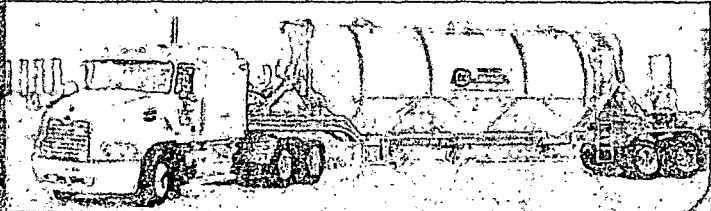
- Attachment # 1 BOP and Choke Manifold Schematic – 3M System
- Attachment # 2 Diagram of Choke Manifold Equipment

Contact Information:

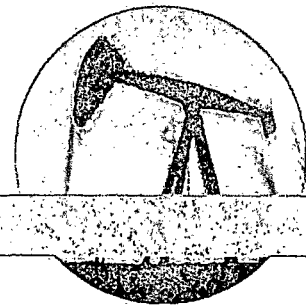
Proposed 9 December 2013 by:
James Chen
Drilling Engineer, ConocoPhillips Company
Phone (281) 206-5244
Cell (832) 768-1647


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TXI ENERGY SERVICES



TXI Energy Services provides specialized drilling products and petrochemical support services to the energy industry. Whether we're supplying well cement and additives for the next deep water project in the Gulf of Mexico or implementing new environmental procedures, our group shares a commitment to improved performance.



Petrochemical Support Services

TXI is dedicated to providing environmental services that benefit people and the planet. Our Energy Services division removes and recycles a variety of non-hazardous by-products from petrochemical refineries and provides solidification materials to remediation sites.

Drilling Products

TXI Lightweight Oil/Well Cement is a low-density cement that can be mixed in a range of 12.0 to 14.2 pounds per gallon. In addition to being the world's only manufacturer of lightweight oil/well cement, TXI also manufactures and distributes two classifications of well cements that meet the American Petroleum Institute specifications:

- Class A: a "general purpose" cement for use at low to moderate temperatures
- Class C: a moderate sulfate-resistant (MSR) cement for depths to 8000 feet
- Other Special Cements

Cement Additives

TXI Energy Services, in partnership with a worldwide chemical manufacturer, can supply a wide variety of cement additives.

TXI Energy Services

11111 Wilcrest Green, Suite 103, Houston, Texas 77042 Phone 713.820.2611 www.txi.com

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ConocoPhillips MCBU

Buckeye

Garnet Federal

Garnet Federal 5

Original Hole

Plan: Plan Design

Standard Planning Report - Geographic

05 December, 2013

ConocoPhillips

Planning Report - Geographic

Database:	EDM Central Planning	Local Co-ordinate Reference:	Well Garnet Federal 5
Company:	ConocoPhillips MCBU	TVD Reference:	RKB @ 4040.0usft (PD 822)
Project:	Buckeye	MD Reference:	RKB @ 4040.0usft (PD 822)
Site:	Garnet Federal	North Reference:	Grid
Well:	Garnet Federal 5	Survey Calculation Method:	Minimum Curvature
Wellbore:	Original Hole		
Design:	Plan Design		

Project	Buckeye, Lea County, NM		
Map System:	US State Plane 1927 (Exact solution)	System Datum:	Mean Sea Level
Geo Datum:	NAD 1927 (NADCON CONUS)		
Map Zone:	New Mexico East 3001		Using geodetic scale factor

Site	Garnet Federal, New Mexico, Southeast		
Site Position:		Northing:	665,838.65 usft
From:	Lat/Long	Easting:	680,526.85 usft
Position Uncertainty:	3.5 usft	Slot Radius:	8 "
		Latitude:	32° 49' 44.750 N
		Longitude:	103° 44' 44.280 W
		Grid Convergence:	0.32 °

Well	Garnet Federal 5, Deviated Well		
Well Position	+N/-S	0.0 usft	Northing: 666,019.36 usft
	+E/-W	0.0 usft	Easting: 679,582.10 usft
Position Uncertainty	0.0 usft	Wellhead Elevation:	Latitude: 32° 49' 46.590 N
			Longitude: 103° 44' 55.340 W
			Ground Level: 4,027.0 usft

Wellbore	Original Hole				
Magnetics	Model Name	Sample Date	Declination (°)	Dip Angle (°)	Field Strength (nT)
	BGGM2013	12/5/2013	7.53	60.65	48,693

Design	Plan Design			
Audit Notes:				
Version:	1	Phase:	PROTOTYPE	Tie On Depth: 0.0
Vertical Section:	Depth From (TVD) (usft)	+N/-S (usft)	+E/-W (usft)	Direction (°)
	0.0	0.0	0.0	175.06

Plan Sections										
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)	TFO (°)	Target
0.0	0.00	0.00	0.0	0.0	0.0	0.00	0.00	0.00	0.00	
2,047.0	0.00	0.00	2,047.0	0.0	0.0	0.00	0.00	0.00	0.00	
2,778.4	10.97	175.06	2,773.9	-69.5	6.0	1.50	1.50	0.00	175.06	
4,826.0	10.97	175.06	4,784.1	-457.8	39.6	0.00	0.00	0.00	0.00	
5,557.3	0.00	0.00	5,511.0	-527.3	45.6	1.50	-1.50	0.00	180.00	
7,112.3	0.00	0.00	7,066.0	-527.3	45.6	0.00	0.00	0.00	0.00	Garnet Federal 5 (BH)

ConocoPhillips

Planning Report - Geographic

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Company:	ConocoPhillips MCBU	TVD Reference:	RKB @ 4040.0usft (PD 822)
Project:	Buckeye	MD Reference:	RKB @ 4040.0usft (PD 822)
Site:	Garnet Federal	North Reference:	Grid
Well:	Garnet Federal 5	Survey Calculation Method:	Minimum Curvature
Wellbore:	Original Hole		
Design:	Plan Design		

Planned Survey										
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Map Northing (usft)	Map Easting (usft)	Latitude	Longitude	
0.0	0.00	0.00	0.0	0.0	0.0	666,019.36	679,582.10	32° 49' 46.590 N	103° 44' 55.340 W	
85.0	0.00	0.00	85.0	0.0	0.0	666,019.36	679,582.10	32° 49' 46.590 N	103° 44' 55.340 W	
Conductor										
100.0	0.00	0.00	100.0	0.0	0.0	666,019.36	679,582.10	32° 49' 46.590 N	103° 44' 55.340 W	
200.0	0.00	0.00	200.0	0.0	0.0	666,019.36	679,582.10	32° 49' 46.590 N	103° 44' 55.340 W	
300.0	0.00	0.00	300.0	0.0	0.0	666,019.36	679,582.10	32° 49' 46.590 N	103° 44' 55.340 W	
400.0	0.00	0.00	400.0	0.0	0.0	666,019.36	679,582.10	32° 49' 46.590 N	103° 44' 55.340 W	
500.0	0.00	0.00	500.0	0.0	0.0	666,019.36	679,582.10	32° 49' 46.590 N	103° 44' 55.340 W	
600.0	0.00	0.00	600.0	0.0	0.0	666,019.36	679,582.10	32° 49' 46.590 N	103° 44' 55.340 W	
700.0	0.00	0.00	700.0	0.0	0.0	666,019.36	679,582.10	32° 49' 46.590 N	103° 44' 55.340 W	
800.0	0.00	0.00	800.0	0.0	0.0	666,019.36	679,582.10	32° 49' 46.590 N	103° 44' 55.340 W	
886.0	0.00	0.00	886.0	0.0	0.0	666,019.36	679,582.10	32° 49' 46.590 N	103° 44' 55.340 W	
Rustler										
900.0	0.00	0.00	900.0	0.0	0.0	666,019.36	679,582.10	32° 49' 46.590 N	103° 44' 55.340 W	
936.0	0.00	0.00	936.0	0.0	0.0	666,019.36	679,582.10	32° 49' 46.590 N	103° 44' 55.340 W	
Surface										
1,000.0	0.00	0.00	1,000.0	0.0	0.0	666,019.36	679,582.10	32° 49' 46.590 N	103° 44' 55.340 W	
1,038.0	0.00	0.00	1,038.0	0.0	0.0	666,019.36	679,582.10	32° 49' 46.590 N	103° 44' 55.340 W	
Salado										
1,100.0	0.00	0.00	1,100.0	0.0	0.0	666,019.36	679,582.10	32° 49' 46.590 N	103° 44' 55.340 W	
1,200.0	0.00	0.00	1,200.0	0.0	0.0	666,019.36	679,582.10	32° 49' 46.590 N	103° 44' 55.340 W	
1,300.0	0.00	0.00	1,300.0	0.0	0.0	666,019.36	679,582.10	32° 49' 46.590 N	103° 44' 55.340 W	
1,400.0	0.00	0.00	1,400.0	0.0	0.0	666,019.36	679,582.10	32° 49' 46.590 N	103° 44' 55.340 W	
1,500.0	0.00	0.00	1,500.0	0.0	0.0	666,019.36	679,582.10	32° 49' 46.590 N	103° 44' 55.340 W	
1,600.0	0.00	0.00	1,600.0	0.0	0.0	666,019.36	679,582.10	32° 49' 46.590 N	103° 44' 55.340 W	
1,700.0	0.00	0.00	1,700.0	0.0	0.0	666,019.36	679,582.10	32° 49' 46.590 N	103° 44' 55.340 W	
1,800.0	0.00	0.00	1,800.0	0.0	0.0	666,019.36	679,582.10	32° 49' 46.590 N	103° 44' 55.340 W	
1,900.0	0.00	0.00	1,900.0	0.0	0.0	666,019.36	679,582.10	32° 49' 46.590 N	103° 44' 55.340 W	
2,000.0	0.00	0.00	2,000.0	0.0	0.0	666,019.36	679,582.10	32° 49' 46.590 N	103° 44' 55.340 W	
2,047.0	0.00	0.00	2,047.0	0.0	0.0	666,019.36	679,582.10	32° 49' 46.590 N	103° 44' 55.340 W	
Tansill										
2,100.0	0.80	175.06	2,100.0	-0.4	0.0	666,019.00	679,582.13	32° 49' 46.586 N	103° 44' 55.340 W	
2,187.0	2.10	175.06	2,187.0	-2.6	0.2	666,016.81	679,582.32	32° 49' 46.565 N	103° 44' 55.338 W	
Yates										
2,200.0	2.30	175.06	2,200.0	-3.1	0.3	666,016.31	679,582.36	32° 49' 46.560 N	103° 44' 55.337 W	
2,300.0	3.80	175.06	2,299.8	-8.3	0.7	666,011.02	679,582.82	32° 49' 46.507 N	103° 44' 55.332 W	
2,400.0	5.30	175.06	2,399.5	-16.2	1.4	666,003.13	679,583.50	32° 49' 46.429 N	103° 44' 55.325 W	
2,500.0	6.80	175.06	2,498.9	-26.7	2.3	665,992.63	679,584.41	32° 49' 46.325 N	103° 44' 55.315 W	
2,544.4	7.46	175.06	2,543.0	-32.2	2.8	665,987.15	679,584.88	32° 49' 46.271 N	103° 44' 55.309 W	
Seven Rivers										
2,600.0	8.30	175.06	2,598.1	-39.8	3.4	665,979.55	679,585.54	32° 49' 46.196 N	103° 44' 55.302 W	
2,700.0	9.80	175.06	2,696.8	-55.5	4.8	665,963.89	679,586.89	32° 49' 46.041 N	103° 44' 55.287 W	
2,778.4	10.97	175.06	2,773.9	-69.5	6.0	665,949.82	679,588.11	32° 49' 45.902 N	103° 44' 55.274 W	
2,800.0	10.97	175.06	2,795.1	-73.6	6.4	665,945.72	679,588.46	32° 49' 45.861 N	103° 44' 55.270 W	
2,900.0	10.97	175.06	2,893.3	-92.6	8.0	665,926.76	679,590.10	32° 49' 45.673 N	103° 44' 55.252 W	
3,000.0	10.97	175.06	2,991.5	-111.6	9.6	665,907.80	679,591.74	32° 49' 45.486 N	103° 44' 55.234 W	
3,100.0	10.97	175.06	3,089.7	-130.5	11.3	665,888.84	679,593.38	32° 49' 45.298 N	103° 44' 55.216 W	
3,160.4	10.97	175.06	3,149.0	-142.0	12.3	665,877.38	679,594.37	32° 49' 45.184 N	103° 44' 55.205 W	
Queen										
3,200.0	10.97	175.06	3,187.8	-149.5	12.9	665,869.88	679,595.02	32° 49' 45.110 N	103° 44' 55.198 W	
3,300.0	10.97	175.06	3,286.0	-168.4	14.6	665,850.93	679,596.66	32° 49' 44.923 N	103° 44' 55.180 W	
3,400.0	10.97	175.06	3,384.2	-187.4	16.2	665,831.97	679,598.30	32° 49' 44.735 N	103° 44' 55.162 W	
3,500.0	10.97	175.06	3,482.4	-206.4	17.8	665,813.01	679,599.94	32° 49' 44.547 N	103° 44' 55.144 W	

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Project:	Buckeye	MD Reference:	RKB @ 4040.0usft (PD 822)
Site:	Garnet Federal	North Reference:	Grid
Well:	Garnet Federal 5	Survey Calculation Method:	Minimum Curvature
Wellbore:	Original Hole		
Design:	Plan Design		

Planned Survey										
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Map Northing (usft)	Map Easting (usft)	Latitude	Longitude	
3,573.0	10.97	175.06	3,554.0	-220.2	19.0	665,799.17	679,601.13	32° 49' 44.410 N	103° 44' 55.131 W	
Grayburg										
3,600.0	10.97	175.06	3,580.5	-225.3	19.5	665,794.05	679,601.57	32° 49' 44.359 N	103° 44' 55.126 W	
3,700.0	10.97	175.06	3,678.7	-244.3	21.1	665,775.09	679,603.21	32° 49' 44.172 N	103° 44' 55.108 W	
3,800.0	10.97	175.06	3,776.9	-263.2	22.8	665,756.13	679,604.85	32° 49' 43.984 N	103° 44' 55.090 W	
3,900.0	10.97	175.06	3,875.0	-282.2	24.4	665,737.17	679,606.49	32° 49' 43.796 N	103° 44' 55.072 W	
4,000.0	10.97	175.06	3,973.2	-301.2	26.0	665,718.21	679,608.13	32° 49' 43.609 N	103° 44' 55.054 W	
4,018.1	10.97	175.06	3,991.0	-304.6	26.3	665,714.78	679,608.43	32° 49' 43.575 N	103° 44' 55.051 W	
San Andres										
4,100.0	10.97	175.06	4,071.4	-320.1	27.7	665,699.25	679,609.77	32° 49' 43.421 N	103° 44' 55.036 W	
4,200.0	10.97	175.06	4,169.6	-339.1	29.3	665,680.29	679,611.41	32° 49' 43.233 N	103° 44' 55.018 W	
4,300.0	10.97	175.06	4,267.7	-358.0	31.0	665,661.33	679,613.05	32° 49' 43.046 N	103° 44' 55.000 W	
4,400.0	10.97	175.06	4,365.9	-377.0	32.6	665,642.37	679,614.69	32° 49' 42.858 N	103° 44' 54.983 W	
4,500.0	10.97	175.06	4,464.1	-396.0	34.2	665,623.42	679,616.33	32° 49' 42.670 N	103° 44' 54.965 W	
4,600.0	10.97	175.06	4,562.2	-414.9	35.9	665,604.46	679,617.96	32° 49' 42.483 N	103° 44' 54.947 W	
4,700.0	10.97	175.06	4,660.4	-433.9	37.5	665,585.50	679,619.60	32° 49' 42.295 N	103° 44' 54.929 W	
4,800.0	10.97	175.06	4,758.6	-452.9	39.1	665,566.54	679,621.24	32° 49' 42.107 N	103° 44' 54.911 W	
4,826.0	10.97	175.06	4,784.1	-457.8	39.6	665,561.62	679,621.67	32° 49' 42.058 N	103° 44' 54.906 W	
4,900.0	9.86	175.06	4,856.9	-471.1	40.7	665,548.28	679,622.82	32° 49' 41.926 N	103° 44' 54.893 W	
5,000.0	8.36	175.06	4,955.6	-486.9	42.1	665,532.51	679,624.18	32° 49' 41.770 N	103° 44' 54.878 W	
5,100.0	6.86	175.06	5,054.7	-500.1	43.2	665,519.32	679,625.32	32° 49' 41.640 N	103° 44' 54.866 W	
5,200.0	5.36	175.06	5,154.2	-510.7	44.1	665,508.71	679,626.24	32° 49' 41.535 N	103° 44' 54.856 W	
5,300.0	3.86	175.06	5,253.9	-518.7	44.8	665,500.70	679,626.93	32° 49' 41.455 N	103° 44' 54.848 W	
5,400.0	2.36	175.06	5,353.7	-524.1	45.3	665,495.30	679,627.40	32° 49' 41.402 N	103° 44' 54.843 W	
5,467.3	1.35	175.06	5,421.0	-526.3	45.5	665,493.13	679,627.59	32° 49' 41.380 N	103° 44' 54.841 W	
Glorieta										
5,500.0	0.86	175.06	5,453.7	-526.9	45.5	665,492.50	679,627.64	32° 49' 41.374 N	103° 44' 54.840 W	
5,557.3	0.00	0.00	5,511.0	-527.3	45.6	665,492.07	679,627.68	32° 49' 41.370 N	103° 44' 54.840 W	
Paddock										
5,600.0	0.00	0.00	5,553.7	-527.3	45.6	665,492.07	679,627.68	32° 49' 41.370 N	103° 44' 54.840 W	
5,700.0	0.00	0.00	5,653.7	-527.3	45.6	665,492.07	679,627.68	32° 49' 41.370 N	103° 44' 54.840 W	
5,800.0	0.00	0.00	5,753.7	-527.3	45.6	665,492.07	679,627.68	32° 49' 41.370 N	103° 44' 54.840 W	
5,849.3	0.00	0.00	5,803.0	-527.3	45.6	665,492.07	679,627.68	32° 49' 41.370 N	103° 44' 54.840 W	
Blinebry										
5,900.0	0.00	0.00	5,853.7	-527.3	45.6	665,492.07	679,627.68	32° 49' 41.370 N	103° 44' 54.840 W	
6,000.0	0.00	0.00	5,953.7	-527.3	45.6	665,492.07	679,627.68	32° 49' 41.370 N	103° 44' 54.840 W	
6,100.0	0.00	0.00	6,053.7	-527.3	45.6	665,492.07	679,627.68	32° 49' 41.370 N	103° 44' 54.840 W	
6,200.0	0.00	0.00	6,153.7	-527.3	45.6	665,492.07	679,627.68	32° 49' 41.370 N	103° 44' 54.840 W	
6,300.0	0.00	0.00	6,253.7	-527.3	45.6	665,492.07	679,627.68	32° 49' 41.370 N	103° 44' 54.840 W	
6,400.0	0.00	0.00	6,353.7	-527.3	45.6	665,492.07	679,627.68	32° 49' 41.370 N	103° 44' 54.840 W	
6,500.0	0.00	0.00	6,453.7	-527.3	45.6	665,492.07	679,627.68	32° 49' 41.370 N	103° 44' 54.840 W	
6,600.0	0.00	0.00	6,553.7	-527.3	45.6	665,492.07	679,627.68	32° 49' 41.370 N	103° 44' 54.840 W	
6,700.0	0.00	0.00	6,653.7	-527.3	45.6	665,492.07	679,627.68	32° 49' 41.370 N	103° 44' 54.840 W	
6,800.0	0.00	0.00	6,753.7	-527.3	45.6	665,492.07	679,627.68	32° 49' 41.370 N	103° 44' 54.840 W	
6,900.0	0.00	0.00	6,853.7	-527.3	45.6	665,492.07	679,627.68	32° 49' 41.370 N	103° 44' 54.840 W	
6,912.3	0.00	0.00	6,866.0	-527.3	45.6	665,492.07	679,627.68	32° 49' 41.370 N	103° 44' 54.840 W	
Tubb										
7,000.0	0.00	0.00	6,953.7	-527.3	45.6	665,492.07	679,627.68	32° 49' 41.370 N	103° 44' 54.840 W	
7,100.0	0.00	0.00	7,053.7	-527.3	45.6	665,492.07	679,627.68	32° 49' 41.370 N	103° 44' 54.840 W	
7,102.0	0.00	0.00	7,055.7	-527.3	45.6	665,492.07	679,627.68	32° 49' 41.370 N	103° 44' 54.840 W	
Production										
7,112.3	0.00	0.00	7,066.0	-527.3	45.6	665,492.07	679,627.68	32° 49' 41.370 N	103° 44' 54.840 W	

ConocoPhillips

Planning Report - Geographic

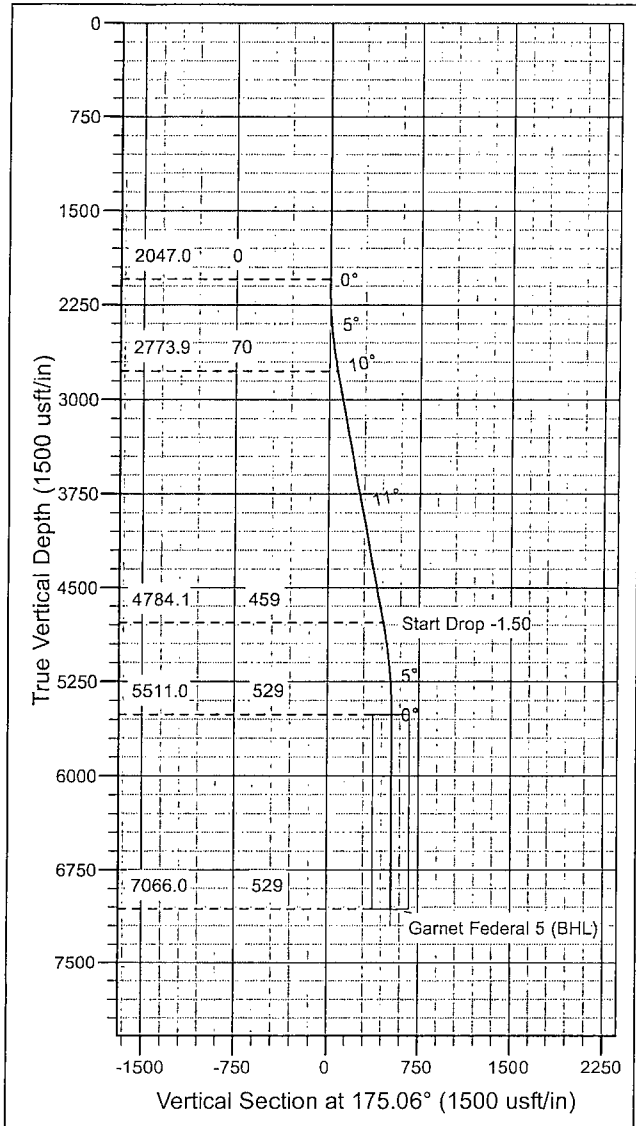
Database:	EDM Central Planning	Local Co-ordinate Reference:	Well Garnet Federal 5
Company:	ConocoPhillips MCBU	TVD Reference:	RKB @ 4040.0usft (PD 822)
Project:	Buckeye	MD Reference:	RKB @ 4040.0usft (PD 822)
Site:	Garnet Federal	North Reference:	Grid
Well:	Garnet Federal 5	Survey Calculation Method:	Minimum Curvature
Wellbore:	Original Hole		
Design:	Plan Design		

Design Targets									
Target Name									
- hit/miss target	Dip Angle	Dip Dir.	TVD	+N/-S	+E/-W	Northing	Easting	Latitude	Longitude
- Shape	(°)	(°)	(usft)	(usft)	(usft)	(usft)	(usft)		
Garnet Federal 5 (BHL)	0.00	0.00	7,066.0	-527.3	45.6	665,492.07	679,627.68	32° 49' 41.370 N	103° 44' 54.840 W
- plan hits target center									
- Circle (radius 150.0)									

Casing Points				
Measured Depth	Vertical Depth		Casing Diameter	Hole Diameter
(usft)	(usft)	Name	(")	(")
85.0	85.0	Conductor	16	20
936.0	936.0	Surface	8-5/8	12-1/4
7,102.0	7,055.7	Production	5-1/2	7-7/8

Formations					
Measured Depth	Vertical Depth			Dip	Dip Direction
(usft)	(usft)	Name	Lithology	(°)	(°)
886.0	886.0	Rustler		0.00	
1,038.0	1,038.0	Salado		0.00	
2,047.0	2,047.0	Tansill		0.00	
2,187.0	2,187.0	Yates		0.00	
2,544.4	2,543.0	Seven Rivers		0.00	
3,160.4	3,149.0	Queen		0.00	
3,573.0	3,554.0	Grayburg		0.00	
4,018.1	3,991.0	San Andres		0.00	
5,467.3	5,421.0	Glorieta		0.00	
5,557.3	5,511.0	Paddock		0.00	
5,849.3	5,803.0	Blinberry		0.00	
6,912.3	6,866.0	Tubb		0.00	

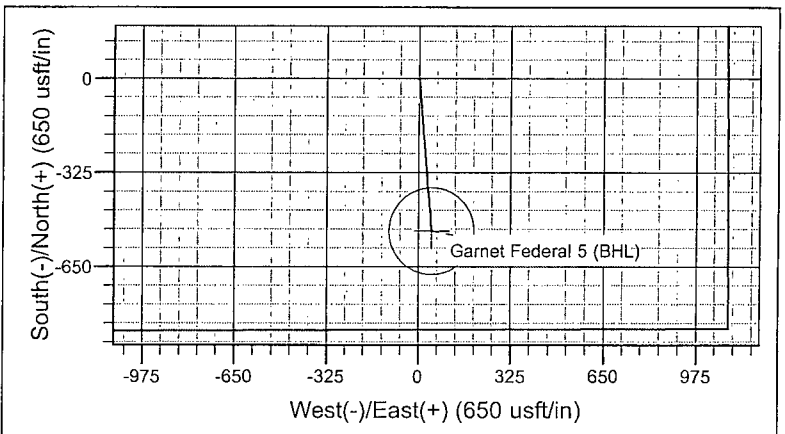
Proposed Directional Well Plan



Project: Buckeye
 Site: Garnet Federal
 Well: Garnet Federal 5
 Wellbore: Original Hole
 Design: Plan Design

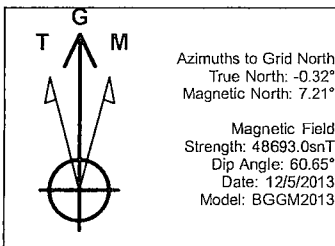
WELL DETAILS: Garnet Federal 5						
+N/-S	+E/-W	Northing	Ground Level:	4027.0	Latitude	Longitude
0.0	0.0	666019.36	Easting	679582.10	32° 49' 46.590 N	103° 44' 55.340 W

SECTION DETAILS										
Sec	MD	Inc	Azi	TVD	+N/-S	+E/-W	Dleg	TFace	VSec	Target
1	0.0	0.00	0.00	0.0	0.0	0.0	0.00	0.00	0.0	
2	2047.0	0.00	0.00	2047.0	0.0	0.0	0.00	0.00	0.0	
3	2778.4	10.97	175.06	2773.9	-69.5	6.0	1.50	175.06	69.8	
4	44826.0	10.97	175.06	4784.1	-457.8	39.6	0.00	0.00	459.5	
5	55557.3	0.00	0.00	5511.0	-527.3	45.6	1.50	180.00	529.3	
6	7112.3	0.00	0.00	7066.0	-527.3	45.6	0.00	0.00	529.3	Garnet Federal 5 (BHL)



CASING DETAILS			
TVD	MD	Name	Size
85.0	85.0	Conductor	16
936.0	936.0	Surface	8-5/8
7055.7	7102.0	Production	5-1/2

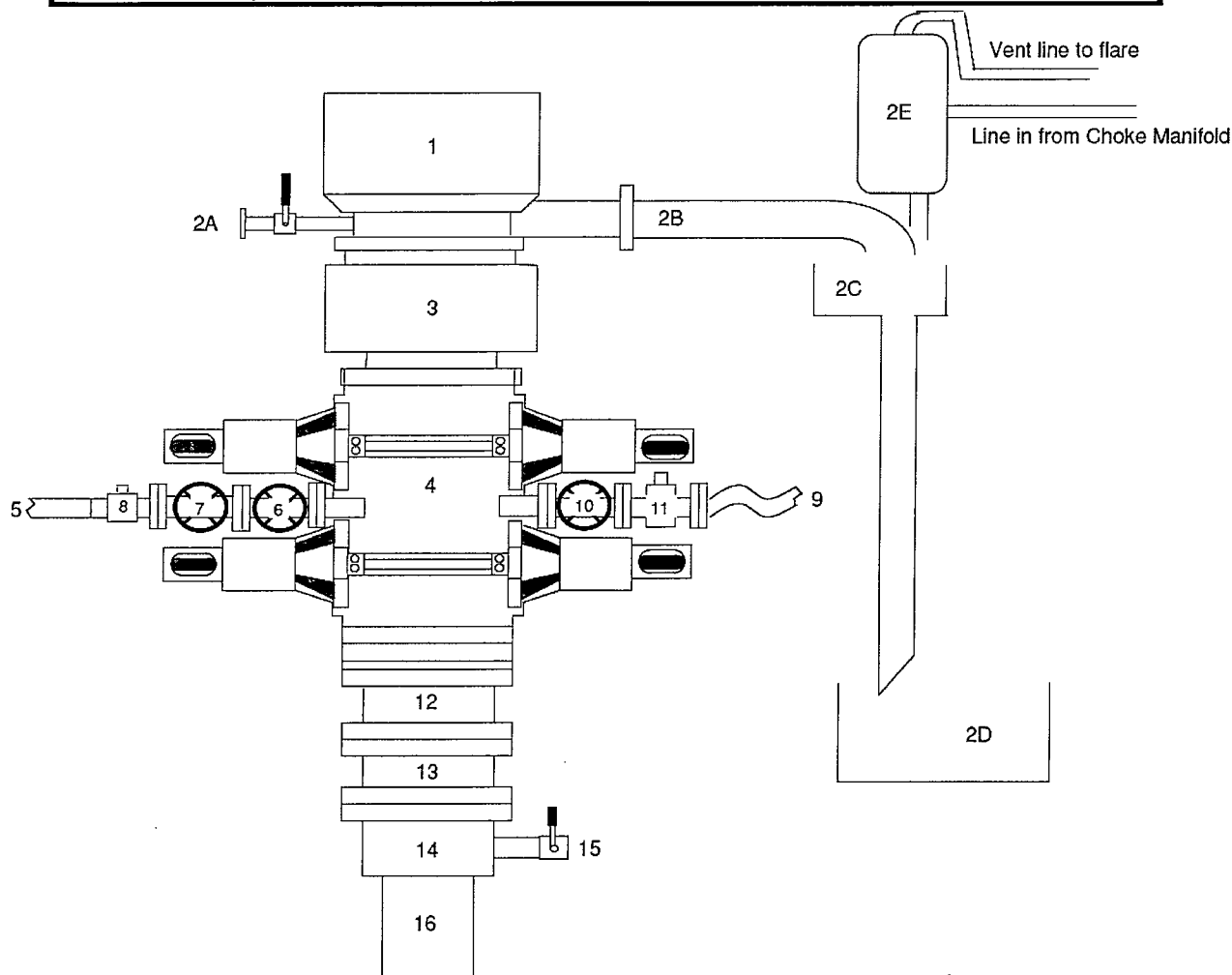
TVD	Path	MD	Path	Formation
886.0	886.0			Rustler
1038.0	1038.0			Salado
2047.0	2047.0			Tansill
2187.0	2187.0			Yates
2543.0	2544.4			Seven Rivers
3149.0	3160.4			Queen
3554.0	3573.0			Grayburg
3991.0	4018.1			San Andres
5421.0	5467.3			Glorieta
5511.0	5557.3			Paddock
5803.0	5849.3			Blinberry
6866.0	6912.3			Tubb



Attachment # 1

BLOWOUT PREVENTER ARRANGEMENT

3M System per Onshore Oil and Gas Order No. 2 utilizing 3M and 5M Rated Equipment

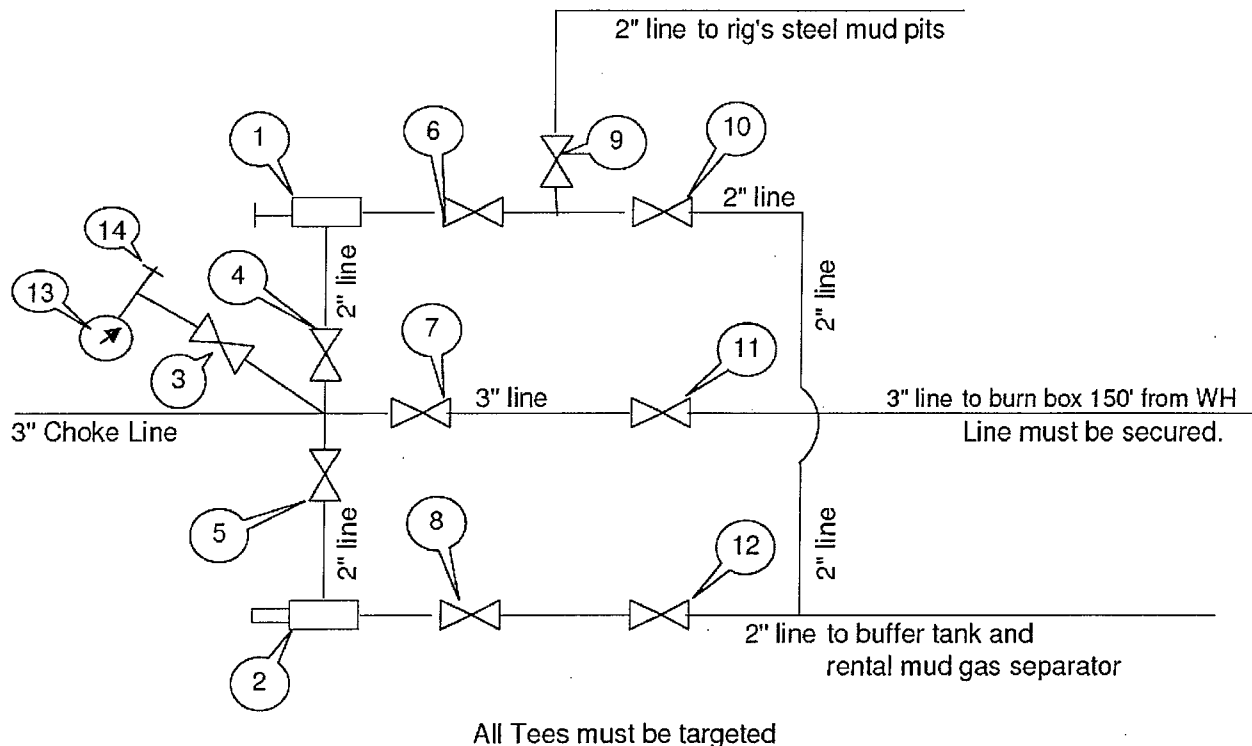


Item	Description
1	Rotating Head, 11"
2A	Fill up Line and Valve
2B	Flow Line (10")
2C	Shale Shakers and Solids Settling Tank
2D	Cuttings Bins for Zero Discharge
2E	Rental Mud Gas Separator with vent line to flare and return line to mud system
3	Annular BOP (11", 3M)
4	Double Ram (11", 3M, equipped with Blind Rams and Pipe Rams)
5	Kill Line (2" flexible hose, 3000 psi WP)
6	Kill Line Valve, Inner (3-1/8", 3000 psi WP)
7	Kill Line Valve, Outer (3-1/8", 3000 psi WP)
8	Kill Line Check Valve (2-1/16", 3000 psi WP)
9	Choke Line (5M Stainless Steel Coflex Line, 3-1/8" 3M API Type 6B, 3000 psi WP)
10	Choke Line Valve, Inner (3-1/8", 3000 psi WP)
11	Choke Line Valve, Outer, (Hydraulically operated, 3-1/8", 3000 psi WP)
12	Adapter Flange (11" 5M to 11" 3M)
13	Spacer Spool (11", 5M)
14	Casing Head (11" 5M)
15	Ball Valve and Threaded Nipple on Casing Head Outlet, 2" 5M
16	Surface Casing

Submitted by: James Chen, Drilling Engineer, Mid-Continent Business Unit, ConocoPhillips Company, 25-Sep-2012

CHOKE MANIFOLD ARRANGEMENT

3M System per Onshore Oil and Gas Order No. 2 utilizing 3M and 5M Equipment



Item	Description
1	Manual Adjustable Choke, 2-1/16", 3M
2	Remote Controlled Hydraulically Operated Adjustable Choke, 2-1/16", 3M
3	Gate Valve, 2-1/16" 5M
4	Gate Valve, 2-1/16" 5M
5	Gate Valve, 2-1/16" 5M
6	Gate Valve, 2-1/16" 5M
7	Gate Valve, 3-1/8" 3M
8	Gate Valve, 2-1/16" 5M
9	Gate Valve, 2-1/16" 5M
10	Gate Valve, 2-1/16" 5M
11	Gate Valve, 3-1/8" 3M
12	Gate Valve, 2-1/16" 5M
13	Pressure Gauge
14	2" hammer union tie-in point for BOP Tester

We will test each valve to 3000 psi from the upstream side.

Submitted by:
 James Chen
 Drilling Engineer, Mid-Continent Business Unit, ConocoPhillips Company
 Date: 21-March-2013

Request for Variance

ConocoPhillips Company

Lease Number: NM LC 080258

Well: Garnet #5

Location: Sec. 15, T17S, R32E

Date: 12/3/2013

Request:

ConocoPhillips Company respectfully requests a variance to install a flexible choke line instead of a straight choke line prescribed in the Onshore Order No. 2, III.A.2.b Minimum standards and enforcement provisions for choke manifold equipment. This request is made under the provision of Onshore Order No. 2, IV Variances from Minimum Standard. The rig to be used to drill this well is equipped with a flexible choke line if the requested variance is approved and determined that the proposed alternative meets the objectives of the applicable minimum standards.

Justifications:

The applicability of the flexible choke line will reduce the number of target tees required to make up from the choke valve to the choke manifold. This configuration will facilitate ease of rig up and BOPE Testing.

Attachments:

- Attachment # 1 Specification from Manufacturer
- Attachment # 2 Mill & Test Certification from Manufacturer

Contact Information:

Program prepared by:

James Chen

Drilling Engineer, ConocoPhillips Company

Phone (832) 486-2184

Cell (832) 768-1647

Date: 26 September 2012



Industrial Products USA, Ltd.

2030 E. 8th Street, Suite B • Greeley, CO 80631

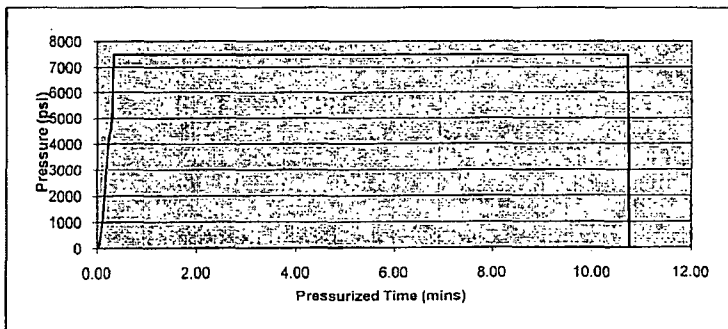
Ph: (970) 346-3751 • Fax: (970) 353-3168 • Toll Free: (866) 771-9739

TEST CERTIFICATE

Customer: PRECISION DRILLING
P.O. #: RIG 822
Invoice #: 27792
Material: 3 1/2" FIREGUARD
Description: 3 1/2" X 10'
Coupling 1: 3 1/2" FLANGE R31
" Serial:
" Quality:
Coupling 2: 3 1/2" FLOATING R31
" Serial:
" Quality:
Working Pressure: 3000
Test Pressure: 7500
Duration (mins): 10

Cert No.: 27792

Date: 9/21/2012



Conducted By: FLORES M.
Test Technician

☒ Acceptable
☐ Not Acceptable



Reliance Eliminator Choke & Kill

This hose can be used as a choke hose which connects the BOP stack to the bleed-off manifold or a kill hose which connects the mud stand pipe to the BOP kill valve.

The Reliance Eliminator Choke & Kill hose contains a specially bonded compounded cover that replaces rubber covered Asbestos, Fibreglass and other fire retardant materials which are prone to damage. This high cut and gouge resistant cover overcomes costly repairs and downtime associated with older designs.

The Reliance Eliminator Choke & Kill hose has been verified by an independent engineer to meet and exceed EUB Directive 36 (700°C for 5 minutes).

Nom. ID		Nom OD		Weight		Min Bend Radius		Max WP	
in.	mm.	in.	mm	lb/ft	kg/m	in.	mm.	psi	Mpa
3	76.2	5.11	129.79	14.5	21.46	48	1219.2	5000	34.47
3-1/2	88.9	5.79	147.06	20.14	29.80	54	1371.6	5000	34.47



Fittings

RC4X5055
RC3X5055
RC4X5575

Flanges

R35 - 3-1/8 5000# API Type 6B
R31 - 3-1/8 3000# API Type 6B

Hammer Unions

All Union Configurations

Other

LP Threaded Connection
Graylock
Custom Ends

Closed Loop System Design, Operating and Maintenance, and Closure Plan

ConocoPhillips Company

Well: Garnet #5

Location: Sec. 15, T17S, R32E

Date: 12/3/2013

ConocoPhillips proposes the following plan for design, operating and maintenance, and closure of our proposed closed loop system for the above named well:

1. We propose to use a closed loop system with steel pits, haul-off bins, and frac tanks for containing all cuttings, solids, mud, water, brine, and liquids. We will not dig a pit, nor will we use a drying pad, nor will we build an earth pit above ground level, nor will we dispose of or bury any waste on location.

All drilling waste and all drilling fluids (fresh water, brine, mud, cuttings, drill solids, cement returns, and any other liquid or solid that may be involved) will be contained on location in the rig's steel pits or in haul-off bins or in frac tanks as needed. The intent is as follows:

- We propose to use the rigs' steel pits for containing and maintaining the drilling fluids.
- We propose to remove cuttings and drilled solids from the mud by using solids control equipment and to contain such cuttings and drilled solids on location in haul-off bins.
- We propose that any excess water that may need to be stored on location will be stored in tanks.

The closed loop system components will be inspected daily by each tour and any needed repairs will be made immediately. Any leak in the system will be repaired immediately, and any spilled liquids and/or solids will be cleaned immediately, and the area where any such spill occurred will be remediated immediately.

2. Cuttings and solids will be removed from location in haul-off bins by an authorized contractor and disposed of at an authorized facility. For this well, we propose the following disposal facility:

R-360 Inc.

4507 West Carlsbad Hwy, Hobbs, NM 88240,

P.O. Box 388; Hobbs, New Mexico 88241

Toll Free Phone: 877.505.4274, Local Phone Number: 432.638.4076

The physical address for the plant where the disposal facility is located is Highway 62/180 at mile marker 66 (33 miles East of Hobbs, NM and 32 miles West of Carlsbad, NM).

The Permit Number for R-360 is NM-01-0006.

A photograph showing the type of haul-off bins that will be used is attached.

3. Mud will be transported by vacuum truck and disposed of at R-360 Inc. at the facility described above.
4. Fresh Water and Brine will be hauled off by vacuum truck and disposed of at an authorized salt water disposal well. We propose the following for disposal of fresh water and brine as needed:
 - Nabors Well Services Company, 3221 NW County Rd; Hobbs, NM 88240, PO 5208 Hobbs, NM, 88241, Permit SWD 092. (Well Location: **Section 3, T19S R37E**)
 - Basic Energy Services, P.O. Box 1869; Eunice, NM 88231 Phone Number: 575.394.2545, Facility located at Hwy 18, Mile Marker 19; Eunice, NM.

James Chen

Drilling Engineer

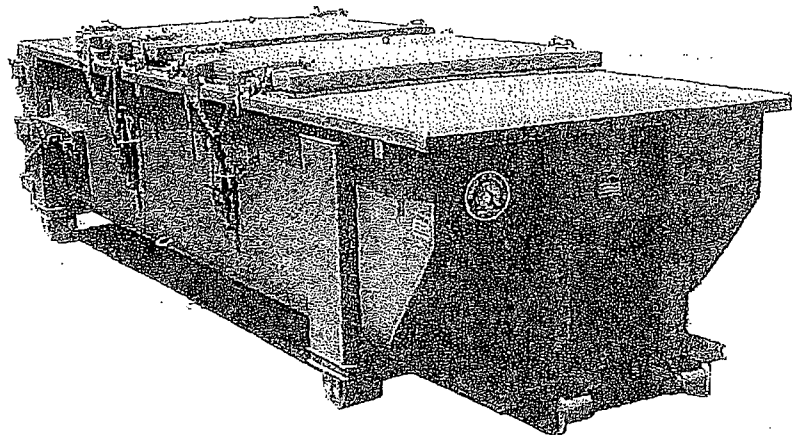
Office: 281-206-5244

Cell: 832.678.1647

SPECIFICATIONS

Heavy Duty Split Metal Rolling Lid

FLOOR: 3/16" PL one piece
 CROSS MEMBER: 3 x 4.1 channel 16" on center
 WALLS: 3/16" PL solid welded with tubing top, inside liner hooks
 DOOR: 3/16" PL with tubing frame
 FRONT: 3/16" PL slant formed
 PICKUP: Standard cable with 2" x 6" x 1/4" rails, gusset at each crossmember
 WHEELS: 10" DIA x 9" long with grease fittings
 DOOR LATCH: 3 Independent ratchet binders with chains, vertical second latch
 GASKETS: Extruded rubber seal with metal retainers
 WELDS: All welds continuous except sub-structure crossmembers
 FINISH: Coated inside and out with direct to metal, rust inhibiting acrylic enamel color coat
 HYDROTESTING: Full capacity static test
 DIMENSIONS: 22'-11" long (21'-8" inside), 99" wide (88" inside), see drawing for height
 OPTIONS: Steel grit blast and special paint, Ampliroll, Heli and Dino pickup
 ROOF: 3/16" PL roof panels with tubing and channel support frame
 LIDS: (2) 68" x 90" metal rolling lids spring loaded, self-raising
 ROLLERS: 4" V-groove rollers with delrin bearings and grease fittings
 OPENING: (2) 60" x 82" openings with 8" divider centered on container
 LATCH: (2) independent ratchet binders with chains per lid
 GASKETS: Extruded rubber seal with metal retainers



CONT.	A	B
20 YD	41	53
25 YD	53	65
30 YD	65	77

