Form 3160-5 (June 2015) DF B SUNDRY Do not use th	bad R	FORM APPROVED OMB NO. 1004-0137 Expires: January 31, 2018 5. Lease Serial No. NMLC063228 CIGNIA Clease or Tribe Name CIGNIA CLEASE OF CA/Agreement, Name and/or No. 8. Well Name and No.							
DEC 0 gauantooned we	CDE	Lightian Unitee or Tribe Name							
SUBMITIN		Y. Mor CA/Agreement, Name and/or No.							
<ol> <li>Type of Well</li> <li>Gas Well</li> <li>Otl</li> </ol>	her				8. Well Name and No. TRISTE DRAW 25 FEDERAL 5H				
2. Name of Operator CIMAREX ENERGY COMPA		ARICKA EAS @cimarex.com			9. API Well No. 30-025-42105-00-X1				
3a. Address 202 S CHEYENNE AVE SUIT TULSA, OK 74103	FE 1000	3b. Phone No Ph: 918.56	. (include area code) 0.7060		10. Field and Pool or E TRISTE DRAW-				
4. Location of Well (Footage, Sec., 7	T., R., M., or Survey Description,	)			11. County or Parish, S	State			
Sec 25 T23S R32E SESE 370 32.269494 N Lat, 103.623858					LEA COUNTY, I	, NM			
12. CHECK THE A	PPROPRIATE BOX(ES)	TO INDICA	TE NATURE OF	F NOTICE,	REPORT, OR OTH	IER DATA			
TYPE OF SUBMISSION			TYPE OF	ACTION					
Notice of Intent	Acidize	Dee	pen Iraulic Fracturing	_	ion (Start/Resume)	□ Water Shut-Off			
Subsequent Report	□ Alter Casing □ Subsequent Report □ Final Abandonment Notice □ Change Plans				ation	<ul> <li>Well Integrity</li> <li>Other</li> </ul>			
Final Abandonment Notice					arily Abandon	Change to Original A PD			
	Convert to Injection		g Back	U Water I					
13. Describe Proposed or Completed Op If the proposal is to deepen direction Attach the Bond under which the wo following completion of the involve testing has been completed. Final A determined that the site is ready for the final of the first second	ally or recomplete horizontally, ork will be performed or provide d operations. If the operation re- bandonment Notices must be fil	give subsurface the Bond No. o sults in a multin	locations and measure n file with BLM/BIA le completion or reco	Required su	ertical depths of all pertin bsequent reports must be new interval, a Form 316	ent markers and zones. filed within 30 days 0-4 must be filed once			
Cimarex respectfully request well. Cimarex proposes to cl disturbance is required for the	hange the SHL there by cl	iginal drilling hanging the o	plan for the abov lirectional plan. N	e reference lo additiona	d I				
Approved: 370 FSL & 1270 FEL, Sec 25	-23S-23F								
Proposed: 310 FSL & 1270 FEL, Sec 25			SEE	ATTA					
Please also change the casin Surface:		DW:	SEE ATTACHED FOR CONDITIONS OF APPROVAL						
<ol> <li>I hereby certify that the foregoing is</li> <li>Commit</li> </ol>	Electronic Submission #	ENERGY CO	MPANY, sent to t	he Hobbs	-				
Name (Printed/Typed) ARICKA	EASTERLING		Title REGUL	ATORY AN	ALYST				
Signature (Electronic	Submission)		Date 11/22/20	016					
	THIS SPACE FO	R FEDER	L OR STATE	OFFICE U	SE				
Approved By	luto		Title AFM -	-lands	k Minerals	Date 12/02/16			
Conditions of approval, if any, are attached certify that the applicant holds legal or equivient would entitle the applicant to condu-	uitable title to those rights in the	not warrant or subject lease	Office Car	Isbad	Field DI	FRICE.			
Title 18 U.S.C. Section 1001 and Title 43 States any false, fictitious or fraudulent				willfully to ma	ake to any department or	agency of the United			
(Instructions on page 2) ** BLM REV	ISED ** BLM REVISED	) ** BLM R	EVISED ** BLM	I REVISED	) ** BLM REVISEI	D**			

# Additional data for EC transaction #358826 that would not fit on the form

### 32. Additional remarks, continued

Hole size: 17-1/2" Csg size: 13-3/8' Weight:48 Grade: H-40/J-55 Hybrid Conn: STC Set Depth: 1270'

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Intermediate: Hole size: 12-1/4" Csg size:9-5/8" Weight: 36 Grade:J-55 Conn: LTC Set Depth: 5000'

Production Hole size: 8-3/4" Csg size: 5-1/2" Weight:17 Grade:L-80 Conn:LTC/BTC Set Depth: 14464'

Please see the attached drilling plan for changes to cement design and other wellbore changes.

## **1. Geological Formations**

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See

TVD of target 9,860PiloMD at TD 14,464Dee

Pilot Hole TD N/A Deepest expected fresh water

Formation	Depth (TVD) from KB	Water/Mineral Bearing/Target Zone	Hazards
Rustler	1240	N/A	
Salt	1730	N/A	
Base of salt	4800	N/A	
Lamar	4990	N/A	
Delaware Sands	5030	N/A	
Brushy Canyon	7360	Hydrocarbons	
Bone Spring	8850	Hydrocarbons	
Avalon Shale	9370	Hydrocarbons	
Avalon Target	9860	Hydrocarbons	

# 2. Casing Program

Hole Size	Casing Depth From	Casing Depth To	Casing Size	Weight (lb/ft)	Grade	Conn.	SF Collapse	SF Burst	SF Tension
17 1/2	0	1270	13-3/8"	48.00	H-40/J-55 Hybrid	ST&C	1.27	2.98	5.28
12 1/4	0	5000	9-5/8"	36.00	J-55	LT&C	1.17	1.34	2.52
8 3/4	0	9122	5-1/2"	17.00	L-80	LT&C	1.44	1.77	2.02
8 3/4	9122	14464	5-1/2"	17.00	L-80	BT&C	1.33	1.64	31.64
				BLM	BLM Minimum Safety Factor		1.125	1	1.6 Dry 1.8 Wet

All casing strings will be tested in accordance with Onshore Oil and Gas Order #2 III.B.1.h

	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Does casing meet API specifications? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y
Will the intermediate pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	N
f yes, does production casing cement tie back a minimum of 50' above the Reef?	N
s well within the designated 4 string boundary.	N
s well located in SOPA but not in R-111-P?	N
f yes, are the first 2 strings cemented to surface and 3rd string cement tied back 500' into previous casing?	N
s well located in R-111-P and SOPA?	N
f yes, are the first three strings cemented to surface?	N
s 2nd string set 100' to 600' below the base of salt?	N
s well located in high Cave/Karst?	N
f yes, are there two strings cemented to surface?	N
For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	N
s well located in critical Cave/Karst?	N
f yes, are there three strings cemented to surface?	N
the second s	

# Cimarex Energy Co., Triste Draw 25 Federal #5H

# 3. Cementing Program

Intermediate

Production

Casing	# Sks	Wt. Ib/gal	Yld ft3/sack	H2O gal/sk	500# Comp. Strength (hours)	ength					
Surface	605	13.50	1.75	8.83	15.5	15.5 Lead: Class C + Bentonite + Calcium Chloride + LCM					
	165 14.80 1.34			6.32	9.5						
Intermediate	937	12.90	1.88	9.65	30	Lead: 35:65 (Poz:C) + Salt + Bentonite + LCM + Retarder					
	292 14.80 1.34		6.32	9.5							
Production	578	10.80	2.35	9.60	17:43	Lead: Tuned Light I Class H					
	1143	14.20	1.30	5.86	14:30	0 Tail: 50:50 (Poz:H) + Salt + Bentonite + Fluid Loss + Dispersant + SMS					
Casing String			тос			% Excess					
Surface						0					

0

4800

44

17

Drilling Plan

### 4. Pressure Control Equipment

BOP installed and tested before drilling which hole?	Size	Min Required WP	Туре		Tested To
8 3/4	13 5/8	3M	Annular	Х	50% of working pressure
			Blind Ram	х	
			Pipe Ram		3M
			Double Ram	х	
			Other		

BOP/BOPE will be tested by an independent service company to 250 psi low and the high pressure indicated above per Onshore Order 2 requirements. The System may be upgraded to a higher pressure but still tested to the working pressure listed in the table above. If the system is upgraded all the components installed will be functional and tested.

Pipe rams will be operationally checked each 24 hour period. Blind rams will be operationally checked on each trip out of the hole. These checks will be noted on the daily tour sheets. Other accessories to the BOP equipment will include a Kelly cock and floor safety valve (inside BOP) and choke lines and choke manifold. See attached schematics.

	On E	ation integrity test will be performed per Onshore Order #2. xploratory wells or on that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Se tested in accordance with Onshore Oil and Gas Order #2 III.B.1.i.
Х	A var	iance is requested for the use of a flexible choke line from the BOP to Choke Manifold. See attached for specs and hydrostatic test chart.
	Ν	Are anchors required by manufacturer?

### Cimarex Energy Co., Triste Draw 25 Federal #5H

### 5. Mud Program

Depth Туре Weight (ppg) Viscosity Water Loss 0' to 1270' FW Spud Mud 1315 8.30 - 8.80 28 N/C 1270' to 5000' Brine Water 9.60 - 10.10 30-32 N/C 5000' to 14464' FW/Cut Brine 8.70 - 9.20 30-32 N/C

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times.

What will be used to monitor the loss or gain of fluid?

PVT/Pason/Visual Monitoring

#### 6. Logging and Testing Procedures

Logging, Coring and Testing								
х	Will run GR/CNL fromTD to surface (horizontal well - vertical portion of hole). Stated logs run will be in the Completion Report and submitted to the BLM.							
	No logs are planned based on well control or offset log information.							
	Drill stem test?							
	Coring?							

Additional Logs Planned	Interval
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### 7. Drilling Conditions

Condition	
BH Pressure at deepest TVD	4717 psi
Abnormal Temperature	No

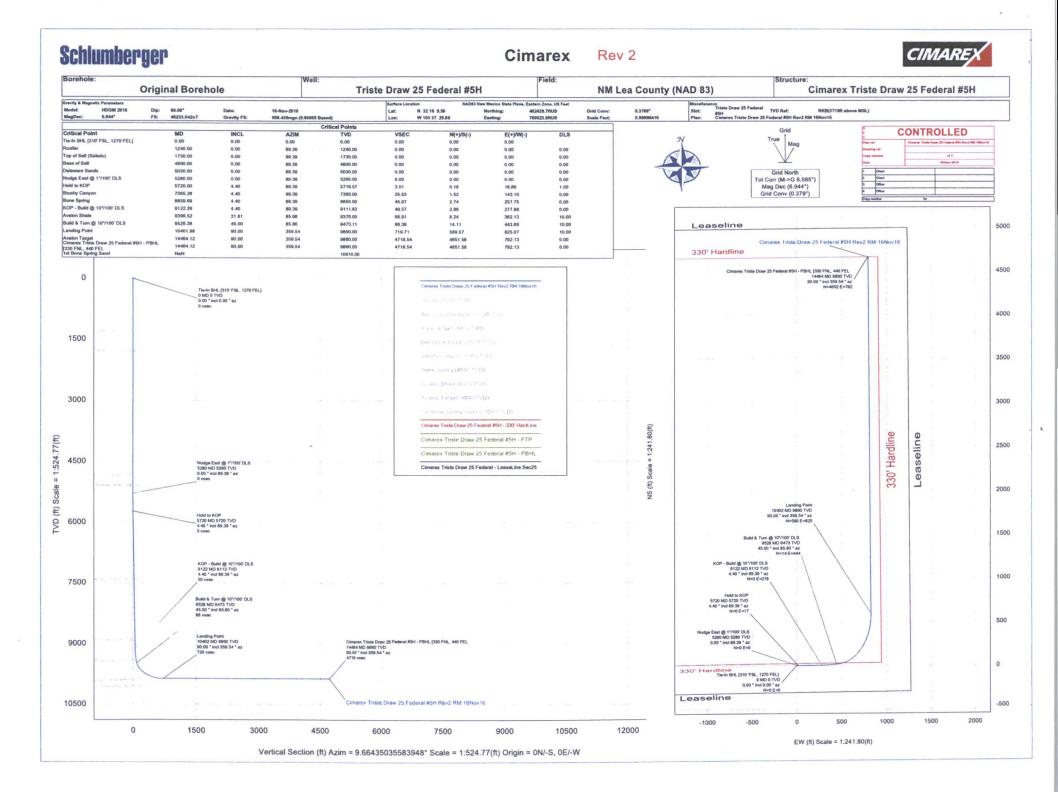
Hydrogen Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the operator will comply with the provisions of Onshore Oil and Gas Order #6. If Hydrogen Sulfide is encountered, measured values and formations will be provided to the BLM.

X H2S is present

X H2S plan is attached

8. Other Facets of Operation

4



Comments	MD	Incl	Azim Grid	TVD	VSEC	NS	EW	DLS	Northing	Easting	Latitude	Longitude
comments	(ft)	(°)	(°)	(ft)	(ft)	(ft)	(ft)	(°/100ft)	(ftUS)	(ftUS)	(N/S ° ' ")	(E/W ° ' ")
	8400.00	4.40	89.39	8391.67	39.68	2.37	222.48	0.00	462442.07	760846.07	N 32 16 9.59 W	103 37 23.30
	8500.00	4.40	89.39	8491.37	41.05	2.45	230.15	0.00	462442.15	760853.74	N 32 16 9.59 W	V 103 37 23.21
	8600.00	4.40	89.39	8591.08	42.42	2.53	237.82	0.00	462442.23	760861.41	N 32 16 9.59 W	V 103 37 23.12
	8700.00	4.40	89.39	8690.78	43.79	2.61	245.50	0.00	462442.31	760869.09	N 32 16 9.59 W	V 103 37 23.03
	8800.00	4.40	89.39	8790.49	45.16	2.70	253.17	0.00	462442.40	760876.76	N 32 16 9.59 W	V 103 37 22.94
	8900.00	4.40	89.39	8890.20	46.53	2.78	260.84	0.00	462442.48	760884.43	N 32 16 9.59 W	V 103 37 22.85
	9000.00	4.40	89.39	8989.90	47.89	2.86	268.51	0.00	462442.56	760892.10	N 32 16 9.59 W	V 103 37 22.76
	9100.00	4.40	89.39	9089.61	49.26	2.94	276.18	0.00	462442.64	760899.77	N 32 16 9.59 W	V 103 37 22.67
KOP - Build @ 10°/100' DLS	9122.29	4.40	89.39	9111.83	49.57	2,96	277.89	0.00	462442.66	760901.48	N 32 16 9.59 W	V 103 37 22.65
	9200.00	12.16	86.89	9188.67	51.91	3.44	289.06	10.00	462443.14	760912.65	N 32 16 9.60 W	V 103 37 22.52
	9300.00	22.16	86.24	9284.10	58.64	5.25	318.48	10.00	462444.95	760942.07	N 32 16 9.61 W	V 103 37 22.18
	9400.00	32.16	85.98	9372.96	69.35	8.36	363.97	10.00	462448.06	760987.55	N 32 16 9.64 W	V 103 37 21.65
	9500.00	42.16	85.83	9452.55	83.71	12.68	424.14	10.00	462452.38	761047.73	N 32 16 9.68 W	V 103 37 20.95
Build & Turn @ 10°/100' DLS	9528.38	45.00	85.80	9473.11	88.39	14.11	443.66	10.00	462453.81	761067.24	N 32 16 9.69 W	V 103 37 20.72
	9600.00	45.77	75.79	9523.47	104.86	22.27	493.85	10.00	462461.97	761117.43	N 32 16 9.77 W	V 103 37 20.13
	9700.00	48.24	62.53	9591.82	141.98	48.34	561.84	10.00	462488.04	761185.42	N 32 16 10.03 W	V 103 37 19.34
	9800.00	52.10	50.50	9655.99	194.48	90.75	625.54	10.00	462530.45	761249.12	N 32 16 10.44 W	V 103 37 18.60
	9900.00	57.06	39.82	9714.05	260.78	148.22	683.00	10.00	462587.92	761306.58	N 32 16 11.01 W	V 103 37 17.92
	10000.00	62.81	30.37	9764.21	338.86	219.00	732.49	10.00	462658.70	761356.06	N 32 16 11.70 W	V 103 37 17.34
	10100.00	69.14	21.88	9804.96	426.36	300.94	772.49	10.00	462740.63	761396.06	N 32 16 12.51 W	V 103 37 16.87
	10200.00	75.85	14.10	9835.06	520.60	391.55	801.79	10.00	462831.24	761425.36	N 32 16 13.41 W	V 103 37 16.52
	10300.00	82.80	6.78	9853.59	618.73	488.08	819.50	10.00	462927.76	761443.07	N 32 16 14.36 V	V 103 37 16.31
	10400.00	89.86	359.68	9859.99	717.76	587.59	825.08	10.00	463027.27	761448.65	N 32 16 15.34 W	V 103 37 16.23
Landing Point	10401.98	90.00	359.54	9860.00	719.71	589.57	825.07	10.00	463029.25		N 32 16 15.36 V	
	10500.00	90.00	359.54	9860.00	816.21	687.59	824.27	0.00	463127.26		N 32 16 16.33 W	
	10600.00	90.00	359.54	9860.00	914.65	787.59	823.46	0.00	463227.26		N 32 16 17.32 W	
	10700.00	90.00	359.54	9860.00	1013.09	887.58	822.65	0.00	463327.25		N 32 16 18.31 W	
	10800.00	90.00	359.54	9860.00	1111.53	987.58	821.84	0.00	463427.24		N 32 16 19.30 W	
	10900.00	90.00	359.54	9860.00	1209.97	1087.58	821.03	0.00	463527.23	761444.60		
	11000.00	90.00	359.54	9860.00	1308.41	1187.57	820.22	0.00	463627.23		N 32 16 21.28 V	
	11100.00	90.00	359.54	9860.00	1406.86	1287.57	819.41	0.00	463727.22		N 32 16 22.27 V	
	11200.00	90.00	359.54	9860.00	1505.30	1387.57	818.60	0.00	463827.21		N 32 16 23.26 V	
	11300.00	90.00	359.54	9860.00	1603.74	1487.56	817.79	0.00	463927.21		N 32 16 24.25 V	
	11400.00	90.00	359.54	9860.00	1702.18	1587.56	816.98	0.00	464027.20		N 32 16 25.24 V	
	11500.00	90.00	359.54	9860.00	1800.62	1687.56	816.17	0.00	464127.19		N 32 16 26.23 V	
	11600.00	90.00	359.54	9860.00	1899.06	1787.55	815.35	0.00	464227.19		N 32 16 27.22 W	
	11700.00	90.00	359,54	9860.00	1997.50	1887.55	814.54	0.00	464327.18		N 32 16 28.21 W	
	11800.00	90.00	359.54	9860.00	2095.95	1987.55	813.73	0.00	464427.17		N 32 16 29.20 W	
	11900.00	90.00	359.54	9860.00	2194.39	2087.54	812.92	0.00	464527.16		N 32 16 30.19 W	
	12000.00	90.00	359.54	9860.00	2292.83	2187.54	812.11	0.00	464627.16		N 32 16 31.18 W	
	12100.00	90.00	359.54	9860.00	2391.27	2287.54	811.30	0.00	464727.15		N 32 16 32.17 W	
	12200.00	90.00	359.54	9860.00	2489.71	2387.53	810.49	0.00	464827.14		N 32 16 33.15 W	
	12300.00	90.00	359.54	9860.00	2588.15	2487.53	809.68	0.00	464927.14		N 32 16 34.14 W	
	12400.00	90.00	359,54	9860.00	2686.59	2587.53	808.87	0.00	465027.13	761432.44		
	12500.00	90.00	359.54	9860.00	2785.04	2687.52	808.06	0.00	465127.12		N 32 16 36.12 V	
	12600.00	90.00	359.54	9860.00	2883.48	2787.52	807.25	0.00	465227.11		N 32 16 37.11 V	
	12700.00	90.00	359.54	9860.00	2981.92	2887.52	806.44	0.00	465327.11		N 32 16 38.10 V	
	12800.00	90.00	359.54	9860.00	3080.36	2987.51	805.62	0.00	465427.10		N 32 16 39.09 W N 32 16 40.08 W	
	12900.00	90.00	359.54	9860.00	3178.80	3087.51	804.81	0.00	465527.09		N 32 16 40.08 W	
	13000.00	90.00	359.54	9860.00	3277.24	3187.51	804.00	0.00	465627.09		N 32 16 41.07 V	
	13100.00	90.00	359.54	9860.00	3375.68	3287.50	803.19	0.00	465727.08		N 32 16 42.06 V	
	13200.00	90.00	359.54	9860.00	3474.13	3387.50	802.38	0.00	465827.07		N 32 16 44.04 V	
	13300.00	90.00	359.54	9860.00	3572.57	3487.50	801.57	0.00	465927.06		N 32 16 45.03 V	
	13400.00	90.00	359.54	9860.00	3671.01	3587.49	800.76	0.00	466027.06		N 32 16 45.03 V	
	13500.00	90.00	359.54	9860.00	3769.45	3687.49	799.95	0.00	466127.05		N 32 16 46.02 V	
	13600.00	90.00	359.54	9860.00	3867.89	3787.49	799.14	0.00	466227.04		N 32 16 48.00 V	
	13700.00	90.00	359.54	9860.00	3966.33	3887.48	798.33	0.00	466327.04	/01421.90	02 10 40.00 V	100 07 10.20

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.

Schlumberger

# Cimarex Triste Draw 25 Federal #5H Rev2 RM 16Nov16 Proposal Geodetic



Report

(Non-Def Plan)

Report Date:	November 16, 2016 - 10:09 AM	Survey / DLS Computation:	Minimum Curvature / Lubinski
Client:	Cimarex	Vertical Section Azimuth:	9.664 ° (Grid North)
Field:	NM Lea County (NAD 83)	Vertical Section Origin:	0.000 ft. 0.000 ft
Structure / Slot:	Cimarex Triste Draw 25 Federal #5H / Triste Draw 25 Federal #5H	TVD Reference Datum:	RKB
Well:	Triste Draw 25 Federal #5H	TVD Reference Elevation:	3719.000 ft above MSL
Borehole:	Original Borehole	Seabed / Ground Elevation:	3692,000 ft above MSL
UWI / API#:	Unknown / Unknown	Magnetic Declination:	6.944 °
Survey Name:	Cimarex Triste Draw 25 Federal #5H Rev2 RM 16Nov16	Total Gravity Field Strength:	998.4364mgn (9.80665 Based)
Survey Date:	November 16, 2016	Gravity Model:	GARM
Tort / AHD / DDI / ERD Ratio:	132.369 ° / 5261.088 ft / 6.009 / 0.534	Total Magnetic Field Strength:	48233.642 nT
Coordinate Reference System:	NAD83 New Mexico State Plane, Eastern Zone, US Feet	Magnetic Dip Angle:	60.080 °
Location Lat / Long:	N 32° 16' 9.58349", W 103° 37' 25.88767"	Declination Date:	November 16, 2016
Location Grid N/E Y/X:	N 462439.700 ftUS, E 760623.600 ftUS	Magnetic Declination Model:	HDGM 2016
CRS Grid Convergence Angle:	0.3788 °	North Reference:	Grid North
Grid Scale Factor:	0.99996416	Grid Convergence Used:	0.3788 °
Version / Patch:	2.10.254.0	Total Corr Mag North->Grid North:	6.5655 °
		Local Coord Referenced To:	Well Head

Comments	MD (ft)	Incl (°)	Azim Grid (°)	TVD (ft)	VSEC (ft)	NS (ft)	EW (ft)	DLS (°/100ft)	Northing (ftUS)	Easting (ftUS)	Latitude (N/S ° ' ")	Longitude (E/W ° ' ")
Tie-In SHL [310' FSL, 1270 FEL]	0.00	0.00	0.00	0.00	0.00	0.00	0.00	N/A	462439.70	760623.60 N	32 16 9.58 V	/ 103 37 25.89
	100.00	0.00	89.39	100.00	0.00	0.00	0.00	0.00	462439.70	760623.60 N	32 16 9.58 V	/ 103 37 25.89
	200.00	0.00	89.39	200.00	0.00	0.00	0.00	0.00	462439.70	760623.60 N	32 16 9.58 V	103 37 25.89
	300.00	0.00	89.39	300.00	0.00	0.00	0.00	0.00	462439.70	760623.60 N	32 16 9.58 V	/ 103 37 25.89
	400.00	0.00	89.39	400.00	0.00	0.00	0.00	0.00	462439.70	760623.60 N	32 16 9.58 V	103 37 25.89
	500.00	0:00	89.39	500,00	0.00	0.00	0.00	0.00	462439.70	760623.60 N	32 16 9.58 V	/ 103 37 25.89
	600.00	0.00	89.39	600.00	0.00	0.00	0.00	0.00	462439.70	760623.60 N	32 16 9.58 V	/ 103 37 25.89
	700.00	0.00	89.39	700.00	0.00	0.00	0.00	0.00	462439.70	760623.60 N	32 16 9.58 V	/ 103 37 25.89
	800.00	0.00	89.39	800.00	0.00	0.00	0.00	0.00	462439.70	760623.60 N	32 16 9.58 V	103 37 25.89
	900.00	0.00	89.39	900.00	0.00	0.00	0.00	0.00	462439.70	760623.60 N	32 16 9.58 V	/ 103 37 25.89
	1000.00	0.00	89.39	1000.00	0.00	0.00	0.00	0.00	462439.70	760623.60 N	32 16 9.58 W	/ 103 37 25.89
	1100.00	0.00	89.39	1100.00	0.00	0.00	0.00	0.00	462439.70	760623.60 N	32 16 9.58 W	/ 103 37 25.89
	1200.00	0.00	89.39	1200.00	- 0.00	0.00	0.00	0.00	462439.70	760623.60 N	32 16 9.58 W	/ 103 37 25.89
	1300.00	0.00	89.39	1300.00	0.00	0.00	0.00	0.00	462439.70	760623.60 N	32 16 9.58 W	/ 103 37 25.89
	1400.00	0.00	89.39	1400.00	0.00	0.00	0.00	0.00	462439.70	760623.60 N	32 16 9.58 W	103 37 25.89
	1500.00	0.00	89.39	1500.00	0.00	0.00	0.00	0.00	462439.70		32 16 9.58 V	
	1600.00	0.00	89.39	1600.00	0.00	0.00	0.00	0.00	462439.70		32 16 9.58 W	
	1700.00	0.00	89.39	1700.00	0.00	0.00	0.00	0.00	462439.70	760623.60 N	32 16 9.58 V	/ 103 37 25.89
	1800.00	0.00	89.39	1800.00	0.00	0.00	0.00	0.00	462439.70		32 16 9.58 W	
	1900.00	0.00	89.39	1900.00	0.00	0.00	0.00	0.00	462439.70	760623.60 N		
	2000.00	0.00	89.39	2000.00	0.00	0.00	0.00	0.00	462439.70	760623.60 N		
	2100.00	0.00	89.39	2100.00	0.00	0.00	0.00	0.00	462439.70		32 16 9.58 W	
	2200.00	0.00	89.39	2200.00	0.00	0.00	0.00	0.00	462439.70	760623.60 N		
	2300.00	0.00	89.39	2300.00	0.00	0.00	0.00	0.00	462439.70		32 16 9.58 W	
	2400.00	0.00	89.39	2400.00	0.00	0.00	0.00	0.00	462439.70		32 16 9.58 W	
	2500.00	0.00	89.39	2500.00	0.00	0.00	0.00	0.00	462439.70	760623.60 N		
	2600.00	0.00	89.39	2600.00	0.00	0.00	0.00	0.00	462439.70		32 16 9.58 W	
	2700.00	0.00	89.39	2700.00	0.00	0.00	0.00	0.00	462439.70	760623.60 N	32 16 9.58 W	103 37 25.89

# All previous COAS Still apply.

# I. DRILLING

# A. DRILLING OPERATIONS REQUIREMENTS

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)

Lea County Call the Hobbs Field Station, 414 West Taylor, Hobbs NM 88240, (575) 393-3612

- A Hydrogen Sulfide (H2S) Drilling Plan shall be activated 500 feet prior to drilling into the Delaware formation. As a result, the Hydrogen Sulfide area must meet Onshore Order 6 requirements, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, please provide measured values and formations to the BLM.
- Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval. If the drilling rig is removed without approval an Incident of Non-Compliance will be written and will be a "Major" violation.
- 3. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works is located, this does not include the dog house or stairway area.
- 4. The record of the drilling rate along with the GR/N well log run from TD to surface (horizontal well vertical portion of hole) shall be submitted to the BLM office as well as all other logs run on the borehole 30 days from completion. If available, a digital copy of the logs is to be submitted in addition to the paper copies. The Rustler top and top and bottom of Salt are to be recorded on the Completion Report.

# B. CASING

Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#).

Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). Centralizers required on surface casing per Onshore Order 2.III.B.1.f.

Wait on cement (WOC) time prior to drilling out for a primary cement job will be a minimum 18 hours for a water basin, 24 hours in the potash area, or 500 pounds compressive strength, whichever is greater for all casing strings. DURING THIS WOC TIME, NO DRILL PIPE, ETC. SHALL BE RUN IN THE HOLE. Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. IF OPERATOR DOES NOT HAVE THE WELL SPECIFIC CEMENT DETAILS ONSITE PRIOR TO PUMPING THE CEMENT FOR EACH CASING STRING, THE WOC WILL BE 30 HOURS. See individual casing strings for details regarding lead cement slurry requirements.

No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.

Possible water and brine flows in the Salado and Castile Groups. Possible lost circulation in the Delaware and Bone Spring.

- 1. The 13-3/8 inch surface casing shall be set at approximately 1315 feet (in a competent bed below the Magenta Dolomite, which is a Member of the Rustler, and if salt is encountered, set casing at least 25 feet above the salt) and cemented to the surface.
  - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
  - b. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry.
  - c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
  - d. If cement falls back, remedial cementing will be done prior to drilling out that string.

# Intermediate casing shall be kept fluid filled while running into hole to meet BLM minimum collapse requirements.

2. The minimum required fill of cement behind the 9-5/8 inch intermediate casing is:

Cement to surface. If cement does not circulate see B.1.a, c-d above.

Centralizers required on horizontal leg, must be type for horizontal service and a minimum of one every other joint.

- 3. The minimum required fill of cement behind the 5-1/2 inch production casing is:
  - Cement should tie-back at least 200 feet into previous casing string. Operator shall provide method of verification. Excess calculates to 16% Additional cement may be required.
- 4. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.

# C. PRESSURE CONTROL

- 1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in Onshore Oil and Gas Order No. 2 and API RP 53 Sec. 17.
- 2. Variance approved to use flex line from BOP to choke manifold. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor. If the BLM inspector questions the straightness of the hose, a BLM engineer will be contacted and will review in the field or via picture supplied by inspector to determine if changes are required (operator shall expect delays if this occurs).
- 3. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be **2000 (2M)** psi
- 4. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the **9-5/8** intermediate casing shoe shall be **3000 (3M)** psi.
- 5. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
  - a. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead when specified), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).

- b. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer. The operator also has the option of utilizing an independent tester to test without a plug (i.e. against the casing) pursuant to Onshore Order 2 with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for water basin (18 hours) or potash (24 hours) or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).
- c. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.
- d. The results of the test shall be reported to the appropriate BLM office.
- e. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
- f. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.

# D. DRILL STEM TEST

If drill stem tests are performed, Onshore Order 2.III.D shall be followed.

# E. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area.

Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

# TMAK 12022016

233225p APD14-600 Sundry Triste Draw 25 Federal 5H 3002542105 NMLC063228 Cimarex v12.50

### Lesser Prairie-Chicken.

and the second state of the second	surface	csg in a	17 1/2	inch hole.		Design	Factors	SUR	FACE
Segment	#/ft	Grade		Coupling	Joint	Collapse	Burst	Length	Weight
"A"	48.00	Н	40	ST&C	5.10	1.28	0.66	1,315	63,120
"B"				3.°		1. Sec. Sec.		0	0
w/8.4#/g	mud, 30min Sf	c Csg Test psig:	637	Tail Cmt	does not	circ to sfc.	Totals:	1,315	63,120
				ement Volume	s				
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Reg'd	Min Dist
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE	Hole-Cplg
17 1/2	0.6946	770	1280	968	32	8.80	1523	<b>2M</b>	1.56
Burst Frac Gra	dient(s) for Se	gment(s) A,	B=, b All:	0.70, OK.		, v 1944 v 1944 v 1944	r 17 10000 at anose 17 100	u a suu a suu s	
95/8	casing in	side the	13 3/8	N NAVY I NAVY N NAVY	n mar n mar n ma	Design	Factors	INTER	MEDIATE
Segment	#/ft	Grade	an a la	Coupling	Joint	Collapse	Burst	Length	Weight
"A"	36.00	J	55	LT&C	2.52	1.155	0.75	5.000	180,000
"B"	10					an a		0	0
w/8.4#/g	mud, 30min Sf	c Csg Test psig:					Totals:	5,000	180,000
				ieve a top of	0	ft from su		1315	overlap.
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Req'd	Min Dis
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE	Hole-Cpl
12 1/4	0.3132	1229	2153	1668	29	Ar 10.5 2 8.8			
12 1/4	0.0102	1223	2100	1000	29	10.10	2543	3M	0.81
Burst Frac Gra					29 Collapse 1/3		2543	3M	0.81
Burst Frac Gra > 0.70, OK.	dient(s) for Se	egment(s): A,				full OK			U.81
Burst Frac Grad 0.70, OK.		egment(s): A,	B, C, D = 0.7			full OK Design Fa	ctors	PROD	UCTION
Burst Frac Grad 0.70, OK.	dient(s) for Se casing in	gment(s): A, side the Grade	B, C, D = 0.7	, b, c, d All	Collapse 1/3	full OK	ctors		1 1000 i 1000 i 10 1 1000 i 1000 i 10
Burst Frac Grad 0.70, OK. 5 1/2 Segment	dient(s) for Se casing in #/ft	side the Grade L	B, C, D = 0.7	, b, c, d All	Collapse 1/3	<sup>full OK</sup> Design Fa Collapse	<u>ctors</u> Burst	PROD Length	UCTION Weight
Burst Frac Gra 0.70, OK. 5 1/2 Segment "A" "B"	dient(s) for Se casing in #/ft 17.00 <b>17.00</b>	egment(s): A, side the Grade L L	B, C, D = 0.7 9 5/8 80 80 80	, b, c, d All Coupling LT&C	Collapse 1/3 Joint 2.02	full OK <u>Design Fa</u> Collapse 1.44	ctors Burst 1.64	PROD Length 9,122 5,342	UCTION Weigh 155,074 90,814
Burst Frac Gra 0.70, OK. 5 1/2 Segment "A" "B"	dient(s) for Se casing in #/ft 17.00	egment(s): A, side the Grade L L c Csg Test psig:	B, C, D = 0.7 9 5/8 80 80 80	, b, c, d All Coupling LT&C	Collapse 1/3 Joint 2.02	full OK <u>Design Fa</u> Collapse 1.44	<u>ctors</u> Burst 1.64 <b>1.64</b>	PROD Length 9,122 5,342 14,464	UCTION Weigh 155,074 90,814 245,888
Burst Frac Gra 0.70, OK. 5 1/2 Segment "A" "B" w/8.4#/g B	dient(s) for Se casing in #/ft 17.00 17.00 mud, 30min Sfr would be:	egment(s): A, side the Grade L c Csg Test psig:	B, C, D = 0.7 9 5/8 80 80 80	, b, c, d All Coupling LT&C	Collapse 1/3 Joint 2.02 7.36	full OK Design Fa Collapse 1.44 1.25	ctors Burst 1.64 <b>1.64</b> Totals:	PROD Length 9,122 5,342 14,464	UCTION Weight 155,074 90,814 245,888
Burst Frac Gra 0.70, OK. 5 1/2 Segment "A" "B" w/8.4#/g B	dient(s) for Se casing in #/ft 17.00 17.00 mud, 30min Sfo	egment(s): A, side the Grade L c Csg Test psig:	B, C, D = 0.7 9 5/8 80 80 1,115	, b, c, d All Coupling LT&C BUTT	Collapse 1/3 Joint 2.02 7.36 31.64	full OK Design Fa Collapse 1.44 <b>1.25</b> 1.33	ctors Burst 1.64 1.64 Totals: if it were a	PROD Length 9,122 5,342 14,464 vertical we	UCTION Weigh 155,074 90,814 245,888 ellbore.
Burst Frac Grac 0.70, OK. 5 1/2 Segment "A" "B" w/8.4#/g B No Pil	dient(s) for Se casing in #/ft 17.00 17.00 mud, 30min Sfr would be: ot Hole Plan	egment(s): A, side the Grade L c Csg Test psig: nned	B, C, D = 0.7 9 5/8 80 80 1,115 MTD 14464	, b, c, d All Coupling LT&C BUTT Max VTD	Collapse 1/3 Joint 2.02 7.36 31.64 Csg VD 9860	full OK Design Fa Collapse 1.44 1.25 1.33 Curve KOP	ctors Burst 1.64 1.64 Totals: if it were a Dogleg <sup>o</sup> 90	PROD Length 9,122 5,342 14,464 vertical we Severity <sup>o</sup>	UCTION Weigh 155,07 90,814 245,88 ellbore. MEOC
Burst Frac Grac 0.70, OK. 5 1/2 Segment "A" "B" w/8.4#/g B No Pil	dient(s) for Se casing in #/ft 17.00 17.00 mud, 30min Sfr would be: ot Hole Plan	egment(s): A, side the Grade L c Csg Test psig: nned	B, C, D = 0.7 9 5/8 80 80 1,115 MTD 14464	, b, c, d All Coupling LT&C BUTT Max VTD 9860	Collapse 1/3 Joint 2.02 7.36 31.64 Csg VD 9860	full OK <u>Design Fa</u> Collapse 1.44 1.25 1.33 Curve KOP 9122	ctors Burst 1.64 1.64 Totals: if it were a Dogleg <sup>o</sup> 90	PROD Length 9,122 5,342 14,464 vertical we Severity <sup>o</sup> 7	UCTION Weigh 155,07 90,814 245,88 ellbore. MEOC 10402 overlap.
Burst Frac Gra 0.70, OK. 5 1/2 Segment "A" "B" w/8.4#/g B No Pil The c	dient(s) for Se casing in #/ft 17.00 17.00 mud, 30min Sf would be: ot Hole Plan	egment(s): A, side the Grade L c Csg Test psig: nned ne(s) are inte	B, C, D = 0.7 9 5/8 80 1,115 MTD 14464 nded to ach	, b, c, d All Coupling LT&C BUTT Max VTD 9860 iieve a top of	Collapse 1/3 Joint 2.02 7.36 31.64 Csg VD 9860 4800	full OK Design Fa Collapse 1.44 1.25 1.33 Curve KOP 9122 ft from su	ctors Burst 1.64 1.64 Totals: if it were a Dogleg <sup>o</sup> 90 urface or a	PROD Length 9,122 5,342 14,464 vertical we Severity <sup>o</sup> 7 200	UCTION Weigh 155,074 90,814 245,888 ellbore. MEOC 10402
Burst Frac Gra 0.70, OK. 5 1/2 Segment "A" "B" w/8.4#/g B No Pil The c Hole	dient(s) for Se casing in #/ft 17.00 17.00 mud, 30min Sf would be: ot Hole Plan eement volum Annular	egment(s): A, side the Grade L c Csg Test psig: nned ne(s) are inte 1 Stage	B, C, D = 0.7 9 5/8 80 1,115 MTD 14464 nded to ach 1 Stage	, b, c, d All Coupling LT&C BUTT Max VTD 9860 Nieve a top of Min Cu Ft	Collapse 1/3 Joint 2.02 7.36 31.64 Csg VD 9860 4800 1 Stage	full OK Design Fa Collapse 1.44 1.25 1.33 Curve KOP 9122 ft from su Drilling Mud Wt	ctors Burst 1.64 1.64 Totals: if it were a Dogleg <sup>o</sup> 90 urface or a Calc	PROD Length 9,122 5,342 14,464 vertical we Severity <sup>o</sup> 7 200 Req'd	UCTION Weigh 155,074 90,814 245,888 ellbore. MEOC 10402 overlap. Min Dist



United States Department of the Interior Bureau of Land Management Carlsbad Field Office

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Refer to: 3160-3

To: AFM, Lands & Minerals, CFOFrom: Geologist, CFOSubject: Geologic Review of Application for Permit to Drill

Operat	cimarex Ene	rgy Co.			
Well N	ame and Number:	Triste Dra	w 25 Federal-	5H	· · · · · · · · · · · · · · · · · · ·
Potash	: No				
Locatio	on: SHL:370'/S.& 1	270'/S. SEC	C025 T023S, R	032E.(SESE)	
County	Lea .	I	Lease Number	: LC063228	APD Received: 3-4-2014
Groun	d Level Elevation:	3692		Surface Geology:	Qe/Qp-Eolian deposits/Piedmont alluvial deposits
TVD:	9800	MD:	14255		BH Mud Weight: 9
BHP:	4586	MASP:	2430		

# 1. Geologic Marker Tops (from reports on surrounding wells):

					Proposed Well
	DIAMONDTAIL 24 FEDERAL A #001 3002533521	DIAMONDTAIL 23 FEDERAL #002 3002533653	TOMCAT 15 FEDERAL #002 3002533909		Triste Draw 25 Federal-5H T023S, R032E.(SESESEC025
	T23E R32E Sec 24	T23E R32E Sec 23	T23E R32E Sec 15		370'/S.& 1270'/S
	1980FNL 330FWL	1980FNL 660FEL	1980FSL 1980FEL		Unit
	Elevation	Elevation	Elevation		Elevation
Geologic Marker	Depth	Depth	Depth		Estimated Depth
Rustler	1238	1222	1207		1217
Top of Salt	1713	1703	1664		1687
Lamar	4994	4965	4940	-	5032
Bell Canyon	5033	5013	5000	-	5082
Bone Springs Lime	8850	8800	8760	-	8877
1st Bone Spring	10000	9990	-	-	10037
2nd Bone Spring	-	10660	-	-	10662
3rd Bone Spring	-	-	-	-	11932
Wolfcamp	-	-	-	-	12272

## 2. Fresh Water Information

a. Fresh Water:

b. Fresh Water Remarks:

1307

According to well data from the New Mexico Office of the State Engineer's Water Rights Reporting System, there are 25 water wells withn a six-mile radius of the proposed project. Depth to water ranges from 20 to 1533 feet. Usable water can also be found within the Magenta Dolomite Member of the Rustler Formation down to a depth of approximately 1307 feet.

c. Water Basin:

Carlsbad Water Basin

Castile, Salado,

NO

Rustler, Red Beds, Delaware,

1315

5000

### 3. Recommended Casing Setting Depth

a.	Surface	Casing	Depth:	
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- b. Intermediate Casing Depth:
- c. 2nd Interm. Casing Depth

## d. Casing Depth Remarks:

The operator proposes to set surface casing at 1270 feet, which will be too shallow and not adequately protect usable water zones. Instead, set casing in the anhydrite just below the base of the Magenta Dolomite at approximately 1315 feet. If salt is encountered, set casing at least 25 feet above the salt. The operator proposes to set intermediate casing at 5000 feet, which will be in the basal anhydrite of the Castile Formation. This is an acceptable set point.

### 4. Geologic Hazards

### a. Cave/Karst Occurance:

b. Potential (	Cave/Karst	Depth:	_
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c. Possible Water Flows:

d. Possible Lost Circulation:

e. Possible Abnormal Pressure: NO

f. H2S within 1 mile:

### g. H2S Remarks:

H2S has been reported within one-mile of the proposed project. Measurements up to 1000 ppm have been reported from the Cruz and Cruz Draw Pools.

### 5. Additional Remarks

Run GR and CNL logs to the surface.

Geologist: Robert Salaz

Sign Off Date: 6-20-2014