Form 3160-5 (June 2015)

UNITED STATES DEPARTMENT OF THE INTERIOR BUREAU OF LAND MANAGEMENT

OCD Hobbs

FORM APPROVED OMB NO. 1004-0137 Expires: January 31, 2018

SUNDRY Do not use thi abandoned wel	NOTICES AND REPOI s form for proposals to ll. Use form 3160-3 (API	RTS ON WELLS OBB (drill or to re-enter an D) for such proposals.		NM27506 Idian, Allottee or	Tribe Name	
SUBMIT IN	TRIPLICATE - Other inst	ructions on page 2	2017 7. If U	nit or CA/Agreem	nent, Name and/or No.	
Type of Well Gas Well	er	RECEN	ED 8. Well	Name and No. EA 29 FED COM	M P8 12H	
Name of Operator CHEVRON USA INC	Contact: E-Mail: leakejd@ch	DENISE PINKERTON nevron.com		Well No. 025-43271-00-	-X1	
3a. Address 1616 W. BENDER BLVD HOBBS, NM 88240		3b. Phone No. (include area code) Ph: 432-687-7375		eld and Pool or Ex 0025G06S263	ploratory Area 319P-BONE SPRING	
4. Location of Well (Footage, Sec., T.	, R., M., or Survey Description,		11. Co	unty or Parish, Sta	ate	۰
Sec 29 T26S R33E NWNE 13	6FNL 1607FEL		LE/	A COUNTY, N	М	
	/			`		
12. CHECK THE AF	PROPRIATE BOX(ES)	TO INDICATE NATURE OF	F NOTICE, REPO	RT, OR OTHE	ER DATA	
TYPE OF SUBMISSION		TYPE OF	ACTION			
Notice of Intent	☐ Acidize	□ Deepen	☐ Production (Star	rt/Resume)	☐ Water Shut-Off	
_	☐ Alter Casing	☐ Hydraulic Fracturing	□ Reclamation		■ Well Integrity	
☐ Subsequent Report	□ Casing Repair	■ New Construction	□ Recomplete		⊠ Other	
☐ Final Abandonment Notice	☐ Change Plans	□ Plug and Abandon	☐ Temporarily Ab	andon	Change to Original A	
	☐ Convert to Injection	□ Plug Back	■ Water Disposal			
13. Describe Proposed or Completed Ope If the proposal is to deepen directions Attach the Bond under which the wor following completion of the involved testing has been completed. Final Ab- determined that the site is ready for fi	ally or recomplete horizontally, it will be performed or provide operations. If the operation resonandonment Notices must be file inal inspection.	give subsurface locations and measur the Bond No. on file with BLM/BIA sults in a multiple completion or record ed only after all requirements, including	ed and true vertical dep Required subsequent impletion in a new inter- ing reclamation, have be	oths of all pertinent reports must be five val, a Form 3160-	nt markers and zones. iled within 30 days 4 must be filed once	
CHEVRON respectfully requestive system to a 10M system while formation.	sts the ability to change the drilling the production se	ne BOPE rating for the subject ctions that penetrate the Wolfo	well, from a 5M camp			
Please find attached:		SEE ATTACK				

New 9 PT PLAN 10M BOP CHOKE **UH-2 10K** Choke Hose Spec 7.625 Casing Liner 9.625 43.5lb LTC

Inspection & Test Certificate

SEE ATTACHED FOR CONDITIONS OF APPROVAL

14. I hereby certify that t	he foregoing is true and correct. Electronic Submission #385031 verifie For CHEVRON USA IN Committed to AFMSS for processing by ZO	IC. sen	to the Hobbs	
Name (Printed/Typed)	DENISE PINKERTON	Title	PERMITTING SPECIALIST	
Signature	(Electronic Submission)	Date	08/17/2017	
	THIS SPACE FOR FEDERA	L OR	STATE OFFICE USE	
Approved By ZOTA S	TEVENS	TitleP	ETROLEUM ENGINEER	Date 08/24/2017
		Ī		
certify that the applicant ho	any, are attached. Approval of this notice does not warrant or lds legal or equitable title to those rights in the subject lease			
	blicant to conduct operations thereon.	Office	Hobbs	

Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

(Instructions on page 2) ** BLM REVISED ** BLM REVISED ** BLM REVISED ** BLM REVISED **



Additional data for EC transaction #385031 that would not fit on the form

32. Additional remarks, continued

Tenaris XP BTC 5" 18# P110 ICY (3 schematics)

This sundry is at the request of Seven, BLM.

Any questions/concerns should be directefd to Bryson Abney, Chevron Drilling Engr, at 713-372-6447.

CONFIDENTIAL -- TIGHT HOLE
DRILLING PLAN
PAGE: 1

1. FORMATION TOPS

The estimated tops of important geologic markers are as follows:

FORMATION	SUB-SEA TVD	KBTVD	MD
Rustler		800	
Castile		3480	
Lamar		4900	
Bell Canyon		4930	
Cherry Canyon		5970	
Brushy Canyon		7620	
Bone Spring Limestone		9090	
Upr. Avalon		9120	
Top Bone Spring 1		10040	
Top Bone Spring 2		10700	
Top Bone Spring 3		11740	
Wolfcamp		12140	
Wolfcamp A1		12193	
Wolfcamp A2		12,523	
		10.500	
Lateral TD (Wolfcamp A2)		12,523	20000

2. ESTIMATED DEPTH OF WATER, OIL, GAS & OTHER MINERAL BEARING FORMATIONS

The estimated depths at which the top and bottom of the anticipated water, oil, gas, or other mineral bearing formations are expected to be encountered are as follows:

Substance	Formation	Depth
Deepest Expe	ected Base of Fresh Water	700
Water	Rustler	800
Water	Bell Canyon	4930
Water	Cherry Canyon	5970
Oil/Gas	Brushy Canyon	7620
Oil/Gas	Bone Spring Limestone	9090
Oil/Gas	Upr. Avalon	9120
Oil/Gas	Top Bone Spring 1	10040
Oil/Gas	Top Bone Spring 2	10700
Oil/Gas	Top Bone Spring 3	11740
Oil/Gas	Wolfcamp	12140
Oil/Gas	Wolfcamp A1	12193
Oil/Gas	Wolfcamp A2	12,523

All shows of fresh water and minerals will be reported and protected.

3. BOP EQUIPMENT

Will have a minimum of a 10000 psi rig stack (see proposed schematic) for drill out below surface (Wolfcamp is not exposed until drillout of the intermediate casing). Could possibly utilize the 5000 psi rig stack (see proposed schematic) for drill out below surface casing due to the availabity of 10 M annular. (Wolfcamp is not exposed until drillout of the intermediate casing) Stack will be tested as specified in the attached testing requirements. Batch drilling of the surface, intermediate, and production will take place. A full BOP test will be performed unless approval from BLM is received otherwise. Flex choke hose will be used for all wells on the pad (see attached specs) BOP test will be conducted by a third party.

Chevron requests a variance to use a FMC UH2 Multibowl wellhead, which will be run through the rig foor on surface casing. BOPE will be nippled up and tested after cementing surface casing. Subsequent tests will be performed as needed, not to exceed 30 days. The field report from FMC and BOP test information will be provided in a subsequent report at the end of the well. Please see the attached wellhead schematic. An installation manual has been placed on file with the BLM office and remains unchanged from previous submittal.

ONSḤORE ORDER NO. 1 Chevron SD EA 29/32 Fed Com P8 12H Lea County, NM CONFIDENTIAL -- TIGHT HOLE DRILLING PLAN

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4. CASING PROGRAM

a. The proposed casing program will be as follows:

Purpose	From	То	Hole Size	Csg Size	Weight	Grade	Thread	Condition
Surface	0'	800'	17-1/2"	13-3/8"	54.5 #	J55	STC	New
Intermediate	0'	11,500'	12-1/4"	9-5/8"	43.5#	HCK-L80	LTC	New
Liner	10,850'	12,300'	8-1/2"	7-5/8"	29.7 #	HCP-110	H513	New
Production	0'	12,500'	6-3/4"	5.5"	20#	P-110-ICY	TXP BTC	New
(Taper String)	12,500'	20,000'	6-3/4"	5"	18#	P-110 IC	TSH521	New

- b. Casing design subject to revision based on geologic conditions encountered.
- c. ***A "Worst Case" casing design for wells in a particular area is used below to calculate the Casing Safety Factors. If for any reason the casing design for a particular well requires setting casing deeper than the following "worst case" design, then the Casing Safety Factors will be recalcuated & sent to the BLM prior to drilling.
- d. Chevron will fill casing at a minimum of every 20 jts (840') while running for intermediate and production casing in order to maintain collapse SF.

SF Calculations based on the following "Worst Case" casing design:

Surface Casing:

850'

Intermediate Casing:

11,200' TVD

Production Casing:

23,000' MD/12,750' TVD (10,300' VS @ 90 deg inc)

Casing String	Min SF Burst	Min SF Collapse	Min SF Tension	Min SF Tri-Axial
Surface	1.36	3.12	3.17	1.70
Intermediate	1.12	1.44	1.93	1.37
Liner	1.69	5.36	2.50	2.09
Production	1.11	1.23	1.97	1.37

Min SF is the smallest of a group of safety factors that include the following considerations:

	Surf	Int	Liner	Prod
Burst Design				
Pressure Test- Surface, Int, Prod Csg	X	X	X	X
P external: Water				
P internal: Test psi + next section heaviest mud in csg				
Displace to Gas- Surf Csg	X			
P external: Water				
P internal: Dry Gas from Next Csg Point				
Frac at Shoe, Gas to Surf- Int Csg		X	X	
P external: Water				
P internal: Dry Gas, 16 ppg Frac Gradient				
Stimulation (Frac) Pressures- Prod Csg				X
P external: Water				
P internal: Max inj pressure w/ heaviest injected fluid				
Tubing leak- Prod Csg (packer at KOP)				X
P external: Water				
P internal: Leak just below surf, 8.7 ppg packer fluid				
Collapse Design				
Full Evacuation	X	X	X	X
P external: Water gradient in cement, mud above TOC				
P internal: none				
Cementing- Surf, Int, Prod Csg	X	X	X	X
P external: Wet cement				
P internal: water				
Tension Design				
100k lb overpull	X	X	X	X

ONSHORE ORDER NO. 1 Chevron SD EA 29/32 Fed Com P8 12H Lea County, NM CONFIDENTIAL -- TIGHT HOLE DRILLING PLAN

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5. **CEMENTING PROGRAM**

Slurry	Type	Тор	Bottom	Weight	Yield	%Excess	Sacks	Water
Surface				(ppg)	(sx/cu ft)	Open Hole		gal/sk
Tail	Class C	0'	800'	14.8	1.33	50	650	6.57
Intermediate								
Stage 2 Lead	Class C	0'	4570	11.9	2.39	100	1070	13.46
Stage 2 Tail	Class C	4570	4870	14.8	1.33	25	89	6.35
Stage 1 Lead	50:50 Poz Class C	4,870'	10,650'	11.9	2.21	25	1024	12.18
Stage 1 Tail	Class H	10,650'	11,150'	15.6	1.22	25	184	5.37
Liner								
Tail	Class H	10,850'	12,300'	15.6	1.22	17	123	5.34
Production								
Tail	Acid Soluble	10,350'	23,000'	15.6	1.2	10	1000	5.05
Pilot Hole								
Tail	Class H	12,500'	13,000'	17.2	0.97	10	128	3.61

1. Final cement volumes will be determined by caliper.

^{2.} Surface casing shall have at least one centralizer installed on each of the bottom three joints starting with the shoe joint.

^{3.} Production casing will have one horizontal type centralizer on every joint for the first 1000' from TD, then every other joint to EOB, and then every third joint to KOP. Bowspring type centralizers will be run from KOP to intermediate casing.

ONSHORE ORDER NO. 1 Chevron SD EA 29/32 Fed Com P8 12H Lea County, NM CONFIDENTIAL -- TIGHT HOLE DRILLING PLAN

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6. MUD PROGRAM

From	То	Туре	Weight	F. Vis	Filtrate
0'	800'	Spud Mud	8.3 - 8.7	32 - 34	NC - NC
800'	11,150'	Oil Based Mud	8.7-9.2	28 - 30	25-30
11,150'	12,300'	Oil Based Mud	9.5-13.5	70 - 75	25 - 30
12,300'	20,000'	Oil Based Mud	12.0-15.0	70 - 75	25 - 30

A closed system will by utilized consisting of above ground steel tanks. All wastes accumulated during drilling operations will be contained in a portable trash cage and removed from location and deposited in an approved sanitary landfill. Sanitary wastes will be contained in a chemical porta-toilet and then hauled to an approved sanitary landfill.

All fluids and cuttings will be disposed of in accordance with New Mexico Oil Conservation Division rules and regulations.

A mud test shall be performed every 24 hours after mudding up to determine, as applicable: density, viscosity, gel strength, filtration, and pH.

Visual mud monitoring equipment shall be in place to detect volume changes indicating loss or gain of circulating fluid volume. When abnormal pressures are anticipated -- a pit volume totalizer (PVT), stroke counter, and flow sensor will be used to detect volume changes indicating loss or gain of circulating fluid volume.

A weighting agent and lost circulating material (LCM) will be onsite to mitigate pressure or lost circulation as hole conditions dictate.

7. TESTING, LOGGING, AND CORING

The anticipated type and amount of testing, logging, and coring are as follows:

- a. Drill stem tests are not planned.
- b. The logging program will be as follows:

TYPE	Logs	Interval	Timing	Vendor
Mudlogs	2 man mudlog	Int Csg to TD	Drillout of Int Csg	TBD
LWD	MWD Gamma	Int. and Prod. Hole	While Drilling	TBD
Wireline Logs	Quad Combo w/ Di-Pole Sonic, FMI	Production	After production liner	TBD

- c. Conventional whole core samples are not planned.
- d. A Directional Survey will be run.

8. ABNORMAL PRESSURES AND HYDROGEN SULFIDE

a. No abnormal pressures or temperatures are expected. Estimated BHP at intermediate TD is:

No abnormal pressures or temperatures are expected. Estimated BHP at production TD is:

5750 psi 9830 psi

b. Hydrogen sulfide gas is not anticipated. An H2S Contingency plan is attached with this APD in the event that H2S is encountered

BLOWOUT PREVENTOR SCHEMATIC

Minimum Requirements

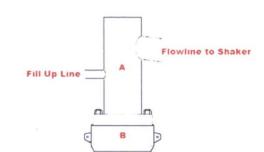
OPERATION : Wolfcamp A/A2 Wells

Minimum System

Pressure Rating : 10,000 psi

SIZE	PRESSURE	DESCRIPTION
SIZE	FRESSURE	DESCRIPTION

Α		N/A	Bell Nipple
В	13 5/8"	10,000 psi	Annular
С	13 5/8"	10,000 psi	Pipe Ram
D	13 5/8"	10,000 psi	Blind Ram
E	13 5/8"	10,000 psi	Mud Cross
F	13 5/8"	10,000 psi	Pipe Ram
	DSA	As required	for each hole size



Kill Line

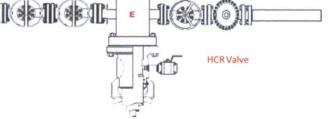
SIZE	PRESSURE	DESCRIPTION
2"	10,000 psi	Gate Valve
2"	10,000 psi	Gate Valve
2"	10,000 psi	Check Valve

Kill Line- 2" minimum

Choke Line to Choke Manifold- 3" minimum

Choke Line

SIZE	PRESSURE	DESCRIPTION	1
3"	10,000 psi	Gate Valve	
3"	10,000 psi	HCR Valve	



Installation Checklist

The following item must be verified and checked off prior to pressure testing of BOP equipment.

The installed BOP equipment meets at least the minimum requirements (rating, type, size, configuration) as shown on this schematic. Components may be substituted for equivalent equipment rated to higher pressures. Additional components may be put into place as long as they meet or exceed the minimum pressure rating of the system.
All valves on the kill line and choke line will be full opening and will allow straight though flow.
The kill line and choke line will be straight unless turns use tee blocks or are targeted with running tess, and will be anchored to prevent whip and reduce vibration.
Manual (hand wheels) or automatic locking devices will be installed on all ram preventers. Hand wheels will also be installed on all manual valves on the choke line and kill line.

A valve will be installed in the closing line as close as possible to the annular preventer to act as a locking device. This valve will remain open unless accumulator is inoperative.

Upper kelly cock valve with handle will be available on rig floor along with safety valve and subs to fit all drill string connections in use.

After Installation Checklist is complete, fill out the information below and email to Superintendent and Drilling Engineer

Wellname:

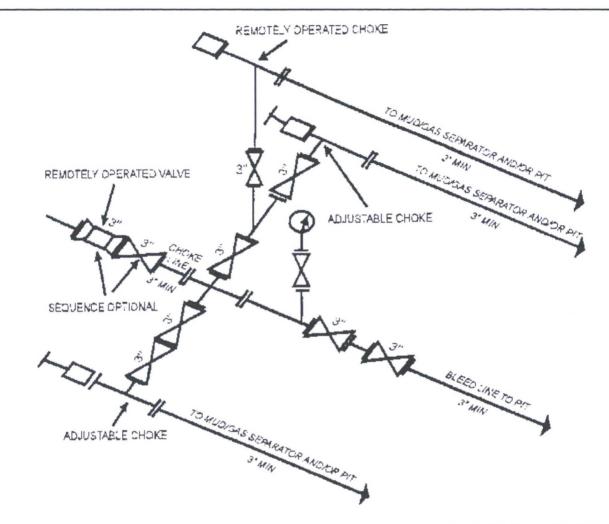
Representative:

Date:

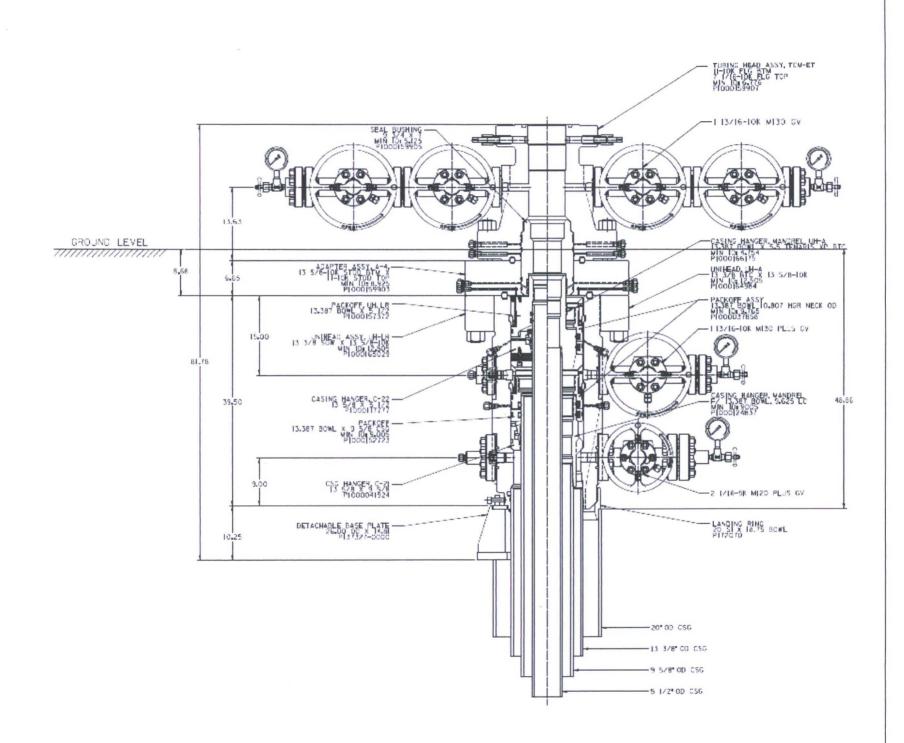
10M Choke Manifold SCHEMATIC

Minimum Requirements

OPERATION: Production and Open Hole Sections **Minimum System Pressure Rating:** 10,000 PSI



10M AND 15M CHOKE MANIFOLD EQUIPMENT - CONFIGURATION OF CHOKES MAY VARY [53 FR 4966], Dec. 9, 1988 and 54 FR 39528, Sept. 27, 1989]



CONTITECH RUBBER Industrial Kft.

No:QC-DB- 231/ 2014

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ContiTech

Hose Data Sheet

CRI Order No.	538332
Customer	ContiTech Oil & Marine Corp.
Customer Order No	4500412631 CBC544771, CBC544769, CBC544767, CBC544763, CBC544768, CBC544745, CBC544744, CBC544746
Item No.	1
Hose Type	Flexible Hose
Standard	API SPEC 16 C
Inside dia in inches	3
Length	45 ft
Type of coupling one end	FLANGE 4.1/16" 10KPSI API SPEC 17D SV SWIVEL FLANGE SOURC/W BX155 ST/ST INLAID R.GR.
Type of coupling other end	FLANGE 4.1/16" 10KPSI API SPEC 17D SV SWIVEL FLANGE SOUR C/W BX155 ST/ST INLAID R.GR.
H2S service NACE MR0175	Yes
Working Pressure	10 000 psi
Design Pressure	10 000 psi
Test Pressure	15 000 psi
Safety Factor	2,25
Marking	USUAL PHOENIX
Cover	NOT FIRE RESISTANT
Outside protection	St.steel outer wrap
Internal stripwound tube	No
Lining	OIL + GAS RESISTANT SOUR
Safety clamp	Yes
Lifting collar	Yes
Element C	Yes
Safety chain	Yes
Safety wire rope	No
Max.design temperature [°C]	100
Min.design temperature [°C]	-20
Min. Bend Radius operating [m]	0,90
Min. Bend Radius storage [m]	0,90
Electrical continuity	The Hose is electrically continuous
Type of packing	WOODEN CRATE ISPM-15

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Casing and Tubing Performance Data

PIPE BODY DATA

		WWW 10 WK 11 KW 10	GEOMETR1	** ** * * * * * *	
Outside Diameter	9.625 in	Wall Thickness	0.435 in	API Drift Diameter	8.599 in
Nominal Weight	43.50 lbs/ft	Nominal ID	8.755 in	Alternative Drift Diameter	8.625 in
Plain End Weight	42.73 lbs/ft	Nominal cross section	12.559 in		
		PE	RFORMANCI		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
Steel Grade	L80	Minimum Yield	80,000 psi	Minimum Ultimate	95,000 psi
Tension Yield	1,005,000 in	Internal Pressure Yield	6,330 psi	Collapse Pressure	3,810 psi
Available Seamless	Yes	Available Welded	No		
		CON	ECTION DA	TA	
TYPE: LTC			GEOMETR)		
Coupling Reg OD	10.625 in:	Threads per in	8	Thread turns make up	3.5
	i	PI	ERFORMANCE		
Steel Grade	L80	Coupling Min Yield	80,000 psi	Coupling Min Ultimate	95,000 psi
Joint Strength	813,000 lbş			Internal Pressure Resistance	6,330 psi

For the latest performance data, always visit our website: www.tenaris.com

June 17 2015



Size: 7.625 in. Wall: 0.375 in.

Weight: 29.70 lbs/ft

Grade: P110-IC

Min. Wall Thickness: 87.5 %

Casing/Tubing: CAS

Connection: Wedge 513™

				PIPE BODY DATA			
GEOMETRY							
in.	Nominal Weight	29.70 lbs/ft	Standard Drift Diameter	6.750 in.			
in.	Wall Thickness	0,375 in.	Special Drift Diameter	N/A			
lbs/ft							
	PERFOR	MANCE					
1000 lbs	Internal Yield	9470 psi	SMYS	110000 psi			
psi							
WEDGE 513™ CONNECTION DATA							
GEOMETRY							
	psi	in. Nominal Weight in. Wall Thickness lbs/ft PERFOR 1000 lbs Internal Yield psi WEDGE 513™ CO	in. Nominal Weight 29.70 lbs/ft in. Wall Thickness 0.375 in. lbs/ft PERFORMANCE 1000 lbs Internal Yield 9470 psi psi WEDGE 513™ CONNECTION DA	in. Nominal Weight 29.70 lbs/ft Diameter in. Wall Thickness 0.375 in. Special Drift Diameter Special Drift Diameter			

	WEDGE 513™ CONNECTION DATA				
	GEOMETRY				
Connection OD	7.625 in.	Connection ID	6.800 in.	Make-Up Loss	4.420 in.
Critical Section Area	5.125 sq. in.	Threads per in.	3.29		
Aled		PERFORM	ANCE		
		PERFORM	AIVCE		
Tension Efficiency	60.0 %	Joint Yield Strength	564 °× 1000 lbs	Internal Pressure Capacity	9470 psi
Compression Strength	707 × 1000 lbs	Compression Efficiency	75.2 %	Bending	40 °/100 ft
External Pressure Capacity	7150 psi				
	MAKE-UP TORQUES				
Minimum	9000 ft-lbs	Optimum	10800 ft-lbs	Maximum (<u>*</u>)	15800 ft-lbs
		OPERATIONAL LIN	IT TORQUES		

BLANKING DIMENSIONS

70000 ft-lbs

Yield Torque

Operating Torque 47000 ft-lbs

January 18 2016



Size: 5.500 in. **Wall**: 0.361 in.

Weight: 20.00 lbs/ft

Grade: P110-ICY

Min. Wall Thickness: 87.5 %

Connection: TenarisXP® BTC

Casing/Tubing: CAS

Coupling Option: REGULAR

		GEOMET	TRY		
Nominal OD	5.500 in.	Nominal Weight	20.00 lbs/ft	Standard Drift Diameter	4.653 in.
Nominal ID	4.778 in.	Wall Thickness	0.361 in.	Special Drift Diameter	N/A
Plain End Weight	19.83 lbs/ft				
		PERFORM	ANCE		
Body Yield Strength	729 x 1000 lbs	Internal Yield	14360 psi	SMYS	125000 psi
Collapse	12100 psi	e			
	TEI	NARISXP® BTC CO		ATA	
		GEOME		Ι	
Connection OD	6.100 in.	Coupling Length	9,450 in.	Connection ID	4.766 in.
Critical Section Area	5.828 sq. in.	Threads per in.	5.00	Make-Up Loss	4.204 in.
		PERFORM	ANCE		
Tension Efficiency	100 %	Joint Yield Strength	729 x 1000 lbs	Internal Pressure Capacity(1)	14360 psi
Structural		Structural	720 1000	Structural	
Compression	100 %	Compression	729 x 1000	Bending(2)	104 °/100 f
Efficiency		Strength			
External Pressure Capacity	12100 psi				
	E	STIMATED MAKE-L	JP TORQUES	3)	
Minimum	11540 ft-lbs	Optimum	12820 ft-lbs	Maximum	14100 ft-lb:
	(a	OPERATIONAL LI	MIT TORQUES	3	
Operating Torque	22700 ft-lbs	Yield Torque	25250 ft-lbs		
		BLANKING DIN	MENSIONS		
		Blanking Din			





TH DS-16.0370 11 ago 16 Rev 00

5" 18.00 ppf P110-ICY - TenarisXP® BTC (min wt 90%) (USC Units)

500000				********	
		PIPE BOD			
Nominal OD	5.000 in.	Nominal Weight	18.00 lbs/ft	Standard Drift Diameter	4.151 in.
Nominal ID	4,276 in.	Wall Thickness	0,362 in.	Special Drift Diameter	-
Plain End Weight	17,95 lbs/ft				
	BREETER	PERFORM	MANCE		
Body Yield Strength	659 x 1000 lbs	Internal Yield (4)	16290 psi	Collapse	14840 psi
		CONNECTIO	ON DATA		
Regular OD	5.720 in.	Coupling Length	9.325 in.	Connection ID	4,264 in,
Critical Section Area	5.275 sq. in.	Threads per in.	5	Make-Up Loss	4.141 in.
NORSH CE	NAME OF STREET	PERFORM	MANCE		
Tension Efficiency	100.0 %	Joint Yield Strength	659 x 1000 lbs	Internal Pressure Capacity (1) (4)	16290 psi
Structural Compression Efficiency	100,0 %	Structural Compression Rating	659 x 1000 lbs	External Pressure Capacity	14840 psi
Structural Bending ⁽²⁾	115°/100 ft				
		MAKE-UP TO	ORQUES ⁽³⁾	建建筑中华的	
Minimum	11480 ft-lbs	Target	12750 ft-lbs	Maximum	14030 ft-1bs
Operating Torque	15800 ft-lbs	Yield Torque	17700 ft-lbs		

⁽¹⁾ Internal Yield pressure related to structural resistance only. Internal pressure leak resistance as per section 10.3 API 5C3 / ISO 10400 - 2007.

⁽²⁾ Structural rating, pure bending to yield (i.e no other loads applied)

⁽³⁾ Torque values calculated for API Modified thread compounds with Friction Factor=1. For other thread compounds please contact us at licensees@oilfield,tenaris.com,

⁽⁴⁾ Minimum wall thickness 90% of nominal



TH DS-16.0372 23 August 2016 Rev 00

5.000" 18.00 lb/ft P110-ICY TenarisHydril Wedge 521®

		No. of the Persons			
		PIPE BOD	DY DATA		
		GEON	1ETRY		
Nominal OD	5,000 in.	Nominal Weight	18.00 lbs/ft	Standard Drift Diameter	4,151 in.
Nominal ID	4.276 in.	Wall Thickness	0.362 in.	Special Drift Diameter	N/A
Plain End Weight	17,95 lbs/ft				
		PERFOR	MANCE		
Body Yield Strength	659 x 1000 lbs	Internal Yield¹	16290 psi	Collapse	14840 psi
		CONNECT	ION DATA METRY		
Box OD (Turned)	5.359 in.	Pin ID (Bored)	4.226 in.	Make-Up Loss	3.62 in.
Critical Section Area	3.891 sq. in.	Threads per in.	3.36		
		PERFOR	MANCE		
Tension Efficiency	73.8 %	Joint Yield Strength	486 x 1000 lbs	Internal Yield¹	16290 psi
Compression Efficiency	88.7 %	Compression Rating	585 x 1000 lbs	Collapse	14840 psi
Bending	85°/100 ft				
		MAKE-UP	TORQUES		
Minimum	6100 ft-lbs	Optimum	7300 ft-lbs	Maximum*	10700 ft-lbs
		OPERATIONAL	LIMIT TORQUES	學可學術學	
Operational	20000 ft-lbs			Yield Torque	30000 ft-lbs

^{*}If you need to use torque values that are higher than the maximum indicated, please contact a local Tenaris technical sales representative

^{1.} Internal Yield Rating is based on 90% RBW.

PECOS DISTRICT CONDITIONS OF APPROVAL

OPERATOR'S NAME:

Chevron USA Inc

LEASE NO.: | NM27506

WELL NAME & NO.: | 12H-SD EA 29 Fed Com P8

SURFACE HOLE FOOTAGE: | 136'/N & 1607'/E

BOTTOM HOLE FOOTAGE | 180'/S & 330'/E

LOCATION: Section 29, T. 26 S., R.33 E., NMPM

COUNTY: Lea County, New Mexico

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Standard Conditions of Approval (COA) apply to this APD. If any deviations to these standards exist or special COAs are required, the section with the deviation or requirement will be checked below.

Special Requirements

Communitization Agreement

Cave/Karst **◯** Drilling

H2S Requirements

Cement Requirements

Logging Requirements

Waste Material and Fluids

SPECIAL REQUIREMENT(S)

Communitization Agreement

- The operator will submit a Communitization Agreement to the Carlsbad Field Office, 620 E Greene St. Carlsbad, New Mexico 88220, at least 90 days before the anticipated date of first production from a well subject to a spacing order issued by the New Mexico Oil Conservation Division. The Communitization Agreement will include the signatures of all working interest owners in all Federal and Indian leases subject to the Communitization Agreement (i.e., operating rights owners and lessees of record), or certification that the operator has obtained the written signatures of all such owners and will make those signatures available to the BLM immediately upon request.
- If the operator does not comply with this condition of approval, the BLM may take enforcement actions that include, but are not limited to, those specified in 43 CFR 3163.1.

In addition, the well sign shall include the surface and bottom hole lease numbers. When the Communitization Agreement number is known, it shall also be on the sign.

Waste Minimization Plan (WMP)

In the interest of resource development, submission of additional well gas capture development plan information is deferred but may be required by the BLM Authorized Officer at a later date.

DRILLING

A. DRILLING OPERATIONS REQUIREMENTS

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)

☐ Lea County

Call the Hobbs Field Station, 414 West Taylor, Hobbs NM 88240, (575) 393-3612

- 1. A Hydrogen Sulfide (H2S) Drilling Plan shall be activated 500 feet prior to drilling into the **Delaware** formation. **As a result, the Hydrogen Sulfide area must meet**Onshore Order 6 requirements, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, please provide measured values and formations to the BLM.
- 2. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval. If the drilling rig is removed without approval an Incident of Non-Compliance will be written and will be a "Major" violation.
- 3. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works is located, this does not include the dog house or stairway area.
- 4. The record of the drilling rate along with the GR/N well log run from TD to surface (horizontal well vertical portion of hole) shall be submitted to the BLM office as well as all other logs run on the borehole 30 days from completion. If available, a digital copy of the logs is to be submitted in addition to the paper copies. The Rustler top and top and bottom of Salt are to be recorded on the Completion Report.

B. CASING

Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.).

Centralizers required on surface casing per Onshore Order 2.III.B.1.f.

Wait on cement (WOC) for Water Basin:

After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least $\underline{8}$ hours. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements.

No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.

Medium Cave/Karst

Possible water flows in the Salado and Castile.

Possible lost circulation in the Red Beds, Rustler, and Delaware.

Abnormal pressures may be encountered within the 3rd Bone Spring Sandstone and Wolfcamp.

- 1. The 13-3/8 inch surface casing shall be set at approximately 850 feet (in a competent bed below the Magenta Dolomite, which is a Member of the Rustler, and if salt is encountered, set casing at least 25 feet above the salt) and cemented to the surface.
 - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
 - b. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry.
 - c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
 - d. If cement falls back, remedial cementing will be done prior to drilling out that string.

2. The minimum required fill of cement behind the 9-5/8 inch intermediate casing is:

Operator has proposed DV tool at depth of ', but will adjust cement proportionately if moved. DV tool shall be set a minimum of 50' below previous shoe and a minimum of 200' above current shoe. Operator shall submit sundry if DV tool depth cannot be set in this range.

a.	First	stage	to	DV	tool	:
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	calculates to 19% - Additional cement may be required.
	have plans as to how they will achieve circulation on the next stage. Excess
	BLM office before proceeding with second stage cement job. Operator should
\boxtimes	Cement to circulate. If cement does not circulate, contact the appropriate

- b. Second stage above DV tool:
- Cement to surface. If cement does not circulate, contact the appropriate BLM office.

Formation below the 9-5/8" shoe to be tested according to Onshore Order 2.III.B.1.i. Test to be done as a mud equivalency test using the mud weight necessary for the pore pressure of the formation below the shoe (not the mud weight required to prevent dissolving the salt formation) and the mud weight for the bottom of the hole. Report results to BLM office.

Medium Cave/Karst: If cement does not circulate to surface on the intermediate casing, the cement on the production casing must come to surface.

- 3. The minimum required fill of cement behind the 5-1/2 inch production casing is:
 - Cement should tie-back at least 200 feet into previous casing string. Operator shall provide method of verification.
- 4. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.

C. PRESSURE CONTROL

- 1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in Onshore Oil and Gas Order No. 2 and API RP 53 Sec. 17.
- 2. Operator has proposed a multi-bowl wellhead assembly. This assembly will only be tested when installed on the surface casing. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be 10,000 (10M) psi.
 - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
 - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
 - c. Manufacturer representative shall install the test plug for the initial BOP test.
 - d. Operator shall perform the intermediate casing integrity test to 70% of the casing burst. This will test the multi-bowl seals.
 - e. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.

10M system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.

- 3. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
 - a. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead when specified), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).
 - b. The tests shall be done by an independent service company utilizing a test plug **not** a **cup** or **J-packer**.

- c. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.
- d. The results of the test shall be reported to the appropriate BLM office.
- e. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
- f. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.

D. DRILL STEM TEST

If drill stem tests are performed, Onshore Order 2.III.D shall be followed.

E. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area.

Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

ZS 082417

Segment	#/ft	Grade		Coupling	Joint	Design Collapse	Burst	Length	Weight
"A"	54.50		55	ST&C	11.10	2.94	0.5	850	46,325
"B"	04.00				11.10	2.04	0.0	0	0
The second secon	mud, 30min Sfc	Cea Tost psia:	1 500	Tail Cmt	does	circ to sfc.	Totals:	850	46,325
				ement Volum		circ to sic.	Totals.	000	40,020
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Reg'd	Min Dist
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE	Hole-Cpl
17 1/2	0.6946	650	865	645	34	8.70	2966	3M	1.56
Burst Frac Grad	dient(s) for Se	gment(s) A, (B = , b All :	> 0.70, OK.					
95/8	casing in	recent Military Designation and American	13 3/8	THE RESERVE THE PROPERTY AND PARTY AND PARTY AND PARTY.	oyant	Control of the Contro	Factors	Control of the Contro	MEDIATE
Segment	#/ft	Grade		Coupling	Joint	Collapse	Burst	Length	Weight
"A"	40.00	HCK	55	LT&C	2.03	0.69	0.74	11,500	460,000
"B"								0	0
	mud, 30min Sfo						Totals:	11,500	460,000
The ce	ement volum	e(s) are inter		ieve a top of	0	ft from si	urface or a	850	overlap.
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Req'd	Min Dist
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE	Hole-Cpl
12 1/4	0.3132	look >	0	3662		9.20	5886	10M	0.81
D V Tool(s):			4870				sum of sx	Σ CuFt	Σ%excess
by stage %:		19	71				2367	5163	41
lass 'H' tail cm	nt yld > 1.20						MASP is with	in 10% of 50	00psig, need
Tail cmt		Itan @	#####						
75/8	Liner w	THE RESERVE AND PERSONS ASSESSMENT	mmmm	-		Design Fa	THE RESERVE OF THE PARTY OF THE		NER
Segment	#/ft	Grade		Coupling		Collapse	Burst	Length	Weight
Segment "A"	#/ft 29.70	Grade HCP	110	LT&C	2.39	Collapse 0.78	Burst 0.93	Length 1,380	Weight 40,986
Segment "A" "B"	#/ft 29.70 29.70	Grade HCP HCP	110 110			Collapse	0.93 0.93	1,380 70	Weight 40,986 2,079
"A" "B" w/8.4#/g	#/ft 29.70 29.70 mud, 30min Sfc	Grade HCP HCP Csg Test psig:	110 110	LT&C	2.39 1.75	0.78 0.83	0.93 0.93 Totals:	1,380 70 1,450	Weight 40,986 2,079 43,065
"A" "B" w/8.4#/g	#/ft 29.70 29.70	Grade HCP HCP Csg Test psig:	110 110 1,292	LT&C	2.39 1.75	0.78 0.83	0.93 0.93 Totals:	1,380 70 1,450 vertical we	Weight 40,986 2,079 43,065 ellbore.
"A" "B" w/8.4#/g A	#/ft 29.70 29.70 mud, 30min Sfc	Grade HCP HCP : Csg Test psig:	110 110 1,292	LT&C LT&C	2.39 1.75 13.10 Csg VD	0.78 0.83 0.83 Curve KOP	0.93 0.93 Totals: if it were a	Length 1,380 70 1,450 vertical we Severity	Weight 40,986 2,079 43,065 ellbore.
Segment "A" "B" w/8.4#/g A No Pilo	#/ft 29.70 29.70 mud, 30min sfo would be: of Hole Plan	Grade HCP HCP Cosg Test psig:	110 110 1,292 MTD 12300	LT&C LT&C Max VTD 12230	2.39 1.75 13.10 Csg VD 12230	0.78 0.83 0.83 Curve KOP 12201	0.93 0.93 Totals: if it were a	Length 1,380 70 1,450 vertical we Severity 14	Weight 40,986 2,079 43,065 ellbore. MEOC 12865
Segment "A" "B" w/8.4#/g A No Pilo	#/ft 29.70 29.70 mud, 30min sfo would be: of Hole Plan	Grade HCP HCP Csg Test psig:	110 110 1,292 MTD 12300 nded to ach	LT&C LT&C Max VTD 12230 lieve a top of	2.39 1.75 13.10 Csg VD 12230 3950	0.78 0.83 0.83 Curve KOP 12201 ft from si	Burst 0.93 0.93 Totals: if it were a Doglege 90 urface or a	Length 1,380 70 1,450 vertical we Severity 14 7550	Weight 40,986 2,079 43,065 ellbore. MEOC 12865 overlap.
Segment "A" "B" w/8.4#/g A No Pilo The ce	#/ft 29.70 29.70 mud, 30min Sfo would be: ot Hole Plan ement volume Annular	Grade HCP HCP Cosg Test psig:	110 110 1,292 MTD 12300 nded to ach 1 Stage	LT&C LT&C Max VTD 12230 ileve a top of Min	2.39 1.75 13.10 Csg VD 12230 3950 1 Stage	0.78 0.83 0.83 Curve KOP 12201 ft from si	Burst 0.93 0.93 Totals: if it were a Doglege 90 urface or a Calc	Length 1,380 70 1,450 vertical we Severity ^a 14 7550 Req'd	Weight 40,986 2,079 43,065 ellbore. MEOC 12865 overlap. Min Dist
Segment "A" "B" w/8.4#/g A No Pilo The ce Hole Size	#/ft 29.70 29.70 mud, 30min Sfo would be: ot Hole Plan ement volume Annular Volume	Grade HCP HCP Cosg Test psig: nned e(s) are inter 1 Stage Cmt Sx	110 110 1,292 MTD 12300 nded to ach 1 Stage CuFt Cmt	Max VTD 12230 ileve a top of Min Cu Ft	2.39 1.75 13.10 Csg VD 12230 3950 1 Stage % Excess	0.78 0.83 0.83 Curve KOP 12201 ft from si Drilling Mud Wt	Burst 0.93 0.93 Totals: if it were a Doglege 90 urface or a Calc MASP	Length 1,380 70 1,450 vertical we Severity 14 7550 Req'd BOPE	Weight 40,986 2,079 43,065 ellbore. MEOC 12865 overlap. Min Dist Hole-Cpl
Segment "A" "B" w/8.4#/g A No Pilo The ce Hole Size 8 1/2	#/ft 29.70 29.70 mud, 30min Sfo would be: ot Hole Plan ement volume Annular Volume 0.0770	Grade HCP HCP Cosg Test psig:	110 110 1,292 MTD 12300 nded to ach 1 Stage CuFt Cmt 150	Max VTD 12230 iieve a top of Min Cu Ft 893	2.39 1.75 13.10 Csg VD 12230 3950 1 Stage % Excess -83	0.78 0.83 0.83 Curve KOP 12201 ft from si Drilling Mud Wt 13.50	Burst 0.93 0.93 Totals: if it were a Doglege 90 urface or a Calc	Length 1,380 70 1,450 vertical we Severity ^a 14 7550 Req'd	Weight 40,986 2,079 43,065 ellbore. MEOC 12865 overlap. Min Dist
Segment "A" "B" w/8.4#/g A No Pilo The ce Hole Size 8 1/2 Class 'H' tail cm	#/ft 29.70 29.70 mud, 30min Sfo would be: ot Hole Plan ement volume Annular Volume 0.0770 ot yld > 1.20	Grade HCP HCP Cosg Test psig: nned e(s) are inter 1 Stage Cmt Sx 123	110 110 1,292 MTD 12300 nded to ach 1 Stage CuFt Cmt 150 MASP is wit	Max VTD 12230 lieve a top of Min Cu Ft 893 thin 10% of 500	2.39 1.75 13.10 Csg VD 12230 3950 1 Stage % Excess -83	0.78 0.83 0.83 Curve KOP 12201 ft from si Drilling Mud Wt 13.50 exrta equip?	Burst 0.93 0.93 Totals: if it were a Dogleg° 90 urface or a Calc MASP 7270	Length 1,380 70 1,450 vertical we Severity 14 7550 Req'd BOPE	Weight 40,986 2,079 43,065 ellbore. MEOC 12865 overlap. Min Dist Hole-Cple
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Segment "A" "B" w/8.4#/g A No Pilo The ce Hole Size 8 1/2 Class 'H' tail cmt 5 1/2 Segment "A" "B"	#/ft 29.70 29.70 mud, 30min Sfo would be: ot Hole Plan ement volume 0.0770 at yld > 1.20 dient(s) for Se casing in: #/ft	Grade HCP HCP Cosg Test psig: nned e(s) are inter 1 Stage Cmt Sx 123 gment(s): A, side the Grade P	110 110 1,292 MTD 12300 nded to ach 1 Stage CuFt Cmt 150 MASP is wit B, C, D =	Max VTD 12230 sieve a top of Min Cu Ft 893 thin 10% of 50 CURVE SAFET Coupling BUTT BUTT	2.39 1.75 13.10 Csg VD 12230 3950 1 Stage % Excess -83 00psig, need Y FACTOR IS Joint 1.82 1.95	Collapse 0.78 0.83 0.83 Curve KOP 12201 ft from si Drilling Mud Wt 13.50 exrta equip? TOO CONSERI Collapse 1.27 1.16	Burst 0.93 0.93 Totals: if it were a Dogleg° 90 urface or a Calc MASP 7270 VATIVE Factors Burst 1.42 1.42	Length 1,380 70 1,450 vertical we Severity 14 7550 Req'd BOPE 10M PROD Length 12,201 7,799	Weight 40,986 2,079 43,065 ellbore. MEOC 12865 overlap. Min Dist Hole-Cpl 0.44 UCTION Weight 244,016 155,984
Segment "A" "B" w/8.4#/g A No Pilo The ce Hole Size 8 1/2 Class 'H' tail cmt 5 1/2 Segment "A" "B" "C"	#/ft 29.70 29.70 mud, 30min Sfo would be: ot Hole Plan ement volume 0.0770 at yld > 1.20 dient(s) for Se casing in: #/ft 20.00	Grade HCP HCP Cosg Test psig: nned e(s) are inter 1 Stage Cmt Sx 123 gment(s): A, side the Grade P	110 110 1,292 MTD 12300 12300 12300 12300 12300 MASP is with 150 MASP is with 150, D =	Max VTD 12230 sieve a top of Min Cu Ft 893 thin 10% of 50 CURVE SAFET Coupling BUTT	2.39 1.75 13.10 Csg VD 12230 3950 1 Stage % Excess -83 00psig, need Y FACTOR IS	Collapse 0.78 0.83 0.83 Curve KOP 12201 ft from si Drilling Mud Wt 13.50 exrta equip? TOO CONSERI Collapse 1.27	Burst 0.93 0.93 Totals: if it were a Dogleg° 90 urface or a Calc MASP 7270 VATIVE Factors Burst 1.42	Length 1,380 70 1,450 vertical we Severity 14 7550 Req'd BOPE 10M PROD Length 12,201 7,799 7,500	Weight 40,986 2,079 43,065 ellbore. MEOC 12865 overlap. Min Dist Hole-Cple 0.44 UCTION Weight 244,016 155,984 135,000
Segment "A" "B" w/8.4#/g A No Pilo The ce Hole Size 8 1/2 Class 'H' tail cmt 5 1/2 Segment "A" "B"	#/ft 29.70 29.70 mud, 30min Sfo would be: ot Hole Plan ement volume 0.0770 at yld > 1.20 dient(s) for Se #/ft 20.00 20.00	Grade HCP HCP Cosg Test psig: nned e(s) are inter 1 Stage Cmt Sx 123 gment(s): A, side the Grade P	110 110 1,292 MTD 12300 nded to ach 1 Stage CuFt Cmt 150 MASP is wit B, C, D =	Max VTD 12230 sieve a top of Min Cu Ft 893 thin 10% of 50 CURVE SAFET Coupling BUTT BUTT	2.39 1.75 13.10 Csg VD 12230 3950 1 Stage % Excess -83 00psig, need Y FACTOR IS Joint 1.82 1.95	Collapse 0.78 0.83 0.83 Curve KOP 12201 ft from si Drilling Mud Wt 13.50 exrta equip? TOO CONSERI Collapse 1.27 1.16	Burst 0.93 0.93 Totals: if it were a Dogleg° 90 urface or a Calc MASP 7270 VATIVE Factors Burst 1.42 1.61	Length 1,380 70 1,450 vertical we Severity 14 7550 Req'd BOPE 10M PROD Length 12,201 7,799 7,500 0	Weight 40,986 2,079 43,065 ellbore. MEOC 12865 overlap. Min Dist Hole-Cple 0.44 UCTION Weight 244,016 155,984 135,000
Segment "A" "B" w/8.4#/g A No Pilo The ce Hole Size 8 1/2 Class 'H' tail cmt 5 1/2 Segment "A" "B" "C" "D"	#/ft 29.70 29.70 mud, 30min Sfo would be: ot Hole Plan ement volume 0.0770 at yld > 1.20 dient(s) for Se #/ft 20.00 20.00	Grade HCP HCP Csg Test psig: nned e(s) are inter 1 Stage Cmt Sx 123 gment(s): A, side the Grade P	110 110 1,292 MTD 12300 nded to ach 1 Stage CuFt Cmt 150 MASP is wit B, C, D =	Max VTD 12230 sieve a top of Min Cu Ft 893 thin 10% of 50 CURVE SAFET Coupling BUTT BUTT	2.39 1.75 13.10 Csg VD 12230 3950 1 Stage % Excess -83 00psig, need Y FACTOR IS Joint 1.82 1.95 360.00	Ollapse 0.78 0.83 0.83 Curve KOP 12201 ft from si Drilling Mud Wt 13.50 exrta equip? TOO CONSER' Design Collapse 1.27 1.16 1.51	Burst 0.93 0.93 Totals: if it were a Dogleg° 90 urface or a Calc MASP 7270 VATIVE Factors Burst 1.42 1.42	Length 1,380 70 1,450 vertical we Severity 14 7550 Req'd BOPE 10M PROD Length 12,201 7,799 7,500	Weight 40,986 2,079 43,065 ellbore. MEOC 12865 overlap. Min Dist Hole-Cple 0.44 UCTION Weight 244,016 155,984 135,000
Segment "A" "B" w/8.4#/g A No Pilo The ce Hole Size 8 1/2 Class 'H' tail cmt 5 1/2 Segment "A" "B" "C" "D" w/8.4#/g	#/ft 29.70 29.70 mud, 30min sfo would be: ot Hole Plan ement volume Annular Volume 0.0770 at yld > 1.20 dient(s) for Se, #/ft 20.00 20.00 18.00	Grade HCP HCP Cosg Test psig: nned e(s) are inter 1 Stage Cmt Sx 123 gment(s): A, side the Grade P P	110 110 1,292 MTD 12300 nded to ach 1 Stage CuFt Cmt 150 MASP is wit B, C, D = 7 5/8 110 110 12,684	Max VTD 12230 sieve a top of Min Cu Ft 893 shin 10% of 500 CURVE SAFET Coupling BUTT BUTT BUTT	2.39 1.75 13.10 Csg VD 12230 3950 1 Stage % Excess -83 00psig, need Y FACTOR IS Joint 1.82 1.95	Collapse 0.78 0.83 0.83 Curve KOP 12201 ft from si Drilling Mud Wt 13.50 exrta equip? TOO CONSERI Collapse 1.27 1.16	Burst 0.93 0.93 Totals: if it were a Dogleg° 90 urface or a Calc MASP 7270 VATIVE Factors Burst 1.42 1.61 Totals: if it were a very series of the control	Length 1,380 70 1,450 vertical we Severity 14 7550 Req'd BOPE 10M PROD Length 12,201 7,799 7,500 0 27,500	Weight 40,986 2,079 43,065 ellbore. MEOC 12865 overlap. Min Dist Hole-Cpl 0.44 UCTION Weight 244,016 155,984 135,000 0 535,000
Segment "A" "B" w/8.4#/g A No Pilo The ce Hole Size 8 1/2 Class 'H' tail cmt 5 1/2 Segment "A" "B" "C" "D" w/8.4#/g Bie	#/ft 29.70 29.70 mud, 30min Sfo would be: ot Hole Plan ement volume 0.0770 ot yld > 1.20 dient(s) for Se casing in: #/ft 20.00 18.00 mud, 30min Sfo	Grade HCP HCP Csg Test psig: nned e(s) are inter 1 Stage Cmt Sx 123 gment(s): A, side the Grade P P P Csg Test psig: gn Factors	110 110 1,292 MTD 12300 nded to ach 1 Stage CuFt Cmt 150 MASP is wit B, C, D = 7 5/8 110 110 12,684	Max VTD 12230 sieve a top of Min Cu Ft 893 shin 10% of 500 CURVE SAFET Coupling BUTT BUTT BUTT	2.39 1.75 13.10 Csg VD 12230 3950 1 Stage % Excess -83 00psig, need Y FACTOR IS Joint 1.82 1.95 360.00	Ollapse 0.78 0.83 0.83 Curve KOP 12201 ft from si Drilling Mud Wt 13.50 exrta equip? TOO CONSER' Design Collapse 1.27 1.16 1.51	Burst 0.93 0.93 Totals: if it were a Dogleg° 90 urface or a Calc MASP 7270 VATIVE Factors Burst 1.42 1.61 Totals:	Length 1,380 70 1,450 vertical we Severity 14 7550 Req'd BOPE 10M PROD Length 12,201 7,799 7,500 0 27,500	Weight 40,986 2,079 43,065 ellbore. MEOC 12865 overlap. Min Dist Hole-Cpl 0.44 UCTION Weight 244,016 155,984 135,000 0 535,000
Segment "A" "B" w/8.4#/g A No Pilo The ce Hole Size 8 1/2 Class 'H' tail cmt 5 1/2 Segment "A" "B" "C" "D" w/8.4#/g Bie	#/ft 29.70 29.70 mud, 30min sfo would be: ot Hole Plan ement volume Annular Volume 0.0770 at yld > 1.20 dient(s) for Se, #/ft 20.00 18.00 mud, 30min sfo	Grade HCP HCP Csg Test psig: nned e(s) are inter 1 Stage Cmt Sx 123 gment(s): A, side the Grade P P P Csg Test psig: gn Factors	110 110 1,292 MTD 12300 nded to ach 1 Stage CuFt Cmt 150 MASP is wit B, C, D = 7 5/8 110 110 110 2,684 would be:	Max VTD 12230 sieve a top of Min Cu Ft 893 shin 10% of 500 CURVE SAFET Coupling BUTT BUTT BUTT	2.39 1.75 13.10 Csg VD 12230 3950 1 Stage % Excess -83 00psig, need Y FACTOR IS Joint 1.82 1.95 360.00	Collapse 0.78 0.83 0.83 Curve KOP 12201 ft from si Drilling Mud Wt 13.50 exrta equip? TOO CONSERV Design Collapse 1.27 1.16 1.51	Burst 0.93 0.93 Totals: if it were a Dogleg° 90 urface or a Calc MASP 7270 VATIVE Factors Burst 1.42 1.61 Totals: if it were a very series of the control	Length 1,380 70 1,450 vertical we Severity 14 7550 Req'd BOPE 10M PROD Length 12,201 7,799 7,500 0 27,500 ertical wellte	Weight 40,986 2,079 43,065 ellbore. MEOC 12865 overlap. Min Dist Hole-Cpl 0.44 UCTION Weight 244,016 155,984 135,000 0 535,000 oore. MEOC
Segment "A" "B" w/8.4#/g A No Pilo The ce Hole Size 8 1/2 Class 'H' tail cmt 5 1/2 Segment "A" "B" "C" "D" w/8.4#/g B ie 500799	#/ft 29.70 29.70 mud, 30min sfo would be: ot Hole Plan ement volume Annular Volume On tyld > 1.20 dient(s) for Se, #/ft 20.00 18.00 mud, 30min sfo gment Desi	Grade HCP HCP HCP Csg Test psig: nned e(s) are inter 1 Stage Cmt Sx 123 gment(s): A, side the Grade P P Csg Test psig: gn Factors	110 110 1,292 MTD 12300 nded to ach 1 Stage CuFt Cmt 150 MASP is wit B, C, D = 7 5/8 110 110 110 2,684 would be: MTD 20000	Max VTD 12230 sieve a top of Min Cu Ft 893 shin 10% of 500 CURVE SAFET Coupling BUTT BUTT BUTT BUTT Max VTD	2.39 1.75 13.10 Csg VD 12230 3950 1 Stage % Excess -83 00psig, need Y FACTOR IS Joint 1.82 1.95 360.00 4.63 Csg VD	Collapse 0.78 0.83 0.83 Curve KOP 12201 ft from si Drilling Mud Wt 13.50 exrta equip? TOO CONSERV Design Collapse 1.27 1.16 1.51	Burst 0.93 0.93 Totals: if it were a Dogleg° 90 urface or a Calc MASP 7270 VATIVE Factors Burst 1.42 1.61 Totals: if it were a v Dogleg°	Length 1,380 70 1,450 vertical we Severity 14 7550 Req'd BOPE 10M PROD Length 12,201 7,799 7,500 0 27,500 ertical wellt Severity	Weight 40,986 2,079 43,065 ellbore. MEOC 12865 overlap. Min Dist Hole-Cpl 0.44 UCTION Weight 244,016 155,984 135,000 0 535,000 oore. MEOC
Segment "A" "B" w/8.4#/g A No Pilo The ce Hole Size 8 1/2 Class 'H' tail cmt 5 1/2 Segment "A" "B" "C" "D" w/8.4#/g B ie 500799	#/ft 29.70 29.70 mud, 30min sfo would be: ot Hole Plan ement volume Annular Volume On tyld > 1.20 dient(s) for Se, #/ft 20.00 18.00 mud, 30min sfo gment Desi	Grade HCP HCP HCP Csg Test psig: nned e(s) are inter 1 Stage Cmt Sx 123 gment(s): A, side the Grade P P Csg Test psig: gn Factors	110 110 1,292 MTD 12300 nded to ach 1 Stage CuFt Cmt 150 MASP is wit B, C, D = 7 5/8 110 110 110 2,684 would be: MTD 20000	Max VTD 12230 sieve a top of Min Cu Ft 893 shin 10% of 500 CURVE SAFET Coupling BUTT BUTT BUTT BUTT BUTT 13000	2.39 1.75 13.10 Csg VD 12230 3950 1 Stage % Excess -83 00psig, need Y FACTOR IS Joint 1.82 1.95 360.00 4.63 Csg VD 12575	Collapse 0.78 0.83 0.83 Curve KOP 12201 ft from si Drilling Mud Wt 13.50 exrta equip? TOO CONSERV Design Collapse 1.27 1.16 1.51	Burst 0.93 0.93 Totals: if it were a Dogleg° 90 urface or a Calc MASP 7270 VATIVE Factors Burst 1.42 1.61 Totals: if it were a v Dogleg° 90	Length 1,380 70 1,450 vertical we Severity 14 7550 Req'd BOPE 10M PROD Length 12,201 7,799 7,500 0 27,500 ertical wellt Severity 12	Weight 40,986 2,079 43,065 ellbore. MEOC 12865 overlap. Min Dist Hole-Cpl 0.44 UCTION Weight 244,016 155,984 135,000 0 535,000 oore. MEOC 12951.8 overlap.
Segment "A" "B" w/8.4#/g A No Pilo The ce Hole Size 8 1/2 Class 'H' tail cmt 5 1/2 Segment "A" "B" "C" "D" w/8.4#/g Bie 500799 The ce	#/ft 29.70 29.70 mud, 30min sfc would be: of Hole Plan ement volume 0.0770 of tyld > 1.20 dient(s) for Se, #/ft 20.00 20.00 18.00 mud, 30min sfc gment Desi	Grade HCP HCP Csg Test psig: nned e(s) are inter 1 Stage Cmt Sx 123 gment(s): A, side the Grade P P Csg Test psig: gn Factors 19999 e(s) are inter 1 Stage	110 110 1,292 MTD 12300 nded to ach 1 Stage CuFt Cmt 150 MASP is wit B, C, D = 7 5/8 110 110 110 2,684 would be: MTD 20000 nded to ach 1 Stage	Max VTD 12230 iieve a top of Min Cu Ft 893 thin 10% of 500 CURVE SAFET Coupling BUTT BUTT BUTT BUTT Max VTD 13000 iieve a top of	2.39 1.75 13.10 Csg VD 12230 3950 1 Stage % Excess -83 00psig, need Y FACTOR IS Joint 1.82 1.95 360.00 4.63 Csg VD 12575 0 1 Stage	Collapse 0.78 0.83 0.83 Curve KOP 12201 ft from si Drilling Mud Wt 13.50 exrta equip? TOO CONSERV Design Collapse 1.27 1.16 1.51	Burst 0.93 0.93 Totals: if it were a Dogleg° 90 urface or a Calc MASP 7270 VATIVE Factors Burst 1.42 1.61 Totals: if it were a v Dogleg° 90 urface or a	Length 1,380 70 1,450 vertical we Severity 14 7550 Req'd BOPE 10M PROD Length 12,201 7,799 7,500 0 27,500 ertical wellt Severity 12 12300 Req'd	Weight 40,986 2,079 43,065 ellbore. MEOC 12865 overlap. Min Dist Hole-Cple 0.44 UCTION Weight 244,016 155,984 135,000 0 535,000 oore. MEOC 12951.8 overlap. Min Dist
Segment "A" "B" w/8.4#/g A No Pilo The ce Hole Size 8 1/2 Class 'H' tail cmt 5 1/2 Segment "A" "B" "C" "D" w/8.4#/g Bie 500799 The ce Hole	#/ft 29.70 29.70 mud, 30min sfc would be: of Hole Plan ement volume 0.0770 of yld > 1.20 dient(s) for Se casing in: #/ft 20.00 18.00 mud, 30min sfc gment Desi 0.20999999 ement volume Annular	Grade HCP HCP Csg Test psig: nned e(s) are inter 1 Stage Cmt Sx 123 gment(s): A, side the Grade P P Csg Test psig: gn Factors 19999 e(s) are inter	110 110 1,292 MTD 12300 nded to ach 1 Stage CuFt Cmt 150 MASP is wit B, C, D = 7 5/8 110 110 110 2,684 would be: MTD 20000 nded to ach	Max VTD 12230 iieve a top of Min Cu Ft 893 thin 10% of 500 CURVE SAFET Coupling BUTT BUTT BUTT BUTT BUTT 13000 iieve a top of Min	2.39 1.75 13.10 Csg VD 12230 3950 1 Stage % Excess -83 00psig, need Y FACTOR IS Joint 1.82 1.95 360.00 4.63 Csg VD 12575 0	Collapse 0.78 0.83 0.83 Curve KOP 12201 ft from si Drilling Mud Wt 13.50 exrta equip? TOO CONSERT Design Collapse 1.27 1.16 1.51 1.24 Curve KOP 12201 ft from si Drilling	Burst 0.93 0.93 Totals: if it were a Dogleg° 90 urface or a Calc MASP 7270 VATIVE Factors Burst 1.42 1.61 Totals: if it were a v Dogleg° 90 urface or a Calc	Length 1,380 70 1,450 vertical we Severity 14 7550 Req'd BOPE 10M PROD Length 12,201 7,799 7,500 0 27,500 ertical wellt Severity 12 12300	Weight 40,986 2,079 43,065 ellbore. MEOC 12865 overlap. Min Dist Hole-Cplg 0.44 UCTION Weight 244,016 155,984 135,000 0 535,000 oore. MEOC 12951.88