

Case No.

7361

Application

Transcripts.

Small Exhibits

ETC



July 23, 1982

Mr. Michael E. Stogner
New Mexico Oil Conservation Division
P. O. Box 2088
State Land Office Building
Santa Fe, New Mexico 87501

RE: NMOC Case No. 7362
Designation of Tight
Formation, Dakota Formation
(Basin Dakota Field)
San Juan County, New Mexico

Dear Mr. Stogner:

Your letter of June 4, 1982 requested additional information concerning our exhibit 13 of the subject tight gas case. I'm sorry for the delay in answering your letter.

Our phone conversation with Mr. Victor Zabel of the Federal Energy Regulatory Commission in Washington, D.C., indicated the purpose of their request was to establish wells listed in our exhibit 13 as gas wells.

We do not distinguish between oil and condensate production when reporting production to the commission. All of the wells listed in our exhibit 13 are gas wells with GOR's ranging from 26000:1 to dry gas.

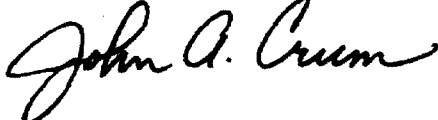
- 1) The oil production and reserves listed in our exhibit 13 is associated condensate production.
- 2) Each well listed in exhibit 13 was stimulated through hydraulic fracturing techniques.
- 3) There is no actual oil production from the wells listed in exhibit 13. The production shown is condensate production. API gravity for these wells is in the 50 to 60 degree range.

Mr. Michael E. Stogner
Page Two
July 23, 1982

If you need further information, please let me know.

Sincerely,

SOUTHLAND ROYALTY COMPANY



John A. Crum
District Reservoir Engineer

JAC/eg

XC: Mr. Steve Palho-SRC-Ft. Worth
Mr. Howard Kilchrist
Director of NGPA Compliance
Federal Energy Regulatory Commission
825 N. Capitol Street, N.E.
Washington, D.C. 20462



STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENT
OIL CONSERVATION DIVISION

BRUCE KING
GOVERNOR
LARRY KEHOE
SECRETARY

June 4, 1982

POST OFFICE BOX 2088
STATE LAND OFFICE BUILDING
SANTA FE, NEW MEXICO 87501
(505) 827-2434

Steve Palko
Southland Royalty Company
1000 Ft. Worth Club Building
Ft. Worth, Texas 76102

RE: NMOCD Case No. 7361,
Designation of Tight
Formation, Dakota Formation
(Basin-Dakota Field) San
Juan County, New Mexico

Dear Mr. Palko:

As per our telephone conversation Friday, June 4, 1982, Michael Boyle with the Federal Energy Regulatory Commission in Washington, D. C. requested to the New Mexico Oil Conservation Division the following supplemental information concerning Exhibit No. 13. (See attached copy.)

- 1) is this reported oil production either, actual crude production or condensate
- 2) is this reported oil production from wells that were stimulated
- 3) please submit actual production history from those wells having oil production

Please submit to this office three copies of the requested supplemental information.

If we may be of any assistance, please call. Thank you.

Sincerely,

Michael E. Stogner
Petroleum Engineer

MES/dp

cc: W. Perry Pearce
General Counsel
New Mexico Oil Conservation
Division
Santa Fe, NM 87501

SAC EXHIBIT NO. **13**

F

SAN JUAN COUNTY, NEW MEXICO

Operator	Lease	Well No.	Location	Cumulative Production (1-1-80)		Remaining Reserves (1-1-80)		Ultimate Reserves	
				Gas (MCF)	Oil (BBLs)	Gas (MCF)	Oil (BBLs)	Gas (MCF)	Oil (BBLs)
Tenneco	Wilkins	1	NE-24-32N-10W	29,306	0	0	0	29,306	0
Tenneco	Barnes	1	NE-26-32N-11W	261,364	0	0	0	261,364	0
Southland Royalty	Decker	4	SW-10-32N-12W	129,055	456	110,757	0	239,812	456
Southland Royalty	Hubbard	2	SW-11-32N-12W	71,276	177	75,749	0	147,025	177
Southland Royalty	Chamberlain	1	NE-14-32N-12W	47,873	60	0	0	47,873	60
Southland Royalty	Hubbard	3	NE-15-32N-12W	41,700	0	0	0	41,700	0
Southland Royalty	Hubbard	4	SW-15-32N-12W	117,951	0	353,699	701	471,650	1,872
Southland Royalty	Culpepper Martin	12	SW-20-32N-12W	66,173	1,062	49,440	635	117,613	1,697
Southland Royalty	Culpepper	15	NE-21-32N-12W	82,784	1,045	53,714	181	135,498	1,226
Southland Royalty	Culpepper Martin	5	SW-22-32N-12W	118,654	2,677	21,889	1,624	140,543	4,301
Tenneco	Moore	1	NE-25-32N-12W	150,109	0	0	0	150,109	0
Tenneco	Hubbard	1	SE-25-32N-12W	430,872	0	118,134	0	549,006	0
Southland Royalty	Decker	2	NE-26-32N-12W	86,930	285	46,571	0	133,501	285
Tenneco	Moore "C"	2	NE-26-32N-12W	384,093	1,284	250,514	0	634,607	1,284
Tenneco	Moore "C"	1	SE-27-32N-12W	500,205	1,803	175,347	0	675,552	1,803
Southland Royalty	Culpepper Martin	4	SW-28-32N-12W	96,795	1,533	188,831	2,182	285,626	3,715
Southland Royalty	Culpepper Martin	13	SW-29-32N-12W	64,312	837	101,373	152	185,685	989
Southland Royalty	Culpepper Martin	10	SW-32-32N-12W	402,396	3,513	352,593	690	754,989	4,203
Southland Royalty	Culpepper Martin	3	SW-33-32N-12W	256,054	1,535	361,566	1,928	617,640	3,463
Southland Royalty	Culpepper Martin	17	SE-33-32N-12W	77,114	591	1,335,936	7,636	1,411,050	8,227
Consolidated Oil & Gas	Rapley	1	SW-26-32N-13W	98,297	491	0	0	98,297	491
Benson-Montin-Greer	La Plata	1	SW-30-32N-13W	183,726	0	187,451	0	371,177	0
Benson-Montin-Greer	La Plata	2	NE-30-32N-13W	319,414	0	302,340	0	621,754	0
Consolidated Oil & Gas	Robinson Bros.	1	SE-34-32N-13W	126,755	526	0	0	128,755	526
Consolidated Oil & Gas	Montoya	1	NE-35-32N-13W	39,880	0	18,166	0	59,046	0
Consolidated Oil & Gas	Montoya	1K	NE-35-32N-13W	20,003	759	294,268	8,526	314,271	9,285
Supron Energy	White State	1	NE-36-32N-13W	37,720	63	0	0	37,720	63
Consolidated Oil & Gas	Pan American State	1	SW-36-32N-13W	158,858	1,538	29,974	290	188,832	1,828
Delhi-Taylor	Consolidated Oil & Gas	4	SW-27-31N-10W	432,580	0	0	0	432,580	0
Tenneco	Atlantic "A"	1	SW-34-31N-10W	200,942	0	0	0	200,942	0
Southland Royalty	Atlantic	2	SW-35-31N-11W	238,504	375	0	0	238,504	375
Tenneco	Tilt	2		5,293,695	21,781	4,428,332	24,545	9,724,027	46,326
Average	Totals	31		170,764	702	142,850	792	315,614	1,494



STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENT
OIL CONSERVATION DIVISION

BRUCE KING
GOVERNOR
LARRY KEHOE
SECRETARY

June 4, 1982

POST OFFICE BOX 2088
STATE LAND OFFICE BUILDING
SANTA FE, NEW MEXICO 87501
(505) 827-2434

Steve Palko
Southland Royalty Company
1000 Ft. Worth Club Building
Ft. Worth, Texas 76102

RE: NMOCD Case No. 7361,
Designation of Tight
Formation, Dakota Formation
(Basin-Dakota Field) San
Juan County, New Mexico

Dear Mr. Palko:

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Please submit to this office three copies of the requested supplemental information.

If we may be of any assistance, please call. Thank you.

Sincerely,

Michael E. Stogner
Petroleum Engineer

MES/dp

cc: W. Perry Pearce
General Counsel
New Mexico Oil Conservation
Division
Santa Fe, NM 87501

BEFORE EXAMINER NUTTER
OIL CONSERVATION DIVISION

582 EXHIBIT NO. 13

CASE NO.

CUMULATIVE PRODUCTION AND ULTIMATE RESERVES
BASIN DAKOTA FIELD
SAN JUAN COUNTY, NEW MEXICO

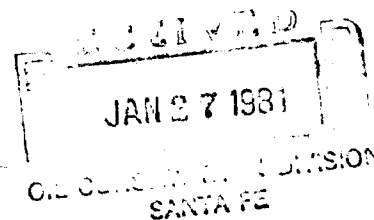
Operator	Lease	Well No.	Location	Cumulative Production (1-1-80)		Remaining Reserves (1-1-80)		Ultimate Reserves	
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Southland Royalty	Tift	31		5,293,695	21,781	4,428,332	24,545	9,722,027	46,326
Average				170,764	702	142,850	792	313,614	1,494

Candidates
Ex 1 thru 19
Complete
incl
affidavit



Consolidated Oil & Gas, Inc.

LINCOLN TOWER BUILDING
1960 LINCOLN STREET
DENVER, COLORADO 80295
(303) 861-5252



Mr. Daniel S. Nutter
Oil Conservation Division
P.O. Box 2088
Santa Fe, NM 87501


Re: Case No. 7116

Dear Mr. Nutter:

Enclosed are additional exhibits and testimony in the above-referenced case. We've included four copies of each and a prepaid mailer for forwarding everything to the FERC.

Very truly yours,

CONSOLIDATED OIL & GAS, INC.


Lynn Teschendorf
Attorney

LHT/mek

JAMES B. COONEY, P.A.

ATTORNEYS AT LAW

811 WEST APACHE

P. O. BOX 268

FARMINGTON, NEW MEXICO 87401

JAMES B. COONEY (1908-1979)
RICHARD T. C. TULLY
RICHARD L. LEE

(505) 327-3388

December 31, 1980

Joe D. Ramey, Director
New Mexico Oil Conservation Division
Post Office Box 2088
Santa Fe, New Mexico 87501

Re: Tom Bolack
Tommy Bolack #1 Well
Township 30 North, Range 12 West, NMPM
Section 1: S/2
Containing 320 acres, more or less
San Juan County, New Mexico

Dear Mr. Ramey:

In NMOCD Case No. 6993 held August 6, 1980, Tom Bolack requested an order pooling all of the mineral interests in the Dakota Formation underlying the above captioned lands. William R. Speer, Consulting Geologist, P. O. Box 255, Farmington, New Mexico 87401, was the expert witness testifying on behalf of Tom Bolack in this matter.

On September 10, 1980 the NMOCD issued Order No. R-6455 which pooled all mineral interests in the Dakota Formation underlying these lands in order to form a standard 320 acre gas spacing and proration unit to be dedicated to the Tommy Bolack #1 Well. This Order further provided, among other things, a 200% charge for the risk involved in drilling this well.

A review of the testimony of Mr. Speer in this matter shows that the current NGPA Section 103, "New Onshore Production Wells", natural gas prices for the Dakota Formation was not a sufficient economic incentive to drill the Tommy Bolack #1 Well. The Examiner for this hearing, Daniel S. Nutter, asked Mr. Speer the question of why the well was proposed to be drilled if the anticipated production from the Dakota Formation would result in a non-commercial well. Mr. Speer responded that this well was only being drilled because of the potential dual completion of this well with another formation besides the Dakota Formation.

Joe D. Ramey, Director
New Mexico Oil Conservation Division
December 31, 1980
Page Two

Further, it was the professional opinion of Mr. Speer that if this well was capable of producing from only the Dakota Formation, then the well would not be drilled at the present time. As mentioned above, the NMOCD entertained this information when it ordered a 200% charge for the risk involved in drilling this well.

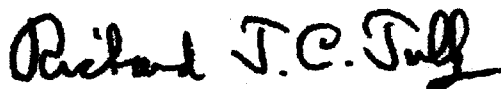
On December 30, 1980 a NMOCD Hearing was held for Case No. 7116. This case concerned the application of Southland Royalty Company for the designation of a "tight formation" in San Juan County, New Mexico for the Dakota Formation. At this hearing, Southland Royalty Company proposed the designation of the Dakota Formation underlying portions of Townships 31 and 32 North, Ranges 10, 11, 12, and 13 West, containing 93,860 acres, more or less, as a tight formation under the NGPA. The testimony by the witness for Southland Royalty Company did not testify as to the designation of the Dakota Formation for the above captioned lands, but did provide information on wells and lands located within one mile of this well. After the witness for Southland Royalty Company finished his testimony, Consolidated Oil and Gas Company, Inc. presented testimony for additional lands to be included within the application of Southland Royalty Company. The amendment of the application of Southland Royalty Company to add the additional acreage requested by Consolidated Oil and Gas was taken under advisement by the NMOCD Examiner during the hearing.

Due to the confusion of the current status of Southland Royalty Company's tight sands application and the request by Consolidated Oil and Gas Company, Inc. to add additional lands to this application, it is respectfully requested that Tom Bolack also be allowed an opportunity for designation of the Dakota Formation underlying the above captioned lands as a tight formation under the NGPA. As a further note, 120 acres of the 320 acres dedicated to the Tommy Bolack #1 Well for the Dakota Formation are owned by Southland Royalty Company under the Federal Oil and Gas Lease SF 077482.

Joe D. Ramey, Director
New Mexico Oil Conservation Division
December 31, 1980
Page Three

Thank you in advance for your assistance and cooperation in this matter. Please advise if you need further information.

Sincerely,



Richard T. C. Tully

RTCT:sak

cc: Honorable Tom Bolack
Route 3 South, Box 47
Farmington, New Mexico 87401

Tommy Bolack and Terry Bolack,
Co-Personal Representatives of the
Estate of Alice N. Bolack, Deceased
Route 3 South, Box 47
Farmington, New Mexico 87401

William R. Speer
Consulting Geologist
P. O. Box 255
Farmington, New Mexico 87401

Larry Van Ryan
Production Superintendent
Southland Royalty Company
Post Office Box 570
Farmington, New Mexico 87401

William F. Carr, Esq.
Campbell and Black, P.A.
P. O. Box 2208
Santa Fe, New Mexico 87501

Lynn Teschendorf, Attorney
Consolidated Oil & Gas Company, Inc.
Lincoln Tower Bldg.
1860 Lincoln Street
Denver, Colorado 80295

BEFORE THE
STATE OF NEW MEXICO
OIL CONSERVATION DIVISION

In the matter of the application of
Southland Royalty Company for designation
of a tight formation, San Juan County,
New Mexico

Case No. 7116

AFFIDAVIT

I, FLOYD E. ELLISON, being first duly sworn, depose and state that:

Permeability Calculations

Exhibits 5, 6 and 7 show the permeability calculations for the Wilmerding 1-M in Section 10, T31N, R13W, Kline 1-M in Section 10, T31N, R13W and Senter 1-M in Section 24, T31N, R13W based on the flow tests previously submitted (which were witnessed by New Mexico Oil Conservation Division personnel). In all cases the permeability calculations using Darcy's flow equation show the in situ permeability to be well below 0.1 md.

Well Cost Estimate

Consolidated's drilling and completion well cost estimate for an average depth 7,000' single Dakota completion totals \$475,400 (see Exhibit 19). These costs are based on our experience in drilling and completing a number of wells this past year in the immediate area. Several significant differences with the Southland Royalty cost estimate are:

1. Consolidated's use of \$16/ft. vs. Southland's \$14/ft. The \$16/ft. figure is our most recent quoted price and corresponds with inquiries we have made of other operators' footage prices. We have a working interest in a well recently drilled in the area in which the operator was required to pay \$19.51/ft.
2. Consolidated's average mud and water costs are well above those shown on the Southland estimate. Some mud and water costs have been as low as Southland's estimate, but we have experienced severe lost circulation in the Mesaverde, Gallup and/or Dakota zones in several wells which brings the average mud and water cost to our estimate.
3. The recent requirement by both the state and USGS to cement across the Ojo Alamo and circulate cement to surface requires additional DV tools and cement. Southland's cementing and cementing tools estimate is below the costs we have been experiencing in our most recent wells.
4. Completion Costs. Consolidated's completion procedure differs in several ways from Southland's. Consolidated has recently been including the tight lower Dakota in its completions because we believe enough additional reserves can be added in certain wells to justify the additional completion expense. A major cause of the increased expense is the necessity to perforate, stimulate, and clean up the upper and lower Dakota separately. The tight lower Dakota has an approximate 800 - 1,000# higher treatment and ISIP than does the upper Dakota

which makes it necessary to frac and clean up the zone before moving on to the upper Dakota completion. Consolidated has also been using nitrogen in its frac treatments to aid clean up but its use does add to stimulation costs.

Economics

Based on Consolidated Oil & Gas's required after tax economic criteria, Consolidated needs approximately 650 MMCF of gas reserves with Section 103 prices and 335 MMCF of gas reserves with 2 X 103 prices to justify drilling a single Dakota completion, as shown on Exhibit 8. These reserve requirements are considerably above what we used to justify our drilling program in the area this past year and above what Southland Royalty has indicated they need. The required larger reserves are the result of these major differences:

1. The majority of our wells this past year were dual completions with the Mesaverde reserves helping pay out the drilling and completion costs.
2. The drilling and completion costs have increased dramatically with the differences between Consolidated and Southland Royalty's estimates having been previously discussed.
3. The net interest (after deducting royalty interest and overriding royalty interest) on Consolidated operated properties in the area is 75.5% vs. Southland Royalty's indicated 86.5%. The majority of Consolidated's properties are 75% leases due to Consolidated having to give up an additional 12.5% ORR before it could farm-in the acreage and drill the original wells in the 1950's and 1960's. This is a major cut out of the income without any offsetting help on the expense side.
4. The required rate of return (ROR) after taxes for Consolidated is 20% vs. Southland Royalty's indicated 15%. Consolidated cannot justify less than a 20% ROR in the present money market when we pay over 20% for the money we borrow. Investors, including Consolidated, can receive more than 15% interest on CD's without assuming any risk so surely assuming risk is worth something above the 15% Southland proposed.

Exhibit 9 shows the assumptions used for our economic calculations and Exhibits 10, 11, 12 and 13 show the before and after taxes economics for 300 MMCFG, 400 MMCFG, 500 MMCFG and 650 MMCFG reserves with 103 pricing and Exhibits 14, 15, 16, 17 and 18 show the before and after taxes economics for 200 MMCFG, 300 MMCFG, 400 MMCFG, 500 MMCFG and 650 MMCFG reserves for 2 X 103 pricing.

Protection of Fresh Water

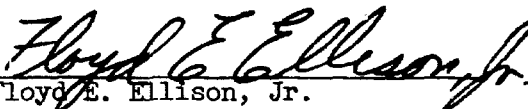
State and federal regulations currently provide for the protection of any fresh water aquifers that are being used or are expected to be used in the foreseeable future for domestic or agricultural water supplies. Three potential fresh water bearing formations in the area of interest are the San Jose, Nacimiento and Ojo Alamo. These three formations occur from the surface of the ground to a depth of approximately 1,000 feet in T31N, R13W and the western half of T31N, R12W.

The NMOCB by Rule 106 and the federal government regulations for protection of fresh water in oil and gas related activities both require the casing and cementing program to be designed to seal off fresh water bearing formations from

oil and gas bearing formations. They fulfill this requirement by having the oil and gas operator cement the production casing with sufficient cement to bring it above the Dakota several hundred feet, to usually cement across the Mesaverde zone when it is productive, and then to circulate cement to surface from several hundred feet below the base of the Ojo Alamo formation. Additionally, surface casing is set and cemented to surface when drilling begins which protects the top several hundred feet.

The above casing and cementing programs provide adequate protection to the fresh water sands even though large stimulation treatments are required in the tight Dakota producing formation which is about 5,900 feet below the deepest fresh water zone.


Exhibits 5 through 19 were prepared by me or under my direction and supervision.


Floyd E. Ellison, Jr.
Vice President - Operations

STATE OF COLORADO)
) ss
CITY AND COUNTY OF DENVER)

On this 22nd day of January, 1981, before me personally appeared Floyd E. Ellison, Jr., to me known to be the person described in and who executed the foregoing Affidavit before me, and who acknowledged to me that he executed it as his own free act and deed.

WITNESS my hand and seal on this day and year last above written.


Notary Public

My Commission Expires:
My commission expires June 13, 1983

CONSOLIDATED OIL & GAS, INC.
Senter 1-M
NE/4 SE/4 24-T31N-R13W
San Juan County, New Mexico

Lower Dakota

Perforations 6898', 6902', 6906', 6910', 6914', 6918',
6934', 6938', 6942', 6946', 6950', 6954', & 6958',
(13-.33" diameter perforations)

Acidized with 500 gallons 15% NE acid using 25 ball sealers.
Balled off @ 3200#.

Swabbed well down to get acid back.

5/20-21/80

Tefteller, Inc. ran flow test on Dakota perforations
6898'-6958'.

5/20/80

12:45 p.m.

2.73 MCF/D

3:45 p.m.

1.91 MCF/D

7:00 a.m.

1.91 MCF/D

Test witnessed by Frank Chavez and Rich Simmons of NMOCC,
Tobby Tefteller and Len Alexander with Tefteller and
Aubrey Prather with Consolidated Oil & Gas, Inc.

Upper Dakota

Perforations 6740', 6745', 6759', 6776', 6782', 6786',
6794', 6808', 6810', 6814', and 6816'.

Acidized with 500 gallons 15% NE acid using 22 ball sealers.
Balled off @ 3500#.

Swabbed well down.

6/4-5/80

Tefteller, Inc. ran flow test on Dakota perforations
6740'-6816'.

Flowed total 21 hours. Well stabilized @ approximately
52 MCF/D rate over last 16½ hours.

Test witnessed by Rich Simmons with NMOCC, Tefteller testers,
and Barney Jones with Consolidated Oil & Gas, Inc.

NO oil produced

*used 1000 lbs of Darcy
Refracturing material*

BEFORE EXAMINER NUTTER	
OIL CONSERVATION DIVISION	
106	EXHIBIT NO. 4
CASE NO. 7116	

CONSOLIDATED OIL & GAS, INC.
Wilberding 1-M
NE/4 NW/4 10-T31N-R13W
San Juan County, New Mexico

Lower Dakota Perforations 6788', 6798', 6828', 6830', 6833', 6838',
6841', and 6846', (8-.32" diameter perforations)
Acidized with 250 gallons 7½% NE acid using 16 ball sealers.
Swabbed well down.
9/11/80 Flowed well through Critical Prover using 1/8" orifice
plate. Gas rate too small to measure.
Test witnessed by Charles Gholson with NMOCC and Barney Jones
with Consolidated Oil & Gas, Inc.
Did not test Upper Dakota.

*actually less than 1000 bbl
Lower Dak only if no acid
(much more in Upper Dak)*

*witness: Perm would call to
less than 1 MD*

BEFORE EXAMINER NUTTER OIL CONSERVATION DIVISION COG EXHIBIT NO. <u>2</u> CASE NO. <u>7116</u>

CONSOLIDATED OIL & GAS, INC.
Kline 1-M
NE/4 SE/4 10-T31N-R13W
San Juan County, New Mexico

Lower Dakota

Perforations 6655', 6658', 6668', 6672', 6676', 6715',
6720', 6724', 6729', 6734', and 6736', (9-.29" holes)

Acidized with 300 gallons 7½% NE acid using 21 ball sealers.
Balled off @ 5000#.

Swabbed down and recovered water and acid.

Flowed well through Critical Prover using 1/8" orifice plate.
Produced 5 hours with maximum rate of 12.85 MCF/D.

8/22/80

Test witnessed by Rich Simmons of NMOCC and Chink Ashbrook
with Consolidated Oil & Gas, Inc.

Upper Dakota

Perforations 6506', 6512', 6520', 6527', 6532', 6540', 6550',
6557', 6565', 6572', 6577', 6584', 6592', 6612', 6617', 6621',
and 6629', (17 perforations .32" diameter)

Acidized with 500 gallons 7½% NE acid with 30 ball sealers.
Balled off @ 5500#.

Swabbed well down.

Flowed well 4 hours through Critical Prover using 1/8"
orifice plate. Gas rate too small to measure.

8/28/80

Test witnessed by Richard H. Simmons of NMOCC and Chink
Ashbrook with Consolidated Oil & Gas, Inc.

would call to show them APD

BEFORE EXAMINER NUTTER	
OIL CONSERVATION DIVISION	
LOG	EXHIBIT NO. 3
CASE NO.	7110

CONSOLIDATED OIL & GAS, INC.
WILMERDING NO. 1M
NE/4 NW/4 10-T31N-R13W
BASIN DAKOTA FIELD
SAN JUAN COUNTY, NEW MEXICO

Data:

	<u>Lower Dakota</u>	<u>Upper Dakota</u>
Midperforations	6817'	6697'
Og	To Small To Measure	Not Tested
h (log)	27'	57'
K (permeability)	Inadequate gas to compute flow rate and permeability (K) is much less than oil md.	

EXHIBIT 5

CONSOLIDATED OIL & GAS, INC.

KLITE NO. 1M

NE/4 SE/4 10-31N-13W

BASIN DAKOTA FIELD

Calculation of Permeability Using Darcy's Law:

Data:

	<u>Lower Dakota</u>	<u>Upper Dakota</u>
Midperforations	6696'	6567'
Qg	12850 SCF (test)	Gas Too Small To Measure
h	38' feet (log)	
Pwf	38 Psia	
Pe	2592 Psia	
g _g	.70	
T	186°-646°R	
re	1320 feet	
rw	0.02 feet	
Psc	668 Psia	
Tsc	392° Rankin	
Ug	.014 cp	
Z	0.91	

Where:

Qg = gas flow rate	rw = wellbore radius
h = net pay	Psc = pseudo critical pressure
Pwf = flowing bottomhole pressure	Tsc = pseudo critical temperature
Pe = shut-in bottomhole pressure at drainage radius, re	Ug = gas viscosity
g _g = gas specific gravity	Z = compressibility factor for gas
T = bottomhole temperature	
re = drainage radius for 160 acre spacing	

Formula:

$$K = \frac{Qg U_g T Z \ln(.61 re / rw)}{703 h (P_e^2 - P_{wf}^2)}$$

$$K = \frac{12850 \times .014 \times 646 \times .91 \times \ln(.61 \times \frac{1320}{.02})}{703 \times 33 \times (2592^2 - 38^2)}$$

$$K = .0000049 \text{ D}$$

$$K = .0049 \text{ md.}$$

CONSOLIDATED OIL & GAS, INC.
 SENTER NO. 1M
 NE/4 SE/4 24-T31N-R13W
 BASIN DAKOTA FIELD
 SAN JUAN COUNTY, NEW MEXICO

Calculation of Permeability Using Darcy's Law:

Data:

	<u>Lower Dakota</u>	<u>Upper Dakota</u>
Midperforations	6928	6728
Qg Scf (test)	2730	52000
h feet (log)	58	51
Pwf Psia	20	32
Pe by analogy & tests	2658	2592
Gg typical gravity field gas	.70	.70
T calculated	186°F (646°R)	186°F (646°R)
re feet	1320	1320
rw feet	.20	.20
Psc Psia	668	668
Tsc °Rankin	392°R	392°R
Ug cps (calc.)	.014	.014
Z (calc)	.91	.91

Where:

Qg = gas flow rate
 h = net pay
 Pwf = flowing bottomhole pressure
 Pe = shut-in bottomhole pressure
 at drainage radius, re
 gg = gas specific gravity
 T = bottomhole temperature
 re = drainage radius for 160 acre
 spacing

rw = wellbore radius
 Psc = pseudo critical pressure
 Tsc = pseudo critical temperature
 Ug = gas viscosity
 Z = compressibility factor
 for gas

Formula:

$$Q_g = \frac{703Kh(Pe^2 - Pwf^2)}{UgTZ \ln(.61re/rw)} \quad \text{and } K = \frac{Q_g Ug TZ \ln(.61re/rw)}{703h(Pe^2 - Pwf^2)}$$

Lower Dakota

$$K = \frac{2730(.014)(646)(.91) \ln(.61 \times \frac{1320}{20})}{(703)(58)(2658^2 - 20^2)}$$

$$= .00000068 \text{ D}$$

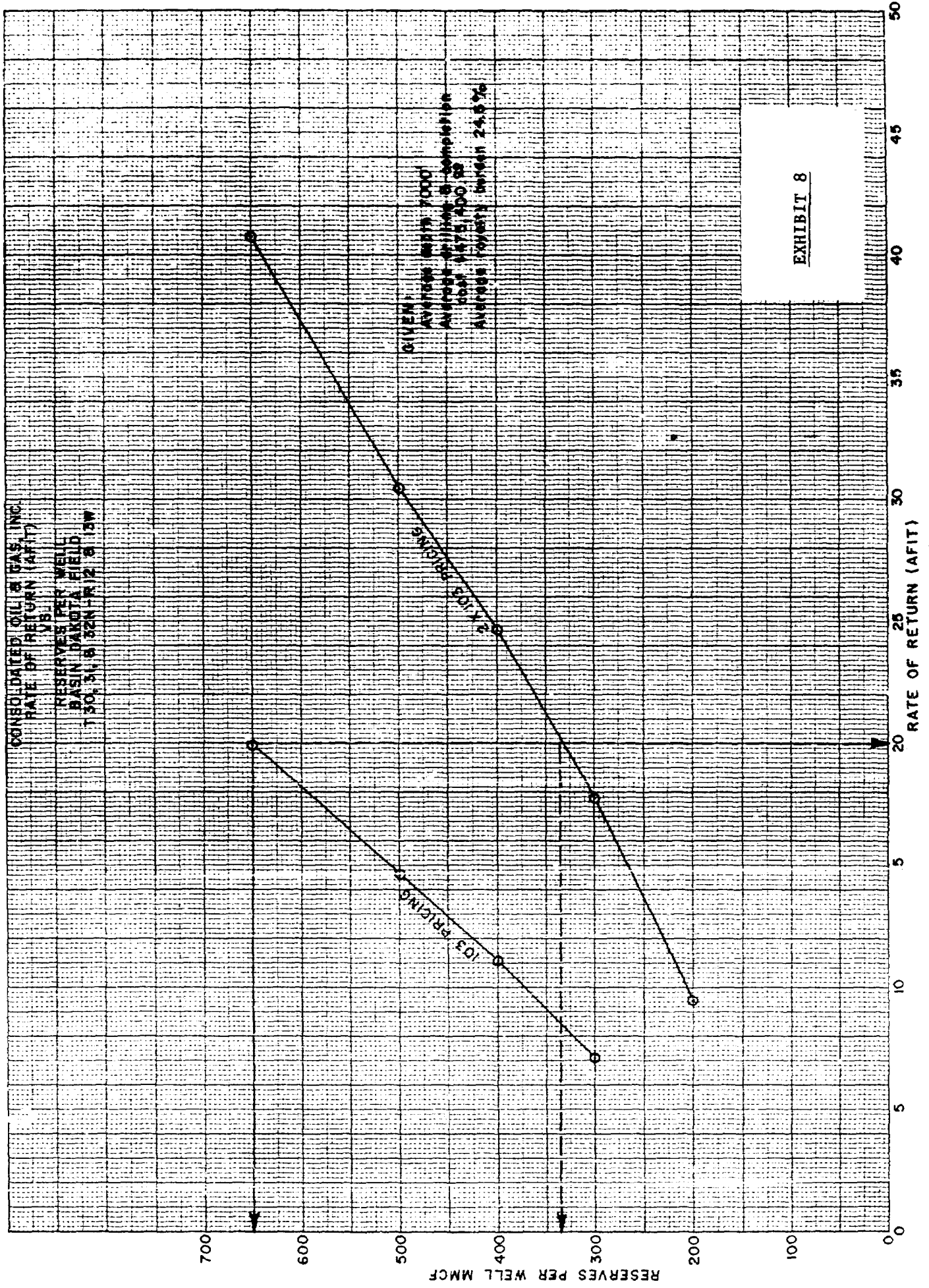
$$= \underline{\underline{.00068 \text{ md.}}}$$

Upper Dakota

$$K = \frac{52000(.014)(646)(.91) \ln(.61 \times \frac{1320}{20})}{(703)(51)(2592^2 - 32^2)}$$

$$= .0000146 \text{ D}$$

$$= \underline{\underline{.0146 \text{ md.}}}$$



CONSOLIDATED OIL & GAS, INC.

ASSUMPTIONS USED IN MAKING ECONOMIC

CALCULATIONS

BASIN DAKOTA FIELD

SAN JUAN COUNTY, NEW MEXICO

Drilling and completion costs (including Tank Battery)	\$475,400
Operating Costs \$/mo	150
Depth	7000'
Consolidated Working Interest	100.00
Royalty Interest Typical to Consolidated Holdings	24.5
Initial Stabilized Production Rate(MCFD)	
200 MMCF Reserves	89
300 MMCF Reserves	150
400 MMCF Reserves	189
500 MMCF Reserves	232
650 MMCF Reserves	400
Liquid Yield (Bbls/MMCF)	3.85
Fully Adjusted Gas Price as of October 1, 1981 (\$/Mcf)	\$3.11
Maximum Gas Price (\$/Mcf)	\$10.42
Maximum Oil Price (\$/Bbl)	\$50.00
Rate of Price Escalation %	\$7.00
Severance tax (%)	\$8.00
Deregulation Tax Data, Base Oil Price	\$14.11
Windfall Profit Tax Rate %	\$30.00

TYPICAL WELL NO. 2
 BASIN DAKOTA
 SAN JUAN CO., NEW MEXICO
 100 MCF PER WELL 103 PRICE
 CONSOLIDATED OIL & GAS
 ECONOMICS OF DEVELOPMENT

RESERVE AND ECONOMICS
 AS OF DATE 1 / 1/1981

DATE: 01/16/81.
 TIME: 17.04.46.
 FILE: TYPW2
 PROJ: 3

END GROSS OIL GROSS GAS OIL TO NET GAS TO NET REVENUE TO NET INVESTMENT NET OPER EXPENSES NET INCOME BEFORE FIT NET INCOME CUM. DISC	20.000 PCT
MO-YR PRODUCTION PRODUCTION INTEREST INTEREST INTEREST INTEREST	
MB MB MB MB MB	
12-81 .052 13.500 .039 10.192 30.441 475.400 1.800 -446.759 -446.759 -449.344	
12-82 .213 55.523 .161 41.920 133.991 0. 1.926 132.065 -314.694 -351.316	
12-83 .151 39.166 .114 29.571 101.073 0. 2.061 99.012 -215.682 -291.132	
12-84 .112 29.108 .085 21.976 80.197 0. 2.205 77.992 -137.690 -252.310	
12-85 .087 22.484 .065 16.976 66.157 0. 2.359 63.798 -73.892 -226.306	
12-86 .068 17.890 .052 13.507 56.177 0. 2.525 53.652 -20.240 -208.397	
12-87 .056 14.574 .042 11.003 48.897 0. 2.701 46.195 25.956 -193.770	
12-88 .047 12.101 .035 9.136 43.421 0. 2.891 40.530 66.486 -186.698	
12-89 .039 10.209 .030 7.708 39.168 0. 3.092 36.076 102.562 -180.085	
12-90 .034 8.728 .026 6.590 35.829 0. 3.310 32.519 135.081 -175.204	
12-91 .029 7.547 .021 5.698 33.078 0. 3.540 29.533 164.619 -171.573	
12-92 .025 6.592 .019 4.977 30.841 0. 3.600 27.241 191.860 -168.831	
12-93 .022 5.806 .017 4.383 29.011 0. 3.600 25.411 217.271 -166.737	
12-94 .020 5.153 .015 3.891 27.520 0. 3.600 23.920 241.191 -165.122	
12-95 .018 4.605 .014 3.476 26.274 0. 3.600 22.673 263.867 -163.869	
9 TOT .973 252.986 .735 191.904 782.077 475.400 42.810 263.867 263.867 -163.869	
AFTER .181 47.014 .136 35.496 336.646 0. 91.117 245.529 509.396 -159.661	
TOTAL 1.154 300.000 .871 226.500 1118.723 475.400 133.927 509.396 509.396 -159.661	
CUM. 0. 0. NET OIL REVENUE 34.553	
ULT. 1.154 300.000 NET GAS REVENUE 1084.170	
CUM NET INC/INV(1) 1.07 NET PROD REVENUE 0.	
GROSS WELLS 1 CUM NET PW/INV(1) -134	
MONTHS 1ST YEAR 12 LIFE (YEARS) 40.31	
INITIAL W.I., PCT 100.0000 RATE OF RETURN,PCT 10.37	
	75.5000

DATE: 01/16/81
TIME: 17.20.11.
FILE: TYPW2
PROJ: 3

AS OF DATE: 1/1/1981

END- MO-YR	NET OIL MB-----	NET GAS MMF-----	REVENUE TO INT. M\$-----	OPER. EXPENSE M\$-----	NET INCOME M\$-----	CAPITAL INVEST. M\$-----	DEPR. M\$-----	DEPL. M\$-----	INCOME TAX M\$-----	CASH FLOW M\$-----	CUM. NET PW M\$-----
12-81	.039	10.192	30.441	1.800	28.641	475.400	52.965	0.	-61.834	-384.924	-393.293
12-82	.161	41.920	133.991	1.926	132.065	0.	45.401	0.	41.599	90.466	-326.142
12-83	.114	29.571	101.073	2.205	99.012	0.	38.918	0.	28.845	70.167	-283.492
12-84	.085	21.976	80.197	2.359	77.992	0.	33.360	0.	21.423	56.569	-255.334
12-85	.065	16.976	66.157	2.359	63.798	0.	28.597	0.	16.897	46.901	-236.217
12-86	.052	13.507	56.177	2.525	53.652	0.	24.513	0.	13.987	39.665	-222.977
12-87	.042	11.003	48.897	2.701	46.196	0.	21.013	0.	12.088	34.108	-213.654
12-88	.035	9.136	43.421	2.891	40.530	0.	18.012	0.	10.809	29.721	-207.001
12-89	.030	7.708	39.168	3.092	36.076	0.	15.440	0.	9.905	26.171	-202.204
12-90	.026	6.590	35.829	3.310	32.519	0.	13.235	0.	9.256	23.263	-198.712
12-91	.021	5.698	33.078	3.540	29.538	0.	11.345	0.	8.733	20.805	-196.155
12-92	.019	4.977	30.841	3.600	27.241	0.	9.725	0.	8.408	18.833	-194.259
12-93	.017	4.383	29.041	3.600	25.441	0.	8.336	0.	8.196	17.215	-192.840
12-94	.015	3.891	27.520	3.600	23.920	0.	7.146	0.	8.052	15.868	-191.769
12-95	.014	3.476	26.276	3.600	22.676	0.	6.125	0.	7.944	14.732	-190.955
8 TOT	.735	191.004	782.077	42.810	739.267	475.400	354.130	0.	144.308	119.561	-190.955
AFTER	.136	35.496	336.646	21.117	245.529	0.	36.770	0.	100.205	145.325	-188.384
TOTAL	.871	226.500	1118.723	133.927	984.796	475.400	370.900	0.	244.513	264.886	-188.384
RECAP											
INTEREST FRACTION		GROSS	M.I.	NET						DIS	PW OF NET
OIL RESERVES, MB	1.000000	1.000000	1.000000	.755000		LIFE (YEARS)				PCT	M\$
GAS RESERVES, MMCF	1.154	1.154	1.154	.871		GROSS OIL WELLS				---	----
PRODUCTS	0.	0.	0.	0.		GROSS GAS WELLS				S	46.322
REVENUE, M\$	1617.726	1617.726	1118.723	0.		RATE OF RETURN, PCT				10	-68.754
OPERATING EXPENSE, M\$	133.927	133.927	133.927	133.927		DISCOUNT RATE, PCT				15	-139.728
TANGIBLES, M\$	370.900	370.900	370.900	370.900		PAYOUT YEARS				20	-188.385
INTANGIBLES, M\$	104.500	104.500	104.500	104.500						30	-251.770
										40	-291.882
										50	-319.812
INITIAL OIL PRICE (\$/B)			44.23			M.I. BEFORE PAYOUT, PCT		100.00		70	-356.357
INITIAL GAS PRICE (\$/M)			3.1100			M.I. AFTER PAYOUT, PCT		100.00		100	-387.734

TYPICAL WELL NO. 1
 BASIN DAKOTA
 SAN JUAN CO., NEW MEXICO
 400 MCF PER WELL 101 PRICE
 CONSOLIDATED OIL & GAS
 ECONOMICS OF DEVELOPMENT

RESERVE AND ECONOMIC
 AS OF DATE 1 / 1/1981

DATE: 01/16/81.
 TIME: 14.24.22.
 FILE: TYPE
 PROJ: 1

END GROSS OIL GROSS GAS OIL TO NET GAS TO NET REVENUE TO NET INVESTMENT NET OPER NET INCOME CUMULATIVE CUM. DISC	NO-YR PRODUCTION INTEREST INTEREST INTEREST INTEREST	20.000 PCT								
-----NB-----	-----NB-----	-----NB-----								
12-81	.065	16.860	.049	12.729	38.019	475.400	1.800	-439.181	-439.181	-442.475
12-82	.284	73.944	.214	55.828	178.457	0.	1.926	176.531	-262.450	-311.441
12-83	.200	51.934	.151	39.210	134.016	0.	2.061	131.955	-130.495	-231.233
12-84	.148	38.477	.112	29.050	106.009	0.	2.205	103.804	-26.691	-179.563
12-85	.114	29.651	.086	22.387	87.224	0.	2.359	84.865	57.574	-144.971
12-86	.091	23.550	.069	17.780	73.994	0.	2.525	71.469	129.443	-121.115
12-87	.073	19.155	.055	14.462	64.248	0.	2.701	61.547	190.490	-104.292
12-88	.061	15.886	.046	11.994	56.981	0.	2.891	54.090	245.080	-92.185
12-89	.052	13.388	.039	10.108	51.393	0.	3.092	48.301	293.381	-83.331
12-90	.044	11.437	.034	8.635	46.930	0.	3.310	43.620	337.001	-76.784
12-91	.038	9.882	.028	7.461	43.313	0.	3.540	39.773	376.774	-71.895
12-92	.033	8.625	.025	6.512	40.363	0.	3.600	36.763	413.537	-68.195
12-93	.029	7.593	.022	5.732	37.948	0.	3.600	34.348	447.085	-65.363
12-94	.026	6.737	.020	5.087	35.975	0.	3.600	32.375	480.260	-63.178
12-95	.023	6.016	.017	4.542	34.309	0.	3.600	30.709	510.969	-61.481
S TOT	1.281	333.135	.967	251.517	1029.179	475.400	42.810	510.969	510.969	-61.481
AFTER	.257	66.865	.194	50.483	479.930	0.	113.385	366.545	877.514	-55.715
TOTAL	1.538	400.000	1.161	302.000	1509.109	475.400	156.195	877.514	877.514	-55.715
CUM.	0.	0.	NET OIL REVENUE	46.139	NET GAS REVENUE	1462.970	5 PCT	399.260	40 PCT	-239.118
ULT.	1.538	400.000	NET PROD REVENUE	0.	NET PROD REVENUE	0.	10 PCT	168.950	50 PCT	-286.561
CUM NET INC/INV(1)	1.85	1	CUM NET PW/INV(1)	-12	CUM NET PW/INV(1)	-12	15 PCT	33.973	60 PCT	-320.769
GROSS WELLS	1	1	LIFE (YEARS)	46.50	LIFE (YEARS)	46.50	20 PCT	-55.715	80 PCT	-366.248
MONTHS 1ST YEAR	12	12	RATE OF RETURN,PCT	16.89	RATE OF RETURN,PCT	16.89	30 PCT	-169.281	100 PCT	-394.431
INITIAL W.I., PCT	100.0000	100.0000	INITIAL W.I., PCT	75.5000	INITIAL W.I., PCT	75.5000				

EXHIBIT 11

TYPICAL WELL NO. 1
 BASIN DAKOTA
 SAN JUAN CO., NEW MEXICO
 400 MMF PER WELL 103 PRICE
 CONSOLIDATED OIL & GAS
 ECONOMICS OF DEVELOPMENT

DATE: 01/16/81
 TIME: 14.34.00.
 FILE: TYPW
 PROJ: 1

AFTER TAX ECONOMICS
 AS OF DATE: 1/1/1981

END- MO-YR	NET OIL MMF	NET GAS MMF	REVENUE TO INT. M\$	OPER. EXPENSE M\$	NET INCOME M\$	CAPITAL INVEST. M\$	DEPR. M\$	DEPL. M\$	INCOME TAX M\$	CASH FLOW M\$	CUM. NET PW M\$
12-81	.049	12.729	38.019	1.800	36.219	475.400	52.965	0.	-55.772	-383.408	-391.919
12-82	.214	55.828	178.457	1.926	176.531	0.	45.401	0.	60.320	116.211	-305.659
12-83	.151	39.210	134.016	2.061	131.955	0.	38.918	0.	42.797	89.158	-251.465
12-84	.112	29.050	106.009	2.205	103.804	0.	33.360	0.	32.404	71.400	-215.925
12-85	.086	22.387	87.224	2.359	84.865	0.	28.597	0.	25.883	58.982	-191.883
12-86	.069	17.780	73.974	2.525	71.449	0.	24.513	0.	21.600	49.869	-175.237
12-87	.055	14.462	64.248	2.701	61.547	0.	21.013	0.	18.646	42.901	-163.511
12-88	.046	11.994	56.981	2.891	54.090	0.	18.012	0.	16.596	37.494	-155.118
12-89	.039	10.108	51.393	3.092	48.301	0.	15.440	0.	15.116	33.185	-149.035
12-90	.034	8.635	46.930	3.310	43.620	0.	13.235	0.	13.977	29.643	-144.586
12-91	.028	7.461	43.313	3.540	39.773	0.	11.345	0.	13.077	26.696	-141.304
12-92	.025	6.512	40.363	3.600	36.763	0.	9.725	0.	12.437	24.326	-138.856
12-93	.022	5.732	37.948	3.600	34.348	0.	8.336	0.	11.965	22.383	-137.011
12-94	.020	5.087	35.975	3.600	32.375	0.	7.146	0.	11.605	20.770	-135.607
12-95	.017	4.542	34.309	3.600	30.709	0.	6.125	0.	11.308	19.401	-134.537
9 TOT	.967	251.517	1029.179	42.810	986.369	475.400	334.130	0.	251.959	259.009	-134.537
AFTER	.194	50.483	479.930	113.385	366.545	0.	36.770	0.	151.696	214.848	-131.057
TOTAL	1.161	302.000	1509.109	156.195	1352.914	475.400	370.900	0.	403.655	473.858	-131.057

RECAP

INTEREST FRACTION	1.000000	1.000000	W.I.	NET	LIFE (YEARS)	46.50	DIS	PW OF NET
OIL RESERVES, MB	1.538	1.538			GROSS OIL, WELLS	0.	PCT	M\$
GAS RESERVES, MMCF	400.000	400.000			GROSS GAS WELLS	1.000		
PRODUCTS	0.	0.			RATE OF RETURN, PCT	11.19		
REVENUE, M\$	2182.032	2182.032		1509.109	DISCOUNT RATE, PCT	20.0		
OPERATING EXPENSE, M\$	156.195	156.195		156.195	PAYOUT YEARS	5.96		
TANGIBLES, M\$	370.900	370.900		370.900				
INTANGIBLES, M\$	104.500	104.500		104.500				
INITIAL OIL PRICE (\$/B)			44.24		W.I. BEFORE PAYOUT, PCT	100.00		
INITIAL GAS PRICE (\$/M)			3.1100		W.I. AFTER PAYOUT, PCT	100.00		

TYPICAL WELL NO. 4
 BASIN DAKOTA
 SAN JUAN CO., NEW MEXICO
 500 MME PER WELL 101 PRICE
 CONSOLIDATED OIL & GAS
 ECONOMICS OF DEVELOPMENT

RESERVES AND ECONOMICS
 AS OF DATE: 1/1/1981

DATE: 01/16/81.
 TIME: 17.04.56.
 FILE: TYPW2
 PROJ: 6

END	MO-YR	GROSS OIL PRODUCTION	GROSS GAS PRODUCTION	OIL TO NET INTEREST	GAS TO NET INTEREST	REVENUE TO INTEREST	NET INVESTMENT	NET OPER EXPENSES	NET INCOME BEFORE FIT	NET INCOME CUMULATIVE	20.000 PCT CUM. DISC NET INCOME
12-81		.080	20.880	.060	15.764	47.072	475.400	1.800	-430.128	-430.128	-434.269
12-82		.355	92.219	.268	69.626	222.584	0.	1.926	220.658	-209.470	-270.480
12-83		.248	64.577	.188	48.755	166.622	0.	2.061	164.561	-44.909	-170.453
12-84		.184	47.743	.139	36.046	131.548	0.	2.205	129.343	84.434	-106.071
12-85		.141	36.733	.106	27.734	108.051	0.	2.359	105.692	190.126	-62.990
12-86		.112	29.138	.085	21.999	91.533	0.	2.525	89.008	279.134	-33.280
12-87		.091	23.677	.068	17.876	79.439	0.	2.701	76.738	355.872	-12.304
12-88		.076	19.620	.058	14.813	70.385	0.	2.891	67.504	423.376	2.806
12-89		.063	16.524	.047	12.476	63.391	0.	3.092	60.299	483.675	13.858
12-90		.055	14.106	.042	10.650	57.908	0.	3.310	54.598	538.273	22.054
12-91		.047	12.184	.035	9.199	53.407	0.	3.540	49.867	588.140	28.183
12-92		.040	10.629	.030	8.025	49.719	0.	3.600	46.119	634.259	32.825
12-93		.036	9.354	.028	7.062	46.759	0.	3.600	43.159	677.418	36.383
12-94		.032	8.295	.024	6.263	44.293	0.	3.600	40.693	718.111	39.129
12-95		.029	7.407	.022	5.592	42.266	0.	3.600	38.666	756.777	41.267
8 TOT		1.789	413.086	1.200	311.880	1274.987	475.400	42.810	756.777	756.777	41.267
AFTER		.334	86.914	.252	65.620	624.729	0.	132.842	491.887	1248.664	48.560
TOTAL		1.923	500.000	1.452	377.500	1899.716	475.400	175.652	1248.664	1248.664	48.560
CUM.		0.	0.				57.749	5 PCT	622.058	40 PCT	-180.457
ULT.		1.923	500.000				1841.967	10 PCT	330.138	50 PCT	-239.670
							0.	15 PCT	160.754	60 PCT	-282.368
								20 PCT	48.560	80 PCT	-339.154
								30 PCT	-93.289	100 PCT	-374.362
CUM NET INC/INV(1)		2.63					.10				
GROSS WELLS		1					51.90				
MONTHS 1ST YEAR		12					23.01				
INITIAL M.I., PCT		100.0000					75.5000				

EXHIBIT 12


```
DATE: 01/16/81.  
TIME: 17.20.23.  
FILE: TYPE2  
PROJ: 6
```

AS OF DATE: 1/ 1/1981

END- NO-YR	NET OIL MB-----	NET GAS MMF-----	REVENUE TO INT. M\$-----	OPER. EXPENSE M\$-----	NET INCOME M\$-----	CAPITAL INVEST. M\$-----	DEPR. M\$-----	DEPL. M\$-----	INCOME TAX M\$-----	CASH FLOW M\$-----	CUM. NET PW M\$-----
12-81	.060	15.764	47.072	1.800	45.272	475.400	52.965	0.	-53.851	-376.276	-385.454
12-82	.268	69.626	222.584	1.926	220.658	0.	45.401	0.	84.123	136.535	-284.108
12-83	.188	48.755	166.622	2.061	164.561	0.	38.918	0.	60.309	104.252	-220.739
12-84	.139	36.046	131.548	2.205	129.343	0.	33.360	0.	46.072	83.271	-179.290
12-85	.106	27.734	108.051	2.359	105.692	0.	28.597	0.	37.006	68.686	-131.293
12-86	.085	21.999	91.533	2.525	89.008	0.	24.513	0.	30.958	58.050	-131.916
12-87	.068	17.876	79.439	2.701	76.738	0.	21.013	0.	26.748	49.990	-118.252
12-88	.058	14.813	70.395	2.891	67.504	0.	18.012	0.	23.756	43.748	-108.459
12-89	.047	12.476	63.391	3.092	60.299	0.	15.440	0.	21.532	38.767	-101.354
12-90	.042	10.650	57.908	3.310	54.598	0.	13.235	0.	19.854	34.744	-76.138
12-91	.035	9.199	53.407	3.540	49.867	0.	11.345	0.	18.491	31.376	-72.282
12-92	.030	8.025	49.719	3.600	46.119	0.	9.725	0.	17.469	28.650	-39.398
12-93	.028	7.062	46.759	3.600	43.159	0.	8.324	0.	16.715	26.444	-37.218
12-94	.024	6.263	44.293	3.600	40.693	0.	7.146	0.	16.103	24.590	-35.558
12-95	.022	5.592	42.266	3.600	38.666	0.	6.125	0.	15.619	23.047	-34.284
S TOT	1.200	311.880	1274.987	42.810	1232.177	475.400	334.130	0.	380.904	375.875	-34.284
AFTER	.252	65.620	624.729	132.842	491.887	0.	36.770	0.	218.456	273.431	-30.110
TOTAL	1.452	377.500	1899.716	175.652	1724.064	475.400	370.900	0.	599.360	649.305	-30.110
RECAP											
INTEREST FRACTION		GR088	M.I.	NET						DIS	PW OF NET
OIL RESERVES,M\$	1.000000	1.000000	1.923	.755000		LIFE (YEARS)		51.90		PCT	M\$
GAS RESERVES,M\$	1.923	1.923	1.452	1.452		GR088 OIL WELLS		0.		---	---
PRODUCITS	500.000	500.000	377.500	377.500		RATE OF RETURN,PCT		14.63		5	278.539
PERVENUE,M\$	0.	0.	0.	0.		DISCOUNT RATE,PCT		20.0		10	99.079
OPERATING EXPENSE,M\$	2746.654	2746.654	1899.716	1899.716		PAYOUT YEARS		4.76		20	-80.111
TANGIBLES,M\$	175.652	175.652	175.652	175.652						30	-173.050
INTANGIBLES,M\$	370.900	370.900	370.900	370.900						40	-231.254
	104.500	104.500	104.500	104.500						50	-271.458
INITIAL OIL PRICE (\$/B)			44.24			M.I. BEFORE PAYOUT,PCT		100.00		70	-323.487
INITIAL GAS PRICE (\$/M)			3.1100			M.I. AFTER PAYOUT,PCT		100.00		100	-367.285

TYPICAL WELL NO. 5
 BASIN DAKOTA
 SAM JUAN CO., NEW MEXICO
 650 MMF PER WELL 103 PRICE
 CONSOLIDATED OIL & GAS
 ECONOMICS OF DEVELOPMENT

R E S E R V E S A N D E C O N O M I C S

AS OF DATE 1 1/ 1/1981

DATE: 01/19/81.
 TIME: 15.51.31.
 FILE: TYP3
 PROJ: 3

END	MO-YR	GROSS OIL PRODUCTION	GROSS GAS PRODUCTION	OIL TO NET INTEREST	GAS TO NET INTEREST	REVENUE TO INTEREST	NET INVESTMENT	NET OPER EXPENSES	NET INCOME BEFORE FIT	NET INCOME CUMULATIVE	CU1, DISC	20.000 PCT
12-81		.138	36.000	.104	27.180	81.160	475.400	1.800	-396.040	-356.040	-403.370	
12-82		.435	113.027	.329	85.335	272.783	0.	1.926	-270.857	-125.183	-202.320	
12-83		.309	80.174	.233	60.532	206.897	0.	2.061	204.836	79.653	-77.812	
12-84		.230	59.826	.174	45.168	164.825	0.	2.205	162.620	242.273	3.133	
12-85		.178	46.353	.134	34.997	136.350	0.	2.359	133.991	376.264	57.750	
12-86		.142	36.970	.107	27.912	116.134	0.	2.525	113.609	488.873	95.672	
12-87		.116	30.175	.088	22.782	101.241	0.	2.701	98.540	588.413	122.606	
12-88		.097	25.095	.073	18.947	90.032	0.	2.891	87.141	675.554	142.112	
12-89		.081	21.198	.061	16.005	81.329	0.	3.092	78.237	753.791	156.452	
12-90		.070	18.144	.053	13.698	74.458	0.	3.310	71.148	824.939	167.132	
12-91		.060	15.706	.045	11.858	68.826	0.	3.540	65.286	890.225	175.157	
12-92		.053	13.727	.040	10.364	64.256	0.	3.600	60.656	950.881	181.262	
12-93		.047	12.101	.036	9.136	60.506	0.	3.600	56.906	1007.787	185.953	
12-94		.041	10.748	.031	8.115	57.375	0.	3.600	53.775	1061.562	189.583	
12-95		.037	9.609	.028	7.255	54.809	0.	3.600	51.209	1112.771	192.413	
S TOT		2.034	528.853	1.536	399.284	1630.981	475.400	42.810	1112.771	1112.771	192.413	
AFTER		.466	121.147	.351	91.466	872.308	0.	162.516	709.792	1822.563	202.173	
TOTAL		2.500	650.000	1.887	490.750	2503.289	475.400	205.326	1822.563	1822.563	202.173	
CUM.	0.	0.	0.	0.	0.	0.	75.165	5 PCT	950.746	40 PCT	-89.618	
ULT.	2.500	650.000	0.	0.	0.	0.	2428.134	10 PCT	565.769	50 PCT	-169.696	
CUM NET INC/INV(1)	3.83	0.	0.	0.	0.	0.	0.	15 PCT	346.324	60 PCT	-218.834	
GROSS WELLS	1	0.	0.	0.	0.	0.	0.	20 PCT	202.173	80 PCT	-290.984	
MONTHS 181 YEAR	12	0.	0.	0.	0.	0.	0.	30 PCT	21.109	100 PCT	-335.965	
INITIAL W.I., PCT	100.0000	0.	0.	0.	0.	0.	75.5000					

TYPICAL WELL NO. 5
BASIN DAKOTA
SAN JUAN CO., NEW MEXICO
450 MMF PER WELL 103 PRICE
CONSOLIDATED OIL & GAS
ECONOMICS OF DEVELOPMENT

DATE: 01/19/81.
TIME: 15.58.58.
FILE: TYPW3
PROJ: 8

A F T E R T A X E C O N O M I C S

AS OF DATE: 1/ 1/1981

END- MO-YR	NET OIL MMF	NET GAS MMF	REVENUE TO INT. M\$	OPER. EXPENSE M\$	NET INCOME M\$	CAPITAL INVEST. M\$	DEPR. M\$	DEPL. M\$	INCOME TAX M\$	CASH FLOW M\$	CUM. NET PW M\$
12-81	.104	27.180	81.160	1.800	79.360	475.400	52.965	0.	-37.489	-358.550	-369.387
12-82	.329	85.335	272.783	1.926	270.857	0.	45.401	0.	108.219	162.638	-248.665
12-83	.233	60.532	206.897	2.061	204.836	0.	38.918	0.	79.641	125.195	-172.566
12-84	.174	45.168	164.825	2.205	162.620	0.	33.360	0.	62.045	100.575	-122.504
12-85	.134	34.997	136.350	2.359	133.991	0.	28.597	0.	50.589	83.402	-88.508
12-86	.107	27.912	116.134	2.525	113.609	0.	24.513	0.	42.766	70.843	-64.861
12-87	.088	22.782	101.241	2.701	98.540	0.	21.013	0.	37.213	61.327	-48.098
12-88	.073	18.947	90.032	2.891	87.141	0.	18.012	0.	33.182	53.959	-36.020
12-89	.061	16.005	81.329	3.092	78.237	0.	15.440	0.	30.143	48.094	-27.205
12-90	.053	13.698	74.458	3.310	71.148	0.	13.235	0.	27.798	43.350	-20.698
12-91	.045	11.858	68.826	3.540	65.286	0.	11.345	0.	25.892	39.394	-15.855
12-92	.040	10.364	64.256	3.600	60.656	0.	9.725	0.	24.447	36.209	-12.211
12-93	.036	9.136	60.506	3.600	56.906	0.	8.336	0.	23.313	33.593	-9.442
12-94	.031	8.115	57.375	3.600	53.775	0.	7.146	0.	22.382	31.393	-7.323
12-95	.028	7.255	54.809	3.600	51.209	0.	6.125	0.	21.640	29.569	-5.688
9 TOT	1.536	399.284	1630.981	42.810	1588.171	475.400	334.130	0.	551.781	560.991	-5.688
AFTER	.351	91.466	872.308	162.516	709.792	0.	36.770	0.	323.051	386.741	-.231
TOTAL	1.887	490.750	2503.289	205.326	2297.963	475.400	370.900	0.	874.832	947.733	-.231

R E C A P

INTEREST FRACTION	1.000000	GROSS	1.000000	W.I.	NET	LIFE (YEARS)	DIS	PW OF NET
OIL RESERVES, MB	2.500		2.500		.755000	GROSS OIL WELLS	PCT	M\$
GAS RESERVES, MMCF	450.000		450.000		490.750	GROSS GAS WELLS	5	449.427
PRODUCTS	0.		0.		0.	RATE OF RETURN, PCT	10	221.599
REVENUE, M\$	3618.829		3618.829		2503.289	DISCOUNT RATE, PCT	15	88.581
OPERATING EXPENSE, M\$	205.326		205.326		205.326	PAYOUT YEARS	20	-.232
TANGIBLES, M\$	370.900		370.900		370.900		30	-113.563
INTANGIBLES, M\$	104.500		104.500		104.500		40	-184.017
INITIAL OIL PRICE (\$/B)			44.24			W.I. BEFORE PAYOUT, PCT	100.00	
INITIAL GAS PRICE (\$/M)			3.1100			W.I. AFTER PAYOUT, PCT	100.00	

TYPICAL WELL NO. 3
 BASIN DAKOTA
 SAN JUAN CO., NEW MEXICO
 200 MME PER WELL 2 X 103 PRICE
 CONSOLIDATED OIL & GAS
 ECONOMICS OF DEVELOPMENT

R E S E R V E S A N D E C O N O M I C S
 AS OF DATE 1 / 1/1981

DATE: 01/16/81.
 TIME: 17.04.53.
 FILE: TYPW2
 PROJ: 5

END	GROSS OIL	GROSS GAS	OIL TO NET	GAS TO NET	REVENUE TO	NET	NET OPER	NET INCOME	CUMULATIVE	DISC
MO-YR	PRODUCTION	PRODUCTION	INTEREST	INTEREST	INTEREST	INVESTMENT	EXPENSES	BEFORE FIT	NET INCOME	NET INCOME
-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
12-81	.031	8.010	.023	6.048	35.369	475.400	1.800	-441.831	-441.831	-444.877
12-82	.142	37.064	.108	27.983	175.112	0.	1.926	173.186	-268.645	-316.326
12-83	.101	26.041	.076	19.661	131.625	0.	2.061	129.564	-139.081	-237.571
12-84	.074	19.297	.056	14.569	104.225	0.	2.205	102.020	-37.061	-186.790
12-85	.057	14.874	.043	11.230	85.867	0.	2.359	83.508	46.447	-152.751
12-86	.045	11.814	.034	8.919	72.894	0.	2.525	70.369	116.816	-129.262
12-87	.037	9.611	.028	7.257	63.406	0.	2.701	60.705	177.521	-112.669
12-88	.031	7.971	.023	6.018	56.253	0.	2.891	53.362	230.883	-100.725
12-89	.026	6.719	.020	5.073	49.480	0.	3.092	46.388	277.271	-92.222
12-90	.022	5.739	.016	4.333	42.292	0.	3.310	38.982	316.253	-86.370
12-91	.019	4.960	.015	3.744	36.559	0.	3.540	33.019	349.272	-82.312
12-92	.017	4.329	.013	3.269	31.923	0.	3.600	28.323	377.595	-79.461
12-93	.014	3.812	.010	2.878	28.076	0.	3.600	24.476	402.071	-77.443
12-94	.013	3.381	.010	2.553	24.922	0.	3.600	21.322	423.393	-76.004
12-95	.012	3.020	.009	2.280	22.275	0.	3.600	18.675	442.068	-74.972
8 TOT	.641	166.642	.484	125.815	960.278	475.400	42.810	442.068	442.068	-74.972
AFTER	.128	33.358	.097	25.185	245.882	0.	111.483	134.399	576.467	-72.272
TOTAL	.769	200.000	.581	151.000	1206.160	475.400	154.293	576.467	576.467	-72.272
CUM.	0.	0.				23.077	5 PCT	288.747	40 PCT	-245.532
ULT.	.769	200.000				1183.083	10 PCT	119.299	50 PCT	-291.713
						0.	15 PCT	7.384	60 PCT	-325.139
							20 PCT	-72.272	80 PCT	-369.629
							30 PCT	-178.295	100 PCT	-397.181
CUM NET INC/INV(1)	1.21					-1.15				
GROSS WELLS	1					45.97				
MONTHS 1ST YEAR	12					15.46				
INITIAL W.I., PCT	100.0000					75.5000				

EXHIBIT 14

DATE: 01/16/81.
TIME: 17.20.19.
FILE: TYPW2
PROJ: 5

AS OF DATE: 1/1/1981

END- MO-YR	NET OIL MB-----	NET GAS MMF-----	REVENUE TO INT. M\$-----	OPER. EXPENSE M\$-----	NET INCOME M\$-----	CAPITAL INVEST. M\$-----	DEPR. M\$-----	DEPL. M\$-----	INCOME TAX M\$-----	CASH FLOW M\$-----	CUM. NET PW M\$-----
12-81	.023	6.048	35.369	1.800	33.569	475.400	52.965	0.	-59.469	-382.361	-390.9700
12-82	.108	27.983	175.112	1.926	173.186	0.	45.401	0.	61.537	111.849	-307.9480
12-83	.076	19.661	131.625	2.061	129.564	0.	38.918	0.	43.510	86.054	-255.9400
12-84	.056	14.569	104.225	2.205	102.020	0.	33.360	0.	32.957	69.063	-221.2630
12-85	.043	11.230	85.867	2.359	83.508	0.	28.597	0.	26.357	57.151	-197.9680
12-86	.034	8.919	72.894	2.525	70.369	0.	24.513	0.	22.011	48.358	-181.8270
12-87	.028	7.257	63.406	2.701	60.705	0.	21.013	0.	19.052	41.653	-170.4410
12-88	.023	6.018	56.253	2.891	53.362	0.	18.012	0.	16.968	36.394	-162.2950
12-89	.020	5.073	49.480	3.092	46.388	0.	15.440	0.	14.855	31.533	-156.5150
12-90	.016	4.333	42.292	3.310	38.982	0.	13.235	0.	12.359	26.623	-152.5190
12-91	.015	3.744	36.559	3.540	33.019	0.	11.345	0.	10.403	22.616	-149.7390
12-92	.013	3.269	31.923	3.600	28.323	0.	9.725	0.	8.927	19.396	-147.7870
12-93	.010	2.878	28.076	3.600	24.476	0.	8.336	0.	7.747	16.729	-146.4080
12-94	.010	2.553	24.922	3.600	21.322	0.	7.146	0.	6.505	14.517	-145.4280
12-95	.009	2.280	22.275	3.600	18.675	0.	6.125	0.	6.024	12.651	-144.7290
8 TOT	.484	125.815	960.278	42.810	917.468	475.400	334.130	0.	229.843	212.226	-144.7290
AFTER	.097	25.185	245.882	111.483	134.399	0.	36.770	0.	46.862	87.537	-142.9420
TOTAL	.581	151.000	1206.160	154.293	1051.867	475.400	370.900	0.	276.705	299.763	-142.9420
RECAP											
INTEREST FRACTION		GR08S	W.I.	NET						DIS	PW OF NET
OIL RESERVES,MB		1.000000	1.000000	.755000						PCT	M\$
GAS RESERVES,MMCF		.769	.769	.581						---	---
PRODUCTS		200.000	200.000	151.000						5	105.241
REVENUE,M\$		0.	0.	0.						10	-10.550
OPERATING EXPENSE,M\$		1741.181	1741.181	1206.160						15	-87.665
TANGIBLES,M\$		154.293	154.293	154.293						20	-142.943
INTANGIBLES,M\$		370.900	370.900	370.900						20	-142.943
		104.500	104.500	104.500						30	-217.253
										40	-265.093
										50	-298.521
										70	-342.122
										100	-379.151
INITIAL OIL PRICE (\$/B)			44.25			W.I. BEFORE PAYOUT,PCT	100.00				
INITIAL GAS PRICE (\$/M)			6.2200			W.I. AFTER PAYOUT,PCT	100.00				

TYPICAL WELL NO. 2
 BASIN DAKOTA
 SAN JUAN CO., NEW MEXICO
 300 MMF PER WELL 2 X 103 PRICE
 CONSOLIDATED OIL & GAS
 ECONOMICS OF DEVELOPMENT

R E S E R V E S A N D E C O N O M I C S
 AS OF DATE 1 / 1/1981

DATE: 01/16/81.
 TIME: 17.04.49.
 FILE: TYPW2
 PROJ: 4

											20.000 PCT
END GROSS OIL GROSS GAS OIL TO NET GAS TO NET REVENUE TO NET NET OPER NET INCOME CUMULATIVE CUM. DISC	MO-YR PRODUCTION PRODUCTION INTEREST INTEREST INTEREST INVESTMENT EXPENSES BEFORE FIT NET INCOME NET INCOME										
MB-----MMF-----MB-----MMF-----MB-----MMF-----MB-----MMF-----MB-----MMF-----MB-----MMF-----											
12-81	.052	13.500	.039	10.192	59.603	475.400	1.800	-417.597	-417.597	-422.910	
12-82	.212	55.054	.160	41.566	260.134	0.	1.926	258.208	-139.389	-231.249	
12-83	.148	38.480	.112	29.053	194.462	0.	2.061	192.401	33.012	-114.300	
12-84	.109	28.412	.082	21.451	153.458	0.	2.205	151.253	184.265	-39.012	
12-85	.084	21.838	.064	16.487	126.079	0.	2.359	123.720	307.985	11.418	
12-86	.067	17.308	.050	13.068	106.824	0.	2.525	104.299	412.284	46.232	
12-87	.054	14.056	.041	10.612	92.726	0.	2.701	90.025	502.309	70.839	
12-88	.044	11.642	.033	8.790	82.121	0.	2.891	79.230	581.539	88.574	
12-89	.038	9.800	.029	7.399	72.173	0.	3.092	69.081	650.620	101.236	
12-90	.032	8.364	.024	6.315	61.634	0.	3.310	58.324	708.944	109.991	
12-91	.028	7.221	.021	5.452	53.236	0.	3.540	49.696	758.640	116.099	
12-92	.024	6.278	.018	4.755	46.417	0.	3.600	42.817	801.457	120.409	
12-93	.022	5.541	.017	4.183	40.868	0.	3.600	37.268	838.725	123.481	
12-94	.018	4.914	.014	3.710	36.191	0.	3.600	32.591	871.316	125.681	
12-95	.017	4.386	.012	3.312	32.335	0.	3.600	28.735	900.051	127.269	
9 TOT	.949	246.814	.716	186.345	1418.261	475.400	42.810	900.051	900.051	127.269	
AFTER	.205	53.186	.155	40.155	392.066	0.	147.513	244.553	1144.604	131.585	
TOTAL	1.154	300.000	.871	226.500	1810.327	475.400	190.323	1144.604	1144.604	131.585	
CUM.	0.	0.									
ULT.	1.154	300.000									
CUM NET INC/INV(1)		2.41									
GROSS WELLS		1									
MONTHS 1ST YEAR		12									
INITIAL W.I., PCT		100.0000									

EXHIBIT 15

TYPICAL WELL NO. 2
 BASIN DAKOTA
 SAN JUAN CO., NEW MEXICO
 300 MFE PER WELL 2 X 101 PRICE
 CONSOLIDATED OIL & GAS
 ECONOMICS OF DEVELOPMENT

DATE: 01/16/81.
 TIME: 17.20.15.
 FILE: TYFW2
 PROJ: 4

AFTER TAX ECONOMICS
 AS OF DATE: 1/1/1981

END- MO-YR	NET OIL MB	NET GAS MMF	REVENUE TO INT. M\$	OPER. EXPENSE M\$	NET INCOME M\$	CAPITAL INVEST. M\$	DEPR. M\$	DEPL. M\$	INCOME TAX M\$	CASH FLOW M\$	CUM. NET PW M\$
12-81	.039	10.192	59.603	1.800	57.803	475.400	52.965	0.	-47.837	-369.759	-379.548
12-82	.160	41.566	260.134	1.926	258.208	0.	45.401	0.	102.147	156.061	-263.708
12-83	.112	29.053	194.462	2.061	192.401	0.	38.918	0.	73.672	118.729	-191.539
12-84	.082	21.451	153.458	2.205	151.253	0.	33.360	0.	56.588	94.665	-144.419
12-85	.064	16.487	126.079	2.359	123.720	0.	28.597	0.	45.659	78.061	-112.601
12-86	.050	13.068	104.824	2.525	102.299	0.	24.513	0.	38.297	66.002	-90.570
12-87	.041	10.612	92.726	2.701	90.025	0.	21.013	0.	33.126	56.899	-75.017
12-88	.033	8.790	82.121	2.891	79.230	0.	18.012	0.	29.385	49.845	-63.860
12-89	.029	7.399	72.173	3.092	69.081	0.	15.440	0.	25.748	43.333	-55.917
12-90	.024	6.315	61.634	3.310	58.324	0.	13.235	0.	21.643	36.681	-50.411
12-91	.021	5.452	53.236	3.540	49.696	0.	11.345	0.	18.408	31.288	-46.565
12-92	.018	4.755	46.417	3.600	42.817	0.	9.725	0.	15.884	26.933	-43.854
12-93	.017	4.183	40.868	3.600	37.268	0.	8.536	0.	13.887	23.381	-41.927
12-94	.014	3.710	36.191	3.600	32.591	0.	7.146	0.	12.214	20.377	-40.552
12-95	.012	3.312	32.335	3.600	28.735	0.	6.125	0.	10.853	17.882	-39.363
S TOT	.716	186.345	1418.261	42.810	1375.451	475.400	334.130	0.	449.674	450.377	-39.563
AFTER	.155	40.155	392.064	147.513	244.553	0.	36.770	0.	99.737	144.817	-36.937
TOTAL	.871	226.500	1810.327	190.323	1620.004	475.400	370.900	0.	549.411	595.194	-36.937

RECAP

INTEREST FRACTION	1.000000	W.I.	NET	LIFE (YEARS)	DIS	PW OF NET
OIL RESERVES, MB	1.154	1.154	.871	GR088 OIL WELLS	PCT	M\$
GAS RESERVES, MMCF	300.000	300.000	226.500	GR088 GAS WELLS	5	308.592
PRODUCTS	0.	0.	0.	RATE OF RETURN, PCT	10	145.691
REVENUE, M\$	2613.276	2613.276	1810.327	DISCOUNT RATE, PCT	15	38.988
OPERATING EXPENSE, M\$	190.323	190.323	190.323	PAYOUT YEARS	20	-36.938
TANGIBLES, M\$	370.900	370.900	370.900		30	-138.459
INTANGIBLES, M\$	104.500	104.500	104.500		40	-203.508
INITIAL OIL PRICE (\$/B)	44.23			W.I. BEFORE PAYOUT, PCT	70	-307.492
INITIAL GAS PRICE (\$/M)	6.2200			W.I. AFTER PAYOUT, PCT	100	-356.805

TYPICAL WELL NO. 1A
BASIN DAKOTA
SAN JUAN CO., NEW MEXICO
400.00 PER WELL 2 X 103 PRICE
CONSOLIDATED OIL & GAS
ECONOMICS OF DEVELOPMENT

RESERVES AND ECONOMICS
AS OF DATE: 1/1/1981

DATE: 01/16/81.
TIME: 14:24.28.
FILE: "YFW"
PROJ: 2

END	MO-YR	GROSS PRODUCTION	OIL	GROSS GAS PRODUCTION	OIL TO NET INTEREST	GAS TO NET INTEREST	REVENUE TO INTEREST	NET INVESTMENT	NET OPER EXPENSES	NET INCOME BEFORE FIT	NET INCOME	CUMULATIVE NET INCOME	20,000 PCT DISC
		MB		MMF	MB	MMF	MB	MB	MB	MB	MB	MB	MB
12-81		.065		16,860	.049	12,729	74,440	475,400	1,800	-402,760	-402,760	-409,462	
12-82		.271		70,407	.205	53,158	332,675	0.	1,926	330,749	-72,011	-163,955	
12-83		.191		49,837	.144	37,627	251,837	0.	2,061	249,776	177,765	-12,131	
12-84		.143		37,134	.108	28,036	200,583	0.	2,205	198,378	376,143	86,614	
12-85		.111		28,738	.084	21,697	165,927	0.	2,359	163,568	539,711	153,286	
12-86		.088		22,901	.066	17,290	141,325	0.	2,525	138,800	678,511	199,616	
12-87		.072		18,677	.054	14,101	123,219	0.	2,701	120,518	799,029	232,559	
12-88		.059		15,524	.045	11,721	109,513	0.	2,891	106,622	905,651	256,425	
12-89		.051		13,108	.039	9,896	96,541	0.	3,092	93,449	999,100	273,534	
12-90		.043		11,214	.032	8,467	82,638	0.	3,310	79,328	1078,428	285,461	
12-91		.037		9,703	.028	7,326	71,513	0.	3,540	67,973	1146,401	293,816	
12-92		.033		8,478	.025	6,401	62,508	0.	3,600	58,908	1205,309	299,746	
12-93		.029		7,472	.022	5,641	55,087	0.	3,600	51,487	1256,796	303,990	
12-94		.025		6,635	.019	5,009	48,891	0.	3,600	45,291	1302,087	307,047	
12-95		.023		5,930	.017	4,478	43,718	0.	3,600	40,118	1342,205	309,264	
\$ TOT		1.241		322,618	.937	243,577	1860,415	475,400	42,810	1342,205	1342,205	309,264	
AFTER		.297		77,382	.224	58,423	570,385	0.	184,514	385,871	1728,076	315,434	
TOTAL		1.538		400,000	1.161	302,000	2430,800	475,400	227,324	1728,076	1728,076	315,434	
CUM.		0.		0.		NET OIL REVENUE	46,389		5 PCT	1057,571	40 PCT	-25,540	
ULT.		1.538		400,000		NET GAS REVENUE	2384,411		10 PCT	701,505	50 PCT	-115,595	
						NET PROD REVENUE	0.		15 PCT	474,477	60 PCT	-180,632	
									20 PCT	315,434	80 PCT	-267,091	
									30 PCT	106,120	100 PCT	-320,649	
CUM NET INC/INV(1)		3.63				CUM NET PW/INV(1)	.66						
GROSS WELLS		1				LIFE (YEARS)	66.25						
MONTHS 1ST YEAR		12				RATE OF RETURN,PCT	37.84						
INITIAL N.I., PCT		100,0000				INITIAL N.I., PCT	75,5000						

EXHIBIT 16

DATE: 01/16/81
TIME: 14.34.08
FILE: TYPE:
PROJ: 2

AS OF DATE: 1/1/1991

END- NO-YR	NET OIL MB-----	NET GAS MMF-----	REVENUE TO INT. M\$-----	OPER. EXPENSE M\$-----	NET INCOME M\$-----	CAPITAL INVEST. M\$-----	DEPR. M\$-----	DEPL. M\$-----	INCOME TAX M\$-----	CASH FLOW M\$-----	CUP. NET PW M\$-----
12-81	.049	12.729	74.440	1.800	72.640	475.400	52.965	0.	-39.018	-363.741	-374.092
12-82	.205	53.158	332.675	1.926	330.749	0.	45.401	0.	131.260	199.489	-226.017
12-83	.144	37.627	251.837	2.061	249.776	0.	38.918	0.	96.995	152.781	-133.150
12-84	.108	28.036	200.583	2.205	198.378	0.	33.360	0.	75.908	122.470	-72.189
12-85	.084	21.697	165.927	2.359	163.568	0.	28.597	0.	62.087	101.481	-30.824
12-86	.046	17.290	141.325	2.525	138.800	0.	24.513	0.	52.572	86.228	-2.042
12-87	.054	14.101	123.219	2.701	120.518	0.	21.013	0.	45.773	74.745	18.380
12-88	.045	11.721	109.513	3.092	106.422	0.	18.012	0.	40.761	45.861	33.130
12-89	.039	9.896	96.541	3.310	93.238	0.	15.440	0.	35.894	57.565	43.682
12-90	.032	8.467	82.638	3.310	79.328	0.	13.235	0.	30.403	48.925	51.025
12-91	.028	7.326	71.513	3.540	67.973	0.	11.345	0.	26.049	41.924	56.179
12-92	.025	6.401	62.508	3.600	58.908	0.	9.725	0.	22.624	36.284	59.831
12-93	.022	5.641	55.057	3.600	51.457	0.	8.336	0.	19.849	31.638	62.439
12-94	.019	5.009	48.891	3.600	45.291	0.	7.146	0.	17.547	27.744	64.311
12-95	.017	4.478	43.718	3.600	40.118	0.	6.125	0.	15.637	24.481	65.664
8 TOT	.937	243.577	1860.415	42.810	1817.605	475.400	334.130	0.	634.331	707.877	65.664
AFTER	.224	58.423	570.385	184.514	385.871	0.	36.770	0.	160.586	225.284	69.362
TOTAL	1.161	302.000	2430.800	227.324	2203.476	475.400	370.900	0.	794.917	933.161	69.362
RECAP											
INTEREST FRACTION		GROSS	W.I.	NET						DIS	PW OF NET
OIL RESERVE,MB	1.000000	1.000000	1.538	.755000						PCT	M\$
GAS RESERVE,MMCF	1.538	1.538	1.161	1.161							
PRODUCTS	0.	0.	0.	0.							
REVENUE,M\$	3508.639	3508.639	2430.800								
OPERATING EXPENSE,M\$	227.324	227.324	227.324								
TANGIBLES,M\$	370.900	370.900	370.900								
INTANGIBLES,M\$	104.500	104.500	104.500								
INITIAL OIL PRICE (\$/B)			44.24			W.I. BEFORE PAYOUT,PCT	100.00				
INITIAL GAS PRICE (\$/M)			6.2200			W.I. AFTER PAYOUT,PCT	100.00				

TYPICAL NO. 4
 BASIN DAKOTA
 SAN JUAN CO., NEW MEXICO
 500 MME PER WELL 2 X 101 PRICE
 CONSOLIDATED OIL & GAS
 ECONOMICS OF DEVELOPMENT

RESERVES AND ECONOMICS
 AS OF DATE: 1/1/1981

DATE: 01/16/81.
 TIME: 17.05.01.
 FILE: TYPW2
 PROJ: 7

END MO-YR	GROSS PRODUCTION	OIL PRODUCTION	GAS PRODUCTION	GAS OIL TO NET INTEREST	NET REVENUE TO INTEREST	NET INVESTMENT	NET OPER EXPENSES	NET INCOME BEFORE FIT	NET INCOME CUMULATIVE	20,000 PCT CUM. DISC NET INCOME
12-81	.080	20.880	.060	15.764	92.177	475.400	1.800	-385.023	-385.023	-393.384
12-82	.336	87.890	.297	44.357	415.275	0.	1.924	413.349	28.326	-86.566
12-83	.239	62.081	.180	44.872	313.739	0.	2.061	311.478	340.004	02.885
12-84	.178	46.184	.134	34.868	249.471	0.	2.205	247.266	587.270	225.964
12-85	.137	35.701	.104	24.955	204.105	0.	2.359	203.746	791.016	309.014
12-86	.109	28.422	.082	21.458	175.390	0.	2.525	172.865	963.881	366.714
12-87	.089	23.144	.067	17.489	152.911	0.	2.701	150.110	1113.991	407.746
12-88	.074	19.242	.056	14.528	135.769	0.	2.891	132.878	1246.869	437.488
12-89	.063	16.238	.048	12.260	119.587	0.	3.092	116.495	1363.364	458.842
12-90	.053	13.886	.040	10.483	102.321	0.	3.310	99.011	1462.375	473.704
12-91	.047	12.011	.035	9.069	88.565	0.	3.540	85.025	1547.400	484.155
12-92	.040	10.492	.030	7.921	77.327	0.	3.600	73.727	1621.127	491.576
12-93	.035	9.243	.027	6.979	68.114	0.	3.600	64.514	1685.641	496.893
12-94	.032	8.205	.024	6.194	60.497	0.	3.600	56.897	1742.538	500.734
12-95	.028	7.333	.021	5.537	54.047	0.	3.600	50.447	1792.985	503.522
8 TOT	1.542	400.972	1.164	302.734	2311.195	475.400	42.810	1792.985	1792.985	503.522
AFTER	.361	99.020	.288	74.766	729.970	0.	212.366	517.610	2310.595	511.352
TOTAL	1.923	500.000	1.452	377.500	3041.165	475.400	255.170	2310.595	2310.595	511.352
CUM.	0.	0.		NET OIL REVENUE	58.048		5 PCT	1442.260	40 PCT	85.847
ULT.	1.923	500.000		NET GAS REVENUE	2983.117		10 PCT	994.152	50 PCT	-26.512
				NET PROD REVENUE	0.		15 PCT	710.035	60 PCT	-107.669
CUM NET INC/INV(1)		4.86		CUM NET PW/INV(1)	1.08		20 PCT	511.352	80 PCT	-215.581
GROSS WELLS		1		LIFE (YEARS)	73.99		30 PCT	250.110	100 PCT	-282.450
MONTHS 1ST YEAR		12		RATE OF RETURN,PCT	47.42					
INITIAL M.I., PCT		100.0000		INITIAL M.I., PCT	75.5000					

EXHIBIT 17

TYPICAL NO. 4
BASIN DAKOTA
SAN JUAN CO., NEW MEXICO
500 MME PER WELL 2 X 103 PRICE
CONSOLIDATED OIL & GAS
ECONOMICS OF DEVELOPMENT

DATE: 01/16/81.
TIME: 17.20.27.
FILE: TYPW2
PROJ: 7

AFTER TAX ECONOMICS
AS OF DATE: 1/1/1981

END- MD-YR	NET OIL MB-----	NET GAS MMF-----	REVENUE TO INT. M\$-----	OPER. EXPENSE M\$-----	NET INCOME M\$-----	CAPITAL INVEST. M\$-----	DEPR. M\$-----	DEPL. M\$-----	INCOME TAX M\$-----	CASH FLOW M\$-----	CUM. NET PW M\$-----
12-81	.060	15.764	92.177	1.800	90.377	475.400	52.965	0.	-32.201	-352.821	-364.594
12-82	.256	66.357	415.275	1.924	413.349	0.	45.401	0.	176.615	236.734	-188.473
12-83	.180	46.872	313.739	2.061	311.678	0.	38.918	0.	130.925	180.753	-78.603
12-84	.134	34.868	249.471	2.205	247.266	0.	33.360	0.	102.675	144.591	-6.632
12-85	.104	26.955	206.105	2.359	203.746	0.	28.597	0.	84.072	119.674	42.148
12-86	.082	21.458	175.390	2.525	172.865	0.	24.513	0.	71.209	101.656	76.080
12-87	.067	17.489	152.811	2.701	150.110	0.	21.013	0.	61.967	88.143	100.173
12-88	.056	14.528	135.769	2.891	132.878	0.	18.012	0.	55.136	77.742	117.575
12-89	.048	12.260	119.587	3.092	116.495	0.	15.440	0.	48.506	67.989	130.037
12-90	.040	10.483	102.321	3.310	99.011	0.	13.235	0.	41.172	57.839	138.719
12-91	.035	9.069	88.565	3.540	85.025	0.	11.345	0.	35.366	49.659	144.823
12-92	.030	7.921	77.327	3.600	73.727	0.	9.725	0.	30.721	43.006	149.151
12-93	.027	6.979	68.114	3.600	64.514	0.	8.336	0.	26.965	37.549	152.246
12-94	.024	6.194	60.497	3.600	56.897	0.	7.146	0.	23.881	33.016	154.475
12-95	.021	5.537	54.047	3.600	50.447	0.	6.125	0.	21.274	29.173	156.088
9 TOT	1.164	302.734	2311.195	42.810	2268.385	475.400	334.130	0.	878.283	914.703	156.088
AFTER	.288	74.766	729.970	212.360	517.610	0.	36.770	0.	230.804	286.807	160.541
TOTAL	1.452	377.500	3041.165	255.170	2785.995	475.400	370.900	0.	1109.087	1201.509	160.541

RECAP

INTEREST FRACTION	1.000000	GROSS	U.I.	NET	LIFE (YEARS)	DIS	PW OF NET
OIL RESERVES, MB	1.923	1.000000	.755000	1.452	GROSS OIL WELLS	PCT	M\$
GAS RESERVES, MMCF	500.000	500.000	377.500	0.	73.99	5	701.975
PRODUCTS	0.	0.	0.	0.	1.000	10	441.349
REVENUE, M\$	4389.581	4389.581	3041.165	145	RATE OF RETURN, PCT	15	277.709
OPERATING EXPENSE, M\$	255.170	255.170	255.170	170	DISCOUNT RATE, PCT	20	160.541
TANGIBLES, M\$	370.900	370.900	370.900	900	PAYOUT YEARS	30	5.518
INTANGIBLES, M\$	104.500	104.500	104.500	500		40	-92.776
						50	-166.616
INITIAL OIL PRICE (\$/B)	44.24					70	-247.650
INITIAL GAS PRICE (\$/M)	6.2200					100	-319.490
					W.I. BEFORE PAYOUT, PCT		
					W.I. AFTER PAYOUT, PCT		

TYPICAL WELL NO. 5A
 BASIN DAKOTA
 SAN JUAN CO., NEW MEXICO
 650 MFE PER WELL 2 X 103 PRICE
 CONSOLIDATED OIL & GAS
 ECONOMICS OF DEVELOPMENT

RESERVE AND ECONOMIC
 AS OF DATE 1 / 1/1981

DATE: 01/19/81.
 TIME: 15.51.36.
 FILE: TYPUS
 PROJ: 9

END	GRASS	OIL	GRASS	OIL	TO	NET	GRASS	TO	NET	REVENUE	TO	NET	OPER	NET	INCOME	CUMULATIVE	20,000
MO-YR	PRODUCTION	PRODUCTION	INTEREST	INTEREST	INTEREST	INTEREST	INVESTMENT	EXPENSES	BEFORE	FIT	NET	INCOME	NET	INCOME	NET	INCOME	DISC
-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
12-81	.138	36.000	.104	27.180	158.927	475.400	1.800	-318.273	-318.273	-318.273	-318.273	-318.273	60.052	302.260	459.439	565.447	639.080
12-82	.433	112.444	.327	84.895	531.288	0.	1.926	529.362	211.087	211.087	211.087	211.087	60.052	302.260	459.439	565.447	639.080
12-83	.305	79.256	.230	59.838	400.533	0.	2.061	398.472	609.561	609.561	609.561	609.561	60.052	302.260	459.439	565.447	639.080
12-84	.226	58.871	.171	44.448	317.977	0.	2.205	315.772	925.333	925.333	925.333	925.333	60.052	302.260	459.439	565.447	639.080
12-85	.175	45.455	.132	34.319	262.431	0.	2.359	260.072	1185.405	1185.405	1185.405	1185.405	60.052	302.260	459.439	565.447	639.080
12-86	.139	36.155	.108	27.297	223.120	0.	2.525	220.595	1406.000	1406.000	1406.000	1406.000	60.052	302.260	459.439	565.447	639.080
12-87	.113	29.445	.085	22.231	194.243	0.	2.701	191.542	1597.542	1597.542	1597.542	1597.542	60.052	302.260	459.439	565.447	639.080
12-88	.094	24.445	.071	18.456	172.480	0.	2.891	169.589	1767.131	1767.131	1767.131	1767.131	60.052	302.260	459.439	565.447	639.080
12-89	.080	20.617	.061	15.565	151.838	0.	3.092	148.746	1915.877	1915.877	1915.877	1915.877	60.052	302.260	459.439	565.447	639.080
12-90	.067	17.625	.050	13.307	129.862	0.	3.310	126.552	2042.429	2042.429	2042.429	2042.429	60.052	302.260	459.439	565.447	639.080
12-91	.059	15.239	.045	11.506	112.345	0.	3.540	108.805	2151.234	2151.234	2151.234	2151.234	60.052	302.260	459.439	565.447	639.080
12-92	.051	13.307	.038	10.047	98.084	0.	3.600	94.484	2245.718	2245.718	2245.718	2245.718	60.052	302.260	459.439	565.447	639.080
12-93	.045	11.720	.034	8.848	86.389	0.	3.600	82.789	2328.507	2328.507	2328.507	2328.507	60.052	302.260	459.439	565.447	639.080
12-94	.040	10.402	.031	7.854	76.676	0.	3.600	73.076	2401.583	2401.583	2401.583	2401.583	60.052	302.260	459.439	565.447	639.080
12-95	.036	9.294	.027	7.017	68.518	0.	3.600	64.918	2466.501	2466.501	2466.501	2466.501	60.052	302.260	459.439	565.447	639.080
8 TOT	2.001	520.275	1.511	392.808	2,94.711	475.400	42.810	2466.501	2466.501	2466.501	2466.501	2466.501	60.052	302.260	459.439	565.447	639.080
AFTER	.499	129.725	.376	97.942	956.245	0.	247.119	709.126	3175.627	3175.627	3175.627	3175.627	60.052	302.260	459.439	565.447	639.080
TOTAL	2.500	650.000	1.887	490.750	3940.956	475.400	289.929	3175.627	3175.627	3175.627	3175.627	3175.627	60.052	302.260	459.439	565.447	639.080
CUM.	0.	0.				75.290											
ULT.	2.500	650.000				3865.666											
CUM NET INC/INV(1)		6.68				1.73											
GRASS WELLS		1				83.64											
MONTHS 1ST YEAR		12				63.31											
INITIAL W.I., PCT		100.0000				75.5000											

EXHIBIT 18

DATE: 01/10/81.
TIME: 15.59.03.
FILE: TYPMS
PROJ: 9

[illegible]

END- MO-YR	NET OIL MB-----	NET GAS MMF-----	REVENUE TO INT. NO-----	OPER. EXPENSE NO-----	NET INCOME NO-----	CAPITAL INVEST. NO-----	DEPR. NO-----	DEPL. NO-----	INCOME TAX NO-----	CASH FLOW NO-----	CUM. NET PM MS-----	
12-81	.104	27.180	158.927	1.800	157.127	475.400	52.965	0.	-161	-318.111	-332.732	
12-82	.327	84.875	531.288	1.924	529.362	0.	45.401	0.	232.301	297.061	-112.232	
12-83	.230	59.838	409.533	2.041	398.472	0.	38.918	0.	172.586	225.886	25.071	
12-84	.171	44.448	317.977	2.205	315.772	0.	33.360	0.	135.558	180.214	114.774	
12-85	.132	34.319	262.481	2.359	260.072	0.	28.597	0.	111.108	148.964	175.494	
12-86	.105	27.297	223.126	2.525	220.595	0.	24.513	0.	94.119	126.476	217.710	
12-87	.085	22.231	194.243	2.701	191.542	0.	21.013	0.	81.854	109.688	247.692	
12-88	.071	18.486	172.480	2.891	169.589	0.	18.012	0.	72.757	96.832	269.367	
12-89	.061	15.565	151.838	3.092	148.746	0.	15.440	0.	63.987	84.759	284.903	
12-90	.050	13.307	129.862	3.310	126.552	0.	13.235	0.	54.392	72.160	295.734	
12-91	.045	11.506	112.345	3.540	108.805	0.	11.345	0.	46.781	62.024	303.358	
12-92	.038	10.047	98.084	3.600	94.484	0.	9.725	0.	40.684	53.800	308.774	
12-93	.034	8.848	86.389	3.600	82.789	0.	8.336	0.	35.737	47.052	312.652	
12-94	.031	7.854	76.676	3.600	73.076	0.	7.146	0.	31.646	41.430	315.448	
12-95	.027	7.017	68.518	3.600	64.918	0.	6.125	0.	28.220	36.698	317.477	
S TOT	1.511	392.808	2984.711	42.810	2941.901	475.400	334.130	0.	1201.569	1264.931	317.477	
AFTER	.376	97.942	956.245	247.119	709.126	0.	36.770	0.	322.731	386.395	323.135	
TOTAL	1.887	490.750	3940.956	289.929	3651.027	475.400	370.900	0.	1524.300	1651.326	323.135	
RECAP		GROSS	W.I.	NET	LIFE (YEARS)	GRUBS OIL WELLS	GRUBS GAS WELLS	RATE OF RETURN,PCT	DISCOUNT RATE,PCT	PAYOUT YEARS	DIB PCT	PM OF NET MS
INTEREST FRACTION		1.000000	1.000000	.755000							5	1006.323
OIL RESERVES,MB		2.500	2.500	1.887							10	678.324
GAS RESERVES,MMCF		650.000	650.000	490.750							15	469.652
PRODUCTS		0.	0.	0.							20	323.135
REVENUE,M\$		5688.415	5688.415	3940.956							30	129.355
OPERATING EXPENSE,M\$		289.929	289.929	289.929							40	6.433
TANGIBLES,M\$		370.900	370.900	370.900							50	-78.478
INTANGIBLES,M\$		104.500	104.500	104.500							70	-187.565
											100	-277.821
INITIAL OIL PRICE (\$/B)			44.24									
INITIAL GAS PRICE (\$/M)			6.2200									
						W.I. BEFORE PAYOUT,PCT	100.00					
						W.I. AFTER PAYOUT,PCT	100.00					



Consolidated Oil & Gas, Inc.

WELL COST ESTIMATE

AVERAGE DAKOTA WELL WITH UPPER & LOWER DAKOTA, 2 FRACS.

AFE No. _____

C.O.G. WI. _____

TO: Drill (X) Recomplete () Work Over ()

State New Mexico

County San Juan

Field Basin Dakota

Lease Name Average Dakota Well

Lease No. _____

Well No. Unnamed No. 1

Location: T31N, R12 & 13W - Average Dakota Well

DETAIL COST ESTIMATE				
INTANGIBLE COSTS	QUANTITY	PRICE	COST OF DRY HOLE	COST OF PRODUCER
Superintendence	15/20	200	3,000	4,000
Labor			1,000	2,500
Hauling			1,500	7,500
Drilling				
To Drill	7,000	16/ft.	112,000	112,000
Day Work - W/DP	2	5,600	11,200	11,200
Day Work - W/out Drill pipe				
Other Completion unit with compl. equip	12	2,500		30,000
Fuel			750	1,500
Water			10,000	14,000
Right of Way Damages			2,500	2,500
Drig. Mud & Chemicals (Have been having LC)			17,500	17,500
Electric & Radioactivity Logs			16,500	19,500
Coring & Core Analysis				
Acidizing & Fracturing 2 fracs using Nitrogen				90,000
Drill Stem Tests				
Gun Perforating 2 Dakota zones				6,000
Cement & Cementing Services Surf. & 3-stage prod.			3,000	17,500
Shoes, Collars, & Centralizers DV tools prod.			1,000	5,000
Welding			250	750
Road & Location			4,000	4,000
Bits & Coreheads				750
Mud Logging				
Plugging Expense			7,500	
Directional Drilling Services				
Overhead			1,500	2,000
Tool Rental				5,000
Contingencies 5%			9,700	17,700
TOTAL INTANGIBLE COSTS			202,900	370,900
PERMANENT EQUIPMENT				
Conductor Pipe " OD				
Surface Casing 8-5/8" OD, 24#	250	10.00	2,500	2,500
Prod. Casing 5 1/2 " OD 15.5#	7000	7.20		50,400
Tubing 1 1/2 " OD	7000	2.30		16,100
Casing Head Assembly			1,500	1,500
Tubing Head Assembly				1,250
Xmas Tree & Manifold Assembly				8,250
Production Packer				
Tubing Catcher				
Bottom Hole Choke				
Miscellaneous Connections				2,000
Production Unit & Tank Battery				22,500
TOTAL Permanent Equipment			4,000	104,500
TOTAL COST OF COMPLETED WELL			206,900	475,400

Date: _____

Recommended by: _____

APPROVED (Company): _____

Approved by: _____

By: _____

Date: _____

January 9, 1981



STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENT
OIL CONSERVATION DIVISION

BRUCE KING
GOVERNOR
LARRY KEHOE
SECRETARY

April 15, 1982

POST OFFICE BOX 2088
STATE LAND OFFICE BUILDING
SANTA FE, NEW MEXICO 87501
(505) 827-2434

Mr. Howard Kilchrist
NGPA Compliance
Federal Energy Regulatory Commission
Department of Energy
825 North Capitol Street, N.E.
Washington, D. C. 20426

Re: Tight Formation
Designations

Dear Mr. Kilchrist:

At the request of members of your staff, I am enclosing copies of the transcript of hearing in Cases 7209, 7317 and 7361 before the New Mexico Oil Conservation Division. I will forward the transcript of Case 7395 shortly.

Please note that the transcript of Case 7361 incorporates the record from the Case 7116 examiner hearing. As you recall, the exhibits forwarded with the Division's recommendation in Case 7361 were the exhibits admitted in the examiner hearing of Case 7116. Therefore the transcript of Case 7361 is composed of two transcripts dated December 30, 1980 and September 29, 1981.

If we can be of further assistance, please advise.

Sincerely,

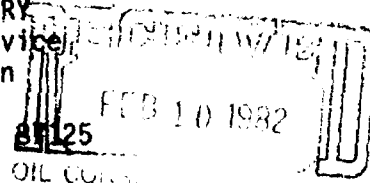
W. PERRY PEARCE
General Counsel

WPP/dr
enc.



United States Department of the Interior

OFFICE OF THE SECRETARY
Minerals Management Service
South Central Region
P. O. Box 26124
Albuquerque, New Mexico 87125



OIL CONSERVATION
FEB 08 1982

Mr. W. Perry Pearce
Oil Conservation Division
State of New Mexico
P. O. Box 2088
Santa Fe, New Mexico 87501

Dear Mr. Pearce:

This jurisdictional agency concurs in the recommendation of the State of New Mexico, Case No. 7361, Order No. R-6884, dated January 12, 1982, that the Dakota formation underlying the described lands in subject order in San Juan County, New Mexico, be designated as a Section 107 tight formation.

It is requested that this concurrence be included with the recommendation submitted to the Federal Energy Regulatory Commission.

Sincerely yours,

James W. Shelton
For Gene F. Daniel
Deputy Minerals Manager
Oil and Gas

FLUID SAMPLE DATA				Date 7-31-80		Ticket Number 727294	
Sampler Pressure _____ P.S.I.G. at Surface				Kind of D.S.T. CASED HOLE		Holliburton Location FARMINGTON	
Recovery: Cu. Ft. Gas _____				Tester MR. BROWN		Witness _____	
cc. Oil _____				Drilling Contractor SPARTAN DRILLING COMPANY DR BC			
cc. Water _____				EQUIPMENT & HOLE DATA			
cc. Mud _____				Formation Tested Basin Dakota			
Tot. Liquid cc. _____				Elevation 6940' Ft.			
Gravity _____ ° API @ _____ ° F.				Net Productive Interval 51' from 7284-7445' Ft.			
Gas/Oil Ratio _____ cu. ft./bbl.				All Depths Measured From Kelly Bushing			
RESISTIVITY _____ CHLORIDE CONTENT _____				Total Depth 7480' Ft.			
Recovery Water _____ @ _____ ° F. _____ ppm				Main Hole/Casing Size 4 1/2" 10.5# Liner			
Recovery Mud _____ @ _____ ° F. _____ ppm				Drill Collar Length _____ I.D. _____			
Recovery Mud Filtrate _____ @ _____ ° F. _____ ppm				Drill Pipe Length 7229.9' I.D. 1.995"			
Mud Pit Sample _____ @ Fresh water ppm				Packer Depth(s) 7249' Ft.			
Mud Pit Sample Filtrate _____ @ _____ ° F. _____ ppm				Depth Tester Valve 7235.5' Ft.			
Mud Weight _____ vis _____ sec.							
TYPE		AMOUNT		Depth Back		Surface	
Cushion		Fresh water 4 bbls.		Pres. Valve		Choke	
1000'						1/8" 5/8"	
Recovered 240		Feet of water					
Recovered		Feet of					
Recovered		Feet of					
Recovered		Feet of					
Recovered		Feet of					
Remarks See production test data sheet							
Q-Questionable							
TEMPERATURE		Gauge No. 7489		Gauge No. 5160		Gauge No.	
Depth:		7245 Ft.		7257.2' Ft.		TIME (00:00-24:00 hrs.)	
24 Hour Clock		24 Hour Clock		Hour Clock		Tool	
Est. ° F.		Blanked Off NO		Blanked Off YES		Blanked Off	
Actual 190 ° F.		Pressures		Pressures		Pressures	
		Field Office		Field Office		Field Office	
Initial Hydrostatic		3375 0 3120.6		3192 0 3117.2		Reported Computed	
Flow Initial		130.8 346.3-0		128 352.5 0		Minutes Minutes	
Flow Final		130.8 150.3		128 147.4		120 126	
Closed in		2383 2382.2		2426.8 2382.1		404 479	
Second Period Flow Initial							
Flow Final							
Closed in							
Third Period Flow Initial							
Flow Final							
Closed in							
Final Hydrostatic		3590 0 3120.6		3320 0 3117.2			

EAST

Lease Name

Well No.

Test No.

Tested Interval

Lease Owner/Co. party Name

Legal Location
Sec. - Twp. - Rng. 14-31N-12WField Area
Basin DakotaCounty
SAN JUANState
NEW MEXICO

7249-7480'

SOUTHLAND ROYALTY COMPANY

(6)

Casing perms. _____		Bottom choke _____		Surf. temp _____ °F		Ticket No. 727294	
Gas gravity _____		Oil gravity _____		GOR _____			
Spec. gravity _____		Chlorides _____		ppm Res. _____		@ _____ °F	
INDICATE TYPE AND SIZE OF GAS MEASURING DEVICE USED _____							

Date Time	a.m. p.m.	Choke Size	Surface Pressure psi	Gas Rate MCF	Liquid Rate BPD	Remarks
2218						On location, made up tools
2218						Trip in hole with tools
0016						On bottom
0056						Hydrospring opened
0056						Moderate blow to surface
0101		Blow Hose	.25#			
0102		"	1			
0103		"	2			
0.04		"	3			
0109		"	3.5			
0118		"	4			
0123		"	4			
0128		"	4.5			
0133		"	4			
0138			4.5			
0142			4.5			Gas to surface
0147		3/4"				Opened choke, flare to pit with 1/8"
						orifice tester
0256						Closed tool
1100						Trip out of hole with tools

SOUTHLAND ROYALTY COMPANY

727294

Lease Owner/Company Name

Ticket Number

B.T. 7489

B.T. 5160

B.T.

Depth 7245'

Depth 7257.2'

Depth

INITIAL FLOW

	Time Defl. .000"	Log $\frac{t+\theta}{\theta}$	PSIG Temp. Corr.	Time Defl. .000"	Log $\frac{t+\theta}{\theta}$	PSIG Temp. Corr.	Time Defl. .000"	Log $\frac{t+\theta}{\theta}$	PSIG Temp. Corr.
0.	.0000		346.3-0	.0000		352.5-0			
1.	.0885		613.3*	.0861		155.9			
2.	.1566		165.5	.1522		160.2			
3.	.2247		163.3	.2184		153.8			
4.	.2928		156.8	.2846		149.5			
5.	.3609		154.6	.3508		149.5			
6.	.4290		150.3	.4170		147.4			
	20 minute intervals								
	*Interval = 26 minutes								
	126 TOTAL MINUTES								
	INITIAL CLOSED IN PRESSURE								
0.	.0000	-----	150.3	.0000	-----	147.4			
1.	.0342	1.132	444.4	.0332	1.132	425.2			
2.	.0684	.862	684.0	.0664	.862	668.8			
3.	.1026	.714	893.2	.0996	.715	886.7			
4.	.1368	.617	1053.8	.1328	.617	1048.8			
5.	.1710	.545	1191.8	.1660	.546	1193.2			
6.	.2052	.490	1323.2	.1992	.490	1326.9			
7.	.2394	.446	1439.6	.2324	.446	1443.7			
8.	.2736	.410	1547.4	.2656	.410	1552.0			
9.	.3078	.379	1644.4	.2988	.379	1647.5			
10.	.3421	.353	1730.6	.3320	.353	1726.1			
11.	.4447	.293	1896.5	.4316	.294	1891.7			
12.	.5473	.251	2000.0	.5312	.252	1997.8			
13.	.6499	.220	2079.9	.6308	.220	2076.4			
14.	.7526	.196	2140.3	.7304	.196	2135.8			
15.	.8552	.177	2187.8	.8300	.177	2184.6			
16.	.9578	.161	2231.0	.9296	.161	2227.1			
17.	1.0605	.148	2265.6	1.0292	.148	2263.2			
18.	1.1631	.136	2293.7	1.1288	.137	2284.4			
19.	1.2657	.127	2319.6	1.2284	.127	2318.4			
20.	1.3684	.118	2343.4	1.3280	.119	2339.6			
21.	1.4710	.111	2360.6	1.4276	.111	2346.0			
22.	1.5736	.105	2375.8	1.5272	.105	2373.6			
23.	1.6350	.101	2382.2	1.5870	.101	2382.1			
	First 10 intervals = 10 minutes each; next 12 intervals = 30 minutes								
	each; last interval = 18 minutes								
	478 TOTAL MINUTES								

Remarks:

Q = Questionable

Gas Production

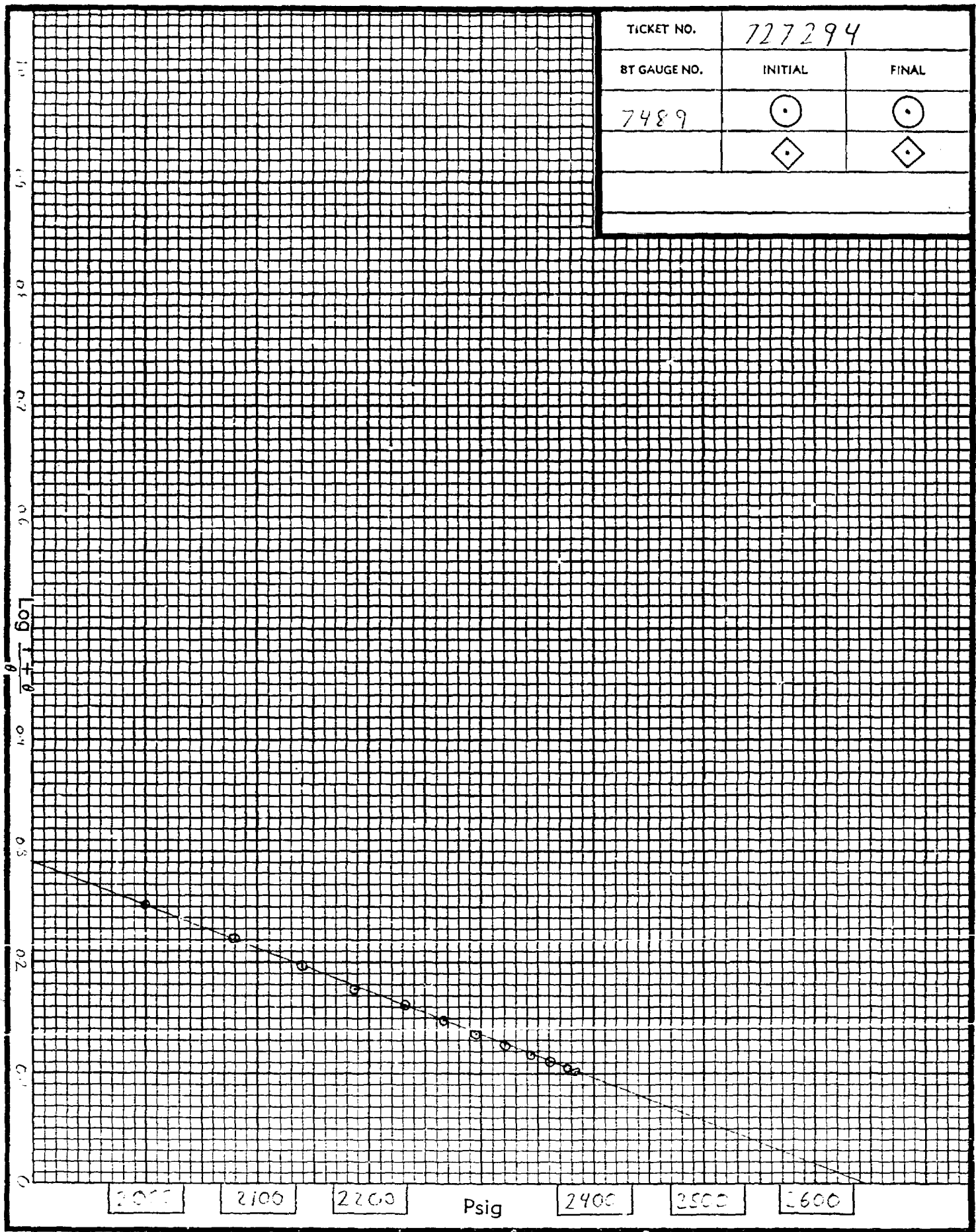
CORRECTED COPY

B.T. Gauge Numbers			7489	5160	Ticket Number		727294	
Initial Hydrostatic			PRESSURE 3121	PRESSURE 3117	Elevation		6940	ft.
Final Hydrostatic			3121	3117	1st Flow		21.6	MCF
1st Flow	Initial	Time	346	353	Production Rate	2nd Flow	-	MCF
	Final	126	150	147		3rd Flow	-	MCF
	Closed In Pressure	478	2382	2382		Hole Size		6.25
2nd Flow	Initial	Time			Footage Tested		51	ft.
	Final				Mud Weight		8.33	lbs./gal.
	Closed In Pressure				Gas Viscosity		.020	cp
3rd Flow	Initial	Time			Gas Gravity		.70	—
	Final				Gas Compressibility		.85	—
	Closed In Pressure				Temperature		190	°F
Extrapolated Static Pressure	1st		2644	2639				
	2nd							
	3rd							
Slope P/10	1st		89	74				
	2nd							
	3rd							

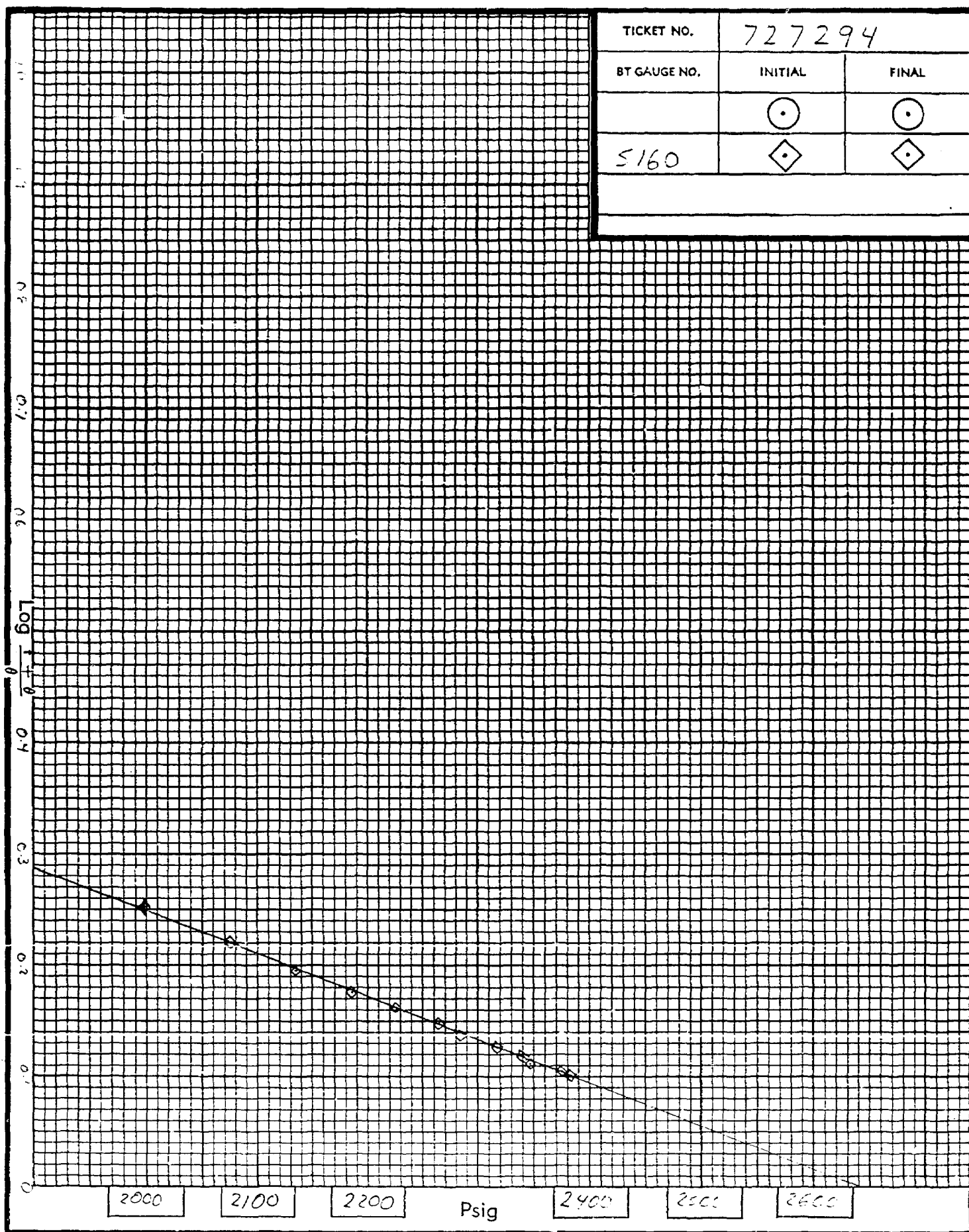
Remarks: (1) Calculations based on rates given by Bob Fielden 8-11-80 and net pay given by Marlin Thompson 10-6-80
(2) Gas gravity changed to 0.70-11-13-80

SUMMARY		B.T. Gauge No. 7489 Depth 7245'			B.T. Gauge No. 5160 Depth 7257'			UNITS
PRODUCT	EQUATION	FIRST	SECOND	THIRD	FIRST	SECOND	THIRD	
Transmissibility	$\frac{Kh}{\mu} = \frac{1637 Q_e ZT}{m}$	2.798			2.807			md. ft. cp
Theoretical Flow Capacity	$Kh = \frac{Kh}{\mu} \mu$.0560			.0561			md. ft.
Average Effective	$K = \frac{Kh}{h}$.00110			.00110			md.
Permeability	$K_1 = \frac{Kh}{h_1}$	-			-			md.
Indicated Flow Capacity	$(Kh)_e = \frac{3200 Q_e \mu ZT \log(0.472 b/r_w)}{P_e^2 - P_r^2}$.0066			.0067			md. ft.
Damage Ratio	$DR = \frac{\text{Theo. Flow Cap}}{\text{Indicated Flow Cap}} \frac{Kh}{(Kh)_e}$	8.454			8.390			-
Indicated	$OF_1 = \frac{Q_e}{P_e^2 - P_r^2} \text{ Max.}$	21.670			21.667			MCFD
Flow Rate	$OF_2 = \frac{Q_e}{\sqrt{P_e^2 - P_r^2}} \text{ Min.}$	21.635			21.634			MCFD
Theoretical	$OF_3 = OF_1 DR \text{ Max.}$	183.205			181.791			MCFD
Potential Rate	$OF_4 = OF_2 DR \text{ Min.}$	182.910			181.509			MCFD
Approx. Radius of Investigation	$b \approx \sqrt{Kt} \text{ or } \sqrt{Kt_0}$.632			.633			ft.
	$b_1 \approx \sqrt{K_1 t} \text{ or } \sqrt{K_1 t_0}$	-			-			ft.
Potentiometric Surface *	$Pot. = (EI - GD) + (2.319 Ps)$	-			-			ft.

NOTICE: These calculations are based upon information furnished by you and taken from Drill Stem Test pressure charts, and are furnished you for your information. In furnishing such calculations and evaluations based thereon, Halliburton is merely expressing its opinion. You agree that Halliburton makes no warranty express or implied as to the accuracy of such calculations or opinions, and that Halliburton shall not be liable for any loss or damage, whether due to negligence or otherwise, in connection with such calculations and opinions.



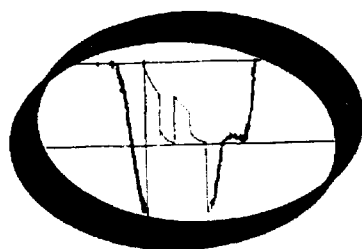
EXTRAPOLATED PRESSURE GRAPH



EXTRAPOLATED PRESSURE GRAPH

	O. D.	I. D.	LENGTH	DEPTH
Drill Pipe or Tubing	2 3/8"	1.995"	7229.9'	
Drill Collars				
Reversing Sub				
Water Cushion Valve				
Drill Pipe				
Drill Collars				
Handling Sub & Choke Assembly				
Dual CIP Valve	3.03"	1"	5'6"	7229.9'
Dual CIP Sampler				
Hydro-Spring Tester	3.03"	1.13"	4'10"	7235.5'
Multiple CIP Sampler				
Extension Joint				
AP Running Case	3.03"	2.31"	4'8 1/2"	7245'
X over				
Hydraulic Jar				
VR Safety Joint	3.03"	1.75"	2'8 1/2"	
Pressure Equalizing Crossover				
X over	3.03"	1.75"	1'	
Packer Assembly	4 1/2"	1.90"	3'4"	7249'
Distributor				
Packer Assembly				
Perforated anchor	2 3/8"	1.90"	4'2"	
Flush Joint Anchor				
Pressure Equalizing Tube				
Blanked-Off B.T. Running Case				
Drill Collars				
Anchor Pipe Safety Joint				
Packer Assembly				
Distributor				
Packer Assembly				
Anchor Pipe Safety Joint				
Side Wall Anchor				
Drill Collars				
Flush Joint Anchor				
Blanked-Off B.T. Running Case	3.03"	2.31"	4'	7257.2'
Total Depth				7480'

Formation Testing Service Report



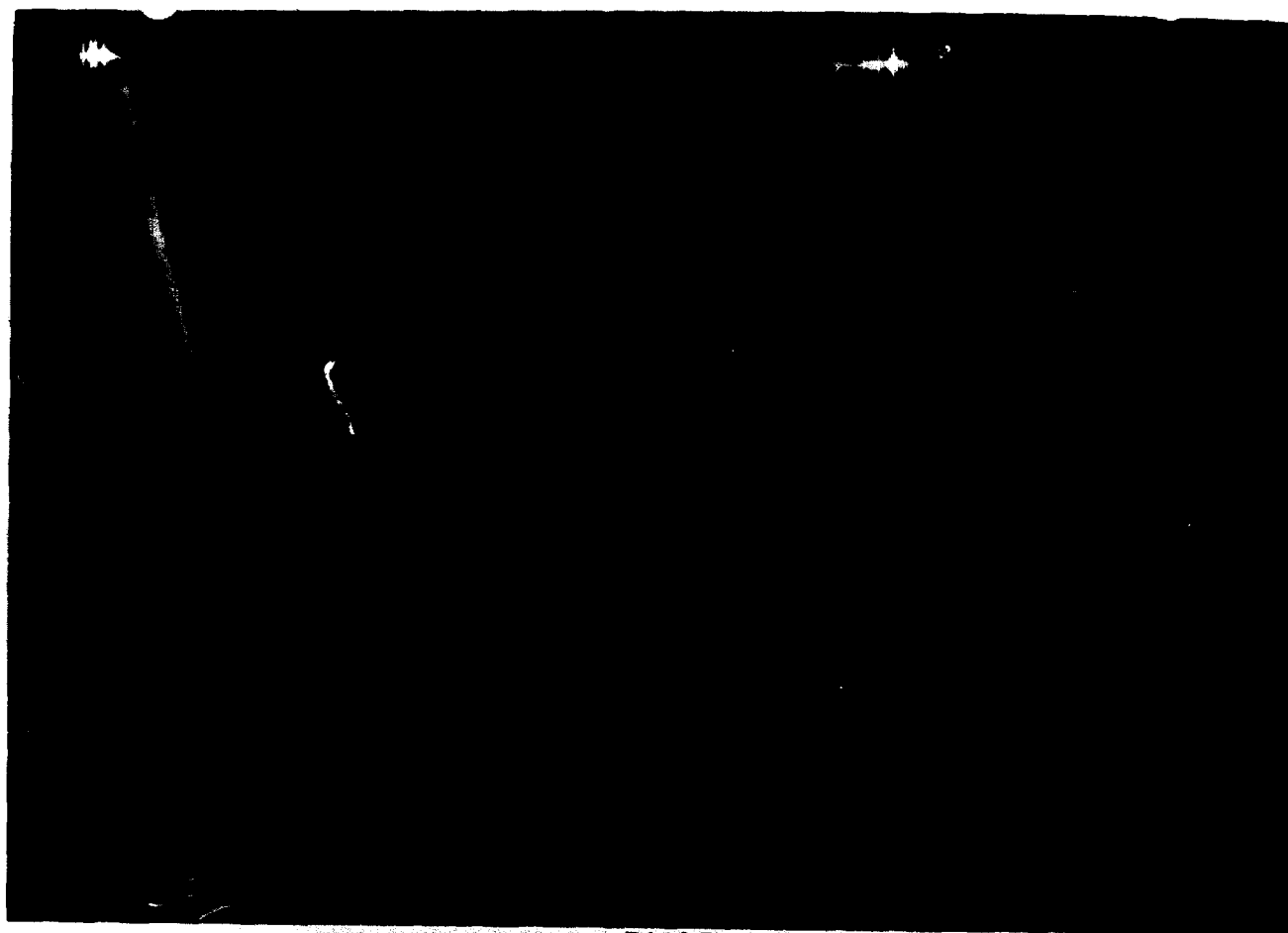
BEFORE EXAMINER NUTTER	
OIL CONSERVATION DIVISION	
<u>SRC</u>	EXHIBIT NO. <u>5</u>
CASE NO. _____	

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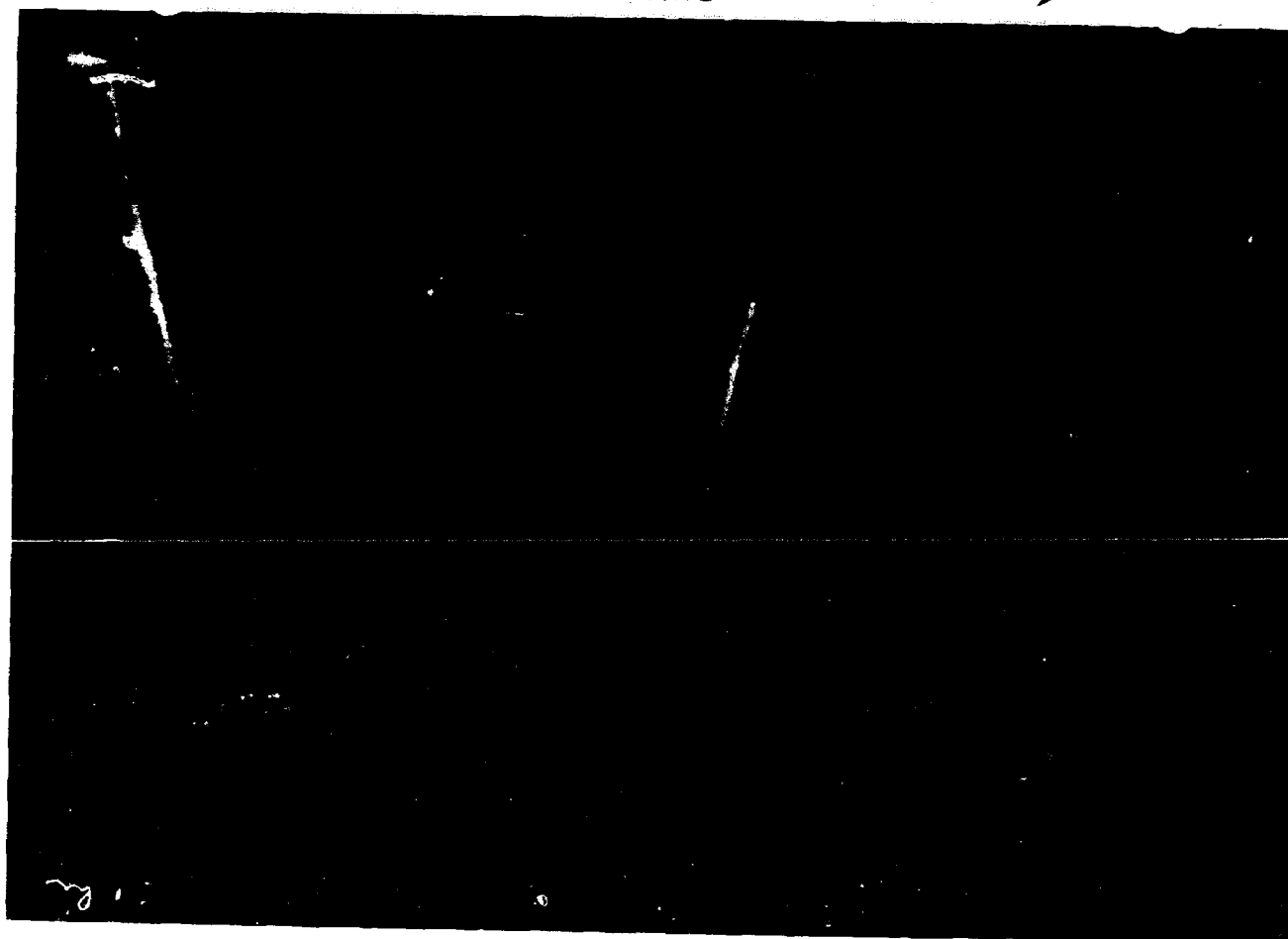
5

HALLIB

PRESSURE



TIME



Each Horizontal Line Equal to 1000 p.s.i.

- b Approximate Re
- b Approximate Re
- D.R. Damage Ratio
- El Elevation
- GD B.F. Gauge Dep
- h Interval Tested
- H Net Pay Thickn
- K Permeability
- K Permeability, F
- m Slope Extrapol
- OF Maximum Indica
- OF Maximum Indica
- OF Theoretical Op
- OF Theoretical Op
- P₁ Extrapolated Sta
- P₂ Final Flow Press
- P₃ Potentiometric S
- Q Average Adjuste
- Q Theoretical Prods
- Q₁ Measured Gas Pro
- R Corrected Recov
- r_w Radius of Well B
- t Flow Time
- t₁ Total Flow Time
- T Temperature Ran
- U Temperature by F
- U₁ Temperature by F
- U₂ Temperature by F
- U₃ Temperature by F

NOMENCLATURE

b	= Approximate Radius of Investigation	Feet
b_1	= Approximate Radius of Investigation (Net Pay Zone h_1)	Feet
D.R.	= Damage Ratio	—
El	= Elevation	Feet
GD	= B.T. Gauge Depth (From Surface Reference)	Feet
h	= Interval Tested	Feet
h_1	= Net Pay Thickness	Feet
K	= Permeability	md
K_1	= Permeability (From Net Pay Zone h_1)	md
m	= Slope Extrapolated Pressure Plot (Psi ² /cycle Gas)	psi/cycle
OF ₁	= Maximum Indicated Flow Rate	MCF/D
OF ₂	= Minimum Indicated Flow Rate	MCF/D
OF ₃	= Theoretical Open Flow Potential with/Damage Removed Max.	MCF/D
OF ₄	= Theoretical Open Flow Potential with/Damage Removed Min.	MCF/D
P_s	= Extrapolated Static Pressure	Psig.
P_f	= Final Flow Pressure	Psig.
P_w	= Potentiometric Surface (Fresh Water *)	Feet
Q	= Average Adjusted Production Rate During Test	bbls/day
Q_1	= Theoretical Production w/Damage Removed	bbls/day
Q_g	= Measured Gas Production Rate	MCF/D
R	= Corrected Recovery	bbls
r_w	= Radius of Well Bore	Feet
t	= Flow Time	Minutes
t_o	= Total Flow Time	Minutes
T	= Temperature Rankine	°R
Z	= Compressibility Factor	—
μ	= Viscosity Gas or Liquid	CP
Log	= Common Log	

* Potentiometric Surface Reference to Rotary Table When Elevation Not Given,
Fresh Water Corrected to 100 °F.

NUMBER, NAME AND
PURPOSE OF EACH EXHIBIT
BASIN DAKOTA FIELD
SAN JUAN COUNTY, NEW MEXICO

<u>Exhibit Number</u>	<u>Exhibit Name</u>	<u>Purpose of Exhibit</u>
1	Completion and Production Map	Show location of Dakota completions, production from Dakota completions, proposed tight gas area, location of cross sections, test wells and dry holes
2	Type Log	Show log characteristics and depth of Dakota formation
3	Cross Section A-A'	Show Dakota formation development in a north-south direction
4	Cross Section B-B'	Show Dakota formation development in an east-west direction
5	Formation Testing Service Report	Show in situ permeability from pressure buildup analysis
6	Darcy Law Calculation	Show in situ permeability from Darcy Law calculation
7	Darcy Law Calculation	Show in situ permeability from Darcy Law calculation
8	Technical Paper	Show relationship of in situ permeability to laboratory permeability
9	Explanation of Paper	Explain method of determining in situ permeability from routine core analysis
10	Core Analysis	Show in situ permeability from core analysis
11	Core Analysis	Show in situ permeability from core analysis

<u>Exhibit Number</u>	<u>Exhibit Name</u>	<u>Purpose of Exhibit</u>
12	Permeability, Gas and Crude Production Data	Show in situ permeability, stabilized production rate and crude production from each test well
13	Cumulative Production and Ultimate Reserves	Show cumulative production and ultimate reserves for each well in the proposed tight formation area
14	Economic Calculation	Show economics of drilling and completing a Dakota well at the 103 gas price
15	Economic Calculation	Show economics of drilling and completing a Dakota well at 200% of the 103 price
16	Economic Assumptions	Show assumptions used in making economic calcula- tions
17	Authority for Expenditure	Show cost to drill and complete a Dakota well

SOUTHLAND ROYALTY COMPANY
PATTERSON "B" COM. 1E
SW-2-31N-12W
BASIN DAKOTA FIELD
SAN JUAN COUNTY, NEW MEXICO

Calculation of Permeability using Darcy's Law:

Data:

Qg = 224,000 SCFD (open hole test)
h = 34 feet (log)
Pwf = 54 psia (measured at surface and calculated to bottomhole)
Pe = 2650 psia (DST in East No. 7E located 9600' to south)
gg = .70
T = 190°F = 650°R (calc.)
re = 1320 feet
rw = 0.20 feet
Psc = 668 psia
Tsc = 392°R
Ug = .014 cps (calc.)
Z = .87 (calc.)

Where:

Qg = gas flow rate	rw = wellbore radius
h = net pay	Psc = pseudo critical pressure
Pwf = flowing bottomhole pressure	Tsc = pseudo critical temperature
Pe = shut-in bottomhole pressure	Ug = gas viscosity
at drainage radius, re	Z = compressibility factor
gg = gas specific gravity	for gas
T = bottomhole temperature	
re = drainage radius for 160 acre spacing	

$$Q_g = 703 K h \frac{(P_e^2 - P_{wf}^2)}{U_g T Z \ln (.61 re/rw)}$$

$$K = \frac{Q_g U_g T Z \ln (.61 re/rw)}{(703 h (P_e^2 - P_{wf}^2))}$$

$$K = \frac{224,000 (.014) (650) (.87) \ln (.61 1320/.20)}{703 (34) (2650^2 - 54^2)}$$

$$K = .0000877 \text{ D.}$$

$$K = .0877 \text{ md.}$$

BEFORE EXAMINER NUTTER	
OIL CONSERVATION DIVISION	
SZC	EXHIBIT NO. 6
CASE NO.	

SOUTHLAND ROYALTY COMPANY
PIERCE NO. 2
SW-30-31N-10W
BASIN DAKOTA FIELD
SAN JUAN COUNTY, NEW MEXICO

Calculation of Permeability using Darcy's Law:

Data:

Qg = 208,000 SCFD (potential test)
h = 55 feet (log)
Pwf = 24 psia (calc.)
Pe = 2520 psia (calc.)
gg = .70
T = 186°F = 646°R (calc.)
re = 1320 feet
rw = .13 feet
Psc = 668 psia
Tsc = 392
Ug = .014 cps (calc.)
Z = .91 (calc.)

Where:

Qg = gas flow rate	re = drainage radius for 160 acre spacing
h = net pay	rw = wellbore radius
Pwf = flowing bottomhole pressure	Psc = pseudo critical pressure
Pe = shut-in bottomhole pressure at drainage radius, re	Tsc = pseudo critical temperature
gg = gas specific gravity	Ug = gas viscosity
T = bottomhole temperature	Z = compressibility factor for gas

$$Q_g = 703Kh \frac{(P_e^2 - P_{wf}^2)}{U_g T Z \ln (.61 re/rw)}$$

$$K = \frac{Q_g U_g T Z \ln (.61 re/rw)}{703 h (P_e^2 - P_{wf}^2)}$$

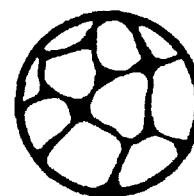
$$K = 208,000 \frac{(.014)(646)(.91) \ln (.61 1320/.13)}{703 (55) (2520^2 - 24^2)}$$

$$K = .0000609 \text{ D.}$$

$$K = .0609 \text{ md.}$$

BEFORE EXAMINER NUTTER	
OIL CONSERVATION DIVISION	
SRC	EXHIBIT NO. 7
CASE NO. _____	

BEFORE EXAMINER NUTTER	
OIL CONSERVATION DIVISION	
SRC	EXHIBIT NO. 8
CASE NO. _____	



Effect of Overburden Pressure and Water Saturation on Gas Permeability of Tight Sandstone Cores

Rex D. Thomas, SPE-AIME, U. S. Bureau of Mines
Don C. Ward, SPE-AIME, U. S. Bureau of Mines

Introduction

Research on the potential of nuclear explosions to stimulate gas production from low-permeability (tight) sandstone reservoirs is being conducted by the U. S. Bureau of Mines in cooperation with the Atomic Energy Commission. This report describes the part of that research that was conducted to establish correlation between permeability measured on dry cores at low external pressure (routine analysis) and permeability at reservoir conditions.

Cores used in this research were obtained from two Plovershare gas-stimulation projects. Project Gasbuggy cores from the Pictured Cliffs formation, Choza Mesa field, Rio Arriba County, N. M., can be described as very fine grained, slightly calcareous, well indurated sandstone. Project Wagon Wheel cores from the Fort Union formation, Pinedale field, Sublette County, Wyo., can be described as very fine grained, slightly calcareous, very well indurated sandstone.

Underground reservoirs are under considerable compressive stress as a result of the weight of overlying rocks (offset somewhat by internal-fluid pressure). The resultant net confining pressure or effective overburden pressure is referred to in this report simply as overburden pressure. The resulting effects on the physical properties of the reservoir rock have been studied.¹⁻⁵ Overburden pressure causes only a small decrease in porosity, which can usually be ignored.⁵ This was confirmed for Project Gasbuggy and Project Wagon Wheel cores. A commercial laboratory found that the porosity of these cores is reduced by about 5

percent of the original porosity. The effect of overburden pressure on permeability, however, is appreciable and varies considerably for different reservoir rocks,^{1,2} causing greater reductions in permeability for low-permeability rocks.^{2,3} The effect of overburden pressure on relative permeability has been found to be small⁴ or nonexistent.⁵

This report presents material that confirms and extends previous research findings on the effect that overburden pressure has upon the permeability of dry cores. Also presented are the results of research on the relative gas permeability of low-permeability cores under overburden pressure.

Apparatus and Procedure

Cylindrical cores 2.0 to 7.5 cm long and 2.5 cm in diameter were cut parallel to the bedding plane. After the cores were dried overnight in a vacuum oven (4.5 psia, 70°C), the gas (N₂) permeability of each core was measured in a Hassler cell. An external pressure of 100 psi over the inlet pressure was used to maintain a good seal between the rubber sleeve and the core.⁶ Permeability was measured at inlet pressures of 45, 60, and 100 psia, with atmospheric pressure at the outlet. A bubble tube and timer were used to measure gas flow rate. Initial permeability (k_i) then was calculated by the Klinkenberg technique to correct for the effect of gas slippage. All other permeabilities reported here were calculated by this method.

In the same manner, permeability was measured at

Research conducted to determine the potential of nuclear explosions to stimulate gas production verifies that the gas permeability of tight sandstone cores is markedly decreased with increasing overburden pressure. Water saturation also reduces the gas permeability by a large amount. The relative permeability, however, does not change significantly with overburden pressure.

increasing external pressures of about 500, 1,000, 2,000, 3,000, 4,000, 5,000, and 6,000 psi. External pressures actually were somewhat higher to compensate for internal pressure. The core and stainless steel end pieces were placed in a rubber sleeve (piece of bicycle innertube) 0.1 cm thick. Rubber cement was used to seal the stainless steel end pieces to the rubber sleeve. Shrinkable plastic tubing proved unsatisfactory because high pressure was required to seal the core. The jacketed core was mounted in a high-pressure cell with distilled water as the external fluid.

Cores used in relative permeability studies were first subjected to high external pressure and then allowed to recover their initial permeability. Bulk volume, dry weight, and porosity were measured by conventional gas-expansion techniques. Cores then were subjected to a vacuum (0.3 psia) for 2 hours, immersed in water, and allowed to stand under a vacuum overnight. The cores were weighed and again subjected to vacuum overnight and weighed again to assure complete saturation. Most of the cores were completely saturated after one night. Porosity values calculated on the basis of water saturation are in good agreement with those measured by conventional gas-expansion techniques.

Water in the core was allowed to evaporate at atmospheric conditions to a saturation of about 70 percent and the core was placed in the holder for 2 hours under external pressure (100 psi above inlet) only so the water saturation was uniform. Gas permeability then was measured at three inlet pressures between 30 and 100 psia with atmospheric pressure at the outlet. This procedure was repeated for decreasing water saturations at the same external pressure. After the permeability was measured the core was weighed to determine if any water was lost. In all cases the amount lost was negligible. After the core was dried in a vacuum oven, the gas permeability at this external pressure was measured. The procedure was repeated for external pressures of 3,000 and 6,000 psi.

Results and Discussion

Effect of Overburden Pressure on Permeability

Core number, length, porosity, and initial permeability of the cores used in this research are shown in Table 1. The core number refers to the depth in feet at which the core was obtained. Typical plots of the effect of simulated overburden pressure on Gasbuggy cores are shown in Fig. 1. The permeability is decreased by about 75 percent at an overburden pressure of 3,000 psi and by 90 percent at 6,000 psi. The hydrostatic loading used in these experiments does not reproduce subsurface conditions exactly; in an actual reservoir the horizontal component of stress is usually less than the vertical component. Since the actual loading is not known, this method probably is as realistic as any other. Cores that contain microfractures are affected to a greater extent, as shown in Fig. 2. In these cores the permeability is decreased by about 95 percent at a simulated overburden pressure of 3,000 psi, with most of the reduction occurring below 2,000 psi.

The data shown in Table 1 and Figs. 1 and 2 were obtained by subjecting the core to successive incre-

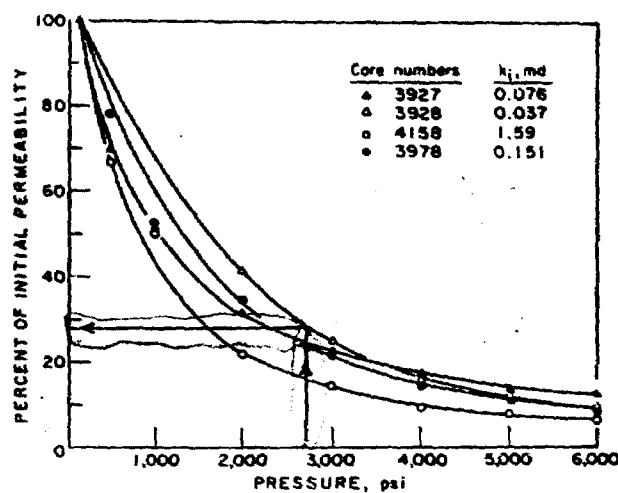


Fig. 1—Effect of overburden pressure on gas permeability of Gasbuggy cores.

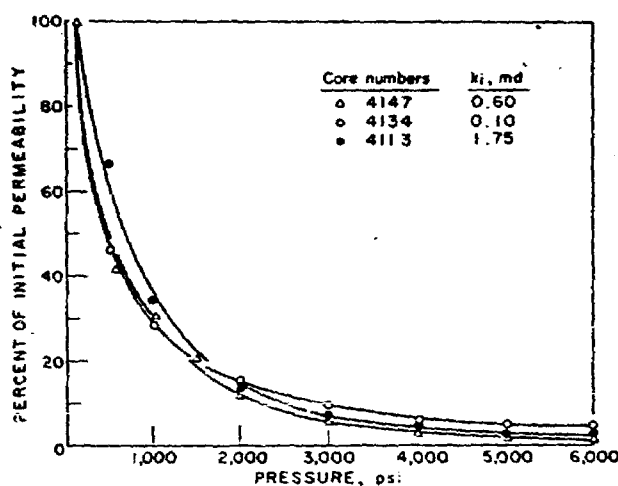


Fig. 2—Effect of overburden pressure on gas permeability of fractured Gasbuggy cores.

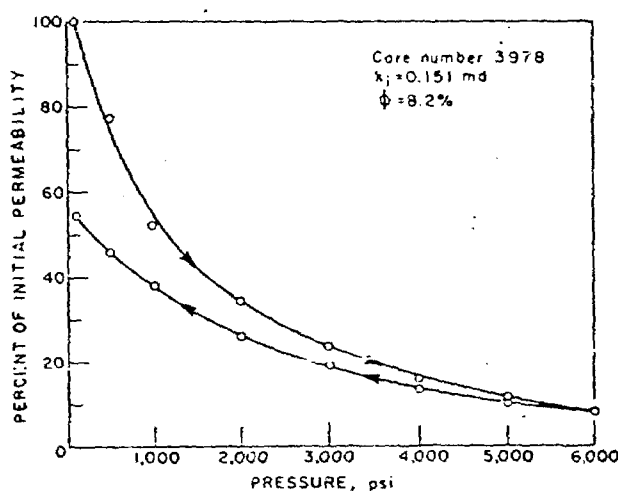


Fig. 3—Hysteresis effect at decreasing confining pressures.

TABLE 1—EFFECT OF OVERBURDEN PRESSURE ON GAS PERMEABILITY

Effective Overburden Pressure (psi):				500	1,000	2,000	3,000	4,000	5,000	6,000
Core Number*	Length (cm)	Porosity (percent)	k,†	Permeability (md)						
Gasbuggy										
3927	2.1	8.1	0.076	0.053	0.040	0.024	0.0175	0.0132	0.0105	0.0095
3928	7.5	8.3	0.037	0.031	0.024	0.015	0.0093	0.0059	0.0046	0.0035
3978	2.1	8.2	0.151	0.118	0.078	0.052	0.036	0.024	0.0175	0.0132
4113**	2.1	10.1	1.75	1.16	0.602	0.252	0.113	0.068	0.042	0.029
4134**	2.1	11.6	0.10	0.046	0.029	0.0153	0.0095	0.0065	0.0055	0.0047
4146**	7.5	11.6	2.40	1.73	1.32	0.31	0.14	0.069	0.052	0.022
4147**	7.5	11.3	0.50	0.247	0.181	0.071	0.034	0.0186	0.0118	0.0082
4158	2.1	13.6	1.59	1.06	0.80	0.35	0.225	0.152	0.116	0.100
Wagon Wheel										
8084	3.8	7.7	0.028	0.022	0.020	0.010	0.0070	0.0047	0.0035	0.0030
8122	3.8	11.4	0.071	0.055	0.048	0.034	0.027	0.024	0.021	0.019
8975**	3.8	8.7	0.039	0.029	0.024	0.0114	0.0073	0.0048	0.0032	0.0025
10156	3.8	8.5	0.068	0.067	0.051	0.032	0.025	0.022	0.018	0.016
10990**	3.8	9.0	0.048	0.020	0.0175	0.0080	0.0050	0.0040	0.0025	0.0019

*Number denotes depth in feet.

**Slightly fractured.

†Initial permeability.

mental increases in external pressure. The core was assumed to be in equilibrium at each pressure when permeability measurements remained constant for 15 minutes, which required between 1 and 2 hours. A period of 30 minutes to an hour was required to attain equilibrium when the inlet pressure was changed. Consequently, each external pressure was maintained for a minimum of 2 hours.

The effect of decreasing external pressure was determined on a few cores, and typical results are shown in Fig. 3. Other researchers^{2,3} have observed and shown that this hysteresis is mainly dependent on the stress history of the core. Cores generally recover their original permeability after 3 to 6 weeks at atmospheric conditions. This time could be shortened by storing the core in an oven at 70°C.

The effect of overburden pressure on the permeability of cores from Project Wagon Wheel is similar to that on cores from Project Gasbuggy, and typical results are shown in Fig. 6. The permeability is decreased to about 30 percent of initial permeability at an overburden pressure of 3,000 psi and to 20 percent at 6,000.

A study of the data in Table 1 indicates that the original porosity of the core and the reduction in permeability caused by overburden pressure are not related. Pore structure (fractures to uniform pores) is probably the governing factor.

Water Saturation Effects

The data in Table 2 show that the permeability decreased with increasing water saturation. The values at 20-, 40-, and 60-percent water saturation were obtained from individual relative-permeability curves for Gasbuggy and Wagon Wheel cores. Relative-permeability curves for three cores from Project Gasbuggy are shown in Fig. 4 with the data points for Core 3978. Data points were omitted for the other cores to avoid confusion. This figure shows that al-

though gas permeability is reduced, the relative gas permeability of Gasbuggy cores is not significantly affected by increased overburden pressure. This conclusion is in agreement with the results of others.^{4,5}

Extremely low values of permeability that resulted from water saturation and overburden pressure required that either long flow times or high inlet pressures (high differential across the core) be used. Since a high inlet pressure increases the end effects by changing the distribution of water in the core, long flow times were required. Although end-effect problems were encountered with the short cores (Cores 3978 and 4158), the permeability of these cores was

TABLE 2—EFFECT OF OVERBURDEN PRESSURE AND WATER SATURATION ON GAS PERMEABILITY

Water Saturation (percent):		0	20	40	60
Core Number	Pressure (psi)	Permeability (md)			
Gasbuggy					
3927	100	0.115	0.099	0.041	0.0023
3927	3,000	0.026	0.023	0.009	0.0005
3927	6,000	0.012	0.010	0.003	0.0002
3978	100	0.112	0.080	0.034	0.011
3978	3,000	0.036	0.026	0.011	0.004
3978	6,000	0.013	0.009	0.004	0.0013
4158	100	0.447	0.335	0.156	0.045
4158	3,000	0.075	0.056	0.026	0.0074
4158	6,000	0.027	0.020	0.010	0.0026
Wagon Wheel					
8084	100	0.038	0.030	0.014	0.0042
8084	3,000	0.012	0.0096	0.0043	0.0013
8084	6,000	0.0070	0.0056	0.0025	0.0008
8122	100	0.074	0.054	0.017	0.006
8122	3,000	0.027	0.020	0.008	0.002
8122	6,000	0.020	0.015	0.006	0.002
10156	100	0.100	0.074	0.029	0.003
10156	3,000	0.028	0.020	0.008	0.0008
10156	6,000	0.017	0.013	0.005	0.0005

high enough to yield reasonable results. Permeability measurements for Core 4161 (7.5 cm long, 0.053 md) required more than 2 hours per reading. These extremely long flow times can cause errors.

End effects, long flow times, and changes in permeability due to water saturation tend to decrease the accuracy of permeability measurements, especially at the higher water saturations.

The initial permeability of many of the dry cores used in this research was not reproducible following saturation and drying. The changes probably were caused by solution of material in the pores and by particle movement. These caused both increases and decreases in permeability. The variation, although sometimes large, usually was less than 5 percent; however, we feel that the relative permeability curves are essentially correct. To eliminate the effects of solution and particle movement, the permeability of the dry core following saturation, rather than the permeability initially measured, was used in calculating relative permeability.

A composite of the relative permeability curves for Gasbuggy cores is shown in Fig. 5. These curves are representative of permeabilities encountered in this formation. At a water saturation of 50 percent, the relative permeability of the cores ranges from 15 to 20 percent and is not affected by overburden pressure.

Similar results were obtained on cores from Project Wagon Wheel, as shown in Table 2 and Fig. 6 with data points for Core 8122. These cores were cut to a length of 3.8 cm to alleviate some of the long flow time and end-effect difficulties encountered with Gasbuggy cores. These curves are representative of the permeabilities encountered in the formation. At a water saturation of 50 percent, the relative permeability of these cores ranges from 12 to 21 percent. The data in these figures show, as do the data from Gasbuggy cores, that relative gas permeability is not significantly affected by increased overburden pressure.

Correlation with Nuclear Stimulation Projects

Many of the basin areas of the Rocky Mountain region consist of thick, low-permeability sandstones containing large quantities of natural gas. This type of reservoir has been the object of the AEC's Plowshare Program experiments, Projects Gasbuggy and Rulison, and proposed Projects Wagon Wheel, WASP, and Rio Blanco. Because most wells in these reservoirs have not been commercial, only limited reservoir-analysis and production-test data are available. Reservoir analysis is most difficult because low permeability requires long-term testing. Also, it is difficult to determine permeability and net pay from these tests. Knowledge of the gas permeability is necessary in predicting gas recovery, and because it is not economical to define the characteristics of different strata by well test, it is desirable to be able to relate laboratory-measured permeability to the true in-situ permeability.

Conventional analysis by a commercial laboratory (confirmed in our laboratory) of about 200 Gasbuggy cores gave an average initial gas permeability of 0.16 md on dry cores and an average water saturation of 48 percent. The effective overburden pressure of this

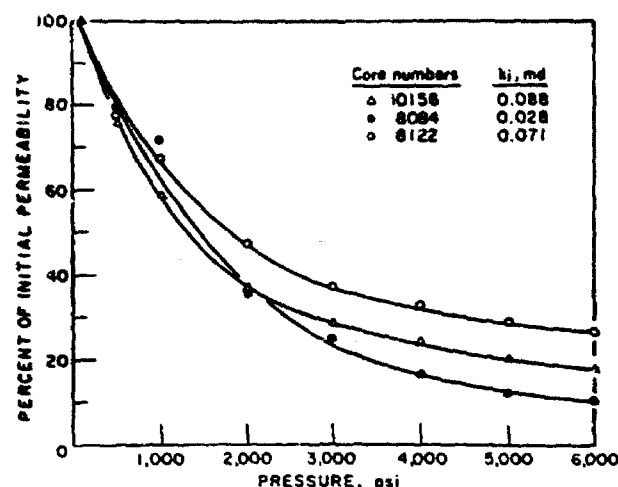


Fig. 4—Effect of overburden pressure on gas permeability of Wagon Wheel cores.

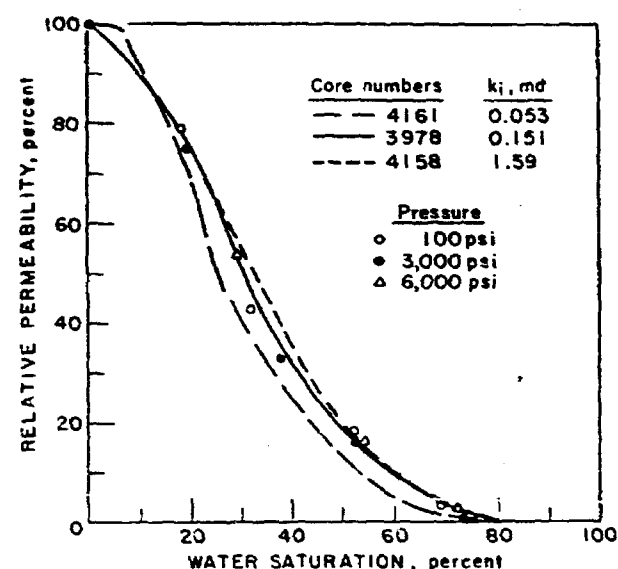


Fig. 5—Relative gas permeability of Gasbuggy cores.

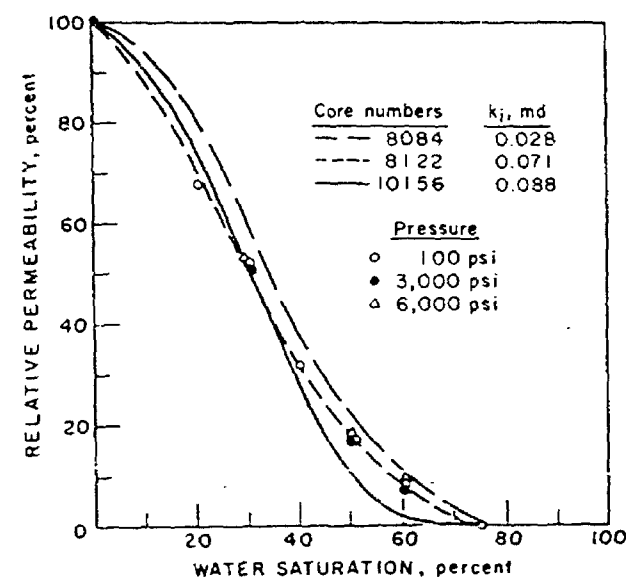


Fig. 6—Relative gas permeability of Wagon Wheel cores.

reservoir is about 3,000 psi. From Fig. 1, the reduction factor resulting from the overburden pressure is 0.25, and the reduction factor for a water saturation of 48 percent (Fig. 5) is 0.20; thus the total reduction is 5 percent of the initial permeability, or 0.008 md. This value compares favorably with permeability determinations of about 0.01 md from both preshot and postshot flow testing at Gasbuggy. The gas reservoir at Project Rulison is similar to that at Gasbuggy, having an average initial dry permeability of 0.11 md and an average water saturation of 45 percent. Simulated in-situ permeability has not yet been measured in the laboratory on Rulison cores; however, using an effective overburden pressure of 5,000 psi and curves of Gasbuggy core data (Figs. 1 and 5), the reduction factor because of overburden pressure would be 0.12 and that for water saturation 0.24. This results in a combined reduction to 3 percent of the initial permeability, or 0.003 md. Postshot production testing at Rulison is not complete, and the only preshot determination of permeability was made from tests of a 32-ft isolated zone that gave an average value of 0.008 md. No cores are available from this zone. Rulison reservoir rock is said to be less compressible than that of Gasbuggy; therefore Gasbuggy pressure-effect data would be expected to indicate a greater reduction for Rulison than actually exists.

The average initial permeability of dry Wagon Wheel cores is 0.068 md, with an average water saturation of 50 percent. An estimated effective overburden pressure of 3,000 psi gives a reduction factor of 0.28 (Fig. 4). Water saturation further reduces permeability by a factor of 0.18 (Fig. 6). Therefore, the total reduction in permeability is to approximately 5 percent of the initial permeability, or 0.0034 md.

Original manuscript received in Society of Petroleum Engineers office June 16, 1971. Revised manuscript received Dec. 20, 1971. Paper (SPE 3634) was presented at SPE 46th Annual Fall Meeting, held in New Orleans, Oct. 3-6, 1971.

This value can be used to predict postshot gas recovery from the proposed Wagon Wheel experiment.

Cores are not yet available from Projects Rio Blanco and WASP.

Conclusions

The gas permeability of tight sandstone cores is markedly decreased with increasing overburden pressure. Most of the decrease takes place at pressures to 3,000 psi. At 3,000 psi, the permeability of unfractured samples ranges from 14 to 37 percent of the initial permeability. In fractured samples, permeability may be reduced to as low as 6 percent of initial permeability.

Water saturation also reduces the gas permeability greatly; however, the relative permeability does not change significantly with overburden pressure.

Permeability calculated from laboratory results are in good agreement with in-situ permeabilities determined from production test data. Although not confirmed, predictions for other projects appear to be reasonable.

References

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2. McLatchie, L. S., Hemstock, R. A. and Young, J. W.: "Effective Compressibility of Reservoir Rocks and Its Effects on Permeability," *Trans., AIME* (1958) 213, 386-388.
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JPT

EXPLANATION OF METHOD USED
TO DETERMINE IN SITU PERMEABILITY
FROM ROUTINE CORE ANALYSIS
BASIN DAKOTA FIELD
SAN JUAN COUNTY, NEW MEXICO

Exhibit No. 8 is a paper entitled "Effect of Overburden Pressure and Water Saturation on Gas Permeability of Tight Sandstone Cores", by Rex D. Thomas and Don C. Ward. This paper presents a method of determining the relationship between routine laboratory and in situ permeability. In this method initial (laboratory) permeability was determined at 100 psi (or less) external pressure. In situ conditions were then simulated by measuring the permeability at various pressures ranging from 500 to 6000 psi. Percent of initial permeability (ratio of permeability at 100 psi to permeability at higher pressures) was then plotted versus pressure. The results of the work is shown in Figure 1, page 121, of the above paper. Using Core No. 3928, which has permeability very near the average of the five test wells in this application, and a bottomhole pressure of 2650 psi, the factor necessary to correct laboratory permeability to in situ permeability is determined to 0.28.

The authors used cores from the Pictured Cliffs formation in a well in Rio Arriba County, New Mexico. This well is located approximately 50 miles southeast of the proposed tight gas area. Cores from the Dakota formation could be expected to provide results very similar to those obtained from the Pictured Cliffs formation.

The water present in the reservoir also causes the in situ permeability to be less than laboratory permeability as is discussed in Exhibit No. 8. No correction, however, has been made for water saturation.

BEFORE EXAMINER NUTTER	
OIL CONSERVATION DIVISION	
SRC	EXHIBIT NO. 9
CASE NO.	

9

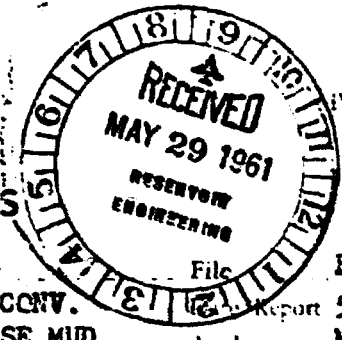
EL PASO NATURAL GAS COMPANY
CASE NO. 8
NE-18-31N-11W
BASIN DAKOTA FIELD
SAN JUAN COUNTY, NEW MEXICO

Depth (feet)	Permeability (md.)
7254-55	.41
55-56	.32
56-57	.11
57-58	.02
58-59	.03
59-60	.12
60-61	.02
61-62	.07
7338-39	.09
39-40	.12
40-41	.04
41-42	.04
42-43	.04
43-44	.04
44-45	.02
45-46	.06
46-47	.07
47-48	.29
48-49	.03
49-50	.14
50-51	.07
51-52	.04
53-54	.56
54-55	.01
55-56	.24
7364-65	.07
65-66	.05
66-67	.08
67-68	.02
68-69	.52
69-70	.03
70-71	.23
71-72	.02
7390-91	.33
91-92	.03
92-93	.02
93-94	.02
Totals	37 4.42
Average Laboratory	.1195
Average In Situ	.0335

BEFORE EXAMINER NUTTER
OIL CONSERVATION DIVISION
SPC EXHIBIT NO. 10
CASE NO. _____

Mitchell

CORE LABORATORIES, INC.
Petroleum Reservoir Engineering
DALLAS, TEXAS



Page No. 1

CORE ANALYSIS RESULTS

Company **EL PASO NATURAL GAS COMPANY** Formation **GRANEROS** File **RP-3-1441**
Well **CASE # 8** Core Type **DIAMOND CONV.** Report **5/26/61**
Field **BASIN LAKOTA** Drilling Fluid **WATER BASE MUD** Analyst **McCOMAS**
County **SAN JUAN** State **NEW MEX.** Elev **6245 GR** Location **SEC 18 T31N R11W**

Lithological Abbreviations

SAND - SD	DO. ON TO DO.	ANHYDRITE - ANH	SANDY SD	FINE - FN	CRYSTALLINE - CLN	BROWN - BRN	FRACTURED FRAC	SLIGHTLY
SHALE - SH	CHERT - CH	CONGLOMERATE - CONG	SHALY SD	MED. COARSE - MC	GRAIN - GRN	GRAY - GR	LAMINATION - LAM	VERY V.
LIME - LM	GYPSEUM - GYP	FOSSILIFEROUS - FORS	CLAY - CLY	COARSE - CO	GRANULAR - GRNL	... GRV - GRV	STYLOLITIC - STV	WITH W.

SAMPLE NUMBER	DEPTH FEET	PERMEABILITY MILLIDARCY	POROSITY PERCENT	RESIDUAL SATURATION		SAMPLE DESCRIPTION AND REMARKS
				PERCENT PORE	TOTAL	
1	7251-52	0.04	3.8	18.4	57.6	VERTICAL FRACTURE
2	52-53	0.65	3.9	17.9	38.3	" "
3	53-54	0.07	3.9	17.9	46.0	" "

7251-7254 This interval is essentially non-productive.

This report contains confidential information and is to be used only for the purpose for which it was prepared. It is not to be distributed outside the company or its subsidiaries without the express written consent of the company. The company assumes no responsibility for the accuracy or completeness of the data or conclusions herein.

CORE LABORATORIES, INC.
Petroleum Reservoir Engineering
DALLAS, TEXAS



Page No. 2

CORE ANALYSIS RESULTS

Company **EL PASO NATURAL GAS COMPANY** Formation **GRANEROS**
Well **CASE # 8** Core Type **DIAMOND CONV.**
Field **BASIN DAKOTA** Drilling Fluid **WATER BASE MUD** Analysts **MCCOMAS**
County **SAN JUAN** State **NEW MEX.** Elev **6245 GR** Location **SEC 18 T31N R11W**

Lithological Abbreviations

SAMPLE NUMBER	DEPTH FEET	PERMEABILITY MILLIDARCY	POROSITY PER CENT	RESIDUAL SATURATION PER CENT PORE		SAMPLE DESCRIPTION AND REMARKS
				OIL	TOTAL WATER	
4	7254-55	0.41	3.4	20.3	53.0	VERTICAL FRACTURE
5	55-56	0.32	4.4	15.9	50.0	"
6	56-57	0.11	3.2	15.6	63.6	"
7	57-58	0.02	3.9	17.9	64.1	"
8	58-59	0.03	3.8	13.1	65.8	"
9	59-60	0.12	3.6	5.6	75.0	"
10	60-61	0.02	3.7	5.4	73.4	"
11	61-62	0.07	3.9	0.0	74.5	"
12	62-63	0.04	4.2	4.8	83.4	"
13	63-64	0.04	4.8	10.4	79.3	"
14	64-65	0.01	3.5	5.7	83.0	"
15	65-66	0.03	3.7	0.0	89.1	"
16	66-67	0.01	3.8	13.1	65.9	"
17	67-68	0.04	4.4	11.4	79.6	"
18	68-69	0.01	4.0	17.5	60.1	"
19	69-70	0.07	3.4	14.7	70.6	"
20	70-71	0.01	3.8	18.4	63.2	"
21	71-72	0.05	5.5	12.7	41.9	"
22	72-73	0.01	4.8	14.5	50.0	"
23	73-74	0.10	4.9	10.2	67.4	"
24	74-75	0.01	5.1	13.7	56.9	"
25	75-76	0.05	5.3	13.2	66.1	"

7254-7276 This interval is essentially non-productive.

inter

CORE LABORATORIES, INC.
Petroleum Reservoir Engineering
DALLAS, TEXAS



CORE ANALYSIS RESULTS

Company **EL PASO NATURAL GAS COMPANY** Formation **DAKOTA**
Well **CASE # 8** Core Type **DIAMOND CONV.**
Field **BASIN DAKOTA** Drilling Fluid **WATER BASE MUD** Analyst **McCOMAS**
County **SAN JUAN** State **NEW MEX.** Log **6245 GR** Location **SEC 18 T31N R11W**

Lithological Abbreviations

SAMPLE NUMBER	DEPTH FEET	PERMEABILITY MILLIDARCY	POROSITY PERCENT	RESIDUAL SATURATION PER CENT PORE		SAMPLE DESCRIPTION AND REMARKS
				OIL	TOTAL WATER	
26	7335-36	0.05	2.8	0.0	85.9	VERTICAL FRACTURE
27	36-37	0.04	2.3	0.0	74.1	"
28	37-38	0.05	2.7	0.0	74.1	"
29	38-39	0.09	3.3	6.1	60.6	"
30	39-40	0.12	3.7	5.4	78.1	"
31	40-41	0.04	2.8	0.0	71.6	"
32	41-42	0.04	1.9	0.0	89.5	"
33	42-43	0.04	4.0	17.5	59.8	"
34	43-44	0.04	2.8	0.0	71.6	"
35	44-45	0.02	2.5	0.0	64.1	"
36	45-46	0.06	4.2	0.0	59.4	"
37	46-47	0.07	4.8	0.0	45.7	"
38	47-48	0.29	5.0	4.0	40.0	"
39	48-49	0.03	4.7	0.0	25.4	"
40	49-50	0.14	7.8✓	0.0	20.4	"
41	50-51	0.07	7.4✓	0.0	24.3	"
42	51-52	0.04	2.2	0.0	77.4	"

7335-7345 This interval is essentially non-productive.

7345-7351 This interval is capable of producing gas, the average characteristics are: Porosity (5.7% average) Total Water saturation (35.8% average), Residual Oil Saturation (0.7% average) and Permeability (0.11 md./ft. average). The fractures in this interval are open and will enhance the permeability quite a bit.

7351-7352 This one foot interval is essentially non-productive.

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Petroleum Research Engineers
DALLAS TEXAS



CORE ANALYSIS RESULTS

Company EL PASO NATURAL GAS COMPANY Formation DAKOTA
Well CASE # 8 Core Type DIAMOND CONV.
Field BASIN DAKOTA Drilling Fluid WATER BASE MUD
County SAN JUAN State NEW MEXICO 6245 GR Location SIC 18 T31N R11W

5/30/61
McCORMIS

Lithological Abbreviations

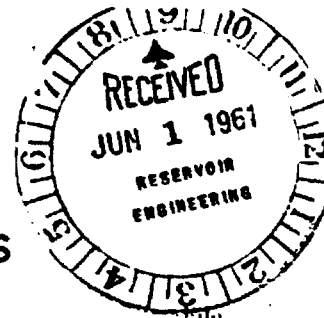
SAMPLE NUMBER	DEPTH FEET	PERMEABILITY MILLIDARREYS	POROSITY PERCENT	RESIDUAL SATURATION PER CENT PORE		SAMPLE TENSILE STRENGTH AND REMARKS
				OIL	TOTAL WATER	
43	7353-54	0.56	1.4	0.0	42.9	VERTICAL FRACTURE
44	54-55	0.01	1.1	0.0	36.3	" "
45	55-56	0.24	2.0	0.0	65.0	" "
46	7363-64	0.02	4.5	0.0	40.0	" "
47	64-65	0.07	6.9	0.0	20.0	" "

7353-7356 This interval is essentially non-productive from the matrix rock. It is possible that the fractures could contribute gas.

7363-7365 This two foot interval is capable of producing a low capacity gas, with most of the gas coming from the fractures.

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DALLAS, TEXAS



Page No. 5

CORE ANALYSIS RESULTS

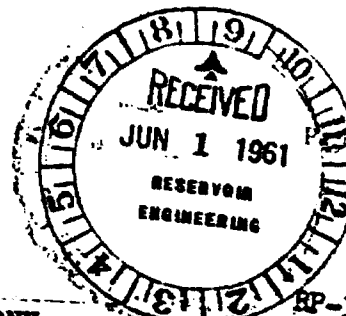
Company **EL PASO NATURAL GAS COMPANY** Formation **DAKOTA** File **RP-3-1441**
Well **CASE # 8** Core Type **DIAMOND CONV.** Date Report **5/31/61**
Field **BASIN DAKOTA** Drilling Fluid **WATER BASE MUD** Analysis **McCOMAS**
County **SAN JUAN** State **NEW MEX.** No. **6245 GR** Location **SEC 18 T31N R11W**

Lithological Abbreviations

SAMPLE NUMBER	DEPTH FEET	PERMEABILITY MILLIDARCY	POROSITY PER CENT	RESIDUAL SATURATION		SAMPLE DESCRIPTION AND REMARKS
				OIL	TOTAL WATER	
48	7365-66	0.05	2.7	0.0	74.0	VERTICAL FRACTURE
49	66-67	0.08	3.9	0.0	51.2	"
50	67-68	0.02	2.2	0.0	95.5	"
51	68-69	0.52	2.2	0.0	63.6	"
52	69-70	0.03	2.7	0.0	74.0	"
53	70-71	0.23	2.6	0.0	96.0	"
54	71-72	0.02	2.6	0.0	96.0	"

7365-7372 This interval is essentially non-productive.

CORE LABORATORIES, INC.
Petroleum Reservoir Engineering
DALLAS, TEXAS



No. 6

CORE ANALYSIS RESULTS

Company **EL PASO NATURAL GAS COMPANY** Formation **DAKOTA**
Well **CASE # 8** Core Type **DIAMOND CONV.**
Field **BASIN DAKOTA** Drilling Fluid **WATER BASE MUD** Date Report **5/31/61**
County **SAN JUAN** State **NEW MEX.** Elev **624' GR** Location **SEC 18 T31N R11W** Analysts **MCCOMAS**

Lithological Abbreviations

SAMPLE NUMBER	DEPTH FEET	PERMEABILITY MILLIDARREYS	POROSITY PER CENT	RESIDUAL SATURATION PER CENT PORE		SAMPLE DESCRIPTION AND REMARKS
				OIL	TOTAL WATER	
55	7375-76	0.17	3.0	0.0	50.0	VERTICAL FRACTURE
56	76-77	0.07	2.0	0.0	65.0	
57	7383-84	0.07	6.2	0.0	33.9	"
58	84-85	0.34	9.4	0.0	28.8	
59	85-86	0.07	6.7	0.0	35.8	"
60	86-87	0.12	3.5	0.0	34.4	
61	87-88	0.02	3.6	0.0	69.5	"
62	7390-91	0.33	2.4	0.0	87.4	
63	91-92	0.03	1.8	0.0	72.2	"
64	92-93	0.02	3.5	0.0	54.4	
65	93-94	0.02	3.5	0.0	57.1	"
66	94-95	0.15	3.7	0.0	45.9	
67	95-96	0.02	2.1	0.0	71.3	"
68	96-97	0.04	2.5	0.0	67.9	
69	97-97.5	0.02	1.4	0.0	64.1	"

7375-7377 This interval is essentially non-productive.

7383-7388 This interval is capable of producing gas, primarily from the fractures. The average characteristics are: Porosity (5.8% average) Total Water saturation (40.4% average) Residual Oil saturation (0.0% average) and Permeability (0.12 md./ft average)

7390-7397.5 This interval is essentially non-productive.

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Petrolicum Reservoir Engineering
DALLAS, TEXAS

CORE ANALYSIS RESULTS



Company EL PASO NATURAL GAS COMPANY Formation DAKOTA File BP-3-1441
Well CASE # 8 Core Type DIAMOND CORE Report 6/1/61
Field BASIN DAKOTA Drilling Fluid WATER BASE MUD Analysts McCOMBS
County SAN JUAN State NEW MEX. Elev. 6245 GR Location SEC 18 T31N R11W

Lithological Abbreviations

SAND - SD	DOLOMITE - DL	ANHYDRITE - ANHY	SANDY - SV	FINE - FN	CRYSTALLINE - CLN	BROWN - BRN	FRACTURED - FRAC	SLIGHTLY - SLT
SHALE - SH	CHERT - CH	CONGLOMERATE - CONG	SHALY - SHY	MEDIUM - MFD	GRAIN - GRN	GRAY - GR	LAMINATION - LAM	VERY - V
LIME - LM	GYPSEUM - GYP	FOSSILIFEROUS - FOS	MUD - MUD	COARSE - CSE	GRANULAR - GRNL	UGGY - UGY	STYLOLITIC - STY	WITH - W

SAMPLE NUMBER	DEPTH FEET	PERMEABILITY MILLIDARCY	POROSITY PER CENT	RESIDUAL SATURATION PER CENT PORE		SAMPLE DESCRIPTION AND REMARKS
				OIL	TOTAL WATER	
70	7122-23	0.01	1.8	0.0	94.6	VERTICAL FRACTURE
71	23-24	0.01	0.6	0.0	66.6	" "
72	24-25	0.01	2.3	0.0	95.6	" "
73	25-26	0.01	1.6	0.0	81.2	" "
74	26-27	0.01	1.9	0.0	89.5	" "

7122-7127 This interval is essentially non-productive.

These analyses were made for information only and are not intended to be used for legal or other purposes. The analyses were made for the purpose of providing information to the client and are not intended to be used for legal or other purposes. The analyses were made for the purpose of providing information to the client and are not intended to be used for legal or other purposes.

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~~3-1443~~

6/2/61

McCombs 20

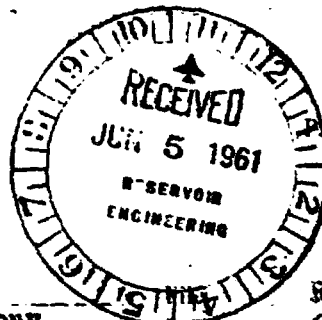
7459 24

These analyses provide some evidence that the combination of a top-down and lateral, such as the one that we have outlined here, where exclusive and contained operations are used to build the hierarchical structure of the network, and the combination of the distributed and the global, where all elements are simultaneously updated, is a promising way to represent and learn the structure of the world. It is important to note that the lack of any evidence of interactions between the two types of operations is probably due to any of a number of methodological issues, such as the lack of a formal model of the network.

CA-20

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Petroleum Reservoir Engineering
DALLAS, TEXAS



Page No. 9

CORE ANALYSIS RESULTS

Company EL PASO NATURAL GAS COMPANY Formation DAKOTA
Well CASE # 8 Core Type DIAMOND CONV.
Field BASIN DAKOTA Drilling Fluid WATER BASE MUD
County SAN JUAN State NEW MEX. Log 6245 GR Location SEC 18 T31N R11W
Date Report 5/2/61
Analyst McCOMAS

Lithological Abbreviations

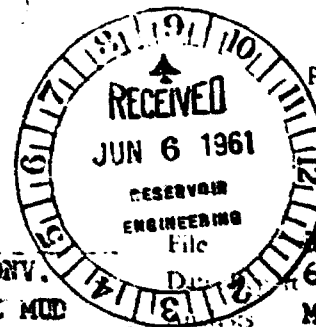
SAMPLE NUMBER	DEPTH FEET	PERMEABILITY MILLIDARCY	POROSITY PER CENT	RESIDUAL SATURATION PER CENT PORE		SAMPLE DESCRIPTION AND REMARKS
				OIL	TOTAL WATER	
78	7462-63	0.03	6.0	0.0	71.8	VERTICAL FRACTURE
79	63-64	0.03	3.5	0.0	74.0	" "
80	64-65	0.02	2.4	0.0	91.6	" "
81	65-66	0.80	5.4	0.0	68.5	" "
82	66-67	0.69	4.0	0.0	10.0	" "

7462-7467 This interval is essentially non-productive. It is possible that continuation of this interval will be low-capacity water productive.

These analyses and interpretations are based on the information and data furnished by the client to whom, and for whom, exclusive and confidential use of this report is made. The analyses and interpretations represent the best knowledge of the laboratory and are subject to change without notice. The analyses and interpretations are not to be used for any other purpose, and the results are not to be used for any other purpose, except as to the productivity, proper operation, and maintenance of the well.

CA-20

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Petroleum Reservoir Engineering
DALLAS, TEXAS



Page No. 10

CORE ANALYSIS RESULTS

Company **EL PASO NATURAL GAS COMPANY** Formation **DAKOTA**
Well **CASE # 8** Core Type **DIAMOND CONV.**
Field **BALDIE DAKOTA** Drilling Fluid **WATER BASE MUD**
County **SAN JUAN** State **NEW MEXICO** Loc. **6245 GR** Location **SEC 18 T31N R11W**
Date **6/4/61** By **MCCOMAS**

Lithological Abbreviations

SAMPLE NUMBER	DEPTH FEET	PERMEABILITY MILLIDARCYS	POROSITY PER CENT	RESIDUAL SATURATION PER CENT PORE		SAMPLE DESCRIPTION AND REMARKS
				OIL	TOTAL WATER	
83	7473-74	0.03	2.7	0.0	62.7	
84	74-75	0.07	4.6	0.0	34.6	
85	75-76	0.30	5.6	0.0	28.5	VERTICAL FRACTURE
86	76-77	0.13	2.5	0.0	72.0	" "
87	77-78	0.10	4.6	0.0	26.0	
88	78-79	0.28	5.0	0.0	39.8	
89	79-80	0.22	6.0	0.0	26.6	
90	80-81	0.39	5.4	0.0	25.8	VERTICAL FRACTURE
91	81-82	22	6.7	0.0	23.8	" "
92	82-83	11	15.0	0.0	75.5	
93	83-84	11	14.4	0.0	81.5	

7473-7482 Although this interval has water saturations normally associated with gas production, it is in permeable contact with interval from 7482 to 7484, which is definitely water productive. Any completion in the interval from 7473 to 7482 would probably result in water.

This analysis report or interpretation is based on observations and materials supplied by the client to whom, and for whose exclusive and confidential use, this report is made. The interpretations or opinions expressed represent the best judgment of Core Laboratories, Inc., and are not to be construed as a warranty or representation, as to the productivity, proper operation, or profitability of any well, gas or other mineral well or sand in connection with which such report is used or relied upon.

22

A circular black and white stamp. The outer ring contains numbers 1 through 12, with the 12 o'clock position at the top. Inside the ring, the word "RECEIVED" is at the top, followed by the date "JUN 6 1961". At the bottom, the words "RESERVOIR" and "ENGINEERING" are stacked. A small triangle points upwards at the 12 o'clock position.

No. 11

CORE ANALYSIS RESULTS

Company	EL PASO NATURAL GAS COMPANY	Formation	DAKOTA	File	RP-3-1441
Well	CASE # 8	Core Type	DIAMOND CONV.	Date Report	6/5/61
Field	BASIN DAKOTA	Drilling Fluid	WATER BASE MUD	Analysts	McCOMAS
Country	SAN JUAN	State	NEW MEX.	Elev	6245 GR
		Location	SFC 18 T31N R11W		

Lithological Abbreviations

SAND-ED SHALE-SH LN-2-LN		OLCLITE-DO. CHERT-CH GYPSUM-GYP	AMPHIBITE-AMPH CONGLOMERATE-CONG FOSSILIFEROUS-FOSS	SANDY-SBY SHALY-SHY LN-1-LNY	FINE-FN MEDIUM-MED COARSE-CSE	CRYSTALLINE-XLN GRAIN-GRN GRANULAR-GRNL	BROWN-BRN GRAY-GY VUGGY-VGY	FRACTURED-FRAC LAMINATION-LAM EVOLUTIC-EVY	SLIGHTLY-SL VERY-V/ WITH-W/
SAMPLE NUMBER	DEPTH FEET	PERMEABILITY MILLIDARCY	POROSITY PER CENT	RESIDUAL SATURATION		SAMPLE DESCRIPTION AND REMARKS			
				PER CENT PORE OIL	TOTAL WATER				
94	7489-90	137	14.9	0.0	64.4				
95	90-91	0.52	7.7	0.0	75.4				
96	91-92	0.25	9.1	2.2	82.4				
97	92-93	19	11.2	0.0	61.6				
98	93-94	149	13.5	0.0	69.6				
99	94-95	97	13.7	1.5	71.5				
100	95-96	0.44	14.1	0.0	71.0				
101	96-97	0.32	15.3	1.3	69.2				
102	97-98	0.11	13.8	0.0	75.6				
103	98-99	0.17	15.2	0.0	77.0				
104	99-7500	128	19.1	0.0	66.0				
105	7500-01	99	16.0	0.0	68.1				
106	01-02	152	16.1	1.2	72.6				
107	02-03	201	16.7	1.2	77.4				
108	03-04	88	17.2	0.0	72.6				
109	04-05	167	17.6	0.0	73.0				
110	05-06	4.4	13.5	0.0	69.5				
111	06-07	0.68	9.1	0.0	74.6				
112	07-08	0.01	8.5	0.0	76.5				
113	08-09	0.07	8.9	0.0	72.0				
114	09-10	0.03	5.9	0.0	61.0				
115	10-11	0.38	6.9	0.0	58.0				
116	11-12	0.08	7.0	0.0	68.5				
117	12-13	0.12	7.2	0.0	85.0				

7489-7513 This interval is water productive.

These analyses, and the associated projections, are based on data that are, and generally applied by the client to select, and for which exclusive and confidential are, this report is made. For our calculations, statistical aspects represent the best understanding of Client data sources, but still errors and omissions, especially, from Client data sources, have and may occur, and our analyses, as made, are based on, and made for, the warranty or representation, as to the productivity, proper operation, and maintenance, of the equipment, and the manner of use, and the maintenance, with which such report is used or relied upon.

EL PASO NATURAL GAS COMPANY
MOORE NO. 8
SW-24-32N-12W
BASIN DAKOTA FIELD
SAN JUAN COUNTY, NEW MEXICO

Depth (feet)	Permeability (md.)
7589-90	.01
7591-92	.01
7593-94	.05
7595-96	.01
7597-98	.07
7599-7600	.01
7601-02	.08
7603-04	.01
7605-06	.01
7607-08	.01
7609-10	.02
7611-12	.01
7670-71	.03
71-72	.05
72-73	.48
73-74	.01
74-75	.01
75-76	.07
76-77	.03
78-79	.01
79-80	.09
80-81	.01
81-82	.11
82-83	.17
83-84	.09
84-85	.01
85-86	.02
86-87	.01
87-88	.04
88-89	.01
89-90	.01
90-91	.29
91-92	.07
92-93	.02
93-94	.01
94-95	.01
95-96	.02
96-97	.02
97-98	.12
Totals	39 2.10
Average Laboratory	.0538
Average In-Situ	.0151

BEFORE EXAMINER NUTTER
OIL CONSERVATION DIVISION

SRC EXHIBIT NO. 11
CASE NO. _____

//



CORE LABORATORIES, INC.

Petroleum Reservoir Engineering

COMPANY EL PASO NATURAL GAS COMPANY DATE ON 4/23/61 FILE NO. RP-3-1425
 WELL MOORE # 8 DATE OFF 5/1/61 ENGRS. McCOMAS
 FIELD BASIN-DAKOTA FORMATION AS NOTED ELEV. 6556 GR
 COUNTY SAN JUAN STATE N. MEXICO DRUG. FLD. WATER BASE MUD CORES DIAMOND CONV.
 LOCATION SEC 24 T32N R12W REMARKS SAMPLED BY CLI AT DIRECTION OF CLIENT

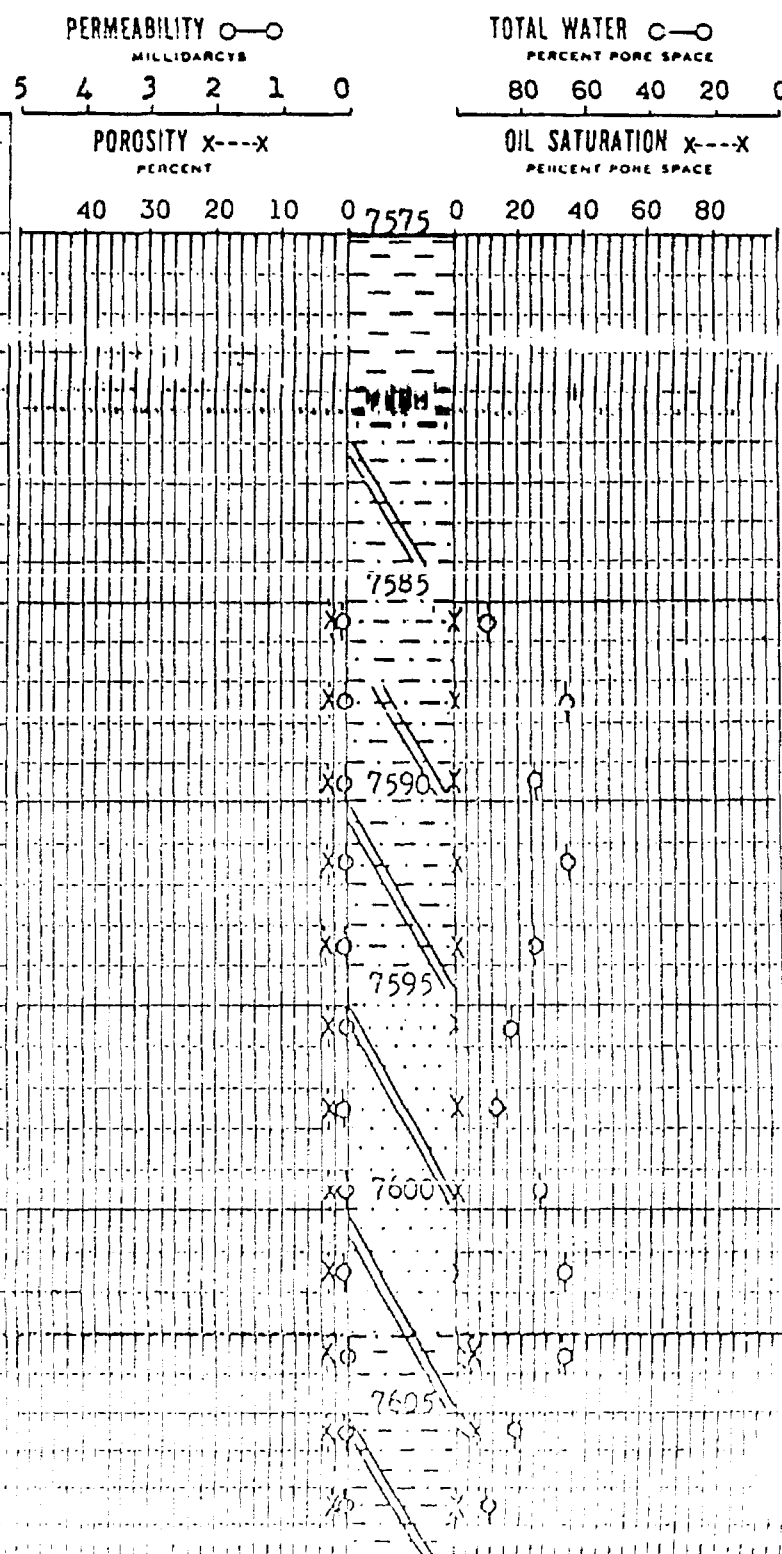
SAND LIMESTONE CONGLOMERATE CHERT
 SHALE DOLOMITE VERTICAL FRACTURE

These analyses, opinions or interpretations are based on observations and material supplied by the client to whom, and for whose exclusive and confidential use, this report is made. The interpretations or opinions expressed represent the best judgment of Core Laboratories, Inc. and its officers and employees, assume no responsibility and make no warranty or representation as to the productivity, proper operation, or profitability of any oil, gas or other mineral well or land in connection with which such report is used or relied upon.

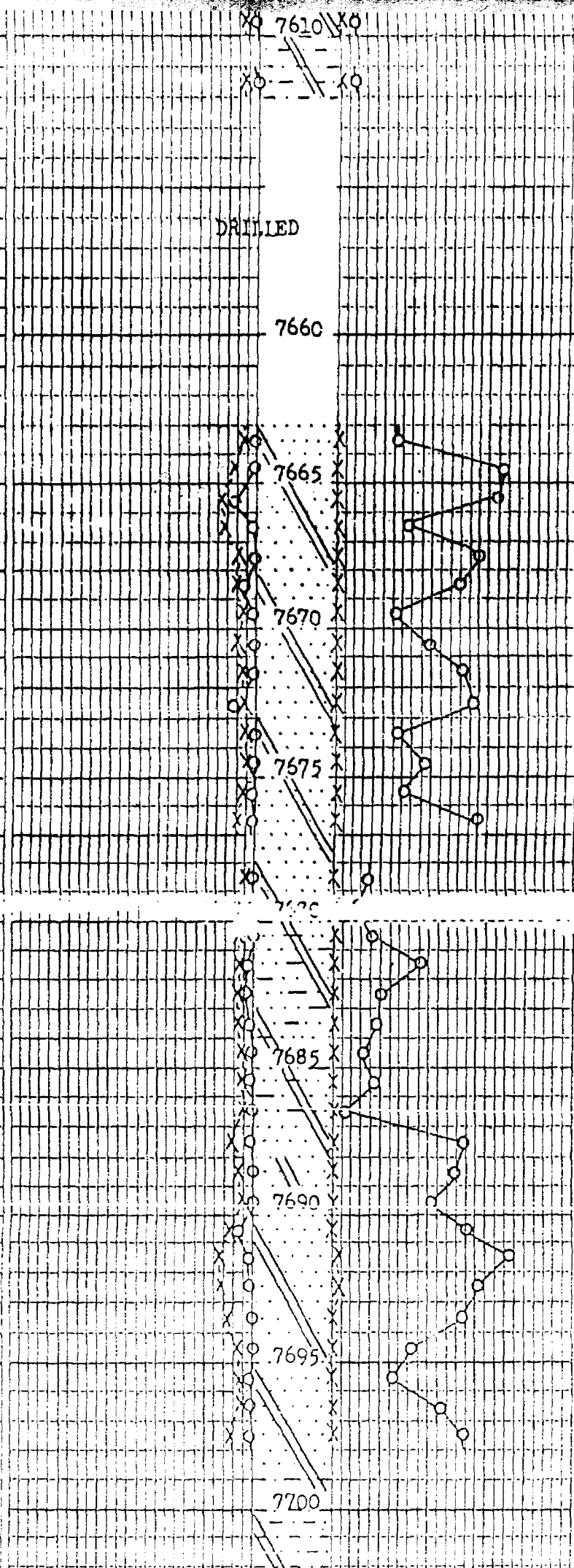
COMPLETION COREGRAPH

TABULAR DATA and INTERPRETATION

SAMPLE NUMBER	DEPTH FEET	PERM. MU.	POROSITY %	RESIDUAL SATURATION % PORE SPACE		# PROD
				OIL	TOTAL WATER	
				GRANEROS		
1	7585-86	0.02	2.5	0.0	88.1	
2	7587-88	<0.01	3.1	0.0	64.7	
3	7589-90	0.01	2.9	0.0	75.9	
4	7591-92	<0.01	3.4	0.0	64.9	
5	7593-94	0.05	3.6	0.0	75.1	
6	7595-96	<0.01	3.4	0.0	82.4	
7	7597-98	0.07	3.1	0.0	87.1	
8	7599-7600	<0.01	3.0	0.0	73.4	
9	7601-02	0.08	3.0	0.0	66.7	
10	7603-04	<0.01	3.3	6.1	66.9	
11	7605-06	0.01	3.3	6.1	81.9	
12	7607-08	<0.01	1.7	0.0	88.4	

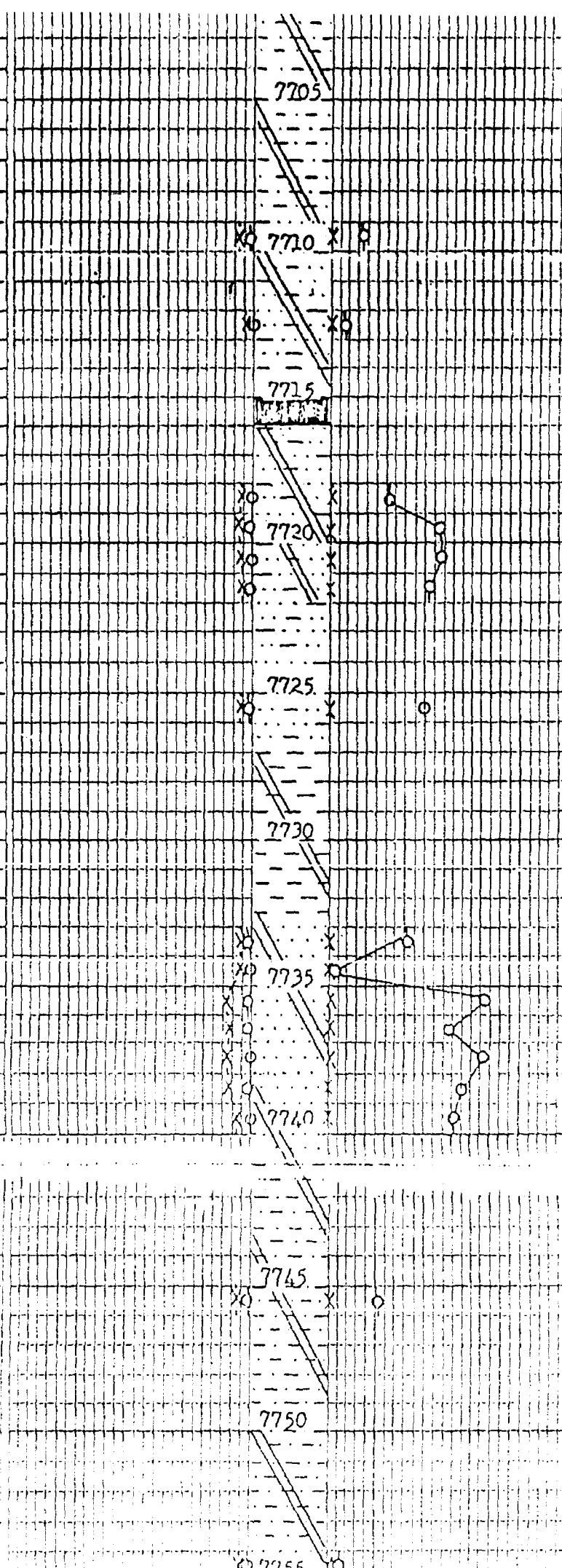


DAKOTA



Petroleum Reservoir Engineering

63	7745-46	40.01	2.4	0.0	79.2
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64	54-55	<0.01	2.0	0.0	79.0
65	55-56	<0.01	2.5	8.0	80.0
66	56-57	<0.01	3.3	6.1	45.5
67	57-58	<0.01	2.9	6.9	55.0

68	7763-64	<0.01	5.2	3.8	92.2
69	64-65	<0.01	2.2	22.5	68.2
70	65-66	<0.01	2.8	17.8	68.1

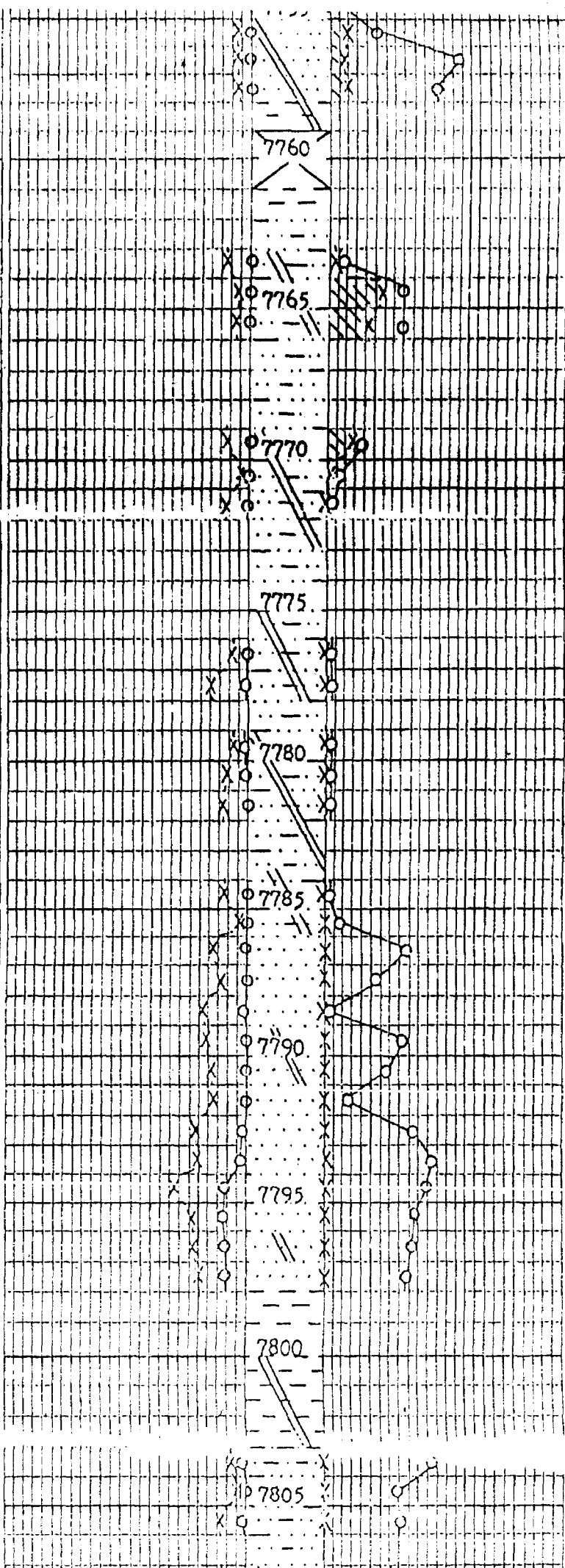
71	7769-70	<0.01	4.8	10.4	85.5
72	70-71	<0.01	1.8	0.0	95.0
73	71-72	0.01	1.2	0.0	97.9

74	7776-77	0.01	3.9	0.0	97.5
75	77-78	0.02	8.0	0.0	97.5

76	7779-80	0.03	3.8	0.0	97.5
77	80-81	0.03	4.5	0.0	97.9
78	81-82	<0.01	4.5	0.0	97.9

79	7784-85	0.01	5.1	0.0	96.0
80	85-86	<0.01	1.4	0.0	93.2
81	86-87	0.02	7.7	0.0	65.0
82	87-88	<0.01	5.3	0.0	78.3
83	88-89	0.05	9.4	0.0	97.6
84	89-90	0.02	8.2	0.0	67.1
85	90-91	0.01	7.6	0.0	72.4
86	91-92	0.01	7.3	0.0	89.0
87	92-93	0.10	11.5	0.0	62.6
88	93-94	0.11	10.6	1.9	54.0
89	94-95	0.11	15.3	0.0	58.2
90	95-96	0.46	11.8	0.0	60.1
91	96-97	0.44	11.5	0.0	63.5
92	97-98	0.43	10.0	0.0	65.0

93	7803-04	0.05	2.6	0.0	54.0
94	04-05	<0.01	1.4	0.0	68.5
95	05-06	0.05	5.6	8.9	67.9

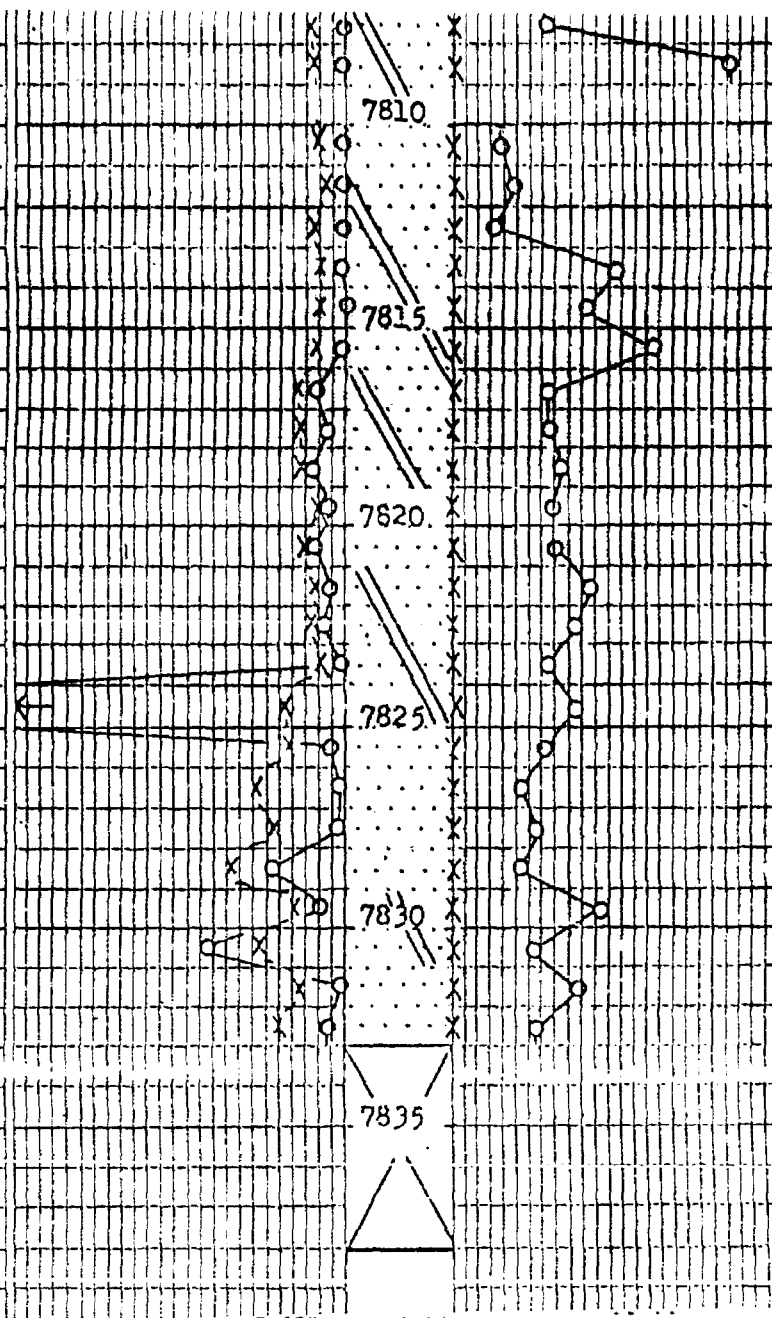




CORE LABORATORIES, INC.

Petroleum Reservoir Engineering

96	7807-08	0.03	5.7	0.0	71.9
97	08-09	0.03	5.2	0.0	15.1
98	7810-11	0.01	4.5	0.0	84.4
99	11-12	0.02	3.1	0.0	81.0
100	12-13	0.02	4.7	0.0	87.3
101	13-14	0.02	4.0	0.0	50.0
102	14-15	0.01	4.0	0.0	59.6
103	15-16	0.02	4.3	0.0	37.1
104	16-17	0.44	7.5	2.7	69.4
105	17-18	0.29	6.9	0.0	69.5
106	18-19	0.52	6.0	0.0	66.6
107	19-20	0.21	3.8	0.0	68.2
108	20-21	0.44	5.0	0.0	68.0
109	21-22	0.23	4.2	0.0	57.0
110	22-23	0.32	5.0	0.0	61.8
111	23-24	0.05	4.0	0.0	70.0
112	24-25	7.7	8.8	0.0	61.3
113	25-26	0.21	8.3	0.0	71.0
114	26-27	0.07	13.9	0.0	79.4
115	27-28	0.12	10.9	0.0	75.2
116	28-29	1.1	17.2	0.0	78.1
117	29-30	0.37	7.9	0.0	54.4
118	30-31	2.1	13.0	0.0	74.6
119	31-32	0.02	6.6	0.0	60.5
120	32-33	0.21	10.0	0.0	74.0



BEFORE EXAMINER NUTTER
OIL CONSERVATION DIVISION
SEC EXHIBIT NO. 12
CASE NO. _____

PERMEABILITY, GAS AND CRUDE PRODUCTION DATA
BASIN DAKOTA FIELD
SAN JUAN COUNTY, NEW MEXICO

Operator/Lease	Well No.	Location	Depth	In Situ Gas Permeability (Md.)	Stabilized Production Rate		Crude Production (BPD)	Remarks
					Measured (MCFD)	Calculated at Atmospheric Pressure (MCFD)		
Southland Royalty Co. East	7E	SW-14-31N-12W	7282-7448	.0011	21.6	21.7	0	Permeability calculated from pressure build-up
Southland Royalty Co. Patterson "B" Com.	1E	SW-2-31N-12W	7212-7385	.0877	224.0	224.1	0	Permeability calculated using Darcy's Law
Aztec Oil & Gas Co. Pierce	2	SW-30-31N-10W	6638-7104	.0609	208.0	208.1	0	Permeability calculated using Darcy's Law
(2) El Paso Natural Gas Co. Case	8	NE-18-31N-11W	7254-7406	.0335	--	--	--	Permeability from core data (1) In situ permeability determined to be 28% of permeability from routine core analysis
(2) El Paso Natural Gas Co. Moore	8	SW-24-32N-12W	7589-7800	.0151	--	--	--	Permeability from core data (1) In situ permeability determined to be 28% of permeability from routine core analysis

and Don C. Ward: "Effect of Overburden Pressure and Water Saturation on Gas Permeability of the Cores", Journal of Petroleum Technology, February, 1972, 120-124 (See Exhibit No. 8)

Permeability was not tested.

BEFORE EXAMINER NUTTER
OIL CONSERVATION DIVISION

SRC EXHIBIT NO. **13**

CASE NO. _____

CUMULATIVE PRODUCTION AND ULTIMATE RESERVES
BASIN DAKOTA FIELD
SAN JUAN COUNTY, NEW MEXICO

Operator	Lease	Well No.	Location	Cumulative Production (1-1-80)		Remaining Reserves (1-1-80)		Ultimate Reserves	
				Gas (MCF)	Oil (BBLs)	Gas (MCF)	Oil (BBLs)	Gas (MCF)	Oil (BBLs)
Tenneco	Wilkins	1	NE-24-32N-10W	29,306	0	0	0	29,306	0
Tenneco	Barnes	1	NE-26-32N-11W	261,364	0	0	0	261,364	0
Southland Royalty	Decker	4	SW-10-32N-12W	129,055	456	110,757	0	239,812	456
Southland Royalty	Hubbard	2	SW-11-32N-12W	71,276	177	75,749	0	147,025	177
Southland Royalty	Chamberlain	1	NE-14-32N-12W	47,873	60	0	0	47,873	60
Southland Royalty	Hubbard	3	NE-15-32N-12W	41,700	0	0	0	41,700	0
Southland Royalty	Hubbard	4	SW-15-32N-12W	117,951	1,171	353,699	701	471,650	1,872
Southland Royalty	Culpepper Martin	12	SW-20-32N-12W	68,173	1,062	49,440	635	117,613	1,697
Southland Royalty	Culpepper	15	NE-21-32N-12W	82,784	1,045	53,714	181	136,498	1,226
Southland Royalty	Culpepper Martin	5	SW-22-32N-12W	118,654	2,677	21,889	1,624	140,543	4,301
Tenneco	Moore	1	NW-25-32N-12W	150,109	0	0	0	150,109	0
Tenneco	Hubbard	1	SE-25-32N-12W	430,872	0	118,134	0	549,006	0
Southland Royalty	Decker	2	NE-26-32N-12W	86,930	285	46,571	0	133,501	285
Tenneco	Moore "C"	2	NW-26-32N-12W	384,093	1,284	250,514	0	634,607	1,284
Tenneco	Moore "C"	1	SE-27-32N-12W	500,205	1,803	175,347	0	675,552	1,803
Southland Royalty	Culpepper Martin	4	SW-28-32N-12W	96,795	1,533	188,831	2,182	285,626	3,715
Southland Royalty	Culpepper Martin	13	SW-29-32N-12W	84,312	837	101,373	152	185,685	989
Southland Royalty	Culpepper Martin	10	SW-32-32N-12W	402,396	3,513	352,593	690	754,989	4,203
Southland Royalty	Culpepper Martin	3	SW-33-32N-12W	256,054	1,535	361,586	1,928	617,640	3,463
Southland Royalty	Culpepper Martin	17	SE-33-32N-12W	77,114	591	1,335,936	7,636	1,411,050	8,227
Consolidat	Ripley	1	SW-26-32N-13W	98,297	491	0	0	98,297	491
Benson-Mor	viata	1	SW-30-32N-13W	183,726	0	187,451	0	371,177	0
Benson-Mo	ca	2	NW-30-32N-13W	319,414	0	302,340	0	621,754	0
Consolidat	ion Bros.	1	SE-34-32N-13W	128,755	526	0	0	128,755	526
Consolidat	ya	1	NE-35-32N-13W	39,880	0	18,166	0	58,046	0
Consolidat	ya	1M	SE-35-32N-13W	20,003	759	294,268	8,526	314,271	9,285
Supron	State	1	NE-36-32N-13W	37,720	63	0	0	37,720	63
Consolidat	American State	1	SW-36-32N-13W	158,858	1,538	29,974	290	188,832	1,828
Delht-Taylur	ntic "A"	4	SW-27-31N-10W	432,580	0	0	0	432,580	0
Tenneco	antic	1	NE-34-31N-10W	200,942	0	0	0	200,942	0
Southland Royalty	Trut	2	SW-35-31N-11W	238,504	375	0	0	238,504	375
Totals		31		5,293,695	21,781	4,428,332	24,545	9,722,027	46,326
Average				170,764	702	142,850	792	313,614	1,494

13

0001:1,Y,GAS,5320,10,1981
0002:3.85,3.85,N,7000,N,N
0003:SRC UNNAMED NO. 1
0004:BASIN DAKOTA
0005:SAN JUAN NEW MEXICO
0006:MINIMUM ECONOMICS-103
0007:6,226,0,0,1,1,1
0008:42.76,3.11,50,10.42,7,7,14.11,70,0.146,7,19
0009:100,13.5,0,0,0,8,8,0
0010:HYP,0,300,350,0,125,END
0011:1981.4,6,121,258,1,0,END

BEFORE EXAMINER NUTTER
OIL CONSERVATION DIVISION

SRC EXHIBIT NO. 14
CASE NO. _____

14

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PREPARED BY: MT
FILE: DATA47
DATE: 12-3-80
INITIAL INVESTMENT DATE: 04/01/1980
INITIAL PRODUCTION DATE: 10/01/1981

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YEAR	GROSS PRODUCTION MBBL/YR	NET PRODUCTION MCF/YR	PRICES \$/BBL \$/MCF	OIL	GAS	REVENUES AND TAXES \$	LEASE OPR. EXP. \$	INCOME \$	DEPRECIATION EXP. \$
						TOTAL	P. TAX	D. TAX	NET
1981	0.	15.	0.	13.	42.76 3.11	2.	39.	41.	3.
1982	0.	42.	0.	36.	45.75 3.33	6.	121.	128.	10.
1983	0.	29.	0.	25.	48.96 3.56	5.	90.	95.	8.
1984	0.	23.	0.	20.	50.00 3.81	4.	75.	79.	6.
1985	0.	19.	0.	16.	50.00 4.08	3.	67.	70.	6.
1986	0.	16.	0.	14.	50.00 4.36	3.	61.	64.	5.
1987	0.	14.	0.	12.	50.00 4.67	2.	58.	60.	5.
1988	0.	13.	0.	11.	50.00 4.99	2.	55.	57.	5.
1989	0.	12.	0.	10.	50.00 5.34	2.	54.	56.	4.
1990	0.	11.	0.	9.	50.00 5.72	2.	53.	54.	4.
1991	0.	10.	0.	9.	50.00 6.12	2.	52.	54.	4.
1992	0.	9.	0.	8.	50.00 6.55	2.	52.	53.	4.
1993	0.	9.	0.	7.	50.00 7.00	1.	52.	53.	4.
1994	0.	8.	0.	7.	50.00 7.49	1.	52.	54.	4.
1995	0.	8.	0.	7.	50.00 8.02	1.	53.	54.	4.
S-TOT	1.	237.	1.	205.	48.67 4.57	38.	934.	973.	78.
AFTER	0.	113.	0.	98.	50.00 10.19	19.	1000.	1019.	81.
TOTAL	1.	350.	1.	303.	49.10 6.39	57.	1934.	1991.	159.
PRICE ASSUMPTIONS									
OIL		GAS		PRODUCTION					
INITIAL PRICE:		\$42.76		\$3.11/PRODUCING DEV. WELLS-GROSS/NET:		1 / 1.00			
AVERAGE PRICE:		\$49.10		\$6.39 DRY DEV. WELLS-GROSS/NET:		0 / 0.00			
MAXIMUM PRICE:		\$50.00		\$10.42 INITIAL DAILY PRODUCTION-					
AVG. ESC. TO MAXM.		7.00%		TOTAL NET:		01.BBLS 151.MCF			
				GROSS/WELL:		01.BBLS 174.MCF			
COST ASSUMPTIONS									
INITIAL LOE/WELL/MO:		\$146.		FLAT LIFE:		5.5 YRS			
ESCALATION RATE:		7.00%		PRODUCTION LIFE:		36.9 YRS			
MAXIMUM LOE/WELL/MO:		\$185.		AVG. PRODUCTION DECLINE/YR.:		7.52 %			
PROD. TAX RATE:		8.00%		YIELD (BBLS/MCF):		3.9MAX. 3.9MIN.			
				AVG. WELL DEPTH (FT.):		7000			
DE-REGULATION TAX DATA									
BASE PRICE/BBL.:		\$14.1		TAX RATE:		70.0%			

SOUTHLAND ROYALTY COMPANY

DRILLING ECONOMICS SUMMARY

PREP. BY: MT

FILE: DATA47

DATE: 12-3-80

PROJECT: SRC UNNAMED NO. 1
 BASIN DAKOTA
 SAN JUAN NEW MEXICO
 MINIMUM ECONOMICS-10

Initial Investment Date: 04/01/1981
 Initial Production Date: 10/01/1981

1. NOT DISCOUNTED (BEFORE INCOME TAX)

Net Income Before Capital: \$1739. Risk Cost: \$226. Ratio: 7.7
 Profit After Capital: \$1360. Capital: \$379. Ratio: 3.6

2. RISK PARAMETERS

Trap: 1.00 Reservoir: 1.00 Hydrocarbon: 1.00 Total(R.F.): 1.00

3. OBJECTIVE TEST

Discounted @7% Before Tax Net Income: \$627.
 Adjusted For Risk: \$627.
 CAPITAL: (Risk Cost*(1-R.F.) + R.F.*Disc. Develop. Cost)*1.25: \$474.
 Above Or Below SRC Objective: \$153.

4. PAYOUT (yrs)

Before Tax: 5.05 ✓ After Tax: 5.74

5. AFTER TAX RATE OF RETURN

No Risk: 15.53 ✓ Risk Adjusted: 15.53

6. COST PER EQUIVALENT BBL & MCF

\$7.34/BBL \$1.22/MCF

7. RISK FACTOR SENSITIVITY

RISK FACTOR	RISK ADJUSTED AFTER TAX ROR	ABOVE OR BELOW SRC OBJECTIVE
0.80	13.2	\$66.
0.60	10.5	\$21.-
0.40	7.0	\$108.-
0.20	2.0	\$195.-
0.10	0.1	\$239.-
0.05	0.1	\$261.-
Minimum: 0.95	15.0	\$132.

8. PROJECT DATA:

Total Life (yrs): 36.9
 Flat Life (yrs): 5.5
 W.I. Before/After Payout: 100.000% / 100.000%
 N.I. Before/After Payout: 86.500% / 86.500%
 Revert. Int. Amount (M\$): 0.
 Excise Tax (M\$): 11.
 Net Oil Reserves (MBBLS): 01.
 Net Gas Reserves (MMCF): 303.
 Gross Producing Wells: 1.
 Gross Develop. Dry Holes: 0.
 Depth (ft): 7000

RISK COSTS (M\$) :

Dryhole: 226.
 Acreage: 00.
 Seismic: 00.
 Total: 226.

9. UNIT PRICING (GAS)

Initial/Maximum: \$3.11/ \$10.42

0001:1,Y,GAS,2280,10,1981
0002:3.85,3.85,N,7000,N,N
0003:SRC UNNAMED NO. 1
0004:BASIN DAKOTA
0005:SAN JUAN NEW MEXICO
0006:MINIMUM ECONOMICS-2 X 103
0007:0,226,0,0,1,1,1
0008:42.76,6.22,50,10.42,7,7,14.11,70,0,146,7,19
0009:100,13.5,0,0,0,8,8,0
0010:HYP,0,300,150,0,125,END
0011:1981.4,6,121,258,1,0,END

BEFORE EXAMINER NUTTER
OIL CONSERVATION DIVISION

SRC EXHIBIT NO. 15

CASE NO. _____

15

PROJECT: SRC UNNAMED NO. 1
SAN JUAN NEW MEXICO

SOUTHLAND ROYALTY COMPANY
BEFORE TAX ECONOMICS - DETAIL REPORT
-- BASIN DAKOTA
-- MINIMUM ECONOMICS-2 X 103

PREPARED BY: MT
FILE: DATA48
DATE: 12-3-80
INITIAL INVESTMENT DATE: 04/01/1981
INITIAL PRODUCTION DATE: 10/01/1981

YEAR	GROSS PRODUCTION MBBL/YR MMCF/YR	NET PRODUCTION MBBL/YR MMCF/YR	PRICES \$/BBL \$/MCF	OIL	GAS	REVENUES AND TAXES \$	NET	LEASE OPR. EXP. \$	INCOME \$	DEVELOP EXP. \$
1981	0.	0.	42.76 6.22	1.	35.	36.	3.	0.	32.	31.
1982	0.	0.	45.75 6.66	3.	118.	121.	10.	0.	110.	95.
1983	0.	0.	48.96 7.12	3.	95.	98.	8.	0.	87.	70.
1984	0.	0.	50.00 7.62	2.	83.	85.	7.	0.	77.	55.
1985	0.	0.	50.00 8.15	2.	75.	77.	6.	0.	70.	46.
1986	0.	0.	50.00 8.72	2.	70.	72.	6.	0.	65.	39.
1987	0.	0.	50.00 9.33	1.	67.	68.	5.	0.	62.	34.
1988	0.	0.	50.00 9.99	1.	65.	66.	5.	0.	60.	30.
1989	0.	0.	50.00 10.42	1.	62.	63.	5.	0.	58.	27.
1990	0.	0.	50.00 10.42	1.	57.	58.	5.	0.	53.	22.
1991	0.	0.	50.00 10.42	1.	53.	54.	4.	0.	49.	19.
1992	0.	0.	50.00 10.42	1.	49.	50.	4.	0.	45.	16.
1993	0.	0.	50.00 10.42	1.	46.	47.	4.	0.	43.	14.
1994	0.	0.	50.00 10.42	1.	44.	45.	4.	0.	41.	12.
1995	0.	0.	50.00 10.42	1.	41.	42.	3.	0.	39.	11.
S-TOT	0.	0.	48.84 8.55	21.	960.	981.	78.	0.	896.	865.
AFTER	0.	0.	50.00 10.42	3.	182.	185.	15.	0.	171.	159.
TOTAL	1.	0.	49.00 8.80	24.	1142.	1167.	93.	0.	1067.	1025.

PRICE ASSUMPTIONS
OIL
GAS
PRODUCTION
OWNERSHIP

INITIAL PRICE: \$42.76
AVERAGE PRICE: \$49.00
MAXIMUM PRICE: \$50.00
AVG. ESC. TO MAXM. 7.00%

PRODUCING DEV. WELLS-GROSS/NET: 1 / 1.00
\$8.80 DRY DEV. WELLS-GROSS/NET: 0 / 0.00
\$10.42 INITIAL DAILY PRODUCTION--
TOTAL NET: 00,000 BBL 65,000 MCF
GROSS/WELL: 00,000 BBL 75,000 MCF

COST ASSUMPTIONS
INITIAL LOE/WELL/MO: \$146.
ESCALATION RATE: 7.00%
MAXIMUM LOE/WELL/MO: \$185.
PROD. TAX RATE: 8.00%

FLAT LIFE: 5.5 YRS
PRODUCTION LIFE: 19.3 YRS
AVG. PRODUCTION DECLINE/YR.: 10.02 %
YIELD (BBL/MCF): 3.9 MAX.
AVG. WELL DEPTH (FT.): 7000

U.I. BEFORE/AFTER PAYOUT: 100.00% 100.00%
N.I. BEFORE/AFTER PAYOUT: 86.50% 86.50%
REVERT. INT. AMOUNT (\$): \$000.1 0.0 YRS
OPERATED: YES

TANCIABLE INVEST. (\$M): \$121.
INTANGIBLE INVEST. (\$M): \$258.
DE-REGULATION TAX DATA
BASE PRICE/BBL: \$14.1
TAX RATE: 70.0%

SOUTHLAND ROYALTY COMPANY
DRILLING ECONOMICS SUMMARY

PREP. BY: MT

FILE: DATA48

DATE: 12-3-80

PROJECT: SRC UNNAMED NO. 1
BASIN DAKOTA
SAN JUAN NEW MEXICO
MINIMUM ECONOMICS-2

Initial Investment Date: 04/01/1981

Initial Production Date: 10/01/1981

1. NOT DISCOUNTED (BEFORE INCOME TAX)

Net Income Before Capital: \$1025. Risk Cost: \$226. Ratio: 4.5
Profit After Capital: \$646. Capital: \$379. Ratio: 1.7

2. RISK PARAMETERS

Trap: 1.00 Reservoir: 1.00 Hydrocarbon: 1.00 Total(R.F.): 1.00

3. OBJECTIVE TEST

Discounted @9% Before Tax Net Income: \$558.

Adjusted For Risk: \$558.

CAPITAL: (Risk Cost*(1-R.F.) + R.F.*Disc. Develop. Cost)*1.25: \$474.

Above Or Below SRC Objective: \$84.

4. PAYOUT (yrs)

Before Tax: 4.89

After Tax: 5.39

5. AFTER TAX RATE OF RETURN

No Risk: 15.23

Risk Adjusted: 15.23

6. COST PER EQUIVALENT BBL & MCF

\$17.13/BBL \$2.86/MCF

7. RISK FACTOR SENSITIVITY

RISK FACTOR	RISK ADJUSTED AFTER TAX ROR	ABOVE OR BELOW SRC OBJECTIVE
0.80	12.6	\$11.
0.60	9.3	\$62.-
0.40	4.7	\$136.-
0.20	0.1	\$209.-
0.10	0.1	\$246.-
0.05	0.1	\$264.-
Minimum: 0.97	15.0	\$75.

8. PROJECT DATA:

Total Life (yrs): 19.3

Flat Life (yrs): 5.5

W.I. Before/After Payout: 100.000%:100.000%

N.I. Before/After Payout: 86.500%: 86.500%

Revert. Int. Amount (M\$): 0.

Excise Tax (M\$): 6.

Net Oil Reserves (MBBLS): 00.

Net Gas Reserves (MMCF): 130.

Gross Producing Wells: 1.

Gross Develop. Dry Holes: 0.

Depth (ft): 7000

RISK COSTS (M\$) :

Dryhole: 226.

Acreage: 00.

Seismic: 00.

Total: 226.

9. UNIT PRICING (GAS)

Initial/Maximum: \$6.22/ \$10.42

ASSUMPTIONS USED IN MAKING ECONOMIC CALCULATIONS
BASIN DAKOTA FIELD
SAN JUAN COUNTY, NEW MEXICO

Drilling and completions costs		378,560.00
Operating costs (\$/well-month)		146.00
Depth (feet)		7,050.00
Southland Royalty working interest (%)		100.00
Royalty interest (%)		13.50
Date of initial production		10-1-81
Initial production rate (MCFD)	103 case	150
	2 x 103 case	75
Liquid yield (BBLs/MMCF)		3.85
Fully adjusted gas price as of 10-1-81 (\$/MCF)	103 case	3.11
	2 x 103 case	6.22
Oil price as of 10-1-81 (\$/BBL)		42.76
Maximum gas price (\$/MCF)		10.42
Maximum oil price (\$/BBL)		50.00
Rate of price escalation (%)		7.00
Severance Tax (%)		8.00
Deregulation Tax data	Base Oil price (\$/BBL)	14.11
	Tax Rate (%)	70.00

BEFORE EXAMINER NUTTER
OIL CONSERVATION DIVISION

SRC EXHIBIT NO. 16

CASE NO. _____

**SOUTHLAND ROYALTY COMPANY
AUTHORITY FOR EXPENDITURE**

- AFE -

☐ ORIGINAL
☐ SUPPLEMENTAL

COMPANY 01 AFE NAME SRC - Unnamed No. 1 DATE 12-2-80
REC. I.D. 01 PROSPECT NAME _____ CODE _____ SEQ. 000 ADD _____

COST CENTER	PROJECT	SUB-PROJECT	AFE NO.	DISTRICT
<input type="checkbox"/> EXPLORATION	<u>San Juan Basin</u>			<u>Farmington</u>
<input checked="" type="checkbox"/> PRODUCTION	<u>170</u>			<u>3025</u>

01 ☐ DRILLING 05 ☐ PLUG & ABANDON 09 ☐ LEASEHOLD PURCH 13 ☐ PROD PROP PURCH
02 ☐ WILDCAT 06 ☐ L & W EQUIPMENT 10 ☐ FARM-IN 14 ☐ WORKOVER
03 ☒ DEVELOPMENT 07 ☐ CONSTRUCTION 11 ☐ GEOPHYSICAL 99 ☐ OTHER
04 ☐ RECOMPLETION 08 ☐ SECONDARY RECOVERY 12 ☐ DHC OR BHC

PROPERTY NO. _____ NAME SRC - Unnamed
WELL NO. 1 NAME Unnamed EST. TOTAL DEPTH 7050'
STATE New Mexico CODE 30 COUNTY San Juan CODE 045
FIELD Basin Dakota
LOCATION T32N, R12W

FORMATION Dakota

OBLIGATIONS _____

LOCATION MEETS ☐ STATE RULES ☒ FIELD RULES, FIELD SPACING 320 ACRES

THIS WELL 320 ACRES

IF JOINT INTEREST PROJECT SUBJECT TO ☐ CARRIED INT ☐ NET PROFIT INT
RIGHT TO CONVERT TO W.I. ☐ OPERATING OWNER & W.I. SRC - 1.0000

JOINT OPERATING AGREEMENT NO. _____

COMPANY W.I. 1.0000 COMPANY REVENUE INTEREST .865

COMPLETED COST				DRY HOLE COST			
I.D.C.	TOTAL	CO-OWNER	CO NET	I.D.C.	TOTAL	CO-OWNER	CO NET
TANGIBLE	<u>257,560</u>		<u>257,560</u>	TANGIBLE	<u>184,180</u>		<u>184,180</u>
L. EQUIP	<u>121,000</u>		<u>121,000</u>		<u>41,440</u>		<u>41,440</u>
				TOTAL	<u>225,620</u>		<u>225,620</u>
TOTAL	<u>378,560</u>		<u>378,560</u>	LESS: DHC			
EXPLORATION, ETC COST				TOTAL	<u>225,620</u>		<u>225,620</u>
				RETIREMENT COST			
				REMOVAL			
				SALV/REC			
				NET COST			

REASON FOR EXPENDITURE Drill and complete a Dakota well.

PROPOSED STARTING DATE _____/_____/_____
LEASE EXPIRATION DATE _____/_____/_____

ESTIMATED COMPLETION DATE _____/_____/_____
DRILLING OBLIGATION DATE _____/_____/_____

APPROVED ☐ REJECTED ☐ IN BUDGET YES ☐ NO ☐ BUDGET # _____

DISTRICT PRODUCTION	DATE	F. W. TITLE & RECORD CLEARANCE	DATE	EXECUTIVE APPROVAL	DATE	F. W. FINANCIAL	DATE
DISTRICT EXPLORATION	DATE	V. P. PRODUCTION	DATE	CO-OWNER	DATE		

BEFORE EXAMINER NUTTER
OIL CONSERVATION DIVISION

SEC EXHIBIT NO. 17

CASE NO. _____

Mar

17

AUTHORIZATION FOR EXPENDITURE

SOUTHLAND ROYALTY COMPANY
1000 FORT WORTH CLUB TOWER
FT. WORTH, TEXAS 76102

COMPANY NO 01
AFE NUMBER 10-13

RECORD ID 02
SEQ 220
14-16

ADD A CHANGE DELETE PROPERTY NUMBER

AFE DATE 12/2/80 NAME SRC - Unnamed No. 1

ORIGINAL O SUPPLEMENTAL PRODUCER DRY HOLE SRC OPERATOR Y MANUAL

AUTHORITY IS REQUESTED TO:

WILDCAT DEV. D Drill and complete a Dakota well.

LOCATION: T32N, R12W, San Juan County, New Mexico

FOOTAGE	TANGIBLE - 249	ESTIMATED COST	
		PRODUCING	DRY HOLE
	01 01 Conductor or Drive Pipe	\$	\$
<u>200'</u>	01 02 Casing 9 5/8", 32.3#, H-40	2,940	2,940
<u>4650'</u>	03 7", 23.0#, K-55	49,200	36,900
<u>1900'</u>	04 4 1/2", 10.5#, K-55	10,130	
<u>350'</u>	05 4 1/2", 11.6#, K-55	2,030	
	06		
	07		
	08		
<u>7000'</u>	02 03 Tubing 2 3/8", 4.7#, J-55	21,560	
	03 10 Wellhead	8,840	1,600
	04 11 Packer		
	04 12 Artificial Lift		
	05 13 Tank Battery	22,270	
	10 14 Other Equipment <u>Liner Hanger</u>	4,030	
	15 TOTAL TANGIBLE 100%	\$121,000	\$ 41,440
	16 SRC <u>1.0000</u> %	\$121,000	\$ 41,440
	INTANGIBLE - 248		
	01 17 Drilling <u>7050'</u> ft. @ \$ <u>14.00</u> /ft.	98,700	98,700
	01 18 Rig, Day Work <u>2</u> Days @ \$ <u>4,700.00</u> /day	9,400	9,400
	01 19 Rig Moving Costs	2,900	1,200
	01 20 Completion Rig <u>3</u> Days @ \$ <u>3,650.00</u> /day	10,950	
	02 21 Roustabout & Miscellaneous Labor	5,000	1,500
	03 22 Auto, Trucking, Barge, Tug	5,350	4,500
	01 23 Roads, Canals, Location, Damages, Cleanup	6,000	6,000
	05 24 Mud, Oil, Water, Chemicals	15,500	13,500
	06 25 Drill Stem Tests		
	06 26 Electric Logs & Bond Logs	10,060	10,060
	07 27 Cement, Centralizer, Scratchers, Service	12,510	7,590
	08 28 Bits, Fuel	4,250	1,500
	08 29 Rental Equipment	7,710	4,730
	09 30 Core & Analyses		
	09 31 Bottle Tests & Sidewall Cores		
	09 32 Perforate	6,660	
	09 33 Acid & Frack	27,500	
	09 34 Geological & Engineering		
	09 35 Mud Logger	600	600
	10 36 Cost of Control Insurance (SRC Only)		
	10 37 Miscellaneous & Unforeseen <u>15%</u> Contingency	33,470	23,900
	11 & 12 38 District & Overhead Expense	1,000	1,000
	39 TOTAL INTANGIBLE 100%	\$257,560	\$184,180
	40 SRC <u>1.0000</u> %	\$257,560	\$184,180
	41 GRAND TOTAL COSTS	\$378,560	\$225,620
	42 SRC <u>1.0000</u> %	\$378,560	\$225,620

AUTHORIZATION REQUESTED

AUTHORIZATION APPROVED

BY: _____

DATE: _____

GEOGRAPHICAL AND GEOLOGICAL DESCRIPTION

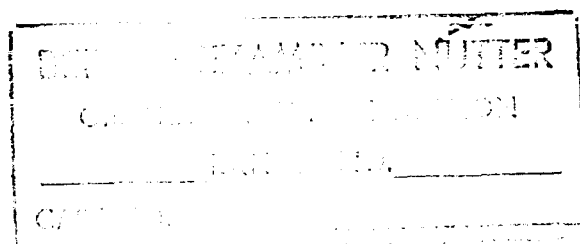
The recommended Dakota area is located in extreme north central San Juan County, New Mexico, adjacent to the Colorado state line and is in the northwestern portion of the San Juan Basin near the Hogback Monocline. The proposed area includes the following:

1. T32N-R10W All sections
2. T32N-R11W All sections except 28, 29, 30, 31, 32 and 33
3. T32N-R12W All sections except 34, 35 and 36
4. T32N-R13W All sections
5. T31N-R10W All sections
6. T31N-R11W Sections 1, 12, 13, 22, 23, 24, 25, 26, 27, 34, 35 and 36 only

This area is shown on Exhibit No. 1.

Exhibit No. 2 is a type log which shows the base of the Mancos, the Greenhorn, the Graneros and the Dakota formations. The vertical limits of the Baskin Dakota gas pool have been defined by the New Mexico Conservation Division to be from the base of the Greenhorn Limestone to a point 400 feet below the base of said formation and consisting of the Graneros formation, the Dakota formation and the productive upper portion of the Morrison formation. The Graneros and first Dakota zones are the producing zones in the Basin Dakota Field. The other Dakota zones and the upper Morrison zone have very low permeability. Production from these zones has been limited to date.

The sediments of the Dakota interval were formed during late Cretaceous time. The Dakota is bounded by an unconformable contact with the Jurassic Morrison below and is grada-



tional with the Cretaceous Mancos shale above and is found at an average dept of 7050 feet. The gross thickness of the formation varies from 200 to 300 feet.

Deposition of the Dakota sediments occurred during a regression of the late Cretaceous sea. This regression resulted in the following sequence of depositional environments from the base upward: 1. Braided stream sandstone; 2. Meandering stream complex (with minor associated coals); 3. Coastal shale; 4. Coastal sandstone. The lower two environments contain sands of minor areal extent whereas the coastal sandstones have significant extent and are seen as northwest-southeast trending linear sand bodies reflecting their beach and off-shore bar depositional history. These upper Dakota sands appear to be the primary Dakota reservoirs.

The Dakota sands are light to dark mottled gray, fine to very fine-grained quartz sands. Silt and clay-sized matrix material can form a significant percentage of the bulk-rock composition. Because the matrix fraction tends to greatly reduce the effective permeability of the reservoir, natural and induced fractures are necessary for production from the Dakota reservoir.

Exhibit Nos. 3 and 4 are cross sections that show the continuity of the Dakota zones across the area of this application. Cross section A-A' shows sand development in a North-South direction while cross-section B-B' shows sand development in a northwest-southeast direction. The permeability of the zones in the area under consideration is lower than in more productive areas such as T31N-R12W. This is indicated by the poor performance of the wells in the proposed area compared to the wells located in T31N-R12W. This is shown by Exhibit No. 1, which is a completion and production map

showing both 1979 annual oil and gas production and the cumulative oil and gas production as of January 1, 1980.

II

GEOLOGICAL AND ENGINEERING DATA

PERMEABILITY

Average in situ permeability for the Dakota formation is 0.1 md or less throughout the recommended area. Several methods were used to determine the average in situ permeability. Each method is described below, and the resulting value of permeability is provided.

1. Pressure Buildup Analysis. In order to determine in situ permeability by this method, it is necessary to produce the well prior to stimulation until it stabilizes then shut it in for a pressure build up with a pressure recorder at the bottom of the hole. This pressure data is then plotted against a time ratio and the slope of the straight line portion of the curve is determined. This slope is used to calculate permeability.

This method was used to determine an average in situ permeability of 0.0011 md in the Southland Royalty Company East No. 7E (See Exhibit No. 5).

2. Darcy's Law Analysis. In order to determine in situ permeability by this method, it is necessary to produce the well under pre-stimulation conditions until both the rate and flowing pressure stabilize. The well is then shut in and the stabilized shut-in pressure determined. With this and other known geological and engineering data, the permeability is calculated using the Darcy flow equation.

This method was used to determine in situ permeability values of 0.0877 and 0.0609 md in the Southland Royalty Company

Patterson "B" Com. No. 1E and Pierce No. 2, respectively (See Exhibit Nos. 6 and 7).

3. Core Analysis. Laboratory permeability is determined by employing coring equipment (bit and barrel) to cut and recover a portion of the reservoir rock. Small plugs are then cut from the rock at one-foot intervals, and the permeability is measured at laboratory conditions. Permeability at reservoir conditions is always less than it is at laboratory conditions because overburden pressure is greater than the pressure used in the laboratory. The higher pressure causes the permeability to be lower. The water that is present in the reservoir rock also causes the in situ permeability to be lower. A paper has been written that presents a method of determining the relationship between laboratory and in situ or reservoir permeability (See Exhibit No. 8).

This method was used to determine average in situ permeability values of 0.0335 and 0.0151 md in the El Paso Natural Gas Company Case No. 8 and Moore No. 8, respectively (See Exhibit Nos. 10 and 11). The laboratory permeabilities for the two wells are 0.1195 and 0.0538, respectively. This data is also shown on Exhibit Nos. 10 and 11. These two exhibits contain the actual core analysis reports plus summary tables showing the analysis of cores taken from only the productive portion of the Dakota formation. The data from these summary tables was used in calculating the average permeability values. This method of determining in situ permeability is explained in Exhibit No. 9.

STABILIZED PRODUCTION RATES

Stabilized production rates were taken on three of the five test wells, the Southland Royalty Company East No. 7E, Patterson "B" Com. No. 1E and Pierce No. 2. The flow rates for

East No. 7E and Patterson "B" Com. No. 1E were taken before stimulation while the flow rate for Pierce No. 2 was taken after stimulation. The production rates were measured at pressures other than atmospheric. These rates were used to determine permeability. The production rates were then calculated at atmospheric conditions by employing the Darcy flow equation. The maximum gas production rate permitted under the tight formation guideline is 290 MCFD for the depth interval 7000-7500 feet. These three wells meet this guideline as shown on Exhibit No. 12. The other two wells, the El Paso Natural Gas Company Cas No. 8 and Moore No. 8, were dry holes and, therefore, did not produce.

OIL PRODUCTION RATES

The three productive test wells did not produce enough oil to measure during the production test. Daily oil production is, therefore, shown to be zero on Exhibit No. 12. None of the wells offsetting the three wells currently produce in excess of five barrels of oil per day as can be seen on Exhibit No. 1; therefore, the daily oil production limit is satisfied.

III

WELLS IN RECOMMENDED FORMATION

Exhibit No. 1 is a completion and production map which shows all of the wells that have produced from the Dakota formation in the geographical area of this application. The map also contains the 1979 annual gas and oil production and the cumulative gas and oil production as of January 1, 1980, as stated previously.

IV

PROTECTION OF FRESH WATER

Existing state and federal regulations will assure that development of the Dakota formation will not adversely affect or impair any fresh water aquifers that are being used or are expected to be used in the foreseeable future for domestic or agricultural water supplies. Three potential fresh water bearing formations occur in the area of interest. These are: 1. San Jose, 2. Nacimiento and 3. Ojo Alamo. The three formations occur from the surface of the ground to an average depth of 1200 feet.

In New Mexico, the Oil Conservation Division is responsible for protecting fresh water while drilling, completing and producing oil and gas wells as provided by Rule 106. This rule requires the casing to be designed to seal off water bearing formations thus separating them from oil and gas bearing formations. Additionally, federal regulations provide for protection of fresh water in oil and gas related activities.

The Dakota formation requires large fracture treatments during completion to provide favorable economics since it is a very tight formation. Fresh water protection is adequate even with these large stimulations. The top of the upper Dakota producing zone is approximately 5800 feet below the deepest fresh water zone thus providing additional insurance that no existing fresh water will be contaminated.

Together, state rules in New Mexico and federal regulations will protect any fresh water supply that may be affected by drilling, completing and producing the Dakota formation in the proposed tight sand area.

V

OTHER RELEVANT INFORMATION

RESERVES AND ECONOMICS

The average estimated ultimate gas recovery for each of the 31 wells in the area of interest that have produced is 313,614 MCF (See Exhibit No. 13). Fifteen of the wells are expected to have ultimate recoveries of less than 200,000 MCF. Gas reserves of 350,000 MCF are required to provide minimum standard economics of 15% rate of return after federal income tax at current 103 prices (See Exhibit No. 14) while gas reserves of only 150,000 MCF are required to provide minimum standard economics at 200% of current 103 prices (See Exhibit No. 15). As indicated, increased prices are necessary to justify drilling Dakota wells in the proposed area because the anticipated recovery is expected to be less than 350,000 MCF, thus causing the wells to be uneconomical at current prices.

Exhibit No. 16 is a tabulation showing the assumptions used in making the economic calculations. Exhibit No. 17 is an Authority for Expenditure showing the cost to drill and complete a Dakota well in the subject area.

MISCELLANEOUS INFORMATION

In addition to completion and production data, Exhibit No. 1 contains the following:

1. Location of cross sections A-A' and B-B'.
2. Location of test wells for which permeability, gas production and oil production rates are submitted.
3. Location of wells that were completed in the Dakota formation but never produced after the initial potential was taken.

4. Location of dry holes that have been drilled in the Dakota formation in the recommended area.

There are two wells in the proposed area that were completed in the Dakota formation but never produced after the initial potential was taken. There are five dry holes in the subject area that were drilled to test the Dakota formation. The failure to make successful Dakota completions in these seven wells provides additional indication that the Dakota formation exhibits very low permeability in the area under consideration.

Three of the test wells, Patterson "A" Com. No. 1E (SW-2-31N-12W), East No. 7E (SW-14-31N-12W) and Case No. 8 (NE-18-31N-11W), are not located in the proposed area. The wells are located near the area, however, where production is more prolific as shown by Exhibit No. 1. The fact that these wells meet the necessary guidelines even in a more productive area indicates that the proposed area will also meet the necessary guidelines.

VI

CONCLUSION

It has been shown in this recommendation that the Dakota formation in the proposed area meets the guidelines necessary to qualify the area for tight formation designation. These include the following:

1. The in situ permeability is less than 0.1 md.
2. The stabilized gas production rate (290 MCFD in the interval 7000-7500 feet) is less than the maximum that is permitted.
3. No well will produce more than five barrels of oil per day.

4. Any fresh water in the area will be adequately protected while the wells are being drilled, completed and produced.

In addition, it has been shown that Dakota wells drilled and completed in the area will not be economical at 103 prices. Added price incentive is, therefore, necessary before the gas reserves in the area can be developed and produced. If the incentive price is allowed to be received for the wells drilled in the recommended area, it is estimated that Southland Royalty Company will recover an additional 14 BCF of gas reserves that would not otherwise be available to existing gas markets.

STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENT
OIL CONSERVATION DIVISION
STATE LAND OFFICE BLDG.
SANTA FE, NEW MEXICO
29 September 1981

COMMISSION HEARING

IN THE MATTER OF:

Application of Southland Royalty
Company for designation of a
tight formation, San Juan County,
New Mexico.

CASE
7361

BEFORE: Commissioner Ramey
Commissioner Arnold

TRANSCRIPT OF HEARING

A P P E A R A N C E S

For the Oil Conservation
Division:

W. Perry Pearce, Esq.
Legal Counsel to the Division
State Land Office Bldg.
Santa Fe, New Mexico 87501

For the Applicant:

William F. Carr, Esq.
CAMPBELL, BYRD, & BLACK P.A.
Jefferson Place
Santa Fe, New Mexico 87501

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I N D E X

HARLAN THOMPSON

Direct Examination by Mr. Carr
(No questions asked on direct.)

Questions by Mr. Chavez

Redirect Examination by Mr. Carr

1
2 MR. RAMEY: Call next Case 7361.

3 MR. PEARCE: Application of Southland
4 Royalty Company for designation of a tight formation, San
5 Juan County, New Mexico.

6 MR. CARR: May it please the Commission,
7 my name is William F. Carr, with the law firm Campbell, Byrd,
8 and Black, P. A., of Santa Fe, appearing on behalf of the
9 applicant.

10 I have one witness who needs to be
11 sworn.

12
13 (Witness sworn.)

14
15 HARLAN THOMPSON

16 being called as a witness and being duly sworn upon his oath,
17 testified as follows, to-wit:

18
19 DIRECT EXAMINATION

20 BY MR. CARR:

21 MR. CARR: May it please the Commission,
22 at this time we would request that the record, including all
23 Southland exhibits offered in the original hearing in Case
24 7116, held on December 30, 1980, be incorporated into the
25 record of this hearing.

1
2 MR. RAMEY: Without objection, why, the
3 Commission will incorporate the record in Case 7116.

4 MR. CARR: May it please the Commission,
5 we do not intend at this time to present additional testimony
6 but have Mr. Thompson here to answer whatever questions you
7 may have.

8 MR. RAMEY: Are there any questions of
9 Mr. Thompson?

10 MR. CHAVEZ: Yes, I have a few.

11 MR. RAMEY: Mr. Chavez.

12
13 QUESTIONS BY MR. CHAVEZ:

14 Q Mr. Thompson, would you please turn to
15 Exhibit Fourteen of the -- of the previous case?

16 A All right. Okay.

17 Q Okay, during the year 1984 through '85 --
18 well, the year 1984, I guess, the hypothetical well in question
19 on this exhibit would at that time, sometime in that year,
20 qualify for stripper gas price, would it not?

21 A Yes, sir, it would.

22 Q Has that been taken into account in the
23 prices in the --

24 A No, it has not.

25 Q Okay. I have done some calculations of

1
2 own I should have made a copy of, but on the exhibit I just
3 pencilled them in there. Does that, those prices seem reason-
4 able to you as to what to expect for stripper gas prices
5 during those years?

6 What I have done is in the year 1984 I
7 just assumed that half the gross production would be at the
8 103 price and half would be at stripper price.

9 A Yes, they -- they look reasonable. I
10 don't, you know, know exactly what it would be, but they
11 appear to be reasonable to me.

12 Q Okay. In consideration of those prices
13 I subtotaled the -- well, I got a new -- generated a new
14 total for the total gas revenue of \$2,118,000, which is an
15 increase of \$184,000 over the previous economics total of
16 \$1934, with an increase of \$15,000 in taxes, to come up with
17 a net income of \$1,908,000, discounted at 9 percent to
18 \$688,000.

19 Do those figures seem reasonable to you?

20 A Yes, they look reasonable.

21 Q Okay. I did not go on to calculate the
22 after tax rate of return because I did not know what tax rate
23 you used and I didn't go into calculating them, but would
24 you assume, then, that perhaps the -- a 9-1/2 percent increase
25 in gross gas revenue might generate the same type of increase

1

6

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in after tax rate of return, say about 9 percent?

3

A No, sir, I don't believe it would be

4

that much. It would be somewhat higher but it wouldn't be

5

that much.

6

Q Okay, about how much? Would it be an

7

8 percent increase?

8

A I think -- I'd have to calculate to be

9

for sure, but I think perhaps it would increase to maybe 18

10

percent, or something like that.

11

Q Okay, but what I meant was it would

12

increase this by 9 or 8 percent.

13

A Okay. All right. Okay.

14

Q Thank you. Well, if it did go as high

15

as 18 percent, then, wouldn't the amount of reserves neces-

16

sary per well decline in order to reach the Southland limit

17

of 15 percent rate of return after taxes?

18

A Yes, it would be reduced slightly.

19

Q Would you perhaps, if we left the record

20

open, present to us a new exhibit showing a well with the

21

cumulative reserves of 313,000, which I think was your cal-

22

culated rate of reserves per well within the area, and showing

23

the changes in the gas price to stripper gas price at the

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time at which the well would be eligible, and submit that

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with the rate of return that would be expected?

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A Yes, sir, I'd be happy to do that.

Q Did you want to take a look at this a moment?

A No, no, that's fine.

Q Okay. Exhibit Fifteen that you presented at the hearing in the previous case in which you testified also does not include the stripper gas price but I don't -- I don't think I'll refer to that at this time.

How many multiple completions did Southland Royalty make within the area that they have requested to be designated as tight formation?

A Very few in that area. Throughout the Basin we make a number of them but not in that particular area.

Q Okay.

A Most of the Mesaverde is already developed in the area, and the Pictured Cliffs is not that prospective, so we don't have that many prospects for dual completion.

Q How many wells have been completed and produced in the Dakota formation, isn't it? It's in your last testimony. Which could be incorporated to the -- in your Exhibit Thirteen -- which, if you'll refer to that, was your listing of producing wells and estimated recoverable reserves?

1
2 A I don't know of any. There may be a few
3 that could be incorporated.

4 Q I remember that there were two in I think
5 it was Township 32, 12.

6 A I'd be happy to check and update the map,
7 if you'd like, but I don't know of any that haven't been made
8 in the Dakota.

9 Q Okay, there are two new wells, I know
10 that for a fact, that weren't shown on the map that you pre-
11 sented in your first exhibit, and then incorporate the data
12 from these wells in the same type of manner and present that,
13 also, as an updated Exhibit Thirteen.

14 A Okay, be happy to do that.
15 I've seen in doing this, I believe we
16 have deleted five sections out of Township 32 North, 12 West,
17 so any -- any wells in those five sections you would not want
18 on the map, is that correct?

19 Q That's right, any area that was deleted,
20 I understand. In 32, 13, you've deleted Sections 30 and 31
21 because they were in the Barker --

22 A Yes, yes, we deleted those, but the
23 Commission deleted five sections, I believe, in 32, 12, and
24 so we would not want to count any wells that were in those
25 five sections, is that correct?

1
2 Q That's fine.

3 MR. CHAVEZ: That's all the questions
4 I have.

5 MR. RAMEY: Any other questions of the
6 witness? Mr. Carr.

7
8 REDIRECT EXAMINATION

9 BY MR. CARR:

10 Q Mr. Thompson, I believe that the December
11 30, 1980, hearing you stated that Southland used a 15 percent
12 rate of return, is that correct?

13 A That is correct.

14 Q Is that the total figure used by South-
15 land?

16 A No, it is not. We're currently using
17 20 percent.

18 Q And why was this figure increased?

19 A Actually because of interest rates. At
20 the time, interest rates went up at that time, almost a year
21 ago, but we were still using the 15 percent, but because
22 they have continued to stay up we have increased our minimum
23 standard to 20 percent, and that's what we're using currently.

24 Q And that is used companywide?

25 A Yes, it is.

1
2 Q And what is the status of the drilling
3 program in the subject area?

4 A We're doing very little in the subject
5 area. In fact, we're doing very little throughout the Basin
6 now.

7 MR. CARR: I have no further questions.

8 MR. RAMEY: Any other questions of the
9 witness?

10 MR. CHAVEZ: Just one more. You used a
11 discount rate of 9 percent. Has that changed?

12 A We're currently using 15 percent, from
13 9 to 15. If we use those new numbers, you know, it's going
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15 gone up significantly since last year, too, so, you know, if
16 we go ahead and use all the assumptions we made last year,
17 everything is going to be out of date.

18 Perhaps it would be better to do a new
19 economic run based on the current prices and current assumptions.
20 Maybe that would be better for Exhibit Fourteen -- Exhibit
21 Thirteen, whichever it is?

22 MR. CHAVEZ: That would be fine.

23 A Okay.

24 MR. RAMEY: Any other questions? The
25 witness may be excused.

1
2 Do you have anything further, Mr. Carr?

3 MR. CARR: Nothing further, Mr. Ramey.

4 MR. RAMEY: All right, we will hold open
5 the record to enable you to update your Exhibit Thirteen and
6 Exhibit Fourteen, is it?

7 MR. THOMPSON: Yes, sir.

8 MR. RAMEY: Is that correct? I won't
9 put a deadline on it. It's to your advantage to get it in
10 as soon as possible.

11 MR. THOMPSON: It will be in the near
12 future.

13 MR. RAMEY: All right. We'll take the
14 case under advisement.

15
16 (Hearing concluded.)
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C E R T I F I C A T E

I, SALLY W. BOYD, C.S.R., DO HEREBY CERTIFY that the foregoing Transcript of Hearing before the Oil Conservation Division was reported by ~~me~~^{*}; that the said transcript is a full, true, and correct record of the hearing, prepared by me to the best of my ability.

Sally W. Boyd CSR

* REPORTER'S NOTE:

This hearing was recorded by Florene Davidson of the Commission's staff in the absence of the reporter. Thereafter, and using the tapes provided by her, the reporter transcribed the said hearing.

SALLY W. BOYD, C.S.R.

Rt. 1 Box 193-B
Santa Fe, New Mexico 87501
Phone (505) 433-7409



BRUCE KING
GOVERNOR
LARRY KEHOE
SECRETARY

STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENT
OIL CONSERVATION DIVISION

January 13, 1982

POST OFFICE BOX 2088
STATE LAND OFFICE BUILDING
SANTA FE, NEW MEXICO 87501
(505) 827-2434

Mr. William F. Carr
Campbell, Byrd & Black
Attorneys at Law
Post Office Box 2208
Santa Fe, New Mexico

Re: CASE NO. 7361
ORDER NO. R-6884

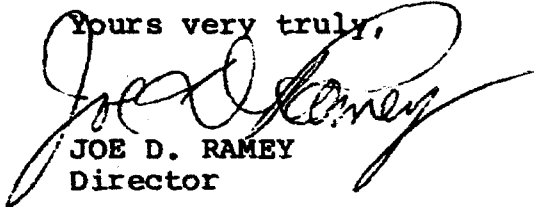
Applicant:

Southland Royalty Company

Dear Sir:

Enclosed herewith are two copies of the above-referenced
Division order recently entered in the subject case.

Yours very truly,


JOE D. RAMEY
Director

JDR/fd

Copy of order also sent to:

Hobbs OCD x
Artesia OCD x
Aztec OCD x

Other _____

CAMPBELL, BYRD & BLACK, P.A.

LAWYERS

POST OFFICE BOX 2208

SANTA FE, NEW MEXICO 87501

Mr. Perry Pearce
Oil Conservation Division
New Mexico Department of
Energy & Minerals
Post Office Box 2088
Santa Fe, New Mexico 87501

CAMPBELL, BYRD & BLACK, P.A.

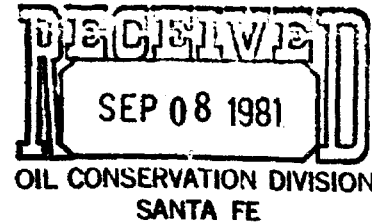
LAWYERS

JACK M. CAMPBELL
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TELEPHONE: (505) 968-4421
TELECOPIER: (505) 963-6043

September 8, 1981

Mr. Allen F. Buckingham
Supervisor
Determination Unit
United States Geological Survey
Post Office Box 26124
Albuquerque, New Mexico 87125



Re: Application of Southland Royalty Company for
Designation of a Tight Formation, San Juan
County, New Mexico

Dear Mr. Buckingham:

On December 30, 1980, the Oil Conservation Division heard Case 7116: the application of Southland Royalty Company for designation of a tight formation, San Juan County, New Mexico. At the time of the hearing, Consolidated Oil & Gas, Inc. appeared and requested that certain additional acreage be included within the designated tight formation. The examiner held that the legal advertisement of the hearing was broad enough to permit the consideration of Consolidated acreage. On August 7, 1981, the Division entered Order R-6747 granting Southland's application. This Order also recommended designation of certain Consolidated lands.

On August 21, 1981, Consolidated filed for a hearing de novo in this case. It is our understanding that the decision entered following the de novo hearing could be appealed further by Consolidated.

Southland Royalty Company has conferred with the Oil Conservation Division and representatives of Consolidated Oil & Gas, Inc. and it has been agreed that the Division will advertise Case 7116 for hearing de novo on September 29, 1981. At the time of the hearing, Southland will request that the Southland Royalty Company acreage included within this application be dismissed from the hearing. Consolidated will then proceed to present its case.

Mr. Allen F. Buckingham
September 8, 1981
Page -2-

Enclosed is a copy of an Amended Application which Southland Royalty Company is filing on this date with the Oil Conservation Commission. As you will note, this application is confined to only Southland Royalty Company land. This application will also be set for hearing on September 29 at which time Southland will ask the Oil Conservation Commission to incorporate the Southland exhibits and testimony offered in Case 7116 on December 30, 1980. We do not anticipate at this time to offer new exhibits or testimony, although we will have representatives of Southland Royalty Company present should questions arise.

We are not, therefore, sending an additional set of exhibits to the United States Geological Survey as required by Oil Conservation Division rules. If you desire such exhibits or have any questions concerning this matter, please advise.

Very truly yours,

William F. Carr

WFC:lr

Enclosure

cc: Mr. Marlin Thompson
Ms. Lynn Teschendorf

bcc: Mr. Perry Pearce

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STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENT
OIL CONSERVATION DIVISION
STATE LAND OFFICE BLDG.
SANTA FE, NEW MEXICO
29 September 1981

COMMISSION HEARING

IN THE MATTER OF:

Application of Southland Royalty
Company for designation of a
tight formation, San Juan County,
New Mexico.

CASE
7361

BEFORE: Commissioner Ramey
Commissioner Arnold

TRANSCRIPT OF HEARING

A P P E A R A N C E S

For the Oil Conservation	W. Perry Pearce, Esq.
Division:	Legal Counsel to the Division
	State Land Office Bldg.
	Santa Fe, New Mexico 87501

For the Applicant:	William F. Carr, Esq.
	CAMPBELL, BYRD, & BLACK P.A.
	Jefferson Place
	Santa Fe, New Mexico 87501

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I N D E X

HARLAN THOMPSON

Direct Examination by Mr. Carr (No questions asked on direct.)	3
Questions by Mr. Chavez	4
Redirect Examination by Mr. Carr	9

1
2 MR. RAMEY: Call next Case 7361.

3 MR. PEARCE: Application of Southland
4 Royalty Company for designation of a tight formation, San
5 Juan County, New Mexico.

6 MR. CARR: May it please the Commission,
7 my name is William F. Carr, with the law firm Campbell, Byrd,
8 and Black, P. A., of Santa Fe, appearing on behalf of the
9 applicant.

10 I have one witness who needs to be
11 sworn.

12
13 (Witness sworn.)

14
15 HARLAN THOMPSON
16 being called as a witness and being duly sworn upon his oath,
17 testified as follows, to-wit:

18
19 DIRECT EXAMINATION

20 BY MR. CARR:

21 MR. CARR: May it please the Commission,
22 at this time we would request that the record, including all
23 Southland exhibits offered in the original hearing in Case
24 7116, held on December 30, 1980, be incorporated into the
25 record of this hearing.

1
2 MR. RAMEY: Without objection, why, the
3 Commission will incorporate the record in Case 7116.

4 MR. CARR: May it please the Commission,
5 we do not intend at this time to present additional testimony
6 but have Mr. Thompson here to answer whatever questions you
7 may have.

8 MR. RAMEY: Are there any questions of
9 Mr. Thompson?

10 MR. CHAVEZ: Yes, I have a few.

11 MR. RAMEY: Mr. Chavez.

12
13 QUESTIONS BY MR. CHAVEZ:

14 Q Mr. Thompson, would you please turn to
15 Exhibit Fourteen of the -- of the previous case?

16 A All right. Okay.

17 Q Okay, during the year 1984 through '85 --
18 well, the year 1984, I guess, the hypothetical well in question
19 on this exhibit would at that time, sometime in that year,
20 qualify for stripper gas price, would it not?

21 A Yes, sir, it would.

22 Q Has that been taken into account in the
23 prices in the --

24 A No, it has not.

25 Q Okay. I have done some calculations of

2 own I should have made a copy of, but on the exhibit I just
3 pencilled them in there. Does that, those prices seem reason-
4 able to you as to what to expect for stripper gas prices
5 during those years?

6 What I have done is in the year 1984 I
7 just assumed that half the gross production would be at the
8 103 price and half would be at stripper price.

9 A Yes, they -- they look reasonable. I
10 don't, you know, know exactly what it would be, but they
11 appear to be reasonable to me.

12 Q Okay. In consideration of those prices
13 I subtotaled the -- well, I got a new -- generated a new
14 total for the total gas revenue of \$2,118,000, which is an
15 increase of \$184,000 over the previous economics total of
16 \$1934, with an increase of \$15,000 in taxes, to come up with
17 a net income of \$1,908,000, discounted at 9 percent to
18 \$688,000.

19 Do those figures seem reasonable to you?

20 A Yes, they look reasonable.

21 Q Okay. I did not go on to calculate the
22 after tax rate of return because I did not know what tax rate
23 you used and I didn't go into calculating them, but would
24 you assume, then, that perhaps the -- a 9-1/2 percent increase
25 in gross gas revenue might generate the same type of increase

1
2 in after tax rate of return, say about 9 percent?

3 A No, sir, I don't believe it would be
4 that much. It would be somewhat higher but it wouldn't be
5 that much.

6 Q Okay, about how much? Would it be an
7 8 percent increase?

8 A I think -- I'd have to calculate to be
9 for sure, but I think perhaps it would increase to maybe 18
10 percent, or something like that.

11 Q Okay, but what I meant was it would
12 increase this by 9 or 8 percent.

13 A Okay. All right. Okay.

14 Q Thank you. Well, if it did go as high
15 as 18 percent, then, wouldn't the amount of reserves neces-
16 sary per well decline in order to reach the Southland limit
17 of 15 percent rate of return after taxes?

18 A Yes, it would be reduced slightly.

19 Q Would you perhaps, if we left the record
20 open, present to us a new exhibit showing a well with the
21 cumulative reserves of 313,000, which I think was your cal-
22 culated rate of reserves per well within the area, and showing
23 the changes in the gas price to stripper gas price at the
24 time at which the well would be eligible, and submit that
25 with the rate of return that would be expected?

1
2 A Yes, sir, I'd be happy to do that.

3 Q Did you want to take a look at this a
4 moment?

5 A No, no, that's fine.

6 Q Okay. Exhibit Fifteen that you presented
7 at the hearing in the previous case in which you testified
8 also does not include the stripper gas price but I don't --
9 I don't think I'll refer to that at this time.

10 How many multiple completions did South-
11 land Royalty make within the area that they have requested
12 to be designated as tight formation?

13 A Very few in that area. Throughout the
14 Basin we make a number of them but not in that particular
15 area.

16 Q Okay.

17 A Most of the Mesaverde is already developed
18 in the area, and the Pictured Cliffs is not that prospective,
19 so we don't have that many prospects for dual completion.

20 Q How many wells have been completed and
21 produced in the Dakota formation, isn't it? It's in your
22 last testimony. Which could be incorporated to the -- in
23 your Exhibit Thirteen -- which, if you'll refer to that, was
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7 if you'd like, but I don't know of any that haven't been made
8 in the Dakota.

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10 that for a fact, that weren't shown on the map that you pre-
11 sented in your first exhibit, and then incorporate the data
12 from these wells in the same type of manner and present that,
13 also, as an updated Exhibit Thirteen.

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15 I've seen in doing this, I believe we
16 have deleted five sections out of Township 32 North, 12 West,
17 so any -- any wells in those five sections you would not want
18 on the map, is that correct?

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20 I understand. In 32, 13, you've deleted Sections 30 and 31
21 because they were in the Barker --

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23 Commission deleted five sections, I believe, in 32, 12, and
24 so we would not want to count any wells that were in those
25 five sections, is that correct?

Q That's fine.

MR. CHAVEZ: That's all the questions I have.

MR. RAMEY: Any other questions of the witness? Mr. Carr.

REDIRECT EXAMINATION

BY MR. CARR:

Q Mr. Thompson, I believe that the December 30, 1980, hearing you stated that Southland used a 15 percent rate of return, is that correct?

A That is correct.

Q Is that the total figure used by Southland?

A No, it is not. We're currently using 20 percent.

Q And why was this figure increased?

A Actually because of interest rates. At the time, interest rates went up at that time, almost a year ago, but we were still using the 15 percent, but because they have continued to stay up we have increased our minimum standard to 20 percent, and that's what we're using currently.

Q And that is used companywide?

A Yes, it is.

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3 program in the subject area?

4 A We're doing very little in the subject
5 area. In fact, we're doing very little throughout the Basin
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10 MR. CHAVEZ: Just one more. You used a
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14 to affect, you know, of course the price of a well now has
15 gone up significantly since last year, too, so, you know, if
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17 everything is going to be out of date.

18 Perhaps it would be better to do a new
19 economic run based on the current prices and current assumptions.
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21 Thirteen, whichever it is?

22 MR. CHAVEZ: That would be fine.

23 A Okay.

24 MR. RAMEY: Any other questions? The
25 witness may be excused.

1 Do you have anything further, Mr. Carr?

2 MR. CARR: Nothing further, Mr. Ramey.

3 MR. RAMEY: All right, we will hold open
4 the record to enable you to update your Exhibit Thirteen and
5 Exhibit Fourteen, is it?
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7 MR. THOMPSON: Yes, sir.

8 MR. RAMEY: Is that correct? I won't
9 put a deadline on it. It's to your advantage to get it in
10 as soon as possible.

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16 (Hearing concluded.)
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C E R T I F I C A T E

I, SALLY W. BOYD, C.S.R., DO HEREBY CERTIFY that the foregoing Transcript of Hearing before the Oil Conservation Division was reported by ~~me~~; that the said transcript is a full, true, and correct record of the hearing, prepared by me to the best of my ability.

Sally W. Boyd CSR

* REPORTER'S NOTE:

This hearing was recorded by Florene Davidson of the Commission's staff in the absence of the reporter. Thereafter, and using the tapes provided by her, the reporter transcribed the said hearing.

SALLY W. BOYD, C.S.R.

Rt. 1 Box 193-B
Santa Fe, New Mexico 87501
Phone (505) 455-7409

STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENT
OIL CONSERVATION COMMISSION

IN THE MATTER OF THE HEARING
CALLED BY THE OIL CONSERVATION
COMMISSION OF NEW MEXICO FOR
THE PURPOSE OF CONSIDERING:

CASE NO. 7361
Order No. R-6884

APPLICATION OF SOUTHLAND ROYALTY
COMPANY FOR DESIGNATION OF A TIGHT
FORMATION, SAN JUAN COUNTY, NEW MEXICO.

ORDER OF THE COMMISSION

BY THE COMMISSION:

This cause came on for hearing at 9 o'clock a.m. on September 29, 1981, at Santa Fe, New Mexico, before the Oil Conservation Commission of New Mexico, hereinafter referred to as the "Commission."

NOW, on this 12th day of January, 1982, the Commission, a quorum being present, having considered the testimony presented and the exhibits received at said hearing, and being fully advised in the premises,

FINDS:

(1) That due public notice having been given as required by law, the Commission has jurisdiction of this cause and the subject matter thereof.

(2) That, pursuant to Section 107 of the Natural Gas Policy Act of 1978, and CFR Section 271.703, applicant Southland Royalty Company requested the designation as a "tight formation" of the Dakota formation underlying the following described lands:

SAN JUAN COUNTY, NEW MEXICO

TOWNSHIP 31 NORTH, RANGE 10 WEST, NMPM
Sections 1 through 36: All

TOWNSHIP 31 NORTH, RANGE 11 WEST, NMPM
Section 1: All
Sections 12 and 13: All
Sections 22 through 27: All
Sections 34 through 36: All

TOWNSHIP 32 NORTH, RANGE 10 WEST, NMPM
Sections 7 through 36: All

-2-

Case No. 7361
Order No. R-6884

TOWNSHIP 32 NORTH, RANGE 11 WEST, NMPM
Sections 7 through 27: All
Sections 34 through 36: All

TOWNSHIP 32 NORTH, RANGE 12 WEST, NMPM
Sections 7 through 33: All

TOWNSHIP 32 NORTH, RANGE 13 WEST, NMPM
Sections 7 through 33: All

containing a total of 92,871 acres, more or less.

(3) That at the hearing, applicant requested dismissal of that portion of the application pertaining to Sections 25 through 27, inclusive, and Sections 32 and 33, all in Township 32 North, Range 12 West, NMPM, containing some 3,200 acres, more or less, leaving for consideration some 89,671 acres, more or less.

(4) That said request for dismissal should be approved, and no further consideration given herein to said lands.

(5) That while the application was for designation of the Dakota formation as a tight formation, the Dakota formation constitutes but a portion of the "Dakota Producing Interval," which, as defined by the Division, comprises the vertical limits of the Basin-Dakota Gas Pool, being from the base of the Greenhorn Limestone to a point 400 feet below the base of said formation and consisting of the Graneros formation, the Dakota formation, and the productive upper limit of the Morrison formation.

(6) That inasmuch as practically all so-called "Dakota" wells drilled in the subject area are, or potentially are, tested in and/or completed in the entire Dakota Producing Interval, and the well data presented at the hearing of this case involves the entire Dakota Producing Interval, the application should be broadened to cover all of said producing interval throughout the area.

(7) That the Dakota Producing Interval, hereinafter referred to as the "Dakota," consists of a near blanket sandstone (probably an almost continuous series of northwest trending barrier beach sandstones composed of fine-grained quartose sandstones and carbonaceous shales with occasional conglomerates and coals in the basal part).

(8) That from the logs available at the hearing, the top of the Dakota in the area ranges from a depth of 5234 feet to 7220 feet and averages some 6753 feet beneath the surface.

-3-

Case No. 7361
Order No. R-6884

(9) That the only test data for flow rates prior to stimulation for wells within the area indicates that the Aztec Pierce Well No. 2 in Section 30, Township 31 North, Range 10 West, NMPM, had a stabilized production rate calculated at atmospheric pressure of 208.1 MCF of gas per day; that other wells in the immediate vicinity of the area but just outside had stabilized production rates calculated at atmospheric pressure prior to stimulation ranging from 21.7 MCF per/day to 224.1 MCF per day.

(10) That none of the stabilized production rates cited above exceeds the maximum stabilized production rate set forth in 18 C.F.R. Section 271.703(c)(2)(i)(B) of 251 MCF per day for wells at the average depth to the top of the formation for this area (6753 feet), and it is not expected that the average well in the area will exceed such rate.

(11) That in situ permeability calculations are available for only two wells in the general area, being the Southland Pierce Well No. 2 and the Southland Patterson "B" Com Well No. 1E; that the in situ permeabilities calculated for said wells are .0609 md and .0877 md, respectively, and average .0743 md.

(12) That the average in situ permeability for all wells in the area is not expected to exceed 0.1 md, the limit set forth in 18 C.F.R. Section 271.703(c)(2)(i)(A).

(13) That prior to stimulation, the average well in the area is expected to produce far less than the maximum five barrels of crude oil per day as set forth in 18 C.F.R. Section 271.703(c)(2)(i)(C).

(14) That 18 C.F.R. Section 271.703(c)(2)(i)(D) provides that "if the formation or any portion thereof was authorized to be developed by infill drilling prior to the date of recommendation and the jurisdictional agency has information which in its judgment indicates that such formation or portion subject to infill drilling can be developed absent the incentive price established in paragraph (a) of this section then the jurisdictional agency shall not include such formation or portion thereof in its recommendation."

(15) That the Division, by its Order No. R-1670-V, dated May 22, 1979, and effective July 1, 1979, approved infill drilling for the Basin-Dakota Gas Pool in San Juan and Rio Arriba Counties, New Mexico, and said pool includes the Dakota Producing Interval in the area under consideration here.

(16) That Southland in this hearing indicated that under current Section 103 prices of the NGPA of 1978, reserves of

-4-

Case No. 7361
Order No. R-6884

350,000 MCF of gas are necessary to provide it with the economics necessary to justify drilling a Dakota well at its current drilling costs, while 150,000 MCF of reserves will justify a well at Section 107(c)(5) prices (tight formations).

(17) That the economics as presented by Southland in this case are reasonable, and lands which indicate recoverable reserves of 350,000 MCF or more of gas should be dismissed from further consideration, while lands indicating recoverable reserves of less than 350,000 MCF of gas should be considered for recommendation as a tight formation.

(18) That the Division, in approving infill drilling for the Basin-Dakota Gas Pool, based its approval on the premise that the reservoir was of low permeability and that 320-acre wells were not draining more than the 160-acre tract upon which they were located.

(19) That the remaining reserves under the 160-acre tract upon which the unit well is not located should be similar to, if not equal to, the original reserves under the 160-acre tract upon which the unit well is located.

(20) That cumulative production figures and estimates of ultimate recoverable reserves were presented at the hearing for some of the developed tracts within the area, while cumulative production figures only are available for the remainder of the developed tracts.

(21) That to determine that under certain lands insufficient reserves are available to justify drilling absent the Section 107 incentive price, it is reasonable to make the following assumptions:

- A. No primary drilling, i.e., no drilling on 320-acre spacing, is prima facie evidence that the lands are edge lands to the reservoir and drilling has not occurred because of the probable marginal nature of the reserves.
- B. Primary drilling has occurred but the calculated total ultimate reserves or the cumulative production for long-connected wells indicates low ultimate recovery (less than 350,000 MCF of gas).

(22) That to determine that under certain lands sufficient reserves may reasonably be expected to be recovered to justify drilling without the Section 107 incentive price, it is reasonable to make the following assumptions:

-5-

Case No. 7361
Order No. R-6884

- A. Calculated ultimate recoverable reserves are 350,000 MCF or more.
- B. Calculated ultimate recoverable reserves are not available, but cumulative recoveries indicate that 350,000 MCF of gas already has been recovered.

(23) That the assumptions in Findings Nos. (21) B. and (22) A. and B. above may reasonably be based on offsetting wells in a given area.

(24) That the evidence indicates that it is unreasonable to expect that wells drilled in the area described in Finding No. (2) above less the area described in Finding No. (3) above will yield an average of 350,000 MCF or more of gas, but that it is reasonable to expect that such wells will yield an average of 150,000 MCF of gas, and that the incentive Section 107 (c)(5) price is necessary to justify drilling in said area.

(25) That there are fresh water aquifers underlying the lands being considered, and these aquifers extend to a depth of approximately 1200 feet.

(26) That there is a vertical distance of some 5500 feet between the base of the lowermost of said aquifers and the top of the Dakota, and this distance, combined with the required casing and cementing program for wells in the area, will assure that development of the Dakota will not adversely affect the fresh water aquifers (during both hydraulic fracturing and waste disposal operations) that are or are expected to be used as a domestic or agricultural water supply.

(27) That the Dakota Producing Interval underlying the following lands meets all of the guidelines set forth in 18 C.F.R. Section 271.703(c)(2)(i), subsections (A), (B), (C), and (D), and should be recommended for designation as a tight formation:

TOWNSHIP 31 NORTH, RANGE 10 WEST, NMPM
Sections 1 through 36: All

TOWNSHIP 31 NORTH, RANGE 11 WEST, NMPM
Section 1: All
Sections 12 and 13: All
Sections 22 through 27: All
Sections 34 through 36: All

TOWNSHIP 32 NORTH, RANGE 10 WEST, NMPM
Sections 7 through 36: All

-6-
Case No. 7361
Order No. R-6884

TOWNSHIP 32 NORTH, RANGE 11 WEST, NMPM
Sections 7 through 27: All
Sections 34 through 36: All

TOWNSHIP 32 NORTH, RANGE 12 WEST, NMPM
Sections 7 through 24: All
Sections 28 through 31: All

TOWNSHIP 32 NORTH, RANGE 13 WEST, NMPM
Sections 7 through 29: All
Sections 32 through 36: All

containing some 89,671 acres, more or less, all in San Juan County, New Mexico.

IT IS THEREFORE ORDERED:

(1) That it be and hereby is recommended to the Federal Energy Regulatory Commission pursuant to Section 107 of the Natural Gas Policy Act of 1978, and 18 C.F.R. Section 271.703, that the Dakota Producing Interval, being from the base of the Greenhorn Limestone to a point 400 feet below the base of said formation and consisting of the Graneros formation, the Dakota formation and the productive upper portion of the Morrison formation, underlying the following described lands in San Juan County, New Mexico, be designated as a tight formation:

TOWNSHIP 31 NORTH, RANGE 10 WEST, NMPM
Sections 1 through 36: All

TOWNSHIP 31 NORTH, RANGE 11 WEST, NMPM
Section 1: All
Sections 12 and 13: All
Sections 22 through 27: All
Sections 34 through 36: All

TOWNSHIP 32 NORTH, RANGE 10 WEST, NMPM
Sections 7 through 36: All

TOWNSHIP 32 NORTH, RANGE 11 WEST, NMPM
Sections 7 through 27: All
Sections 34 through 36: All

TOWNSHIP 32 NORTH, RANGE 12 WEST, NMPM
Sections 7 through 24: All
Sections 28 through 31: All

TOWNSHIP 32 NORTH, RANGE 13 WEST, NMPM
Sections 7 through 29: All
Sections 32 through 36: All

-7-

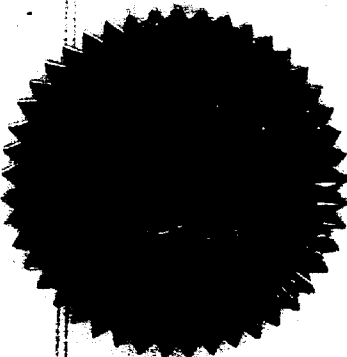
Case No. 7361
Order No. R-6884

containing approximately 89,671 acres, more or less.

(2) That jurisdiction of this cause is retained for the entry of such further orders as the Commission may deem necessary.

DONE at Santa Fe, New Mexico, on the day and year hereinabove designated.

STATE OF NEW MEXICO
OIL CONSERVATION COMMISSION



Emery C. Arnold
EMERY C. ARNOLD, Chairman

ALEX J. ARMIJO, Member

Joe D. Ramey
JOE D. RAMEY, Member & Secretary

S E A L

GEOGRAPHICAL AND GEOLOGICAL DESCRIPTION

The recommended Dakota area is located in extreme north central San Juan County, New Mexico, adjacent to the Colorado state line and is in the northwestern portion of the San Juan Basin near the Hogback Monocline. The proposed area includes the following:

1. T32N-R10W All sections
2. T32N-R11W All sections except 28, 29, 30, 31, 32 and 33
3. T32N-R12W All sections except 34, 35 and 36
4. T32N-R13W All sections
5. T31N-R10W All sections
6. T31N-R11W Sections 1, 12, 13, 22, 23, 24, 25, 26, 27, 34, 35 and 36 only

This area is shown on Exhibit No. 1.

Exhibit No. 2 is a type log which shows the base of the Mancos, the Greenhorn, the Graneros and the Dakota formations. The vertical limits of the Baskin Dakota gas pool have been defined by the New Mexico Conservation Division to be from the base of the Greenhorn Limestone to a point 400 feet below the base of said formation and consisting of the Graneros formation, the Dakota formation and the productive upper portion of the Morrison formation. The Graneros and first Dakota zones are the producing zones in the Basin Dakota Field. The other Dakota zones and the upper Morrison zone have very low permeability. Production from these zones has been limited to date.

The sediments of the Dakota interval were formed during late Cretaceous time. The Dakota is bounded by an unconformable contact with the Jurassic Morrison below and is grada-

tional with the Cretaceous Mancos shale above and is found at an average dept of 7050 feet. The gross thickness of the formation varies from 200 to 300 feet.

Deposition of the Dakota sediments occurred during a regression of the late Cretaceous sea. This regression resulted in the following sequence of depositional environments from the base upward: 1. Braided stream sandstone; 2. Meandering stream complex (with minor associated coals); 3. Coastal shale; 4. Coastal sandstone. The lower two environments contain sands of minor areal extent whereas the coastal sandstones have significant extent and are seen as northwest-southeast trending linear sand bodies reflecting their beach and off-shore bar depositional history. These upper Dakota sands appear to be the primary Dakota reservoirs.

The Dakota sands are light to dark mottled gray, fine to very fine-grained quartz sands. Silt and clay-sized matrix material can form a significant percentage of the bulk-rock composition. Because the matrix fraction tends to greatly reduce the effective permeability of the reservoir, natural and induced fractures are necessary for production from the Dakota reservoir.

Exhibit Nos. 3 and 4 are cross sections that show the continuity of the Dakota zones across the area of this application. Cross section A-A' shows sand development in a North-South direction while cross-section B-B' shows sand development in a northwest-southeast direction. The permeability of the zones in the area under consideration is lower than in more productive areas such as T31N-R12W. This is indicated by the poor performance of the wells in the proposed area compared to the wells located in T31N-R12W. This is shown by Exhibit No. 1, which is a completion and production map

showing both 1979 annual oil and gas production and the cumulative oil and gas production as of January 1, 1980.

II

GEOLOGICAL AND ENGINEERING DATA

PERMEABILITY

Average in situ permeability for the Dakota formation is 0.1 md or less throughout the recommended area. Several methods were used to determine the average in situ permeability. Each method is described below, and the resulting value of permeability is provided.

1. Pressure Buildup Analysis. In order to determine in situ permeability by this method, it is necessary to produce the well prior to stimulation until it stabilizes then shut it in for a pressure build up with a pressure recorder at the bottom of the hole. This pressure data is then plotted against a time ratio and the slope of the straight line portion of the curve is determined. This slope is used to calculate permeability.

This method was used to determine an average in situ permeability of 0.0011 md in the Southland Royalty Company East No. 7E (See Exhibit No. 5).

2. Darcy's Law Analysis. In order to determine in situ permeability by this method, it is necessary to produce the well under pre-stimulation conditions until both the rate and flowing pressure stabilize. The well is then shut in and the stabilized shut-in pressure determined. With this and other known geological and engineering data, the permeability is calculated using the Darcy flow equation.

This method was used to determine in situ permeability values of 0.0877 and 0.0609 md in the Southland Royalty Company

Patterson "B" Com. No. 1E and Pierce No. 2, respectively (See Exhibit Nos. 6 and 7).

3. Core Analysis. Laboratory permeability is determined by employing coring equipment (bit and barrel) to cut and recover a portion of the reservoir rock. Small plugs are then cut from the rock at one-foot intervals, and the permeability is measured at laboratory conditions. Permeability at reservoir conditions is always less than it is at laboratory conditions because overburden pressure is greater than the pressure used in the laboratory. The higher pressure causes the permeability to be lower. The water that is present in the reservoir rock also causes the in situ permeability to be lower. A paper has been written that presents a method of determining the relationship between laboratory and in situ or reservoir permeability (See Exhibit No. 8).

This method was used to determine average in situ permeability values of 0.0335 and 0.0151 md in the El Paso Natural Gas Company Case No. 8 and Moore No. 8, respectively (See Exhibit Nos. 10 and 11). The laboratory permeabilities for the two wells are 0.1195 and 0.0538, respectively. This data is also shown on Exhibit Nos. 10 and 11. These two exhibits contain the actual core analysis reports plus summary tables showing the analysis of cores taken from only the productive portion of the Dakota formation. The data from these summary tables was used in calculating the average permeability values. This method of determining in situ permeability is explained in Exhibit No. 9.

STABILIZED PRODUCTION RATES

Stabilized production rates were taken on three of the five test wells, the Southland Royalty Company East No. 7E, Patterson "B" Com. No. 1E and Pierce No. 2. The flow rates for

East No. 7E and Patterson "B" Com. No. 1E were taken before stimulation while the flow rate for Pierce No. 2 was taken after stimulation. The production rates were measured at pressures other than atmospheric. These rates were used to determine permeability. The production rates were then calculated at atmospheric conditions by employing the Darcy flow equation. The maximum gas production rate permitted under the tight formation guideline is 290 MCFD for the depth interval 7000-7500 feet. These three wells meet this guideline as shown on Exhibit No. 12. The other two wells, the El Paso Natural Gas Company Cas No. 8 and Moore No. 8, were dry holes and, therefore, did not produce.

OIL PRODUCTION RATES

The three productive test wells did not produce enough oil to measure during the production test. Daily oil production is, therefore, shown to be zero on Exhibit No. 12. None of the wells offsetting the three wells currently produce in excess of five barrels of oil per day as can be seen on Exhibit No. 1; therefore, the daily oil production limit is satisfied.

III

WELLS IN RECOMMENDED FORMATION

Exhibit No. 1 is a completion and production map which shows all of the wells that have produced from the Dakota formation in the geographical area of this application. The map also contains the 1979 annual gas and oil production and the cumulative gas and oil production as of January 1, 1980, as stated previously.

IV

PROTECTION OF FRESH WATER

Existing state and federal regulations will assure that development of the Dakota formation will not adversely affect or impair any fresh water aquifers that are being used or are expected to be used in the foreseeable future for domestic or agricultural water supplies. Three potential fresh water bearing formations occur in the area of interest. These are: 1. San Jose, 2. Nacimiento and 3. Ojo Alamo. The three formations occur from the surface of the ground to an average depth of 1200 feet.

In New Mexico, the Oil Conservation Division is responsible for protecting fresh water while drilling, completing and producing oil and gas wells as provided by Rule 106. This rule requires the casing to be designed to seal off water bearing formations thus separating them from oil and gas bearing formations. Additionally, federal regulations provide for protection of fresh water in oil and gas related activities.

The Dakota formation requires large fracture treatments during completion to provide favorable economics since it is a very tight formation. Fresh water protection is adequate even with these large stimulations. The top of the upper Dakota producing zone is approximately 5800 feet below the deepest fresh water zone thus providing additional insurance that no existing fresh water will be contaminated.

Together, state rules in New Mexico and federal regulations will protect any fresh water supply that may be affected by drilling, completing and producing the Dakota formation in the proposed tight sand area.

OTHER RELEVANT INFORMATION

RESERVES AND ECONOMICS

The average estimated ultimate gas recovery for each of the 31 wells in the area of interest that have produced is 313,614 MCF (See Exhibit No. 13). Fifteen of the wells are expected to have ultimate recoveries of less than 200,000 MCF. Gas reserves of 350,000 MCF are required to provide minimum standard economics of 15% rate of return after federal income tax at current 103 prices (See Exhibit No. 14) while gas reserves of only 150,000 MCF are required to provide minimum standard economics at 200% of current 103 prices (See Exhibit No. 15). As indicated, increased prices are necessary to justify drilling Dakota wells in the proposed area because the anticipated recovery is expected to be less than 350,000 MCF, thus causing the wells to be uneconomical at current prices.

Exhibit No. 16 is a tabulation showing the assumptions used in making the economic calculations. Exhibit No. 17 is an Authority for Expenditure showing the cost to drill and complete a Dakota well in the subject area.

MISCELLANEOUS INFORMATION

In addition to completion and production data, Exhibit No. 1 contains the following:

1. Location of cross sections A-A' and B-B'.
2. Location of test wells for which permeability, gas production and oil production rates are submitted.
3. Location of wells that were completed in the Dakota formation but never produced after the initial potential was taken.

4. Location of dry holes that have been drilled in the Dakota formation in the recommended area.

There are two wells in the proposed area that were completed in the Dakota formation but never produced after the initial potential was taken. There are five dry holes in the subject area that were drilled to test the Dakota formation. The failure to make successful Dakota completions in these seven wells provides additional indication that the Dakota formation exhibits very low permeability in the area under consideration.

Three of the test wells, Patterson "A" Com. No. 1E (SW-2-31N-12W), East No. 7E (SW-14-31N-12W) and Case No. 8 (NE-18-31N-11W), are not located in the proposed area. The wells are located near the area, however, where production is more prolific as shown by Exhibit No. 1. The fact that these wells meet the necessary guidelines even in a more productive area indicates that the proposed area will also meet the necessary guidelines.

VI

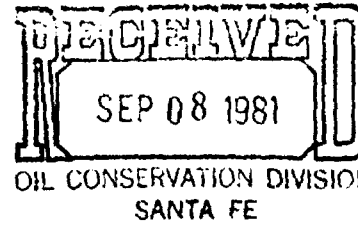
CONCLUSION

It has been shown in this recommendation that the Dakota formation in the proposed area meets the guidelines necessary to qualify the area for tight formation designation. These include the following:

1. The in situ permeability is less than 0.1 md.
2. The stabilized gas production rate (290 MCFD in the interval 7000-7500 feet) is less than the maximum that is permitted.
3. No well will produce more than five barrels of oil per day.

4. Any fresh water in the area will be adequately protected while the wells are being drilled, completed and produced.

In addition, it has been shown that Dakota wells drilled and completed in the area will not be economical at 103 prices. Added price incentive is, therefore, necessary before the gas reserves in the area can be developed and produced. If the incentive price is allowed to be received for the wells drilled in the recommended area, it is estimated that Southland Royalty Company will recover an additional 14 BCF of gas reserves that would not otherwise be available to existing gas markets.



BEFORE THE
OIL CONSERVATION COMMISSION
NEW MEXICO DEPARTMENT OF ENERGY AND MINERALS

IN THE MATTER OF THE APPLICATION
OF SOUTHLAND ROYALTY COMPANY,
FOR DESIGNATION OF TIGHT FORMA-
TION, SAN JUAN COUNTY, NEW MEXICO

Case 2361

APPLICATION

Comes now SOUTHLAND ROYALTY COMPANY, by and through its undersigned attorneys and as provided in the Oil Conservation Division's Special Rules and Procedures for Tight Formation Designations under Section 107 of the Natural Gas Policy Act of 1978 promulgated by Oil Conservation Division Order No. R-6388 on June 30, 1980, hereby makes application for an order designating certain portions of the Dakota formation (Basin Dakota Field) as a tight formation under Section 107 of the Natural Gas Policy Act of 1978 and in support of its application would show the Division:

1. Applicant is the owner and operator of certain interests in the Dakota formation (Basin Dakota Field) underlying the following described lands situated in San Juan County, New Mexico:

Township 31 North, Range 10 West, N.M.P.M.
Sections 1 through 36: All

Township 31 North, Range 11 West, N.M.P.M.
Section 1: All
Sections 12 and 13: All
Sections 22 through 27: All
Sections 34 through 36: All

Township 32 North, Range 10 West, N.M.P.M.
Sections 7 through 36: All

Township 32 North, Range 11 West, N.M.P.M.

Sections 7 through 27: All
Sections 34 through 36: All

Township 32 North, Range 12 West, N.M.P.M.

Sections 7 through 33: All

Township 32 North, Range 13 West, N.M.P.M.

Sections 7 through 29: All
Sections 32 through 36: All

Containing a total of 92,871.00 acres, more or less.

2. The Dakota formation is expected to have an estimated average in situ gas permeability throughout the pay section of less than 0.1 millidarcy per foot.

3. The average depth of the top of the Dakota formation is 7050 feet and the stabilized production rate, against atmospheric pressure, of wells completed for production in said formation, without stimulation, is not expected to exceed 290 mcf of gas per day.

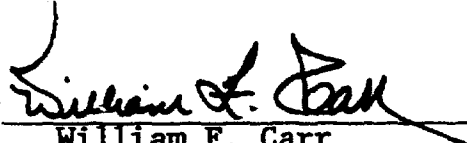
4. No well drilled into the Dakota formation in the above-described area is expected to produce, without stimulation, more than five barrels of crude oil per day.

5. Attached to this application and incorporated herein by reference is a complete set of exhibits which applicant proposes to offer or introduce at the hearing on this application, together with a statement of the meaning and purpose of each exhibit. These exhibits cover all aspects of the required evidentiary data described in Section D of the Oil Conservation Division's Special Rules and Procedures for Tight Sand Formation Designation under Section 107 of the Natural Gas Policy Act of 1978.

WHEREFORE, Applicant prays that this application be set for hearing before the Oil Conservation Commission and that after notice and hearing as required by law, the Commission enter its order recommending to the Federal Energy Regulatory Commission that pursuant to 18 CFR, Section 271.701 - 705, that the Dakota formation underlying the above-described lands be designated a tight formation, and making such other and further provisions as may be proper in the premises.

Respectfully submitted,

CAMPBELL, BYRD & BLACK, P.A.

By 
William F. Carr
Post Office Box 2208
Santa Fe, New Mexico 87501
Attorneys for Applicant

BEFORE THE
OIL CONSERVATION COMMISSION
NEW MEXICO DEPARTMENT OF ENERGY AND MINERALS

RECEIVED
SEP 08 1981
OIL CONSERVATION DIVISION
SANTA FE

IN THE MATTER OF THE APPLICATION
OF SOUTHLAND ROYALTY COMPANY,
FOR DESIGNATION OF TIGHT FORMA-
TION, SAN JUAN COUNTY, NEW MEXICO

Case 7361

APPLICATION

Comes now SOUTHLAND ROYALTY COMPANY, by and through its undersigned attorneys and as provided in the Oil Conservation Division's Special Rules and Procedures for Tight Formation Designations under Section 107 of the Natural Gas Policy Act of 1978 promulgated by Oil Conservation Division Order No. R-6388 on June 30, 1980, hereby makes application for an order designating certain portions of the Dakota formation (Basin Dakota Field) as a tight formation under Section 107 of the Natural Gas Policy Act of 1978 and in support of its application would show the Division:

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Township 31 North, Range 10 West, N.M.P.M.
Sections 1 through 36: All

Township 31 North, Range 11 West, N.M.P.M.
Section 1: All
Sections 12 and 13: All
Sections 22 through 27: All
Sections 34 through 36: All

Township 32 North, Range 10 West, N.M.P.M.
Sections 7 through 36: All

Township 32 North, Range 11 West, N.M.P.M.

Sections 7 through 27: All

Sections 34 through 36: All

Township 32 North, Range 12 West, N.M.P.M.

Sections 7 through 33: All

Township 32 North, Range 13 West, N.M.P.M.

Sections 7 through 29: All

Sections 32 through 36: All

Containing a total of 92,871.00 acres, more or less.

2. The Dakota formation is expected to have an estimated average in situ gas permeability throughout the pay section of less than 0.1 millidarcy per foot.

3. The average depth of the top of the Dakota formation is 7050 feet and the stabilized production rate, against atmospheric pressure, of wells completed for production in said formation, without stimulation, is not expected to exceed 290 mcf of gas per day.

4. No well drilled into the Dakota formation in the above-described area is expected to produce, without stimulation, more than five barrels of crude oil per day.

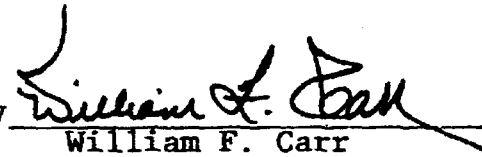
5. Attached to this application and incorporated herein by reference is a complete set of exhibits which applicant proposes to offer or introduce at the hearing on this application, together with a statement of the meaning and purpose of each exhibit. These exhibits cover all aspects of the required evidentiary data described in Section D of the Oil Conservation Division's Special Rules and Procedures for Tight Sand Formation Designation under Section 107 of the Natural Gas Policy Act of 1978.

WHEREFORE, Applicant prays that this application be set for hearing before the Oil Conservation Commission and that after notice and hearing as required by law, the Commission enter its order recommending to the Federal Energy Regulatory Commission that pursuant to 18 CFR, Section 271.701 - 705, that the Dakota formation underlying the above-described lands be designated a tight formation, and making such other and further provisions as may be proper in the premises.

Respectfully submitted,

CAMPBELL, BYRD & BLACK, P.A.

By



William F. Carr
Post Office Box 2208
Santa Fe, New Mexico 87501
Attorneys for Applicant

Land R. 14

T 31N R 12W

secs 5 thru 8

12 thru 25

29 thru 32

7442 acres

T 31N R 13W

secs 12 thru 14: 3

22 thru 28: 7

33 thru 36: 4

14

40
14
2560
640
3200

14 x 640 = 8960 acres

T 32N R 12W

25 thru 27: 3

32 and 33: 2

5

640
3200

5 x 640 = 3200

7442

8960

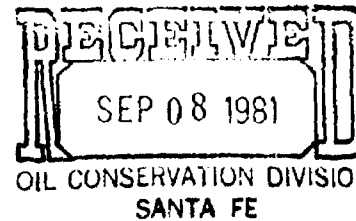
3200

19,602

122,516

19,602

102,914



BEFORE THE
OIL CONSERVATION COMMISSION
NEW MEXICO DEPARTMENT OF ENERGY AND MINERALS

IN THE MATTER OF THE APPLICATION
OF SOUTHLAND ROYALTY COMPANY,
FOR DESIGNATION OF TIGHT FORMA-
TION, SAN JUAN COUNTY, NEW MEXICO

Case 7361

APPLICATION

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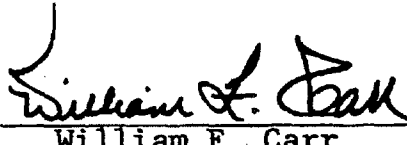
4. No well drilled into the Dakota formation in the above-described area is expected to produce, without stimulation, more than five barrels of crude oil per day.

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WHEREFORE, Applicant prays that this application be set for hearing before the Oil Conservation Commission and that after notice and hearing as required by law, the Commission enter its order recommending to the Federal Energy Regulatory Commission that pursuant to 18 CFR, Section 271.701 - 705, that the Dakota formation underlying the above-described lands be designated a tight formation, and making such other and further provisions as may be proper in the premises.

Respectfully submitted,

CAMPBELL, BYRD & BLACK, P.A.

By 
William F. Carr
Post Office Box 2208
Santa Fe, New Mexico 87501
Attorneys for Applicant

Dockets Nos. 31-81 and 32-81 are tentatively set for October 7, and October 21, 1981. Applications for hearing must be filed at least 22 days in advance of hearing date.

DOCKET: EXAMINER HEARING - WEDNESDAY - SEPTEMBER 23, 1981

9 A.M. - OIL CONSERVATION DIVISION CONFERENCE ROOM
STATE LAND OFFICE BUILDING, SANTA FE, NEW MEXICO

The following cases will be heard before Richard L. Stamets, Examiner or Daniel S. Nutter, Alternate Examiner:

- CASE 7353: Application of Texaco, Inc., for the amendment of Division Order No. R-5530, Lea County, New Mexico. Applicant, in the above-styled cause, seeks the amendment of Order No. R-5530, which authorized its Central Vacuum Unit Area Pressure Maintenance Project, to increase the total project area allowable, or as an alternative, to reclassify the project as a waterflood project.
- CASE 7354: Application of Corona Oil Company, for a pilot steam-enhanced oil recovery project, Guadalupe County, New Mexico. Applicant, in the above-styled cause, seeks authority to institute a pilot steam-enhanced oil recovery project in the Santa Rosa formation by using two existing wells and three additional wells to be drilled to complete a five spot pattern located in the NE/4 NW/4 of Section 17, Township 11 North, Range 26 East.
- CASE 7355: Application of Doyle Hartman for directional drilling and an unorthodox location, Lea County, New Mexico. Applicant, in the above-styled cause, seeks authority to drill his Bates Well No. 3, the surface location of which is 1635 feet from the South line and 1210 feet from the West line of Section 20, Township 25 South, Range 37 East, in such a manner as to bottom it at a depth of 3500 feet in the Jalamat Gas Pool at an unorthodox location 2310 feet from the South line and 1650 feet from the West line of Section 20. The SW/4 of said Section 20 would be dedicated to the well.
- CASE 7356: Application of S & I Oil Company for compulsory pooling, San Juan County, New Mexico. Applicant, in the above-styled cause, seeks an order pooling all mineral interests in the W/2 SW/4 of Section 12, Township 29 North, Range 15 West, Cha Cha-Gallup Oil Pool, to be dedicated to a well to be drilled at a standard location thereon. Also to be considered will be the cost of drilling and completing said well and the allocation of the cost thereof as well as actual operating costs and charges for supervision, designation of applicant as operator of the well, and a charge for risk involved in drilling said well.
- CASE 7357: Application of Union Oil Company of California for compulsory pooling, Lea County, New Mexico. Applicant, in the above-styled cause, seeks an order pooling all mineral interests in the Atoka and Morrow formations underlying the W/2 of Section 16, Township 22 South, Range 33 East, to be dedicated to a well to be drilled at a standard location thereon. Also to be considered will be the cost of drilling and completing said well and the allocation of the cost thereof as well as actual operating costs and charges for supervision, designation of applicant as operator of the well, and a charge for risk involved in drilling said well.
- CASE 7343: (Continued from September 9, 1981, Examiner Hearing)
- Application of Caribou Four Corners, Inc. for compulsory pooling, San Juan County, New Mexico. Applicant, in the above-styled cause, seeks an order pooling all mineral interests in the Cha Cha Gallup Oil Pool underlying the E/2 NW/4 of Section 18, Township 29 North, Range 14 West, to be dedicated to a well to be drilled at a standard location thereon. Also to be considered will be the cost of drilling and completing said well and the allocation of the cost thereof as well as operating costs and charges for supervision, designation of applicant as operator of the well, and a charge for risk involved in drilling said well.
- CASE 7358: Application of John Yuronka for compulsory pooling, Lea County, New Mexico. Applicant, in the above-styled cause, seeks an order pooling all mineral interests in the Langley Mattix Pool underlying the SW/4 of Section 6, Township 23 South, Range 37 East, to form four 40-acre tracts, each to be dedicated to a well to be drilled at a standard location thereon. Also to be considered will be the cost of drilling and completing said wells and the allocation of the cost thereof as well as actual operating costs and charges for supervision, designation of applicant as operator of the wells, and a charge for risk involved in drilling said wells.

CASE 7359: Application of Energy Reserves Group for creation of a new gas pool and an unorthodox location, Roosevelt County, New Mexico.

Applicant, in the above-styled cause, seeks creation of a new Cisco gas pool for its Miller Com Well No. 1, located in Unit M of Section 12, Township 6 South, Range 33 East.

Applicant further seeks approval of an unorthodox location for its Miller "A" Well No. 1-Y, to be drilled 1800 feet from the South line and 1700 feet from the East line of Section 11 of the same township. The S/2 of said Section 11 to be dedicated to the well.

CASE 7345: (Continued from September 9, 1981, Examiner Hearing)

Application of Bass Enterprises Production Company for compulsory pooling, Lea County, New Mexico. Applicant, in the above-styled cause, seeks an order pooling all mineral interests in the Lovington Penn Pool underlying the N/2 NE/4 of Section 13, Township 16 South, Range 36 East, to be dedicated to a well to be drilled at a standard location thereon. Also to be considered will be the cost of drilling and completing said well and the allocation of the cost thereof as well as actual operating costs and charges for supervision, designation of applicant as operator of the well, and a charge for risk involved in drilling said well.

CASE 7360: Application of L. J. Buck for salt water disposal, Lea County, New Mexico.

Applicant, in the above-styled cause seeks authority to dispose of produced salt water into the Seven Rivers formation in the interval from 3221 feet to 3250 feet in his Monco Well No. 2 in Unit M of Section 25, Township 25 South, Range 36 East.

CASE 7352: (Continued from September 9, 1981 Examiner Hearing)

Application of Yates Petroleum Corporation for designation of a tight formation, Eddy County, New Mexico. Applicant, in the above-styled cause, pursuant to Section 107 of the Natural Gas Policy Act 18-CFR Section 271.701-705, seeks the designation as a tight formation of the Permo-Penn and formation underlying all of the following townships:

Township 17 South, Ranges 24 thru
26 East;

18 South, 24 and 25 East;

19 South, 23 thru 25 East;

20 South, 21 thru 24 East;

20 1/2 South, 21 and 22 East;

21 South, 21 and 22 East;

Also Sections 1 thru 12 in
22 South, 21 and 22 East,

All of the above containing a total of 315,000 acres more or less.

CASE 7329: (Readvertised)

Application of Loco Hills Water Disposal Company for an exception to Order No. R-3221, Eddy County, New Mexico

Applicant, in the above-styled cause, seeks an exception to Order No. R-3221 to permit the commercial disposal of produced brine into several unlined surface pits located in the N/2 SW/4 SW/4 of Section 16, Township 17 South, Range 30 East.

Dockets Nos. 31-81 and 32-81 are tentatively set for October 7, and October 21, 1981. Applications for hearing must be filed at least 22 days in advance of hearing date.

DOCKET: COMMISSION HEARING - TUESDAY - SEPTEMBER 29, 1981

9 A.M. - OIL CONSERVATION DIVISION - MORGAN HALL
STATE LAND OFFICE BUILDING, SANTA FE, NEW MEXICO

CASE 7116: (DE NCVO)

Application of Southland Royalty Company for designation of a tight formation, San Juan County, New Mexico. Applicant, in the above-styled cause, seeks the designation of the Dakota formation underlying portions of Township 31 and 32 North, Ranges 10, 11, 12, and 13 West, containing 93,860 acres, more or less, as a tight formation pursuant to Section 107 of the Natural Gas Policy Act and 18 CFR Section 271.701-705.

Upon application of Consolidated Oil & Gas, Inc., this case will be heard Le Novo pursuant to the provisions of Rule 1220.

CASE 7361: Application of Southland Royalty Company for designation of a tight formation, San Juan County, New Mexico. Applicant, in the above-styled cause, seeks the designation of the Dakota formation underlying all or portions of Township 31 North, Ranges 10 and 11 West, and Township 32 North, Ranges 10, 11, 12, and 13 West, containing 92,871 acres more or less, as a tight formation pursuant to Section 107 of the Natural Gas Policy Act and 18 CFR Section 271. 701-705.

CASE 7362: Application of R. A. Mendenhall Associates, Ltd., for compulsory pooling, Eddy County, New Mexico. Applicant, in the above-styled cause, seeks an order pooling all mineral interests in the Delaware Mountain Group formation underlying the NW/4 SE/4 of Section 10, Township 22 South, Range 27 East, to be dedicated to a well to be drilled at a standard location thereon. Also to be considered will be the cost of drilling and completing said well and the allocation of the cost thereof as well as actual operating costs and charges for supervision, designation of applicant as operator of the well, and a charge for risk involved in drilling said well.

CAMPBELL, BYRD & BLACK, P.A.
LAWYERS

JACK M. CAMPBELL
HARL D. BYRD
BRUCE D. BLACK
MICHAEL B. CAMPBELL
WILLIAM F. CARR
BRADFORD C. BERGE
WILLIAM G. WARDLE

RECEIVED
1981
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JEFFERSON PLACE
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POST OFFICE BOX 2208
SANTA FE, NEW MEXICO 87501
TELEPHONE: (505) 988-4421
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September 3, 1981

Mr. Joe D. Ramey, Director
Oil Conservation Division
New Mexico Department of Energy & Minerals
P.O. Box # 2088
Santa Fe, New Mexico 87501

Case 7361

Re: Application of Southland Royalty Company for designation
of a tight formation, San Juan County, New Mexico.

Dear Mr. Ramey:

Southland Royalty Company requests that a hearing be scheduled
before the Oil Conservation Commission to consider its appli-
cation to designate the following acreage within the Basin
Dakota Field as a tight formation under Section 107 of the
Natural Gas Policy Act of 1978:

Township 31 North, Range 10 West, N.M.P.M.
Sections 1 through 36: All

Township 31 North, Range 11 West, N.M.P.M.
Section 1: All
Sections 12 and 13: All
Sections 22 through 27: All
Sections 34 through 36: All

Township 32 North, Range 10 West, N.M.P.M.
Sections 7 through 36: All

Township 32 North, Range 11 West, N.M.P.M.
Sections 7 through 27: All
Sections 34 through 36: All

Township 32 North, Range 12 West, N.M.P.M.
Sections 7 through 33: All

Township 32 North, Range 13 West, N.M.P.M.

Sections 7 through 29: All

Sections 32 through 36: All

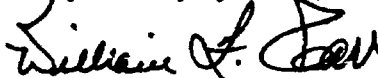
Said area contains 92,871.00 acres, more or less.

Southland requests that this case be advertised for hearing before the full commission on September 29, 1981. A formal application will be filed with the commission at least ten days prior to the hearing date.

At the time of the de novo hearing in Case No. 7116, which is also scheduled for hearing on September 29, 1981, it is Southland's intention to ask that its acreage be dismissed from that application. This will permit Consolidated Oil & Gas, Inc. to seek a tight formation designation for other acreage in Townships 31 and 32 North, Ranges 10 through 13 West.

If you have any questions concerning this matter, please advise.

Very truly yours,



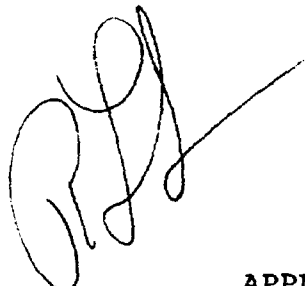
William F. Carr

cc: Lynn Teschendorf, Attorney
Consolidated Oil & Gas, Inc.

HERBIE
DAN

STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENT
OIL CONSERVATION COMMISSION

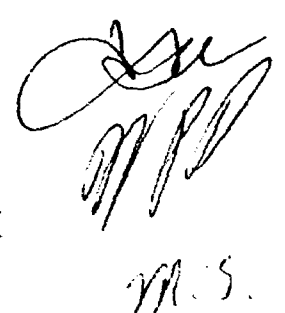
IN THE MATTER OF THE HEARING
CALLED BY THE OIL CONSERVATION
COMMISSION OF NEW MEXICO FOR
THE PURPOSE OF CONSIDERING:



CASE NO. 7361

Order No. R-6884

APPLICATION OF SOUTHLAND ROYALTY
COMPANY FOR DESIGNATION OF A TIGHT
FORMATION, SAN JUAN COUNTY, NEW MEXICO.



M.S.

ORDER OF THE COMMISSION

BY THE COMMISSION:

This cause came on for hearing at 9 o'clock a.m. on
September 29, 1981, at Santa Fe, New Mexico, before the Oil
Conservation Commission of New Mexico, hereinafter referred to
as the "Commission."

NOW, on this _____ day of January, 1982, the Commission, a
quorum being present, having considered the testimony presented
and the exhibits received at said hearing, and being fully
advised in the premises,

FINDS:

(1) That due public notice having been given as required by law, the Commission has jurisdiction of this cause and the subject matter thereof.

(2) That, pursuant to Section 107 of the Natural Gas Policy Act of 1978, and CFR Section 271.703, applicant Southland Royalty Company requested the designation as a "tight formation" of the Dakota formation underlying the following described lands:

SAN JUAN COUNTY, NEW MEXICO

TOWNSHIP 31 NORTH, RANGE 10 WEST, NMPM

Sections 1 through 36: All

TOWNSHIP 31 NORTH, RANGE 11 WEST, NMPM

Section 1: All

Sections 12 and 13: All

Sections 22 through 27: All

Sections 34 through 36: All

TOWNSHIP 32 NORTH, RANGE 10 WEST, NMPM

Sections 7 through 36: All

TOWNSHIP 32 NORTH, RANGE 11 WEST, NMPM

Sections 7 through 27: All

Sections 34 through 36: All

TOWNSHIP 32 NORTH, RANGE 12 WEST, NMPM

Sections 7 through 33: All

TOWNSHIP 32 NORTH, RANGE 13 WEST, NMPM

Sections 7 through 33: All

containing a total of 92,871 acres, more or less.

(3) That at the hearing, applicant requested dismissal of that portion of the application pertaining to Sections 25 through 27, inclusive, and Sections 32 and 33, all in Township 32 North, Range 12 West, NMPM, containing some 3,200 acres, more or less, leaving for consideration some 89,671 acres, more or less.

(4) That said request for dismissal should be approved, and no further consideration given herein to said lands.

(5) That while the application was for designation of the Dakota formation as a tight formation, the Dakota formation constitutes but a portion of the "Dakota Producing Interval," which, as defined by the Division, comprises the vertical limits of the Basin-Dakota Gas Pool, being from the base of the Greenhorn Limestone to a point 400 feet below the base of said formation and consisting of the Graneros formation, the Dakota formation, and the productive upper limit of the Morrison formation.

(6) That inasmuch as practically all so-called "Dakota" wells drilled in the subject area are, or potentially are, tested in and/or completed in the entire Dakota Producing Interval, and the well data presented at the hearing of this case involves the entire Dakota Producing Interval, the application should be broadened to cover all of said producing

interval throughout the area.

(7) That the Dakota Producing Interval, hereinafter referred to as the "Dakota," consists of a near blanket sandstone (probably an almost continuous series of northwest trending barrier beach sandstones composed of fine-grained quartose sandstones and carbonaceous shales with occasional conglomerates and coals in the basal part).

(8) That from the logs available at the hearing, the top of the Dakota in the area ranges from a depth of 5234 feet to 7220 feet and averages some ~~6605~~⁶⁷⁵³ feet beneath the surface.

(9) That the only test data for flow rates prior to stimulation for wells within the area indicates that ~~the~~ Aztec Pierce Well No. 2 in Section 30, Township 31 North, Range 10 West, NMPM, had a stabilized production rate calculated at atmospheric pressure of 208.1 MCF of gas per day; that other wells in the immediate vicinity of the area but just outside had stabilized production rates calculated at atmospheric pressure prior to stimulation ranging from 21.7 MCF per/day to 224.1 MCF per day.

(10) That none of the stabilized production rates cited above exceeds the maximum stabilized production rate set forth in 18 C.F.R. Section 271.703(c)(2)(i)(B) of 251 MCF per day for wells at the average depth to the top of the formation for this area (~~6603~~⁶⁷⁵³ feet), and it is not expected that the average well in the area will exceed such rate.

(11) That in situ permeability calculations are available

for only two wells in the general area, being the Southland Pierce Well No. 2 and the Southland Patterson "B" Com Well No.

1E,
; that the in situ permeabilities calculated for said wells are .0609 md and .0877 md, respectively, and average .0743 md.

(12) That the average in situ permeability for all wells in the area is not expected to exceed 0.1 md, the limit set forth in 18 C.F.R. Section 271.703(c)(2)(i)(A).

(13) That prior to stimulation, the average well in the area is expected to produce far less than the maximum five barrels of crude oil per day as set forth in 18 C.F.R. Section 271.703(c)(2)(i)(C).

(14) That 18 C.F.R. Section 271.703(c)(2)(i)(D) provides that "if the formation or any portion thereof was authorized to be developed by infill drilling prior to the date of recommendation and the jurisdictional agency has information which in its judgment indicates that such formation or portion subject to infill drilling can be developed absent the incentive price established in paragraph (a) of this section then the jurisdictional agency shall not include such formation or portion thereof in its recommendation."

(15) That the Division, by its Order No. R-1670-V, dated May 22, 1979, and effective July 1, 1979, approved infill drilling for the Basin-Dakota Gas Pool in San Juan and Rio Arriba Counties, New Mexico, and said pool includes the Dakota Producing Interval in the area under consideration here.

(16) That Southland in this hearing indicated that under current Section 103 prices of the NGPA of 1978, reserves of 350,000 MCF of gas are necessary to provide it with the economics necessary to justify drilling a Dakota well at its current drilling costs, while 150,000 MCF of reserves will justify a well at Section 107(c)(5) prices (tight formations).

(17) That the economics as presented by Southland in this case are reasonable, and lands which indicate ^{AC} recoverable ~~reserves of 350,000 MCF or more~~ of gas should be dismissed from further consideration, while lands indicating recoverable reserves of less than 350,000 MCF of gas should be considered for recommendation as a tight formation.

(18) That the Division, in approving infill drilling for the Basin-Dakota Gas Pool, based its approval on the premise that the reservoir was of low permeability and that 320-acre wells were not draining more than the 160-acre tract upon which they were located.

(19) That the remaining reserves under the 160-acre tract upon which the unit well is not located should be similar to, if not equal to, the original reserves under the 160-acre tract upon which the unit well is located.

(20) That cumulative production figures and estimates of ultimate recoverable reserves were presented at the hearing for some of the developed tracts within the area, while cumulative production figures only are available for the remainder of the developed tracts.

(21) That to determine that under certain lands insufficient reserves are available to justify drilling absent the Section 107 incentive price, it is reasonable to make the following assumptions:

- A. No primary drilling, i.e., no drilling on 320-acre spacing, is prima facie evidence that the lands are edge lands to the reservoir and drilling has not occurred because of the probable marginal nature of the reserves.
- B. Primary drilling has occurred but the calculated total ultimate reserves or the cumulative production for long-connected wells indicates low ultimate recovery (less than 350,000 MCF of gas).

(22) That to determine that under certain lands sufficient reserves may reasonably be expected to be recovered to justify drilling without the Section 107 incentive price, it is reasonable to make the following assumptions:

- A. Calculated ultimate recoverable reserves are 350,000 MCF or more.
- B. Calculated ultimate recoverable reserves are not available, but cumulative recoveries indicate that 350,000 MCF of gas already has been recovered.

(23) That the assumptions in Findings Nos. (21) B. and (22) A. and B. above may reasonably be based on offsetting wells

in a given area.

(24) That the evidence indicates that it is unreasonable to expect that wells drilled in the area described in Finding No. (2) above less the area described in Finding No. (3) above will yield an average of 350,000 MCF or more of gas, but that it is reasonable to expect that such wells will yield an average of 150,000 MCF of gas, and that the incentive Section 107 (c) (5) price is necessary to justify drilling in said area.

(25) That there are fresh water aquifers underlying the lands being considered, and these aquifers extend to a depth of approximately 1200 feet.

(26) That there is a vertical distance of some ⁵⁵⁰⁰~~5400~~ feet between the base of the lowermost of said aquifers and the top of the Dakota, and this distance, combined with the required casing and cementing program for wells in the area, will assure that development of the Dakota will not adversely affect the fresh water aquifers (during both hydraulic fracturing and waste disposal operations) that are or are expected to be used as a domestic or agricultural water supply.

(27) That the Dakota Producing Interval underlying the following lands meets all of the guidelines set forth in 18 C.F.R. Section 271.703(c)(2)(i), subsections (A), (B), (C), and (D), and should be recommended for designation as a tight formation:

TOWNSHIP 31 NORTH, RANGE 10 WEST, NMPM

Sections 1 through 36: All

TOWNSHIP 31 NORTH, RANGE 11 WEST, NMPM

Section 1: All

Sections 12 and 13: All

Sections 22 through 27: All

Sections 34 through 36: All

TOWNSHIP 32 NORTH, RANGE 10 WEST, NMPM

Sections 7 through 36: All

TOWNSHIP 32 NORTH, RANGE 11 WEST, NMPM

Sections 7 through 27: All

Sections 34 through 36: All

TOWNSHIP 32 NORTH, RANGE 12 WEST, NMPM

Sections 7 through 24: All

Sections 28 through 31: All

TOWNSHIP 32 NORTH, RANGE 13 WEST, NMPM

Sections 7 through 29: All

Sections 32 through 36: All

containing some 89,671 acres, more or less, all in San Juan County, New Mexico.

IT IS THEREFORE ORDERED:

(1) That it be and hereby is recommended to the Federal Energy Regulatory Commission pursuant to Section 107 of the Natural Gas Policy Act of 1978, and 18 C.F.R. Section 271.703, that the Dakota Producing Interval, being from the base of the Greenhorn Limestone to a point 400 feet below the base of said

formation and consisting of the Graneros formation, the Dakota formation and the productive upper portion of the Morrison formation, underlying the following described lands in San Juan County, New Mexico, be designated as a tight formation:

TOWNSHIP 31 NORTH, RANGE 10 WEST, NMPM

Sections 1 through 36: All

TOWNSHIP 31 NORTH, RANGE 11 WEST, NMPM

Section 1: All

Sections 12 and 13: All

Sections 22 through 27: All

Sections 34 through 36: All

TOWNSHIP 32 NORTH, RANGE 10 WEST, NMPM

Sections 7 through 36: All

TOWNSHIP 32 NORTH, RANGE 11 WEST, NMPM

Sections 7 through 27: All

Sections 34 through 36: All

TOWNSHIP 32 NORTH, RANGE 12 WEST, NMPM

Sections 7 through 24: All

Sections 28 through 31: All

TOWNSHIP 32 NORTH, RANGE 13 WEST, NMPM

Sections 7 through 29: All

Sections 32 through 36: All

containing approximately 89,671 acres, more or less.

(2) That jurisdiction of this cause is retained for the entry of such further orders as the Commission may deem necessary.

DONE at Santa Fe, New Mexico, on the day and year hereinabove designated.

STATE OF NEW MEXICO
OIL CONSERVATION COMMISSION

EMERY C. ARNOLD, Chairman

ALEX J. ARMIJO, Member

JOE D. RAMEY, Member & Secretary

S E A L