Form 3160 - 3 FORM APPROVED OMB No. 1004-0137 Expires October 31, 2014 (March 2012) OCD Hobbs UNITED STATES UNORTHODOX 5. Lease Serial No. DEPARTMENT OF THE INTERIOR NMLC 031670 (A) BUREAU OF LAND MANAGEMENT 6. If Indian, Allotee or Tribe Name PLICATION FOR PERMIT TO DRILL OR REENTER 7. If Unit or CA Agreement, Name and No. XDRILL la. Type of work: REENTER Southeast Monument Unit 8. Lease Name and Well No. X Oil Well Gas Well X Single Zone lb. Type of Well: **SEMU** Name of Operator 9. API Well No. 30-025-ConocoPhillips Company 3a. Address 600 N. Dairy Ashford Rd, Office P10-4054 3b. Phone No. (include area code) 10. Field and Pool, or Exploratory K (281)206-5020 Skaggs; Grayburg Houston, TX 77079-1175 HOBBS OCD Location of Well (Report location clearly and in accordance with any State requirements.*) 11. Sec., T. R. M. or Blk. and Survey or Area UL O, Sec. 19, T20S, R38E At surface 155' FSL & 1473' FEL; UL O, Sec. 19, T20S, R38E AUG 0 5 2014 At proposed prod. zone same as above 12. County or Parish 13. State 14. Distance in miles and direction from nearest town or post office* Lea County NM Approximately 10 miles southwest of Hobbs, NM RECEIVED Lea County

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RECEIVED Lea County 15. Distance from proposed* 155' 16. No. of acres in lease location to nearest 641.68 property or lease line, ft. (Also to nearest drig, unit line, if any) 40 acres 19. Proposed Depth 20. BLM/BIA Bond No. on file 18. Distance from proposed location* about 750' to nearest well, drilling, completed, applied for, on this lease, ft. 4207' TD/MD ES0085 22. Approximate date work will start* Elevations (Show whether DF, KDB, RT, GL, etc.) 23. Estimated duration 06/01/2014 3534' GL 7 days 24. Attachments The following, completed in accordance with the requirements of Onshore Oil and Gas Order No.1, must be attached to this form: 1. Well plat certified by a registered surveyor. Bond to cover the operations unless covered by an existing bond on file (see Item 20 above). 2. A Drilling Plan. 5. Operator certification 3. A Surface Use Plan (if the location is on National Forest System Lands, the SUPO must be filed with the appropriate Forest Service Office). Such other site specific information and/or plans as may be required by the Name (Printed/Typed) Susan B. Maunder Title Senior Regulatory Specialist Name (Printed/Typed) Approved by (Sign Steve Caffey Office Title CARLSBAD, IELD OFFICE **FIELD MANAGER** Application approval does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon. APPROVAL FOR TWO YEARS Conditions of approval, if any, are attached. Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction. (Continued on page 2) *(Instructions on page 2)

Lea County Controlled Water Basin

Approval Subject to General Requirements & Special Stipulations Attached

SEE ATTACHED FOR CONDITIONS OF APPROVAL

Operator Certification

HOBBS OCD

AUG 0 5 2014

CONOCOPHILLIPS COMPANY

CERTIFICATION:

RECEIVED

I hereby certify that I, or persons under my direct supervision, have inspected the proposed drill site and access route proposed herein; that I am familiar with the conditions which currently exist; that I have full knowledge of State and Federal laws applicable to this operation; that the statements made in this APD package are, to the best of my knowledge, true and correct; and that the work associated with the operations proposed herein will be performed in conformity with this APD package and the terms and conditions under which it is approved. I also certify that I, or the company I represent, am responsible for the operations conducted under this application with bond coverage provided by Nationwide Bond ES0085. These statements are subject to the provisions of 18 U.S.C. 1001 for the filing of false statements.

Susan B. Maunder

Senior Regulatory Specialist

Well Number: SEMU #244

Drilling Plan ConocoPhillips Company SEMU; Grayburg

SEMU #244

HOBBS OCD

AUG 0 5 2014

Lea County, New Mexico

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1. Estimated tops of geological markers and estimated depths to water, oil, or gas formations:.

The datum for these depths is RKB (which is 13' above Ground Level).

Formations	Top Depths FT MD	Contents
Quaternary	Surface	Fresh Water
Rustler	1357	Anhydrite ·
Salado (top of salt)	1466	Salt
Tansill (base of salt)	2536	Gas, Oil and Water
Yates	2665	Gas, Oil and Water
Seven Rivers	2910	Gas, Oil and Water
Queen	3485	Gas, Oil and Water
Penrose	3631	Gas, Oil and Water
Grayburg	3780	Gas, Oil and Water
San Andres	4007	Gas, Oil and Water
Deepest estimated perforation	4007	Deepest estimated perf. is above Top of San Andres
Total Depth (maximum)	4207	200' below deepest estimated perforation

All of the water bearing formations identified above will be protected by setting of the <u>8-5/8"</u> surface casing <u>25' - 70' into the Rustler formation</u> and circulating of cement from casing shoe to surface in accordance with the provisions of Onshore Oil and Gas Order No. 2 and New Mexico Oil Conservation Division Title 19.

The targeted oil and gas bearing formations identified above will be protected by setting of the _____5-1/2" production casing _____10' off bottom of TD ___ and circulating of cement from casing shoe to surface in accordance with the provisions of Onshore Oil and Gas Order No. 2 and New Mexico Oil Conservation Division Title 19.

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2. Proposed casing program:

See COA Safety Factors Hole Interval Calculated per ConocoPhillips Corporate Criteria Size MD RKB (ft) OD Wt MIY Col Jt Str Type Gr Conn Jt Str DF Collapse Burst (Tension) DF DF (in) From То (inches) (lb/ft) (klbs) Dry/Buoyant (psi) (psi) 40' - 85' 0.5" Line Cond 20 0 16 В N/A N/A N/A NA NA NA (30' - 75' BGL) wall Pipe Alt. 40' - 85' 20 0 13-3/8 PΕ 48# H-40 1730 740 N/A NA NA NA (30' - 75' BGL) Cond Surf 12-1/4 n 1382 - 1427' 8-5/8 24# J-55 STC 2950 1370 244 1.38 2.16 3.06 5-1/2 Prod 7-7/8 0 4152' -- 4197' 17# L-80 LTC 7740 6290 338 3.55 4.99 2.72

The casing will be suitable for H₂S Service. All casing will be new.

The surface and production casing will be set approximately 10' off bottom and we will drill the hole with a 45' range uncertainty for casing set depth to fit the casing string so that the cementing head is positioned at the floor for the cement job.

The production casing will be set 155' to 200' below the deepest estimated perforation to provide rathole for the pumping completion and for the logs to get deep enough to log the interval of interest.

Casing Safety Factors - BLM Criteria:

Туре	Depth	Wt	MIY	Col	Jt Str	Drill Fluid	Burst	Collapse	Tensile-Dry	Tens-Bouy
Surface Casing	1427	24	2950	1370	244000	8.5	4.68	2.17	7.1	8.2
Production Casing	4197	17	7740	6290	338000	10	3.55	2.88	4.74	5.59

Casing Safety Factors – Additional ConocoPhillips Criteria:

ConocoPhillips casing design policy establishes Corporate Minimum Design Factors (see table below) and requires that service life load cases be considered and provided for in the casing design.

ConocoPhillips Corporate Criteria for Minimum Design Factors

	Burst	Collapse	Axial
Casing Design Factors	1.15	1.05	1.4

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Depth Wt Type MIY Col Jt Str Pipe Yield MW Burst Col Ten 35000 Conductor 65 432966 Surface Casing (8-5/8* 24# J-55 STC) 1370 244000 Production Casing (5-1/2" 17# L-80 LTC) 4197 6290 338000 397000 Burst - ConocoPhillips Required Load Cases The maximum internal (burst) load on the Surface Casing occurs when the surface casing is tested to 1500 psi (as per BLM Onshore Order 2 - B. Requirements). The maximum Internal (burst) load on the Production Casing occurs during the tracture stimulation where the maximum allowable working pressure (MAWP) is the pressure that would fit ConocoPhilips Corporate Criteria for Minimum Factors. 8.55 ppg Surface Casing Test Pressure = 1500 _{CSI} Predicted Pore Pressure at TD (PPTD) = Surface Rated Working Pressure (BOPE) = 3000 csi Predicted Frac Gradient at Shoe (CSFG) = 19.23 ppc 10 FF9 Surface Casing Burst Safety Factor = API Burst Rating / Maximum Preciated Surface Pressure (MPSP) 'OR' Maximum Allowable Surface Pressure (MASP) Production Casing MAWP for the Fracture Stroutston = API Burst Reford Corporate Minimum Burst Design Factor Surface Casing Burst Safety Factor: Case #1. MPSP (MWhyd next section) = 1427 0.052 10 747 Case #2. MPSP (Field SW @ BullheadcsF3 + 200 psi) = 1427 0.052 19 23 742 200 885 Case #3. MPSP (Kick Vol @ next section TD) = A 197 0.052 8 55 277 631 Case #4. MPSP (PPTD - GG) = 4197 0.052 8.55 419.7 = 1446 Case #3 & #4 Limited to MPSP (CSFG + 0.2 ppg) = 1427 0.052 x(19.23 0.2 1442 MASP (MWhyd + Test Pressure) = 1427 0.052 8 5 1500 Burst Safety Factor (Max. MPSP or MASP) = 2950 2131 1.38 **Production Casing Burst Safety Factor:** Case #1. MPSP (MWhyd TD) = 4197 0.052 10 2182.44 Case #4. MPSP (PPTD - GG) = 4197 0.052 8 55 419.7 Burst Safety Factor (Max. MPSP) = 3.55 7748 2182 MAWP for the Fracture Stimulation (Corporate Criteria) = 7740 Collapse - ConocoPhillips Required Load Cases The maximum collapse had on the Surface Casing occurs when comenting to surface, 1/3 evacuation to the next casing setting depth, or deepest depth of exposure (full evacuation) The maximum collapse load on the Production Casing occurs when cementing to surface, or 1/3 evacuation to the deepest depth of exposure; and therefore, the external pressure profile for the evacuation cases should be equal to the pore pressure of the horizons on the outside of the casing which we assumed to be PPID. Surface Casing Collapse Safety Factor = API Collapse Rating / Full Evacuation 'OR' Cement Displacement during Cementing to Surface Production Casing Collapse Safety Factor = API Collapse Rating / Maximum Predicted Surface Pressure "OR" Cement Displacement during Cementing to Surface 8.34 ppg 13.6 ppg Cement Disclacement Fluid (FVA) = Top of Cement = 11.5 ррд Surface Cement Lead = Prod Cement Lead = Surface Cement Tail = 14.8 ppg Prod Cement Tell = 14 ppg Top of Surface Tail Cament = 350 a Top of Prod Tail Cement = 3000 a Surface Casing Collapse Safety Factor: Full Evacuation Diff Pressure = 1427 0.052 8.55 Cementing Diff Lift Pressure = 1077 0.052 13.6 11) + (350 0.052 619 1 = 412 1370 Collapse Safety Factor = Production Casing Collapse Safety Factor: 1/3 Evacuation Diff Pressure = [[4197 x 0.052 8 55 4197 0.052 8.34]] = 1259 Cementing Diff Lift Pressure = 1197 0.052 11.5) + (3000 0.052 1820] = 1080 Collapse Safety Factor = 6290 Tensial Strength - ConocoPhillips Required Load Cases The maximum axial (tension) load occurs if casing were to get stuck and pulled on to try to get it unstuck. Maximum Allowable Axial Load for Pipe Yield = API Pipe Yield Strength Rating / Corporate Minimum Axial Design Factor Maximum Allowable Axial Load for Joint = API Joint Strength Rating / Corporate Minimum Axial Design Factor Maximum Allowable Hock Load (Limbed to 75% of Rig Max Load) = Maximum Allowable Axial Load Maximum Allowable Overput Margin = Maximum Allowable Hook Load - Bouyant WI of the String Tensial Safety Factor = API Pipe Yield 'OR' API Joint Strength 'OR' Ris. Max. Load Raling / (Bouyant Wit of String + Minimum Overpul Required)

Rig Max Load (300,000 bs) x 75% = 225000 bs
Minimum Overpul Required = 50000 bs Surface Casing Tensial Strength Safety Factor: Air WI = 34748 Bouvant Wt = 3424R 0.870 29804 Max. Allowable Axial Load (Pipe Yield) = 381000 272143 1.40 Max. Allowable Axial Load (Joint) = 244008 Max. Allowable Hook Load (Limited to 75% of Rig Max Load) = 174286 Max. Allowable Overpull Margin = 174286 3424R 0.870 144482 Tensial Safety Factor = 244000 29804 50000 Production Casing Tensial Strength Safety Factor: 71349 71349 60456 Bouyant Wt = Max. Allowable Axial Load (Pipe Yield) = Max. Allowable Axial Load (Joint) = 397000 1 40 283571 338000 241429 Max. Allowable Hook Load (Limited to 75% of Rig Max Load) = 225000 Max. Allowable Overpull Margin = Tensial Safety Factor = 225000 71349 0.847 164544 300000 7 i 60456 50000 Compression Strength - ConocoPhillips Required Load Cases The maximum axial (compression) load for the well is where the surface casing is landed on the conductor with a support of a plate or landing ring. The surface casing is also calculated to bear 60% of the load but not limited. Any other axial loads such as a snubbing unit or other would need to be added to the load. Compression Safety Factor = API Axial Joint Strength Rating 'OR' API Axial Pice Yield Rating/ Maximum Predicted Load Weltrend Lond = 3000 Es Conductor & Surface Compression Safety Factor Surf Casing Wt (Bouyant) = 34248 0.870 29804 (× 60456 Prod Casing W1 (Bouyant) = 71349 0.847 6.5 Tubing Vot (Air Wt) = 4197 27281 Tubing Fluid Wt = 0.052 0.7854 x 2.441 42 = 6690 4197 6.55 Load on Conductor = Conductor Compression Safety Factor = 432966 127230 3.40 Load on Surface Casing = 127230 60% 76338 Surface Casing Compression Safety Factor = 244000 76338 **SEMU #244** (Date: 1/9/2014) Page 3 of 11

3. Proposed cementing program:

16" or 13-3/8" Conductor:

Cement to surface with rathole mix, ready mix or Class C Neat cement. (Note: The gravel used in the cement is not to exceed 3/8" diameter) TOC at surface.

8-5/8" Surface Casing Cementing Program:

The intention for the cementing program for the Surface Casing is to:

- Place the Tail Slurry from the casing shoe to 350' above the casing shoe,
- Bring the Lead Slurry to surface.

Spacer: 20 bbls Fresh Water

	Slurry	Inter Ft N	rvals MD	Weight ppg	Sx	Vol Cuft	Additives	Yield ft ³ /sx
Lead	Class C	Surface	1032' – 1077'	13.6	450	765	+ 2% Extender + 2% CaCl ₂ + 0.125 lb/sx Lost Circulation Control Agent + 0.2% Defoamer Excess =200% based on gauge hole volume	1.70
Tail	Class C	1032' – 1077'	1382' – 1427'	14.8	300	402	1% CaCl2 Excess = 100% based on gauge hole volume	1.34

Displacement: Fresh Water.



Note: In accordance with the Pecos District Conditions of Approval, we will Wait on Cement (WOC) for a period of not less than 18 hrs after placement or until at least 500 psi compressive strength has been reached in both the Lead Slurry and Tail Slurry cements on the Surface Casing, whichever is greater.

5-1/2" Production Casing Cementing Program – Single Stage Cementing Option:

The intention for the cementing program for the Production Casing – Single Stage Cementing Option is to:

(Date: 1/9/2014)

- Place the Tail Slurry from the casing shoe to above the top of the Grayburg,
- Bring the Lead Slurry to surface.

Spacer: 20 bbls Fresh Water

	Slurry		Intervals Ft MD		Sx	Vol Cuft	Additives	Yield ft³/sx
Lead	C Gas Tight Slurry	Surface	3000'	11.5	400	1292	Class C 94 lb/sx 6% Extender 10% Gas Migration Control 2% Sodium Metasilicate (dry) 1% Cement Bonding Agent 3% Aluminum Silicate 0.125 lb/sx Cello Flake 3 lb/sx LCM-1	3.23
Tail	Poz/C Gas Tight Slurry	3000'	4152' – 4197'	14.0	320	438	(35:65) Poz:C 33 lb/sx 1% Sodium Metasilicate (dry) 1.5% Fluid Loss Control,	1.37

Displacement: Fresh Water with approximately 250 ppm gluteraldehyde biocide.

5-1/2" Production Casing Cementing Program - Two-Stage Cementing Option (Shallow Flow):

ConocoPhillips Company respectfully requests the options to our cementing program. The intention for the cementing program for the Production Casing – Two-Stage Cementing Option is to:

- Provide a contingency plan for using a Stage Tool and Annulus Casing Packer(s) to isolate shallow saltwater or gas flow if either of these events occurs while drilling the well.
- Place the Stage 1 Cement from the casing shoe to surface.
- Proceed with Stage 2 Cement only if cement returns are contaminated or flow was observed after pumping 1st stage.

Spacer: 20 bbls Fresh Water

Stage 1 - Slurry			Intervals Ft MD		Weight Sx ppg		Additives	Yield ft³/sx
Lead	C Gas Tight Slurry	Surface	3000'.	11.5	400	1292	1% Cement Bonding Agent 3% Aluminum Silicate 0.125 lb/sx Cello Flake 3 lb/sx LCM-1	3.23
Tail	Poz/C Gas Tight Slurry	3000'	4152' – 4197'	14.0	320	438	(35:65) Poz:C 33 lb/sx 1% Sodium Metasilicate (dry) 1.5% Fluid Loss Control,	1.37

^{1&}lt;sup>st</sup> stage displacement: FW followed by Weighted Spacer

Spacer: Remaining Weighted Spacer in cementing lines from the 1st stage displacement

St	age 2 - Slurry		Intervals Ft MD		Sx	Vol Cuft	Additives	Yield ft³/sx
Tail	Class C	Surface	Stage Tool ~1450'	14.8	300	402	1% CaCl2 Excess = 100% based on gauge hole volume	1.34

^{2&}lt;sup>nd</sup> stage displacement: Fresh Water

<u>5-1/2" Production Casing Cementing Program – Two-Stage Cementing Option (Lower Zone Losses or Waterflow):</u>

ConocoPhillips Company respectfully requests the options to our cementing program. The intention for the cementing program for the Production Casing – Two-Stage Cementing Option is to:

- Provide a contingency plan for using a Stage Tool and Annulus Casing Packer(s) to isolate losses or waterflow if either of these events occurs while drilling the well.
- Place the Stage 1 Cement from the casing shoe to the stage tool,
- Bring Stage 2 Cement from the stage tool to surface.

Spacer: 20 bbls Fresh Water See COA

Stag	Stade 1 - Slurry		vals #D	Weight ppg	Sx	Vol Cuft	Additives	Yield ft ³ /sx
Lead	Poz/C Gas Tight Slurry	Stage Tool ~2900'	4152' – 4197'	14.0	320	438	(35:65) Poz:C 33 lb/sx 1% Sodium Metasilicate (dry) 1.5% Fluid Loss Control,	1.37

^{1&}lt;sup>st</sup> stage displacement: FW followed by Brine

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Spacer: 20 bbls Fresh Water

Stag	je 2 - Slurry	f ·	vals MD	Weight ppg	Sx	Vol Cuft	Additives	Yield ft ³ /sx
Lead	C Gas Tight Slurry	Surface	Stage Tool ~2900'	11.5	400	1292	Class C 94 lb/sx 6% Extender 10% Gas Migration Control 2% Sodium Metasilicate (dry) 1% Cement Bonding Agent 3% Aluminum Silicate 0.125 lb/sx Cello Flake 3 lb/sx LCM-1	3.23

Displacement: Fresh Water

Proposal for Option to Adjust Production Casing Cement Volumes:

The production casing cement volumes for the proposed single stage and two-stage option presented above are estimates based on gauge hole. We will adjust these volumes based on the caliper log data for each well and our trends for amount of cement returns to surface. Also, if no caliper log is available for any particular well, we would propose an option to possibly increase the production casing cement volume to account for any uncertainty in regard to the hole volume.

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4. Pressure Control Equipment:

A <u>11" 3M</u> system will be installed, used, maintained, and tested accordingly as described in Onshore Oil and Gas Order No. 2.

Our BOP equipment will be:

- Rotating Head
- o Annular BOP, 11" 3M
- o Blind Ram, 11" 3M
- o Pipe Ram, 11" 3M

After nippling up, and every 30 days thereafter or whenever any seal subject to test pressure is broken followed by related repairs, blowout preventors will be pressure tested. BOP will be inspected and operated at least daily to insure good working order. All pressure and operating tests will be done by an independent service company and recorded on the daily drilling reports. BOP will be tested using a test plug to isolate BOP stack from casing. BOP test will include a low pressure test from 250 to 300 psi for a minimum of 10 minutes or until requirements of test are met, whichever is longer. Ram type preventers and associated equipment will be tested to the approved stack working pressure of 3000 psi isolated by test plug. Annular type preventers will be tested to 50 percent of rated working pressure, and therefore will be tested to 1500 psi. Pressure will be held for at least 10 minutes or until provisions of test are met, whichever is longer. Valve on casing head below test plug will be open during testing of BOP stack. BOP will comply with all provisions of Onshore Oil and Gas Order No. 2 as specified. See Attached BOPE Schematic. A variance is respectfully requested to allow for the use of flexible hose. The variance request is included as a separate enclosure with attachments.

5. Proposed Mud System:

The mud systems that are proposed for use are as follows:

DEPTH	TYPE	Density ppg	FV sec/qt	API Fluid Loss cc/30 min	рН	Vol bbl
0 – Surface Casing Point	Fresh Water or Fresh Water Native Mud in Steel Pits	8.5 – 9.0	28 – 40	N.C.	N.C.	150 – 300
Surface Casing Point to TD	Brine (Saturated NaCl ₂) in Steel Pits	10	29	N.C.	10 – 11	300 – 1000
Conversion to Mud at TD	Brine Based Mud (NaCl ₂) in Steel Pits	10	33 – 40	5 – 10	10 – 11	0 – 1000

Gas detection equipment and pit level flow monitoring equipment will be on location. A flow paddle will be installed in the flow line to monitor relative amount of mud flowing in the non-pressurized return line. Mud probes will be installed in the individual tanks to monitor pit volumes of the drilling fluid with a pit volume totalizer. Gas detecting equipment and H2S monitor alarm will be installed in the mud return system and will be monitored. A mud gas separator will be installed and operable before drilling out from the Surface Casing. The gases shall be piped into the flare system. Drilling mud containing H2S shall be degassed in accordance with API RP-49, item 5.14.

In the event that the well is flowing from a waterflow, then we would discharge excess drilling fluids from the steel mud pits through a fas-line into steel frac tanks at an offset location for containment. Depending on the rate of waterflow, excess fluids will be hauled to an approved disposal facility, or if in suitable condition, may be reused on the next well.

No reserve pit will be built.

Proposal for Option to Not Mud Up at TD:

FW, Brine, and Mud volume presented above are estimates based on gauge 12-1/4" or 7-7/8" holes. We will adjust these volume based on hole conditions. We do not plan to keep any weighting material at the wellsite. Also, we propose an option to not mud up leaving only brine in the hole if we have good hole stability.

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6. Logging, Coring, and Testing Program:

- a. No drill stem tests will be done
- b. Remote gas monitoring planned for the production hole section (optional).
- c. No whole cores are planned
- d. The open hole electrical logging program is planned to be as follows:
 - Total Depth to 1700' MD: Spectral Gamma Ray, PE, Resistivity (laterologs), Bulk Density, and Sonic
 - Total Depth to surface Casing Shoe: Caliper
 - Total Depth to surface, Total Gamma Ray and Neutron
 - Total Depth to 2350' MD; Mud Log (optional)
 - Total Depth to 2350' MD : Dielectric Scanner (optional)
 - Formation pressure data (XPT) on electric line if needed (optional)
 - Rotary Sidewall Cores on electric line if needed (optional)
 - FMI (Formation MicroImager) if needed (optional)
 - UBI (Ultrasonic Borehole Imager) if needed (optional)
- e. Cement Bond Log (optional).

7. Abnormal Pressures and Temperatures:

- No abnormal pressures are expected to be encountered.
- Loss of circulation is a possibility in the horizons below the Top of Grayburg. We expect that normal Loss of Circulation Material will be successful in healing any such loss of circulation events.



- o The bottom hole pressure is expected to be 7.8 ppg gradient.
- o The expected Bottom Hole Temperature is 100 degrees F.
- The estimated H₂S concentrations and ROE calculations for the gas in the zones to be penetrated are presented in the table below for the various producing horizons in this area:

FORMATION / ZONE	H2S (PPM)	Gas Rate (MCFD)	ROE 100 PPM	ROE 500 PPM
Seven Rivers	6	50 - 100 MCFD	0	0
Grayburg / San Andres	18360	20 - 50 MCFD	95	43

ConocoPhillips will comply with the provisions of Oil and Gas Order # 6, Hydrogen Sulfide Operations. Also, ConocoPhillips will provide an H2S Contingency Plan (please see copy attached) and will keep this plan updated and posted at the wellsite during the drilling operation.

8. Anticipated starting date and duration of operations:

Well pad and road constructions will begin as soon as all agency approvals are obtained. Anticipated date to drill these wells begin in mid 2014 after receiving approval of the APD.

(Date: 1/9/2014)

Attachments:

- Attachment # 1 Two-stage Cementing Schematic
- Attachment # 2 BOP and Choke Manifold Schematic 3M System
- Attachment # 3...... Diagram of Choke Manifold Equipment

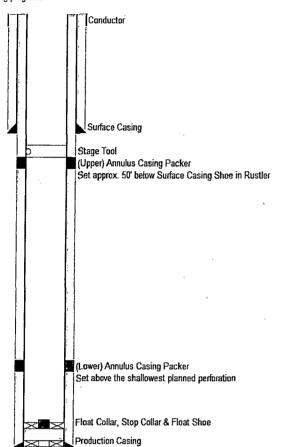
Contact Information:

Proposed 9 January 2014 by: Steven Herrin Drilling Engineer, ConocoPhillips Company Phone (281) 206-5115 Cell (432) 209-7558 SEMU #244

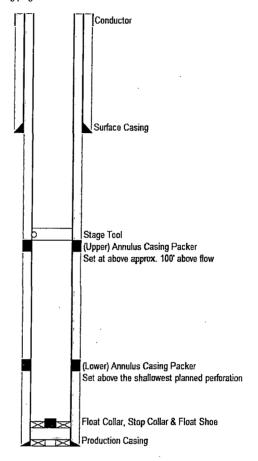
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Attachment # 1

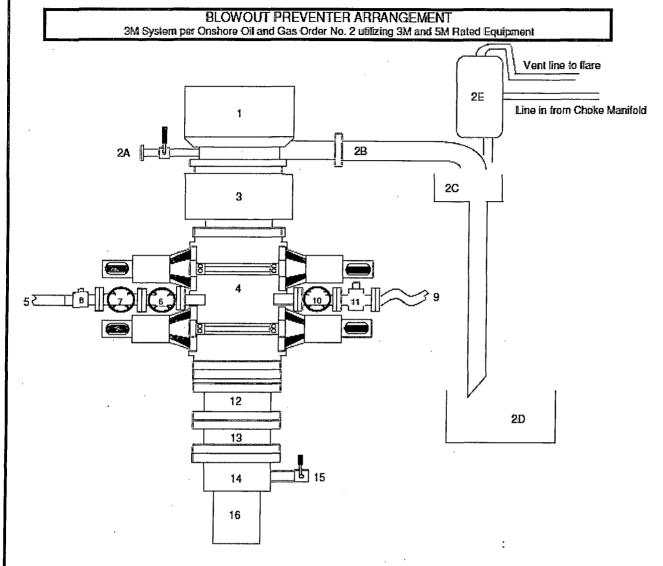
Two-Stage Cementing (Alternative for Shallow Gas / Salt Water / Gas & Water Flow)
Provide contingency plan for using two-stage cementing for the
production casing cement job if gas flow occurs during the
drilling operations. See APD Drill Plan Section 3. Proposed
cementing program.



Two-Stage Cementing (Alternative for Oil / Water / Gas & Water Flow)
Provide contingency plan for using two-stage cementing for the
production casing cement job if oil or water flow occurs during
the drilling operations. See APD Drill Plan Section 3. Proposed
cementing program.



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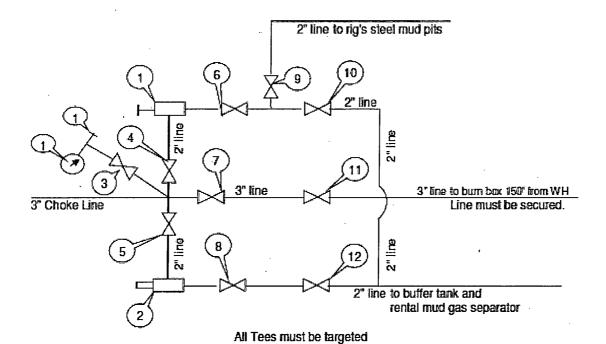
Description Item Rotating Head, 11" Fill up Line and Valve 2A 2B Flow Line (10") 2C Shale Shakers and Solids Settling Tank 2D Cuttings Bins for Zero Discharge Rental Mud Gas Separator with vent line to flare and return line to mud system 2E 3 Annular BOP (11*, 3M) Double Ram (11*, 3M, equipped with Blind Rams and Pipe Rams) 4 Kill Line (2" flexible hose, 3000 psi WP) Kill Line Valve, Inner (3-1/8", 3000 psi WP) 6 7 Kill Line Valve, Outer (3-1/8", 3000 psi WP) Kill Line Check Valve (2-1/16", 3000 psi WP 8 9 Choke Line (5M Stainless Steel Coflex Line, 3-1/8* 3M API Type 6B, 3000 psi WP) Choke Line Valve, Inner (3-1/8", 3000 psi WP) 10 Choke Line Valve, Outer, (Hydraulically operated, 3-1/8", 3000 psi WP) 11 Adapter Flange (11" 5M to 11" 3M) 12 Spacer Spool (11", 5M) 13 Casing Head (11" 5M) 14 15 Ball Valve and Threaded Nipple on Casing Head Outlet, 2" 5M Surface Casing

Submitted by: Steven Herrin, Drilling Engineer, Mid-Continent Business Unit, ConocoPhillips Company, 03-Jan-2014

(Date: 1/9/2014)

CHOKE MANIFOLD ARRANGEMENT

3M System per Onshore Oil and Gas Order No. 2 utilizing 3M and 5M Equipment



Item Description

- Manual Adjustable Choke, 2-1/16", 3M
- Remote Controlled Hydraulically Operated Adjustable Choke, 2-1/16", 3M 2
- 3 Gate Valve, 2-1/16" 5M
- Gate Valve, 2-1/16" 5M 4
- 5 Gate Valve, 2-1/16" 5M
- 6 Gate Valve, 2-1/16" 5M
- 7 Gate Valve, 3-1/8" 3M
- 8 Gate Valve, 2-1/16" 5M
- 9 Gate Valve, 2-1/16" 5M
- 10 Gate Valve, 2-1/16" 5M
- Gate Valve, 3-1/8" 3M 11
- 12 Gate Valve, 2-1/16" 5M
- 13 Pressure Gauge
- 14 2" hammer union tie-in point for BOP Tester

We will test each valve to 3000 psi from the upstream side.

Submitted by:

Steven Herrin

Drilling Engineer, Mid-Continent Business Unit, ConocoPhillips Company

Date: 3-January-2014

Page 11 of 11 (Date: 1/9/2014)

Request for Variance

ConocoPhillips Company

Lease Number: NMLC031670 (A)

Well: SEMU #244

Location: Sec. 19, T20S, R38E

Date: 1/2/2014

Request:

ConocoPhillips Company respectfully requests a variance to install a flexible choke line instead of a straight choke line prescribed in the Onshore Order No. 2, III.A.2.b Minimum standards and enforcement provisions for choke manifold equipment. This request is made under the provision of Onshore Order No. 2, IV Variances from Minimum Standard. The rig to be used to drill this well is equipped with a flexible choke line if the requested variance is approved and determined that the proposed alternative meets the objectives of the applicable minimum standards.

Justifications:

The applicability of the flexible choke line will reduce the number of target tees required to make up from the choke valve to the choke manifold. This configuration will facilitate ease of rig up and BOPE Testing.

Attachments:

- Attachment # 1 Specification from Manufacturer
- Attachment # 2 Mill & Test Certification from Manufacturer

Contact Information:

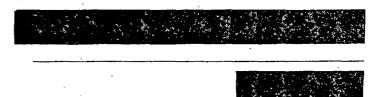
Program prepared by:

Steven Herrin

Drilling Engineer, ConocoPhillips Company

Phone: (281) 206-5115 Cell: (432) 209-7558 Date: 2 January 2014









Reliance Eliminator Choke & Kill

This hose can be used as a choke hose which connects the BOP stack to the bleed-off manifold or a kill hose which connects the mud stand pipe to the BOP kill valve.

The Reliance Eliminator Choke & Kill hose contains a specially bonded compounded cover that replaces rubber covered Asbestos, Fibreglass and other fire retardant materials which are prone to damage. This high cut and gouge resistant cover overcomes costly repairs and downtime associated with older designs.

The Reliance Eliminator Choke & Kill hose has been verified by an independent engineer to meet and exceed EUB Directive 36 (700°C for 5 minutes).

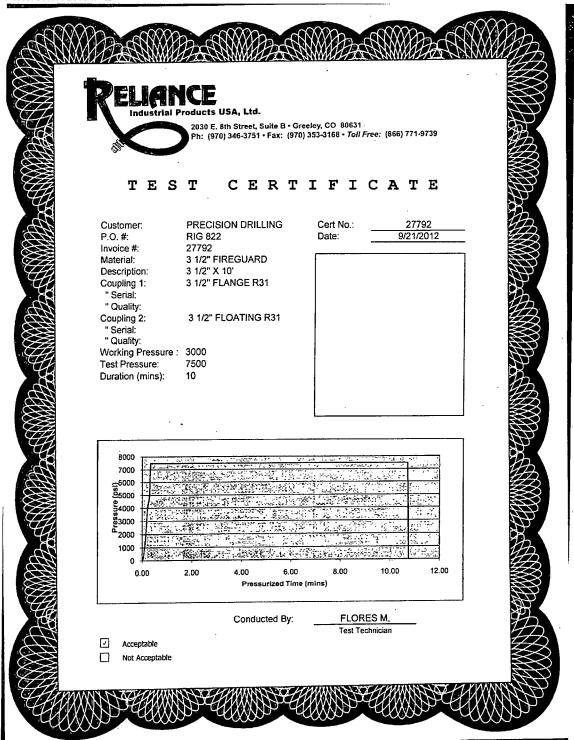
Non	n. ID	Nor	n OD	We	ight	Min Be	nd Radius	Max	WP
in.	mm.	in.	mm	lb/ft	kg/m	in.	mm.	psi	Мра
3	76.2	5.11	129.79	14.5	21.46	48	1219.2	5000	34.47
3-1/2	88.9	5.79	147.06	20.14	29.80	54	1371.6	5000	34.47



Fittings	•
RC4X5055	
RC3X5055	
RC4X5575	

Flanges R35 - 3-1/8 5000# API Type 6B R31 - 3-1/8 3000# API Type 6B Hammer Unions
All Union Configurations

Other
LP Threaded Connectio
Graylock
Custom Ends



Closed Loop System Design, Operating and Maintenance, and Closure Plan

ConocoPhillips Company

Well: SEMU #244

Location: Sec. 19, T20S, R38E

Date: 1/2/2014

ConocoPhillips proposes the following plan for design, operating and maintenance, and closure of our proposed closed loop system for the above named well:

1. We propose to use a closed loop system with steel pits, haul-off bins, and frac tanks for containing all cuttings, solids, mud, water, brine, and liquids. We will not dig a pit, nor will we use a drying pad, nor will we build an earth pit above ground level, nor will we dispose of or bury any waste on location.

All drilling waste and all drilling fluids (fresh water, brine, mud, cuttings, drill solids, cement returns, and any other liquid or solid that may be involved) will be contained on location in the rig's steel pits or in haul-off bins or in frac tanks as needed. The intent is as follows:

- We propose to use the rigs' steel pits for containing and maintaining the drilling fluids.
- We propose to remove cuttings and drilled solids from the mud by using solids control equipment and to contain such cuttings and drilled solids on location in haul-off bins.
- We propose that any excess water that may need to be stored on location will be stored in tanks.

The closed loop system components will be inspected daily by each tour and any needed repairs will be made immediately. Any leak in the system will be repaired immediately, and any spilled liquids and/or solids will be cleaned immediately, and the area where any such spill occurred will be remediated immediately.

2. Cuttings and solids will be removed from location in haul-off bins by an authorized contractor and disposed of at an authorized facility. For this well, we propose the following disposal facility:

R-360 Inc.

4507 West Carlsbad Hwy, Hobbs, NM 88240,

P.O. Box 388; Hobbs, New Mexico 88241

Toll Free Phone: 877.505.4274, Local Phone Number: 432.638.4076

The physical address for the plant where the disposal facility is located is Highway 62/180 at mile marker 66 (33 miles East of Hobbs, NM and 32 miles West of Carlsbad, NM).

The Permit Number for R-360 is NM-01-0006.

A photograph showing the type of haul-off bins that will be used is attached.

- 3. Mud will be transported by vacuum truck and disposed of at R-360 Inc. at the facility described above.
- 4. Fresh Water and Brine will be hauled off by vacuum truck and disposed of at an authorized salt water disposal well. We propose the following for disposal of fresh water and brine as needed:
 - Nabors Well Services Company, 3221 NW County Rd; Hobbs, NM 88240, PO 5208 Hobbs, NM, 88241, Permit SWD 092. (Well Location: Section 3, T19S R37E)
 - Basic Energy Services, P.O. Box 1869; Eunice, NM 88231 Phone Number: 575.394.2545, Facility located at Hwy 18, Mile Marker 19; Eunice, NM.

Steven Herrin Drilling Engineer, ConocoPhillips Company Phone (281) 206-5115 Cell (432) 209-7558

SPECIFICATIONS

FLOOR: 3/16" PLone piece CROSS MEMBER: 3 x 4.1 channel 16" on

WALLS: 3/16" PL solid welded with tubing

top, insi de liner hooks DOOR: 3/16" RL wiln tubing frame

FRONT: 3/16 PL slant formed
FRONT: 3/16 PL slant formed
PICK U.P: Standard cable with 2 x 6 x 1/4 rails, guisset at each crossmember
WHEELS: 10 DIA x 9 long with rease fittings
DOOR LATICH: 3 Independent ratcher
binders, with chains, vertical second laton
GASKETS: Extruded rubber seal with metal retainers

WELDS: All welds continuous except sub

structure crossmembers
FINISH: Coated inside and out with direct to metal, riust inhibiting acrylic enamel color coat.
HYDROTESTING: Full capacity static test DIMEN SIONS: 22:11 long (21:8' inside), 99' wide (88' inside), see drawing for feight OPTIONS: Steel grit blast and special paint. Amplire II, Heil and Dine pickup

ROOF: 3/16" PL roof panels with tubing and channe support frame

LIDS: (2):68" x 90" metal rolling lids spring loaded, self raising ROLLERS: 4" V-groove rollers with defrin

bearings and grease fittings OPENING: (2) 60" x 82" openings

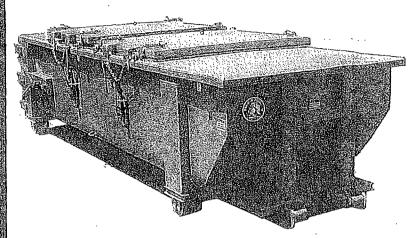
with 8" divider centered on:

container

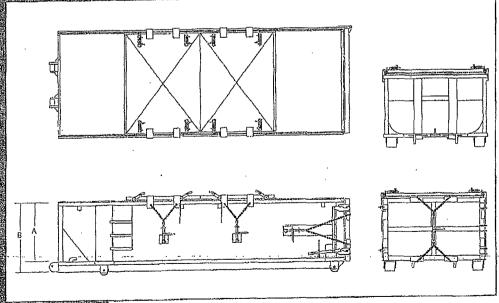
LATCH:(2) independent ratchet binders with chains

GASKETS: Extruded rubber seal with metal retainers

Heavy Duty Split Metal Rolling Lid



CONT.	Α	В
20 YD	41	53
25 YD	53	65
30 YD	65	77



ConocoPhillips

Location Schematic and Rig Layout for Closed Loop System

(PICTURE NOT TO SCALE)

Reviewed by: Steven Herrin Drilling Engineer, ConocoPhillips Company Date: updated January 2014

NOTE: There are two muster areas depending on the prevailing wind direction, generally south in this area. The muster area that is furthest upwind/crosswind will be the designated area for briefing and assessing the situation. In the event a full evacuation is deemed necessary, all personnel will exit the location via the access road. If the main access road is blocked off, they will exit via a secondary road (if available) or walk off route in the upwind/crosswind direction.

